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DI TRENTO



# *Geodesic reference performance limits for space gravitational wave missions*

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*Università di Trento / INFN*

*for the LISA Pathfinder Project*



*Gravitational Wave Advanced Detector Workshop*

*Isola d'Elba, 24 May 2013*



# GW detection as “differential accelerometry” measurement

- Tidal accelerations between 2 or more geodesic reference test masses
- Need reference masses in free-fall(\*) and measurement of their separation

$$\Delta a_h \approx \omega^2 Lh$$

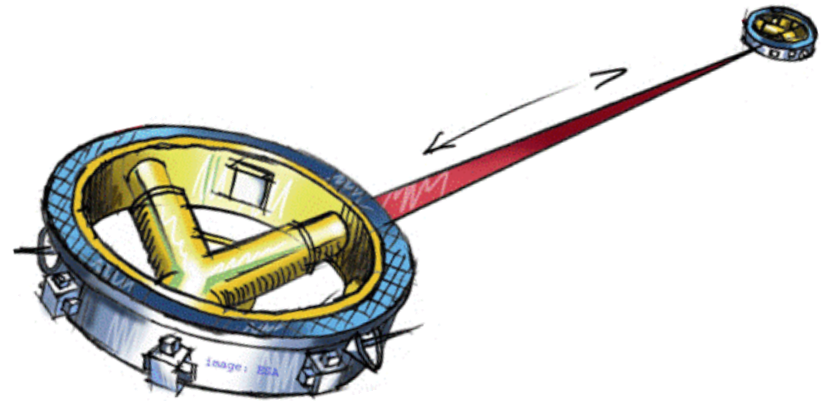
Effective “GW  
acceleration”

$$\Delta a_{\text{measure}} \approx \omega^2 x_n$$

distance  
measurement noise

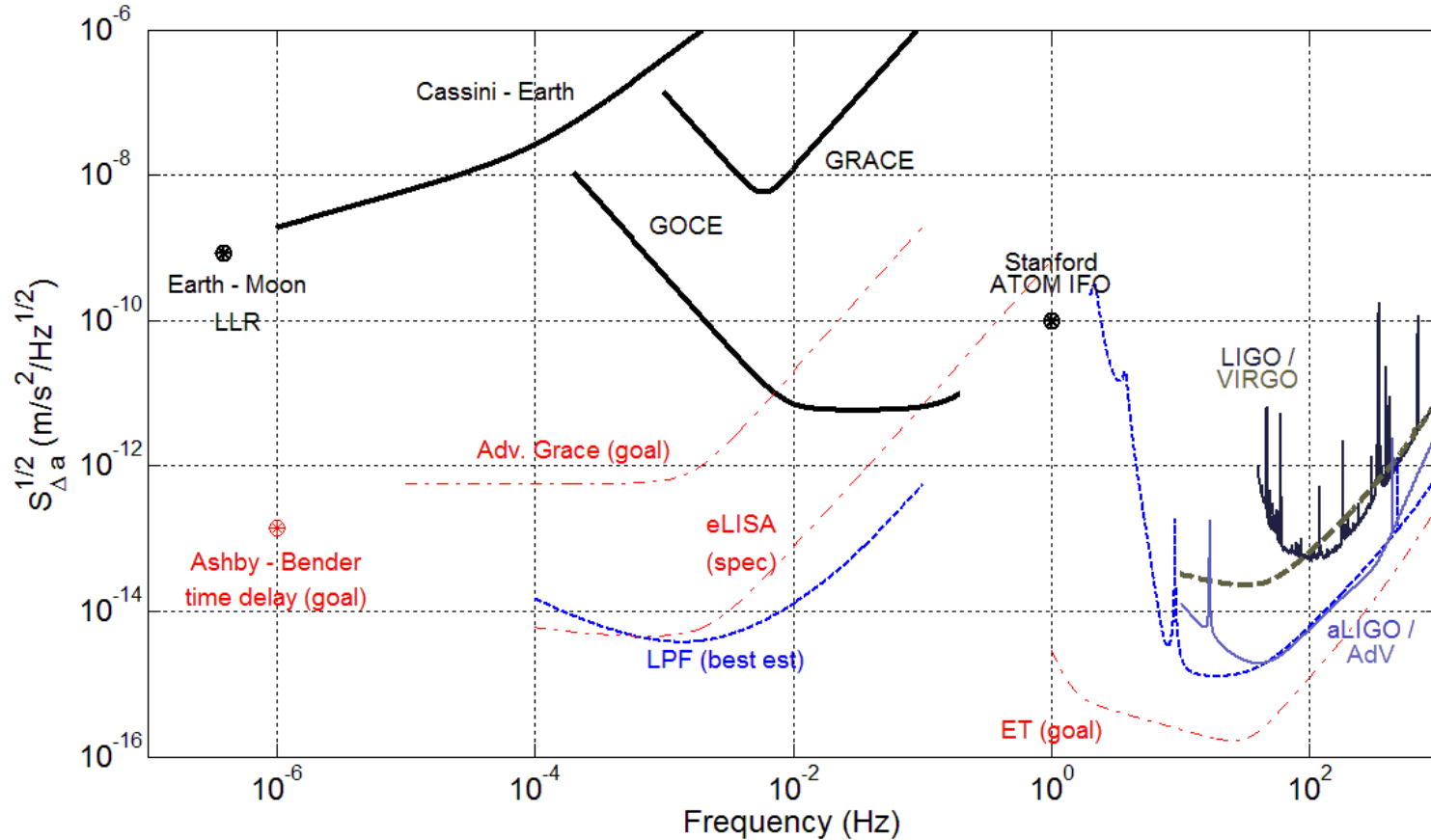
$$\Delta a_{\text{force}} \approx \frac{\Delta f}{m}$$

