



# Background induced in the TPC by the calibration guide tube system

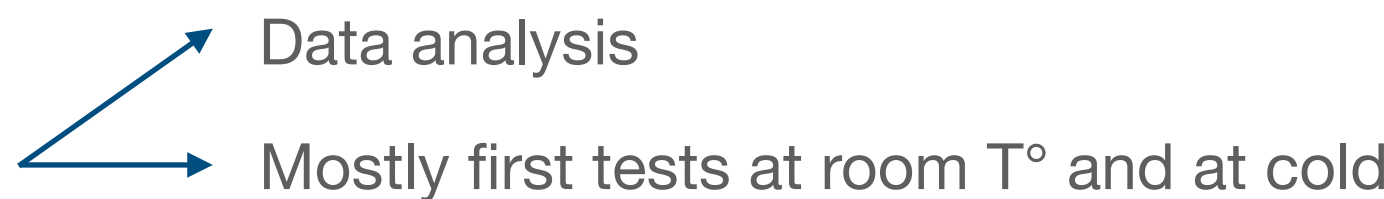
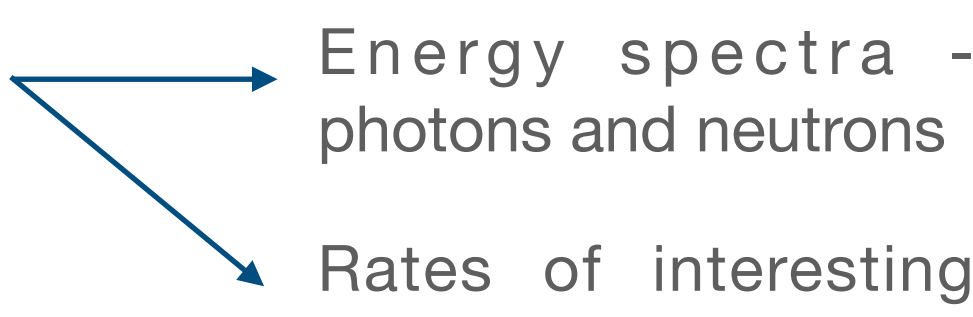
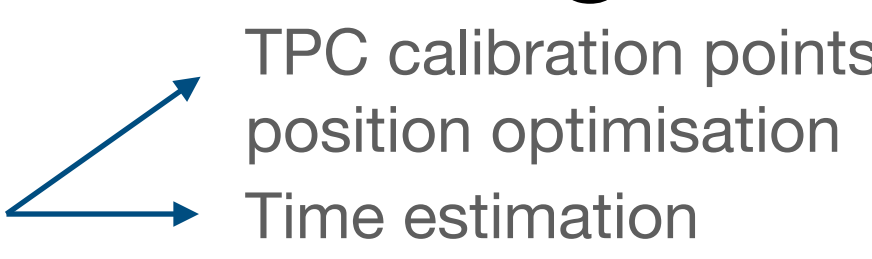
*Material Meeting - 23 November 2021*

**Marie van Uffelen (PhD) & Fabrice Hubaut - CPPM**

# My work for the DS collaboration

- PhD student (2021-> 2024) under the supervision of Fabrice Hubaut (CPPM, Marseille, France)
- Current commitment on TPC calibration with guide tubes:

**Presentation** to the DS calibration working group

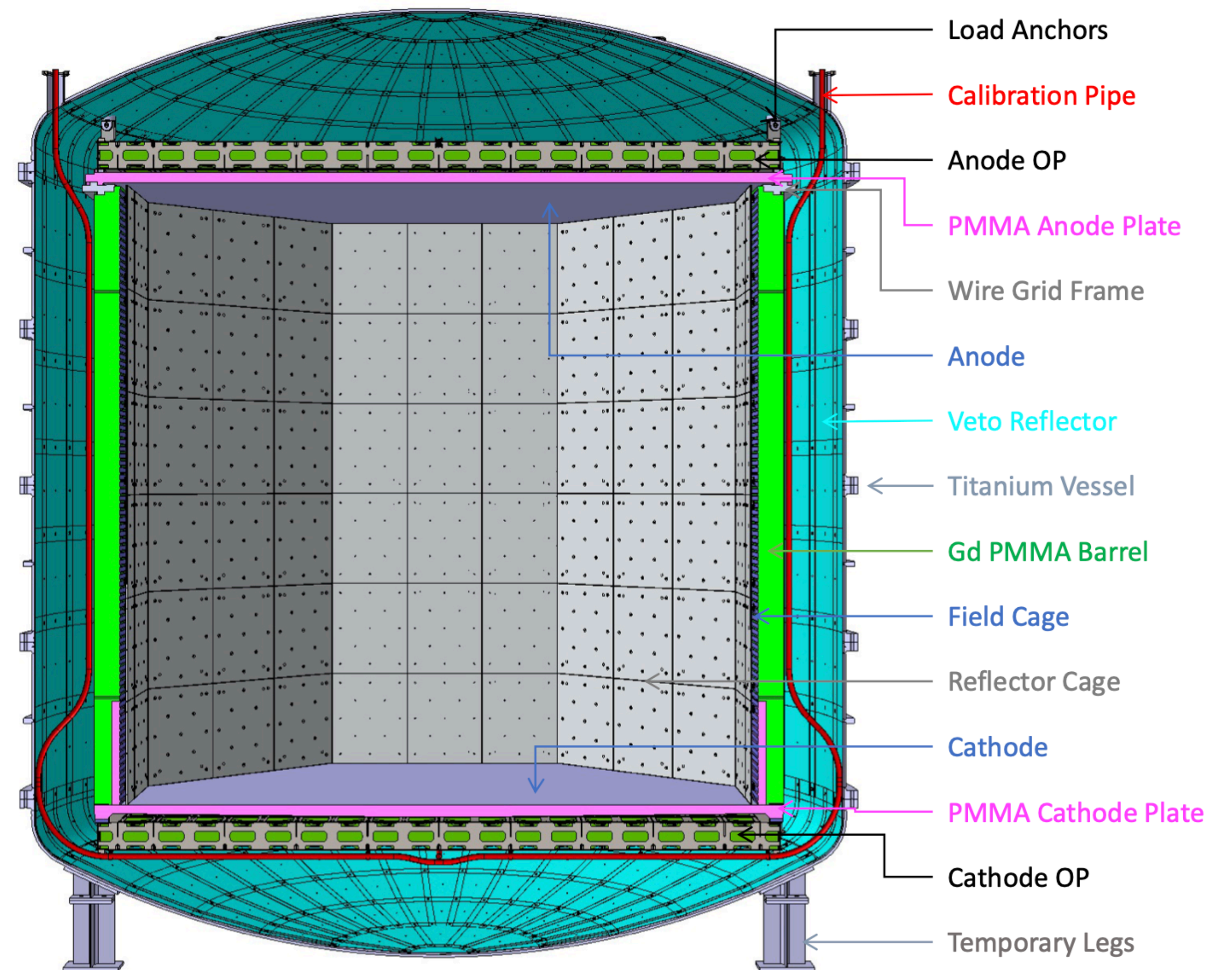
- Hardware work on the guide tube system mock-up 
- **Simulation** of the TPC calibration with plan C configuration 
- Derivation of a TPC calibration **strategy** 