Stray force noise  
(imperfect geodesic  
motion)



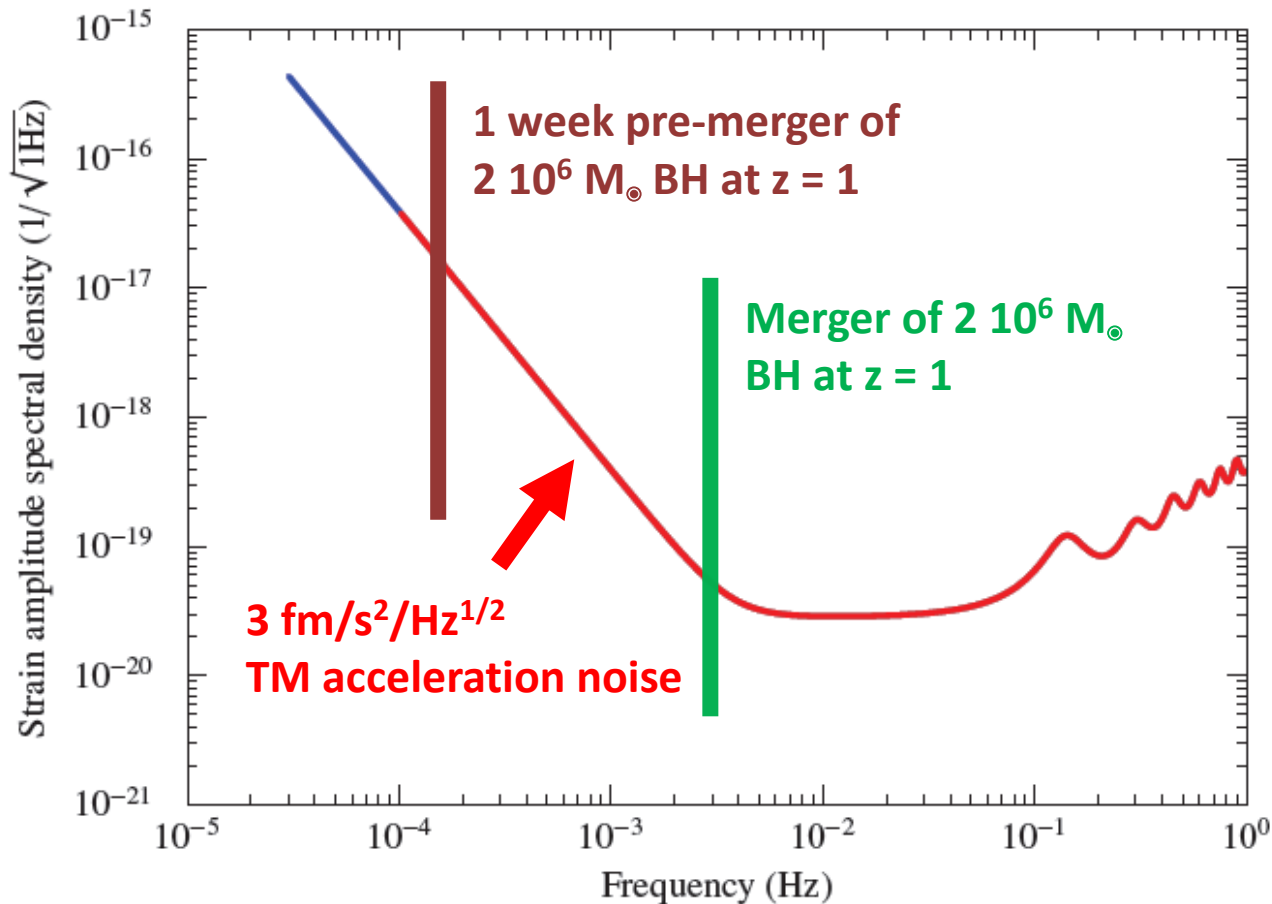
(\*) Force free except for known, calibrated control / suspension forces