➔ Simulation of the **background (ER, NR)** induced in the TPC by the calibration guide tube system

# The calibration guide tube system

Fig from [TDR](#)

- System that enables the circulation of calibration radioactive sources around the TPC during the calibration runs
- The sources will be removed during the WIMP search data taking
- Tubes have a  $\varnothing = 3$  cm, are 1.5 mm thick and made with **titanium** (17 kg)



# Background induced by tubes

## Tubes made with titanium

- **Goal:** estimate ER and NR background induced in the TPC by radioactive contamination in calibration pipes
- **Methodology**
  - Simulate 10 Mevents (for each radio contaminant) with g4ds with full-chain radioactive decays (HP list for hadronic interactions)
  - Count number of events surviving cuts (if none, put a limit at  $<2.3$  events)
    - ER background: single scatter in ROI ( $7.5 < E < 50$  keVee) and fiducial volume (veto 70 cm in z, 30 cm in r)
    - NR background: single scatter in ROI ( $30 < E < 200$  keVnr), fiducial volume (veto 70 cm in z, 30 cm in r) and veto (veto energy  $< 200$  keV for plan C)
  - Normalise to radioactive contamination of the titanium (from DS material group), mass of tubes ( $\sim 17$  kg for a density of  $4.5$  g/cm<sup>3</sup>) and time exposure
- **Started from Alex Kish work and code (see [INT calibration note](#))**
  - First : Reproduce his Plan A results assuming the tubes are ArDM Stainless Steel (which is the worst case scenario). Tubes:  $\varnothing=3$  cm, thick=1.5 mm, 3 (1) cm from TPC wall aside (below)
  - Include Plan C modeling of the guide tube in g4ds (Alex)
  - Produce results ER, NR for Plan C

# Titanium contamination

Activity (mBq/kg) and radiogenic neutron yield per decay, as measured by DarkSide material WG

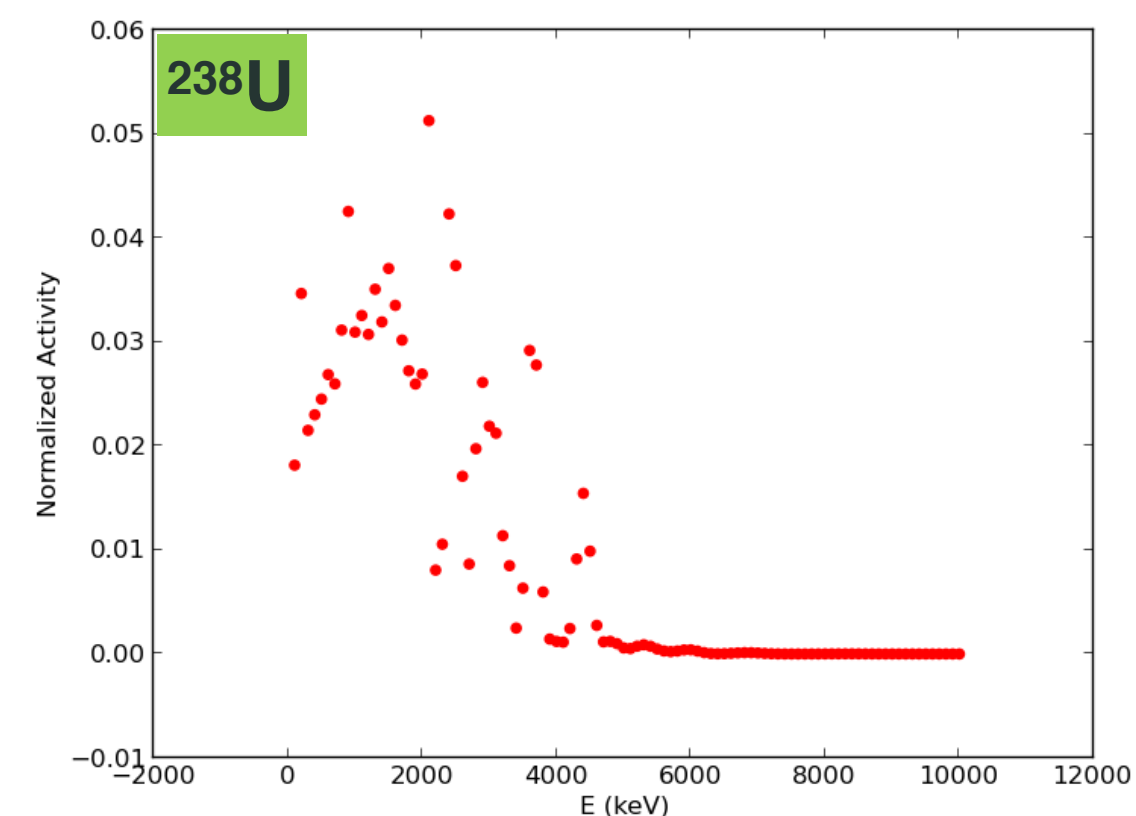
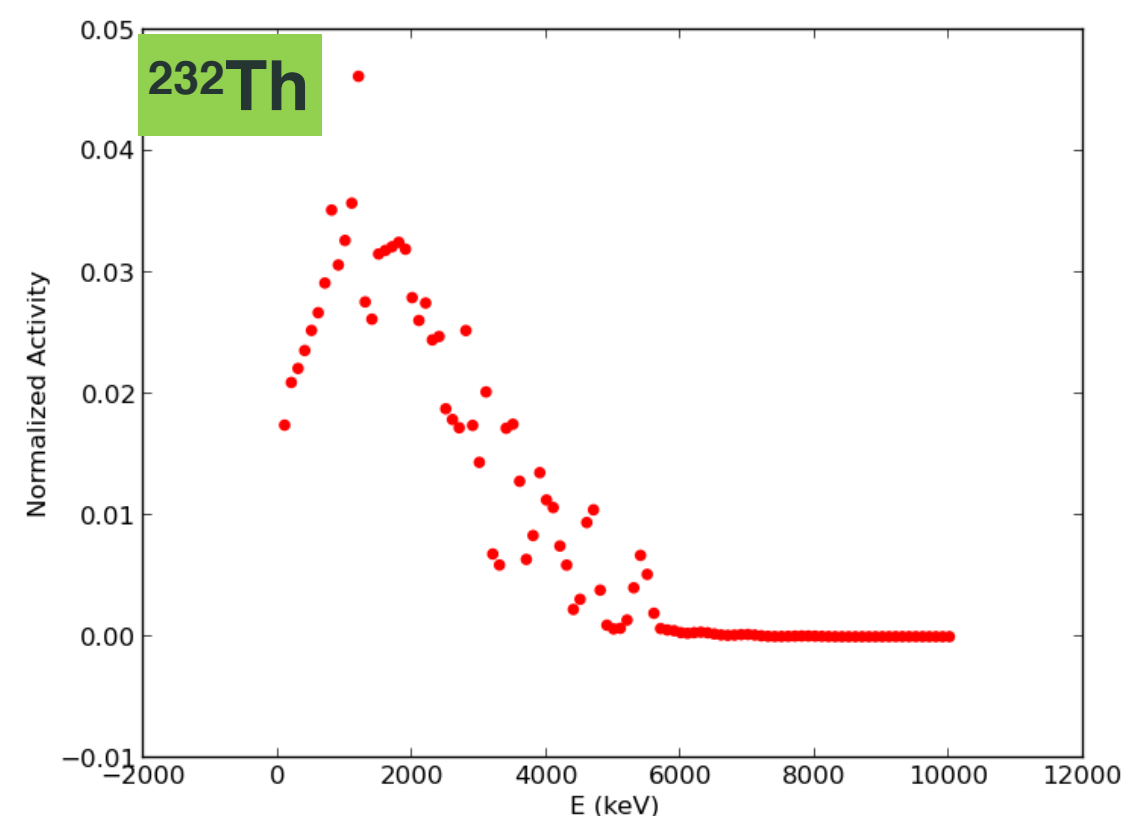
Source: TDR in preparation

	<sup>238</sup> U up	<sup>238</sup> U mid	<sup>238</sup> U low	<sup>232</sup> Th	<sup>235</sup> U	<sup>40</sup> K	<sup>46</sup> Sc
Activity (mBq/kg)	8	0.12	80	0.12	0.37	0.6	3.1
Neutron yield (n/decay)	4.9E-9	2.6E-6	1.6E-8	6.5E-6	2.6E-6	No	No

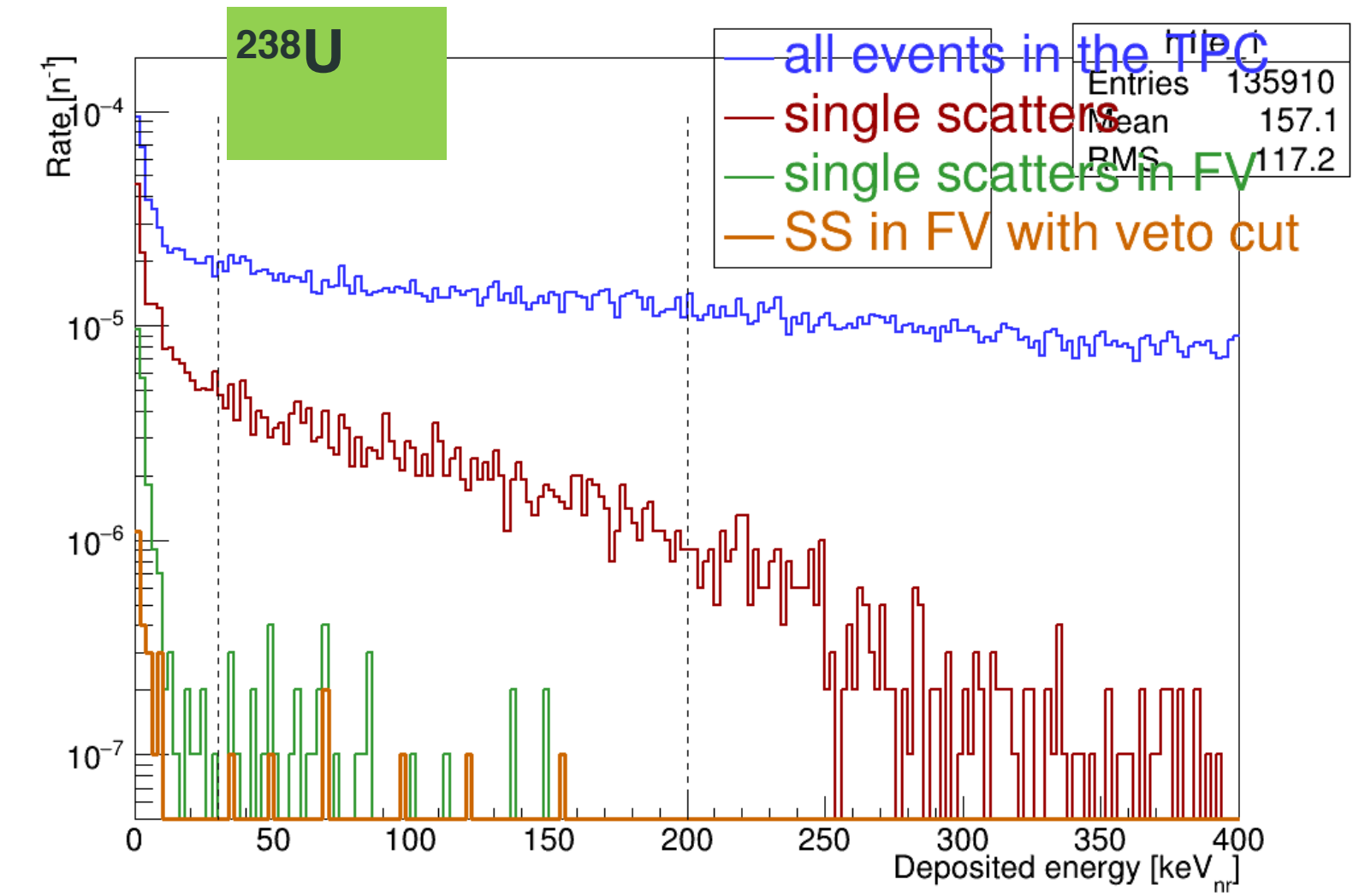
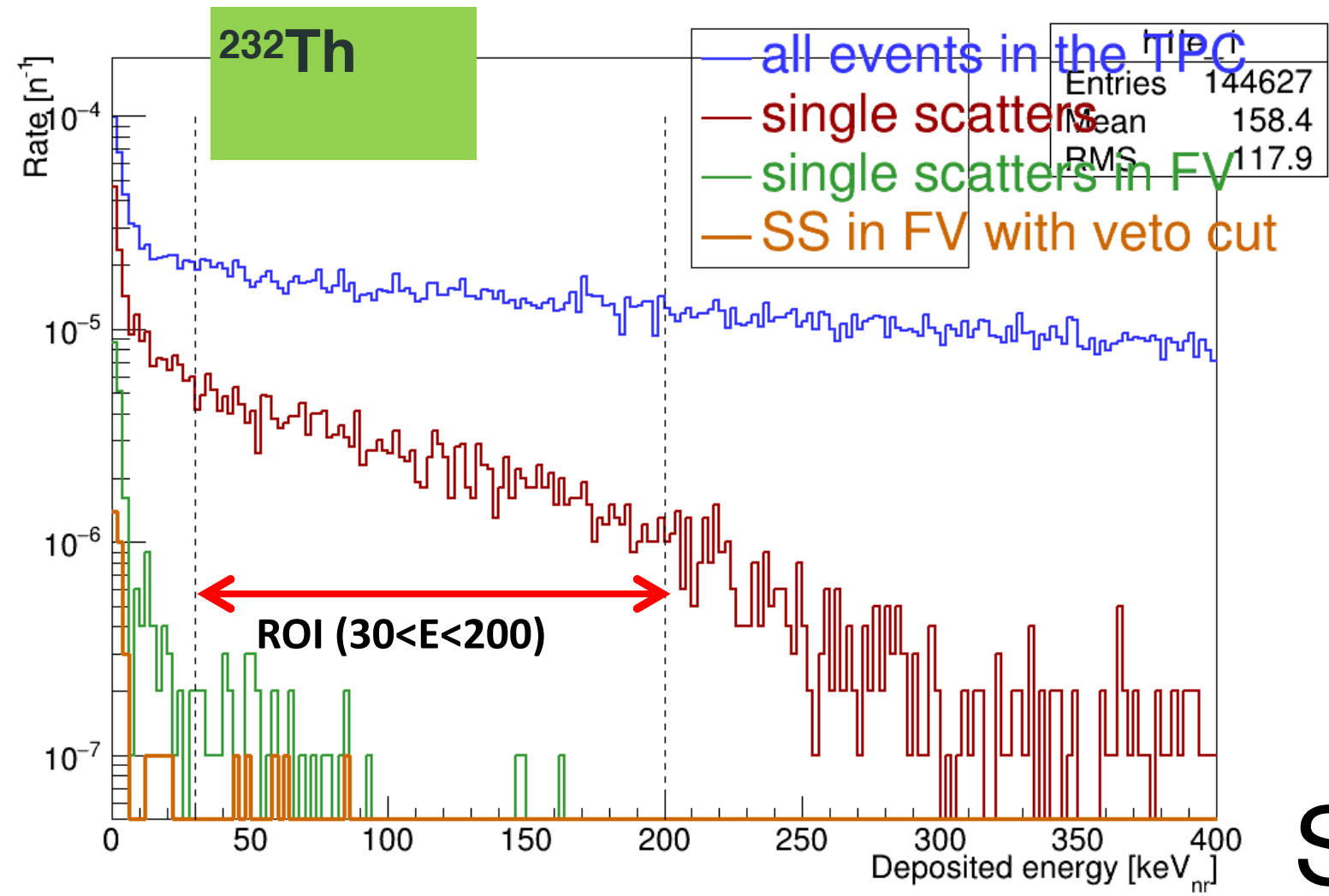
(from (alpha,n) reactions due to natural contamination in <sup>232</sup>Th, <sup>238</sup>U and <sup>235</sup>U and spontaneous fission of <sup>238</sup>U)