# Differential acceleration measurement in experimental gravitation



- space GW observation: requirements and design
- What we know: main limits, tests on ground and space (LISA Pathfinder)
- Extensions of eLISA /LPF GRS heritage to future missions

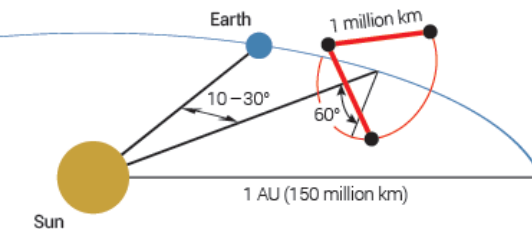
# eLISA Strain Noise and Massive Black Hole Science



- Acceleration noise dominates GW sensitivity below 5 mHz
- Low frequency performance critical to massive black hole science

# eLISA Measurement Concept

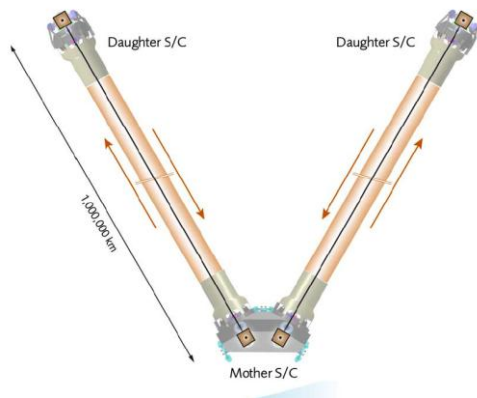
[ESA L2 mission candidate: <http://support.elisascience.org/>]



- synthesized 1 million km Michelson with free-falling TM
- interferometer TM – TM measurement in 3 parts:

TM-SC → SC-SC → SC-TM

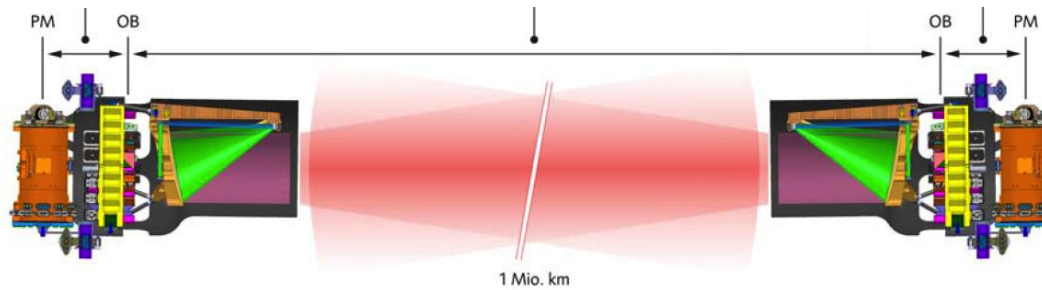
→ **12 pm/Hz<sup>1/2</sup>**



- Drag-free TM → SC follows TM along sensitive axes

→ **3 fm/s<sup>2</sup>/Hz<sup>1/2</sup>**

- nm/Hz<sup>1/2</sup> spacecraft control
- nN force control on non-IFO axes

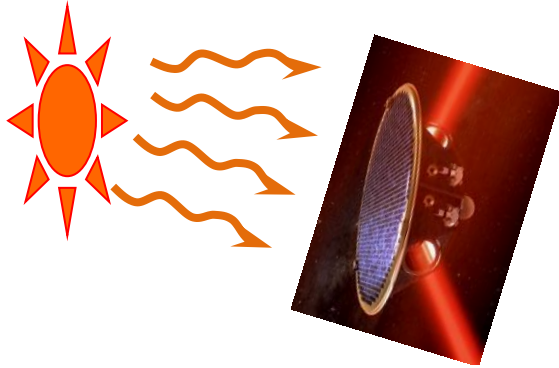


Test mass  
Inside GRS

# The road to eLISA GRS design (what we can't do)

## Spacecraft as a geodesic reference (Cassini, Pioneer)

Solar radiation pressure



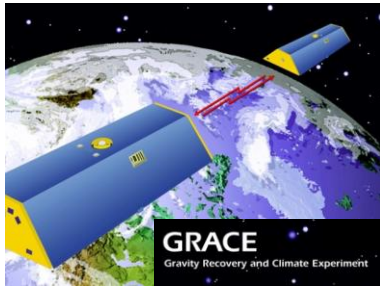
On a 5 m<sup>2</sup> / 300 kg spacecraft

DC acceleration      **100 nm/s<sup>2</sup>**

Fluctuations      **10<sup>-10</sup> m/s<sup>2</sup>/Hz<sup>1/2</sup>**

Locating spacecraft CM also difficult

## A reference TM accelerometer to correct satellite motion

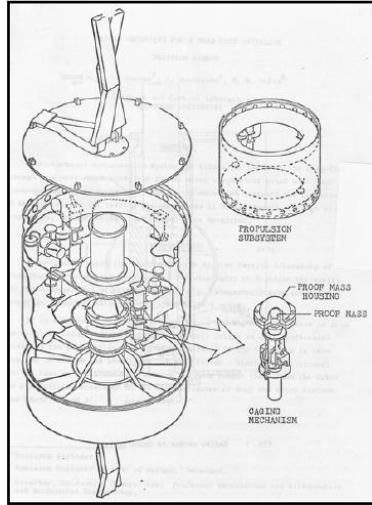


- Microwave ranging between satellites
- Accelerometers corrects for non-inertial spacecraft motion
- Accelerometer TM “forced” to follow spacecraft

→ can't apply 100 nm/s<sup>2</sup> with < fm/s<sup>2</sup>/Hz<sup>1/2</sup> noise

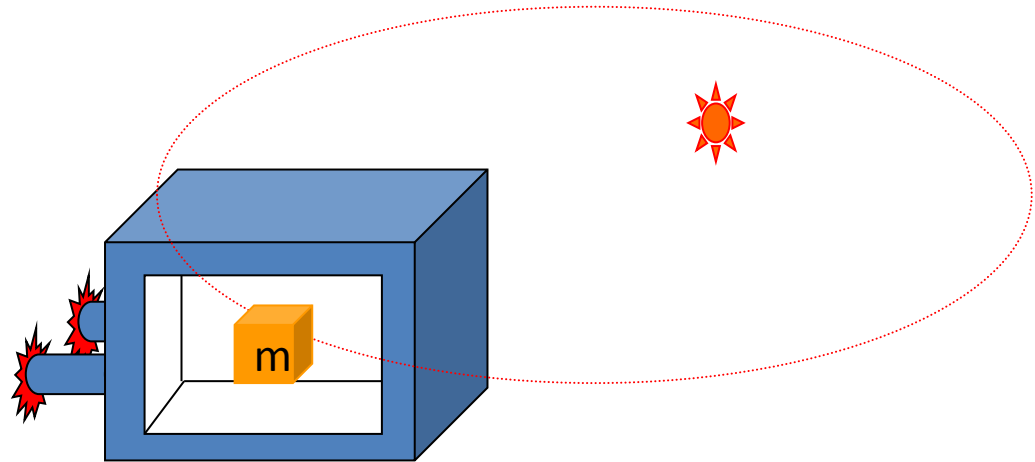
→ Requires “drag-free” spacecraft shielding a free-falling reference TM

# Drag-free control for precision geodesic reference TM



TRIAD, 1972  
[from CQG **28**, 094015 (2011)]

- Triad, GPB
- Control satellite to follow a free-falling reference TM
  - Microthrusters with control gain  $\omega_{DF}^2$
- No forces on TM, at least on measurement axis



$$a_{res} = g + \omega_p^2 \left( x_n + \frac{F_{SC}}{M\omega_{DF}^2} \right)$$

SC jitter  $\Delta x$

Free-fall of TM limited by:

- $g$  – acceleration from noisy stray forces
- $\omega_p^2 * \Delta x$  – elastic coupling \* SC jitter

**For LISA: need free-falling TM (not satellite)**



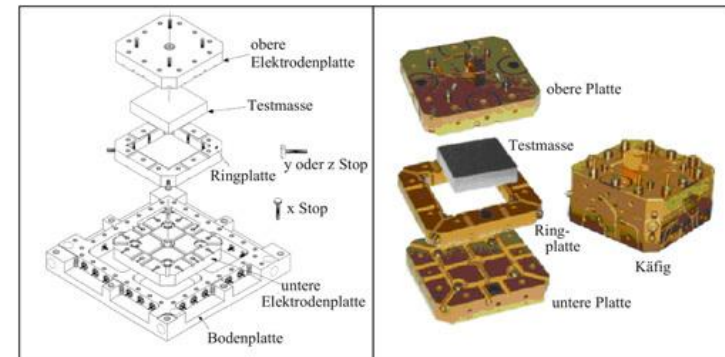
# Existing space electrostatic accelerometers

## TM – electrode gaps of order 100 microns

GPB (30  $\mu\text{m}$ ), GRACE/GOCE/ $\mu$ -Scope (200-300  $\mu\text{m}$ )

With 300  $\mu\text{m}$  gaps

- Electrostatic: 10  $\mu\text{V}/\text{Hz}^{1/2}$ , 10 mV  $\rightarrow$  10  $\text{fN}/\text{Hz}^{1/2}$
- Brownian gas noise,  $10^{-8}$  mB  $\rightarrow$  30  $\text{fN}/\text{Hz}^{1/2}$

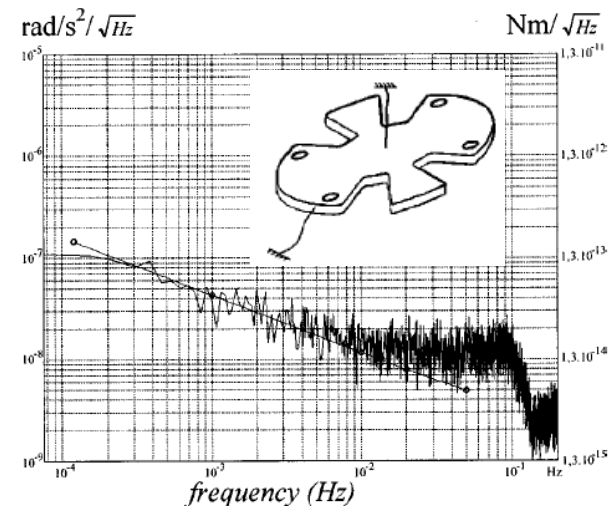


## Thin TM discharge wire

GRACE/GOCE/ $\mu$ -Scope

7  $\mu\text{m}$  Au wire  $\rightarrow$  thermal noise  $\text{pN}/\text{Hz}^{1/2}$  at 1 mHz

**$\rightarrow$  Need big gaps, no strings attached!**

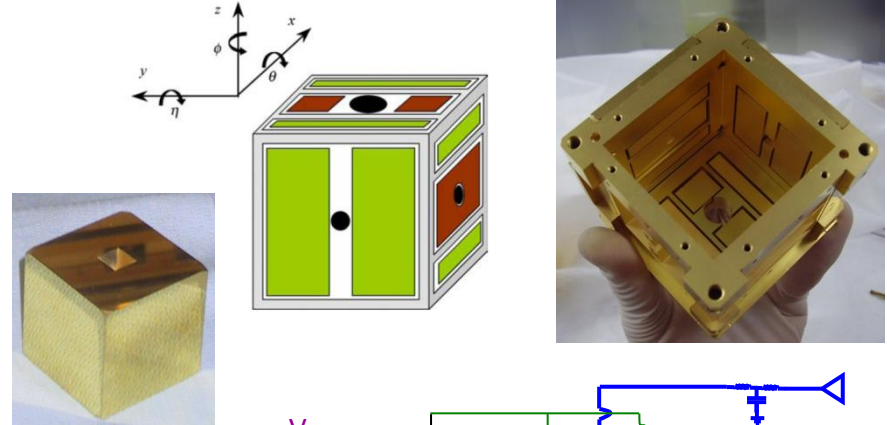


Willemenot and Touboul  
*Rev Sci Inst* **71**, 302 (2000)