Neutron spectra are coded for U (Th) in /g4ds/data/physics/U238(Th232)Titanium.dat

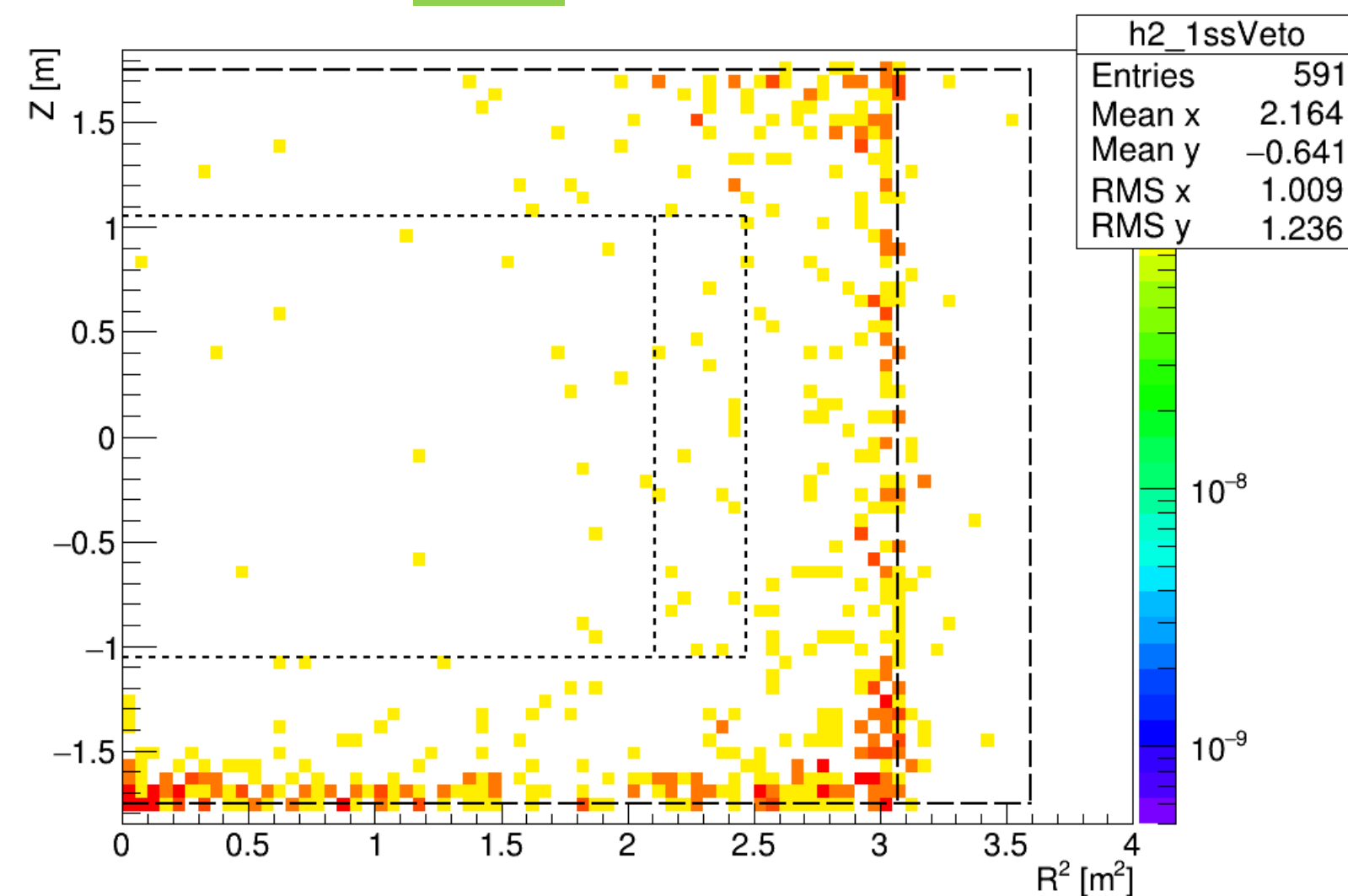
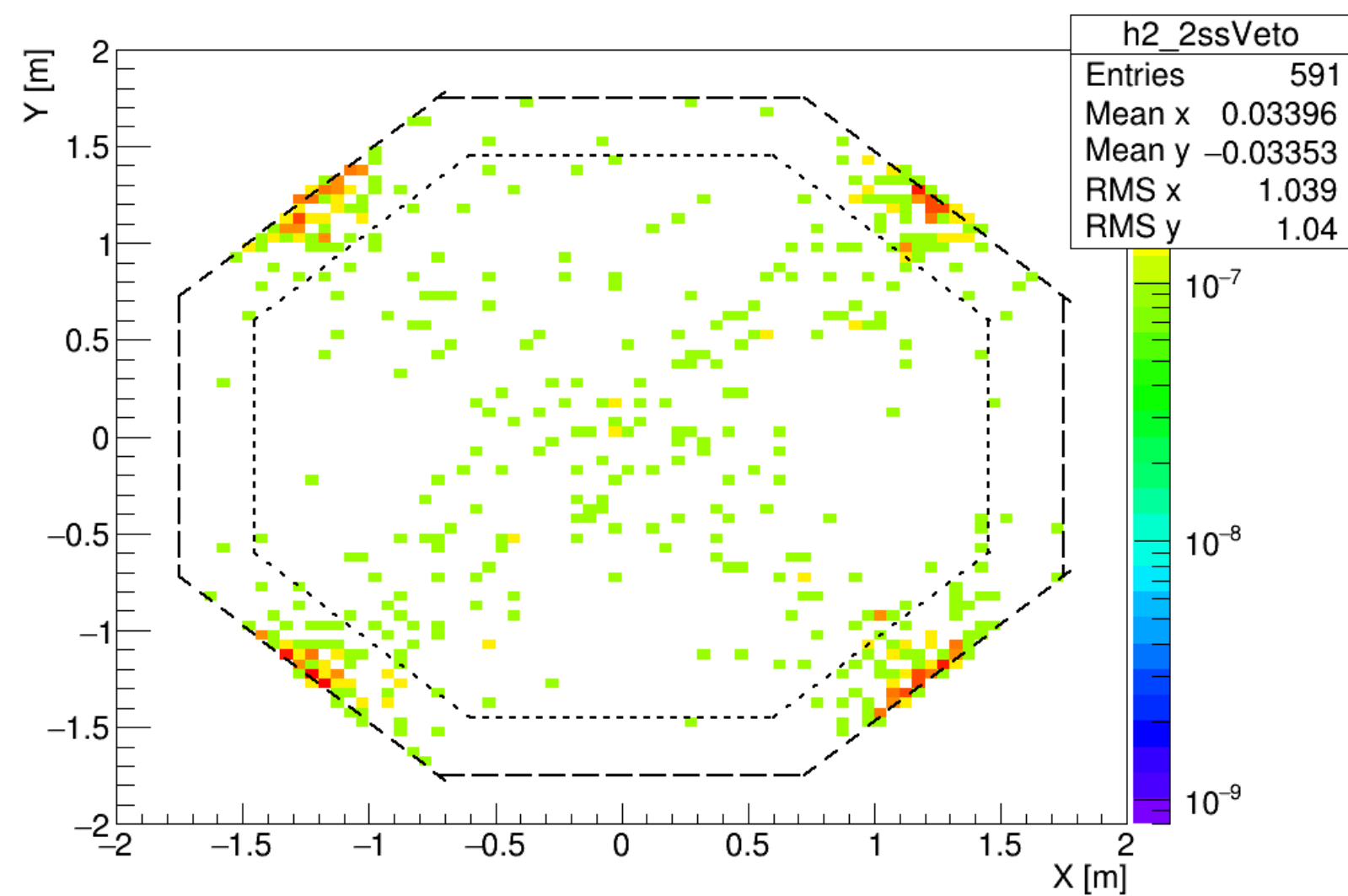
Spectrum for U235 not available in /g4ds/data/physics??



# NR background (1/2)



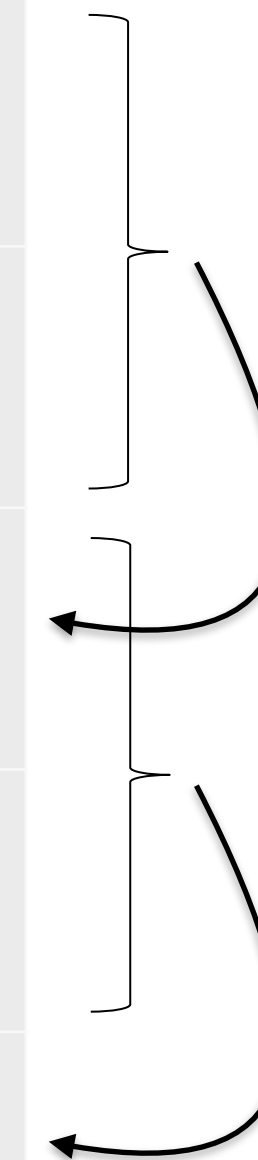
Spatial distributions of SS events after veto cut for  $^{232}\text{Th}$



# NR background (2/2)

## Final computation

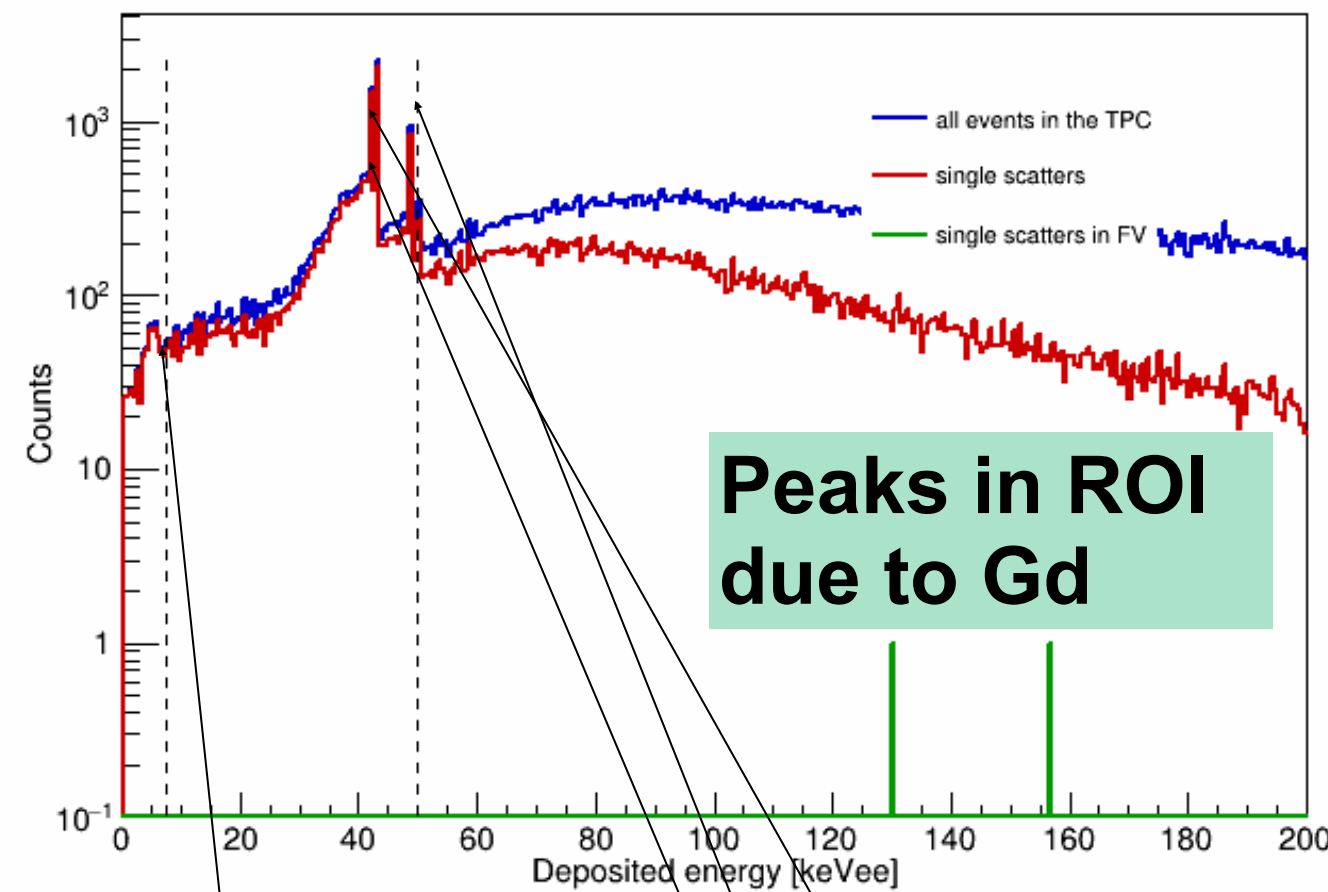
	<sup>238</sup> U up	<sup>238</sup> U mid	<sup>238</sup> U low	<sup>232</sup> Th
Activity (mBq/kg)	8	0.12	80	0.12
Neutron yield (n/ decay)	4.9E-9	2.6E-6	1.6E-8	6.5E-6
Neutron/year for 17 kg	0.02	0.17	0.69	0.42
Surviving events (/10 <sup>7</sup> )	7	7	7	5
NR bknd / 10 years (200 t.y)	1E-07	1E-06	5E-06	2E-06