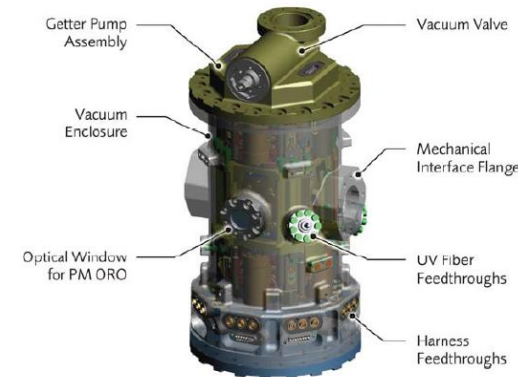
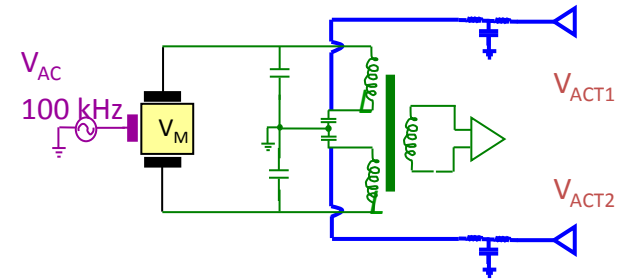
# eLISA / LISA Pathfinder gravitational reference sensor (GRS)

- Defines TM environment
- $\text{nm}/\text{Hz}^{1/2}$  measurement on all axes
  - $10 \text{ pm}/\text{Hz}^{1/2}$  interferometer used on x axis
- nN actuation forces ( $\mu\text{N}$  non-science)