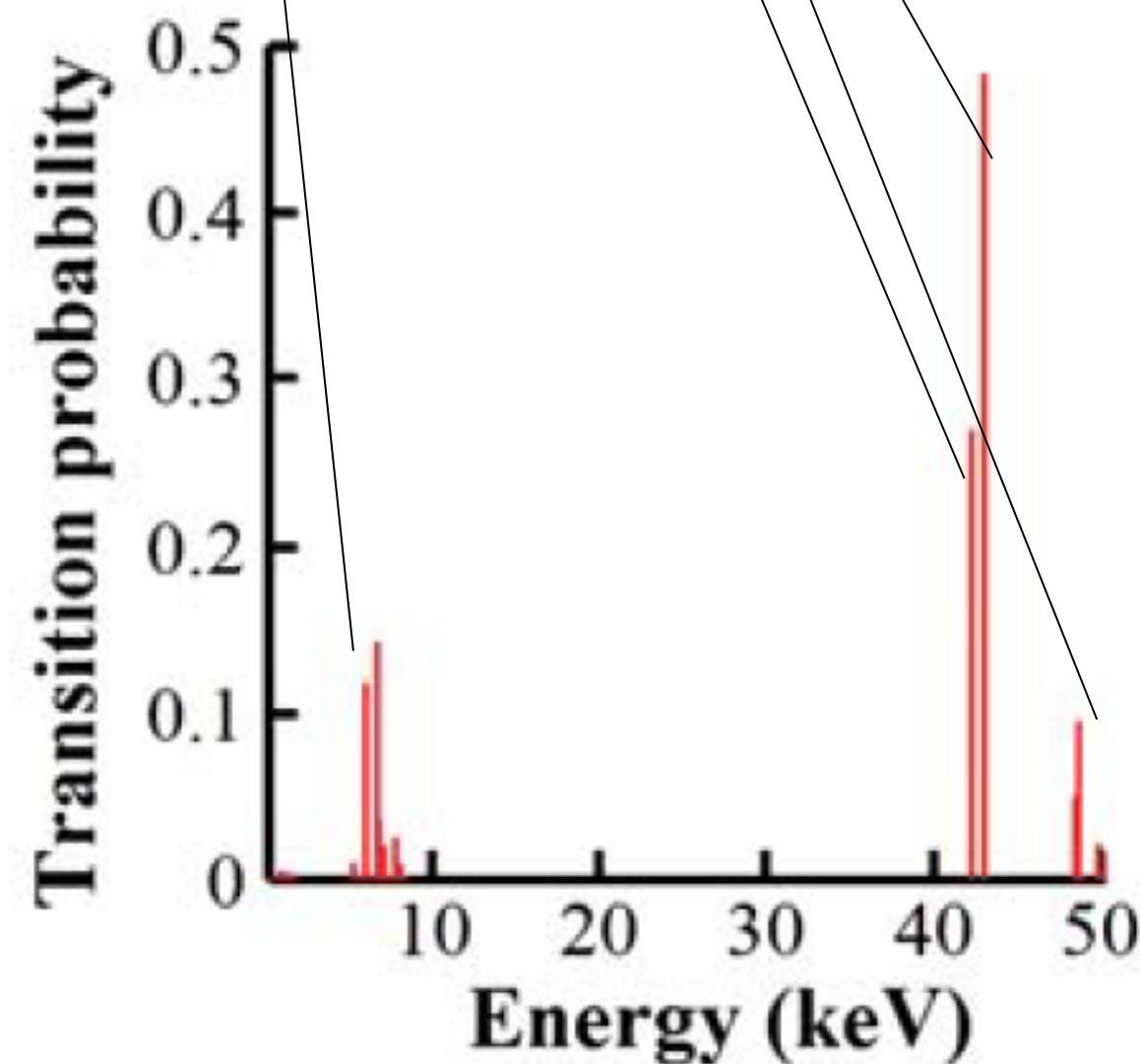
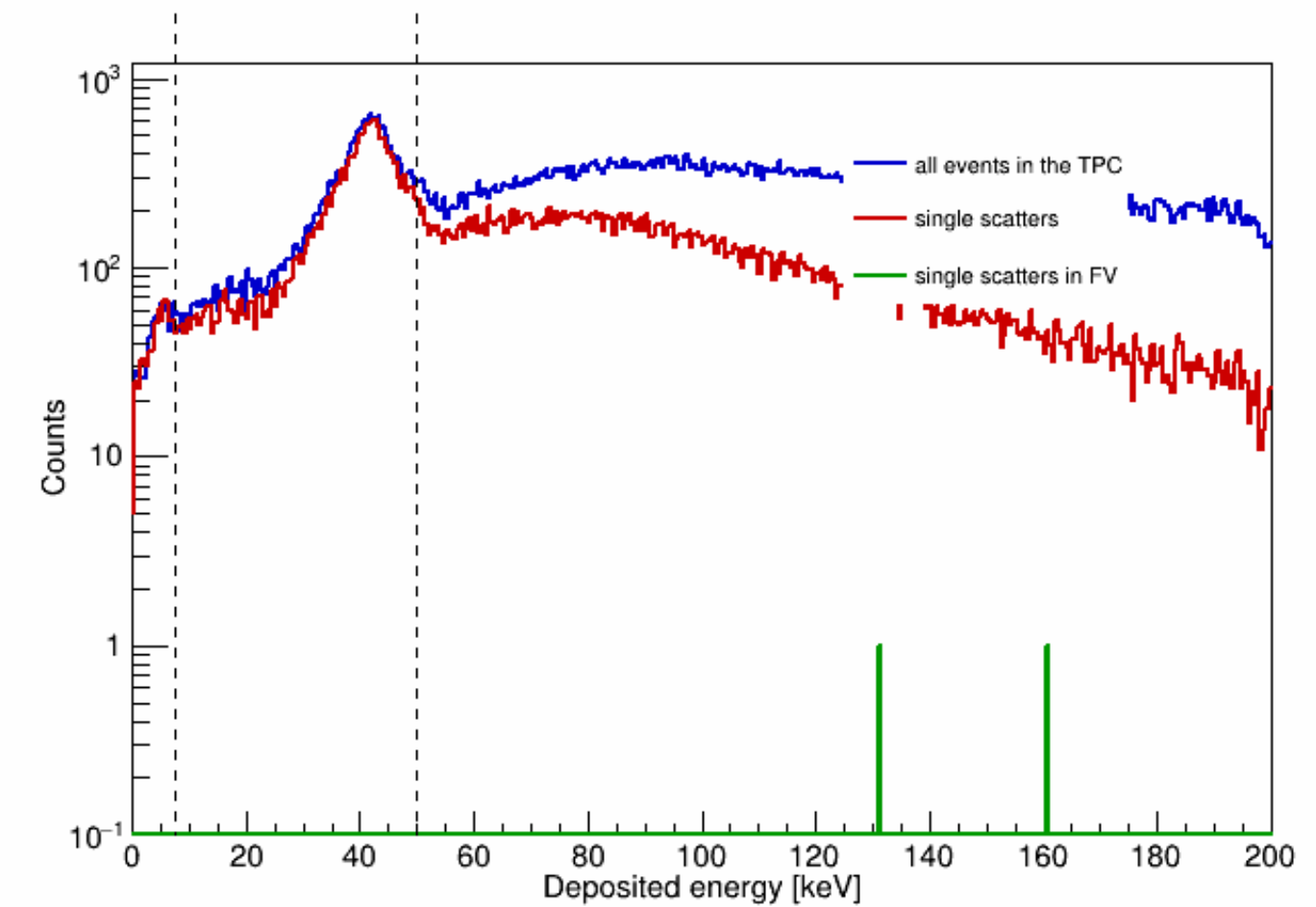
- Negligible (<1 E-5 events) wrt foreseen budget of 0.1 events after 10 years (200 t.y) = <0.01%
- Fully compatible with TDR results (980 kg of T<sub>7</sub> -> 1 E-3 events)

# ER background (1/3)

Gd impact - example of  $^{238}\text{U}$



$$\text{Res}(E) = 0.0023 + 0.334/\sqrt{E}$$



X-rays emitted during atomic relaxation of excited Gd atom

(Gamma-ray rejection, or detection, with gadolinium as a converter, P. Kandlakunta, DOI:10.1093/rpd/ncs031)

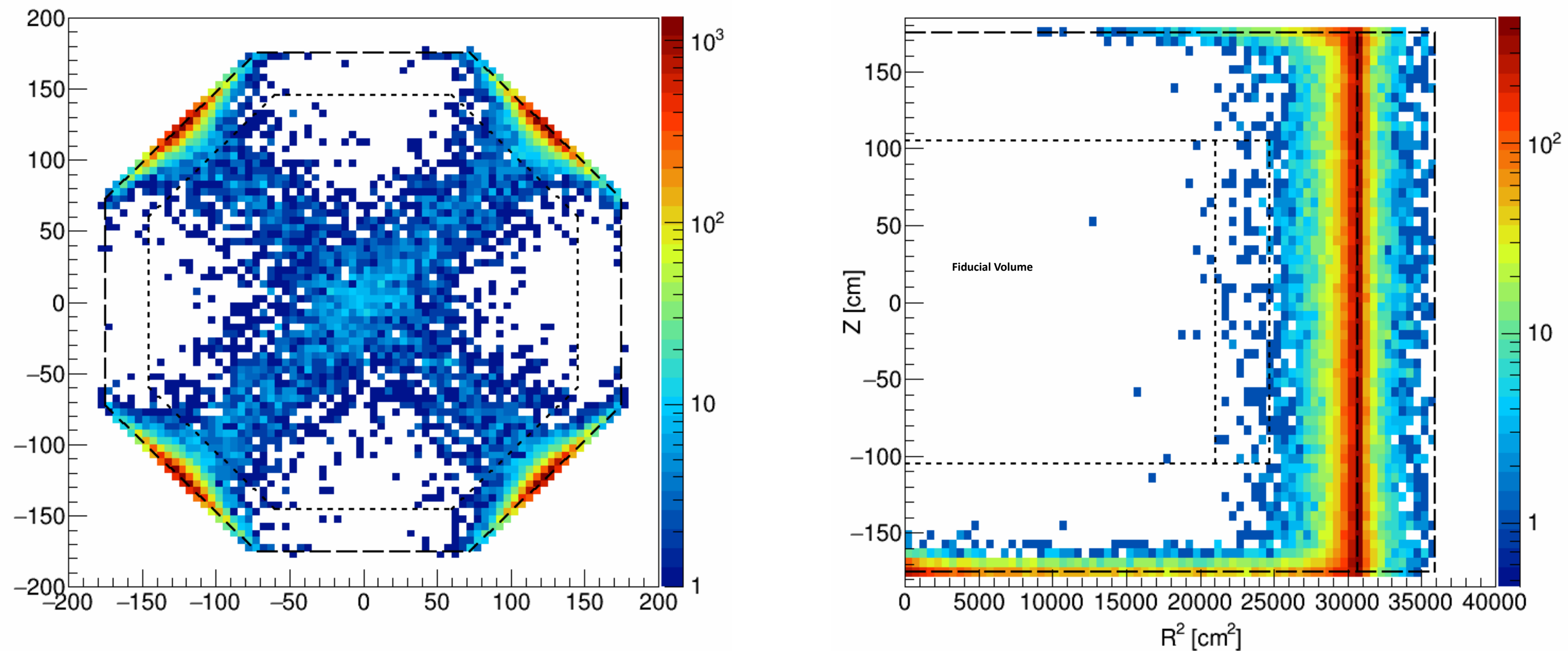
- This induces 10% to 70% more single scatter events at the ROI level in plan C wrt plan A
- However, none event survive the FV cut



# ER background (2/3)

## Events distribution - example of $^{238}\text{U}$

- Spatial distributions of Single Scatter events (no ROI requirement)



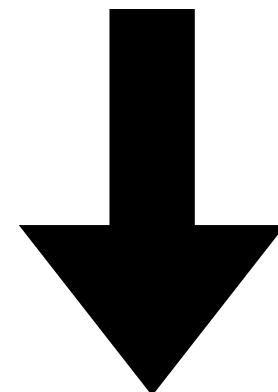
- No event left in fiducial volume after ROI requirement.

# ER background (3/3)

## Final computation

- No event left in fiducial volume after ROI requirement.

	<sup>238</sup> U up	<sup>238</sup> U mid	<sup>238</sup> U low	<sup>232</sup> Th	<sup>235</sup> U	<sup>40</sup> K	<sup>46</sup> Sc
Activity (mBq/kg)	8	0.12	80	0.12	0.37	0.6	3.1



x 17 kg  
x  $3.1 \cdot 10^7$  s/y  
x 2.3 events/ $10^7$  (no events after cuts)

	<sup>238</sup> U up	<sup>238</sup> U mid	<sup>238</sup> U low	<sup>232</sup> Th	<sup>235</sup> U	<sup>40</sup> K	<sup>46</sup> Sc
Events/y	<1.0	<0.02	<10	<0.02	<0.05	<0.07	<0.4

- This is before S2/S1 and PSD requirements ( $10^7$ - $10^8$  rejection) → ER background fully negligible!

# Conclusion

- Background induced by the calibration guide tubes is **negligible** ( $\ll$  budget of 0.1 events per 10 years) for **both ER and NR** sources of background
  - Results compatible with those in the TDR
- Yet, to be exhaustive, we still need to perform the NR background study coming from  $^{235}\text{U}$ , but **the spectrum is not available yet** in /g4ds/data/physics (see slide 4)

**Back up**

# Results quoted in the TDR

## NR bckgd in the TPC (vessel) / NR bckgd in the TPC (tubes)

Material or detector component	Mass [kg]	<sup>238</sup> U upper	<sup>238</sup> U middle	<sup>238</sup> U lower	<sup>232</sup> Th	<sup>235</sup> U	Number of neutrons [200 t yr] <sup>-1</sup>	Efficiency of cuts	Neutrons after cuts [200 t yr] <sup>-1</sup>	Bkg fraction [%]	Optical plane structures $= \frac{1e3}{1e3} = 1n \cdot kg^{-1}$	Tubes $1n \cdot kg^{-1}$
		Activity [mBq/kg]	Activity [mBq/kg]	Activity [mBq/kg]	Activity [mBq/kg]	Activity [mBq/kg]						
		Yield [n/decay]	Yield [n/decay]	Yield [n/decay]	Yield [n/decay]	Yield [n/decay]						
<b>TPC</b>												
Ultrapure acrylic	1978.0	$3.7 \times 10^{-3}$ $8.5 \times 10^{-8}$	1.2 $5.5 \times 10^{-7}$	1.2 $5.5 \times 10^{-8}$	$2.4 \times 10^{-3}$ $8.8 \times 10^{-7}$	$1.7 \times 10^{-4}$ $9.0 \times 10^{-7}$	$4.5 \times 10^2$	$5.8 \times 10^{-6}$	$2.6 \times 10^{-3}$	2.6		
Acrylic	2142.15	$2.5 \times 10^{-1}$ $8.5 \times 10^{-8}$	1.2 $5.5 \times 10^{-7}$	1.2 $5.5 \times 10^{-8}$	$2.4 \times 10^{-1}$ $8.8 \times 10^{-7}$	$1.1 \times 10^{-2}$ $9.0 \times 10^{-7}$	$6.6 \times 10^2$	$6.7 \times 10^{-7}$ $5.8 \times 10^{-6}$	$8.0 \times 10^{-4}$	0.8	$\approx 7 \cdot 10^{-7}$	$\approx 7 \cdot 10^{-7}$
Gd oxide	47.8	6.2 $2.7 \times 10^{-8}$	2.7 $1.2 \times 10^{-7}$	$2.7 \times 10^1$ $1.5 \times 10^{-8}$	2.3 $1.9 \times 10^{-7}$	$2.9 \times 10^{-1}$ $2.1 \times 10^{-7}$	$2.1 \times 10^1$	$6.7 \times 10^{-7}$	$1.4 \times 10^{-5}$	$1.4 \times 10^{-2}$		
Gd-acrylic	47.8	6.2 $8.2 \times 10^{-8}$	2.7 $5.5 \times 10^{-7}$	$2.7 \times 10^1$ $5.5 \times 10^{-8}$	2.3 $8.7 \times 10^{-7}$	$2.9 \times 10^{-1}$ $8.8 \times 10^{-7}$	$8.6 \times 10^1$	$6.7 \times 10^{-7}$	$5.8 \times 10^{-5}$	$5.8 \times 10^{-2}$	$\approx 1 \cdot 10^{-3}$	$\approx 1 \cdot 10^{-5}$
Titanium	980.0	8.0 $4.9 \times 10^{-9}$	$1.2 \times 10^{-1}$ $2.6 \times 10^{-6}$	$8.0 \times 10^1$ $1.6 \times 10^{-8}$	$1.2 \times 10^{-1}$ $6.5 \times 10^{-6}$	$3.7 \times 10^{-1}$ $2.6 \times 10^{-6}$	$1.05 \times 10^3$	$6.7 \times 10^{-7}$ $5.8 \times 10^{-6}$	$9.9 \times 10^{-4}$	0.99	For $10^3$ kg (Ti)	For 10 kg (Ti)
Sulfactant IGEPAL Co-520	47.8	$1.2 \times 10^{-1}$ $8.0 \times 10^{-8}$	1.20 $5.5 \times 10^{-7}$	$1.20 \times 10^1$ $5.5 \times 10^{-8}$	$4.1 \times 10^{-2}$ $8.8 \times 10^{-7}$	$5.5 \times 10^{-3}$ $8.8 \times 10^{-7}$	$2.1 \times 10^1$	$6.7 \times 10^{-7}$	$1.4 \times 10^{-5}$	$1.4 \times 10^{-2}$		
Stainless steel for the TPC	1055.0	$4.0 \times 10^{-1}$ $3.9 \times 10^{-10}$	$4.0 \times 10^{-1}$ $5.8 \times 10^{-7}$	$4.0 \times 10^{-1}$ $9.25 \times 10^{-10}$	$8.0 \times 10^{-1}$ $2.0 \times 10^{-6}$	$1.8 \times 10^{-2}$ $4.6 \times 10^{-7}$	$6.2 \times 10^2$	$5.8 \times 10^{-6}$	$3.6 \times 10^{-3}$	3.6		
Shaping rings copper parts	$1.7 \times 10^{-1}$	$3.3 \times 10^{-1}$ 0.0	1.6 $3.8 \times 10^{-8}$	$1.6 \times 10^1$ 0.0	$1.0 \times 10^{-2}$ $3.1 \times 10^{-7}$	$1.5 \times 10^{-2}$ $1.8 \times 10^{-8}$	$3.4 \times 10^{-3}$	$5.8 \times 10^{-6}$	$2.0 \times 10^{-8}$	$2.0 \times 10^{-5}$		
Shaping rings resistors	$7.1 \times 10^{-3}$	$3.7 \times 10^3$ $3.6 \times 10^{-7}$	$7.0 \times 10^3$ $4.2 \times 10^{-6}$	$8.2 \times 10^3$ $3.1 \times 10^{-7}$	$9.7 \times 10^2$ $7.1 \times 10^{-6}$	$7.1 \times 10^{+2}$ $6.3 \times 10^{-6}$	$1.0 \times 10^2$	$5.8 \times 10^{-6}$	$5.8 \times 10^{-4}$	0.58		
Shaping rings resistors solder	$4.9 \times 10^{-3}$	$2.8 \times 10^1$ $2.5 \times 10^{-9}$	$7.2 \times 10^2$ $2.1 \times 10^{-7}$	$7.2 \times 10^2$ $4.7 \times 10^{-9}$	$2.8 \times 10^1$ $4.2 \times 10^{-7}$	1.3 $2.8 \times 10^{-7}$	$2.6 \times 10^{-1}$	$5.8 \times 10^{-6}$	$1.5 \times 10^{-6}$	$1.5 \times 10^{-3}$		
PCB substrate Arlon 55NT	$6.6 \times 10^{-2}$	53.0 $7.9 \times 10^{-8}$	53.0 $9.6 \times 10^{-7}$	128.0 $5.3 \times 10^{-8}$	70.0 $1.6 \times 10^{-6}$	2.4 $1.3 \times 10^{-6}$	3.7	$5.8 \times 10^{-6}$	$2.1 \times 10^{-5}$	$2.1 \times 10^{-2}$		

TABLE XXII. Simulated radiogenic neutron rates from the detector materials over the full 200 t yr fiducial volume exposure.