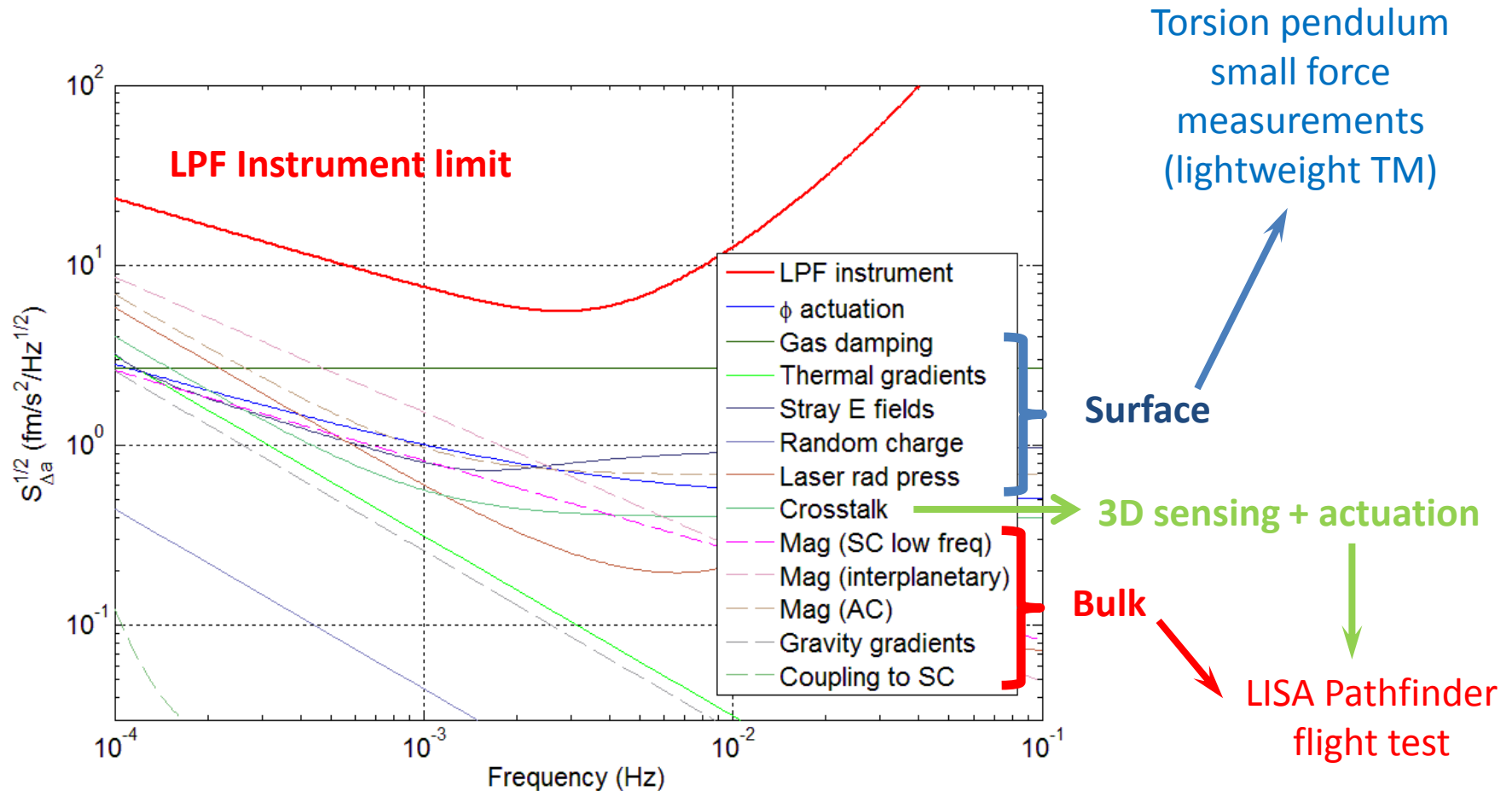
## GRS design for LISA PF / LISA

- 46 mm cubic Au / Pt test mass (2 kg)
- 6 DOF capacitive “gap” sensor w/ AC readout
- Audio freq electrostatic force actuation → avoid DC voltages
- Large gaps (3 – 4 mm) → limit electrostatic disturbances
- High thermal conductivity metal / sapphire → limit thermal gradients
- High vacuum ( $p = 2 \mu\text{Pa}$ ) → limit Brownian, radiometric effects
- UV photoelectric discharge
- Caging mechanism for launch lock

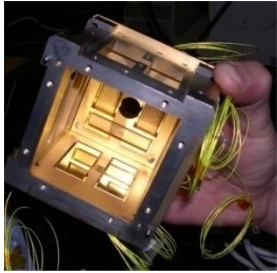


# Sources of acceleration noise

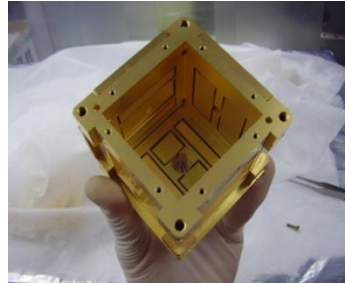
- What do we know about about stray forces and what will we learn with LPF?
- What should we be able to “guarantee” for eLISA and beyond?



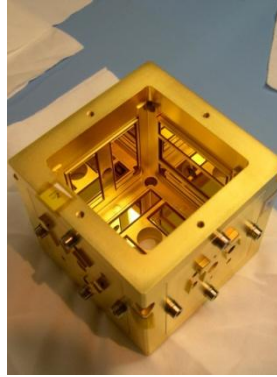
# Torsion pendulum measurement of surface forces: free-fall inside LISA / LPF GRS prototypes



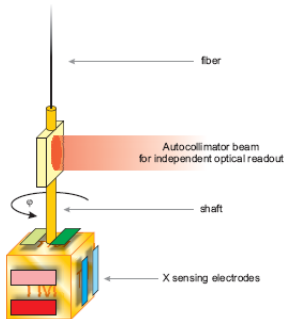
Mo / Shapal EM  
(4 mm gaps,  
LPF geometry)



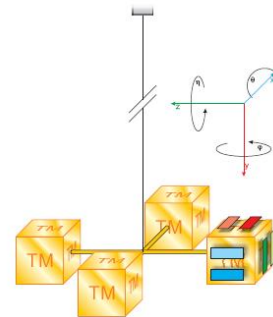
Mo / Sapphire LPF EM



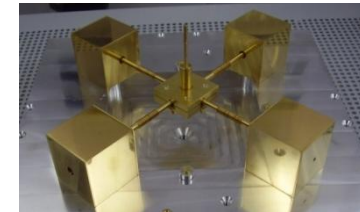
LPF FM-replica +  
ELM electronics



1-mass torsion  
pendulum  
(torques)



4TM pendulum  
(force sensitivity)

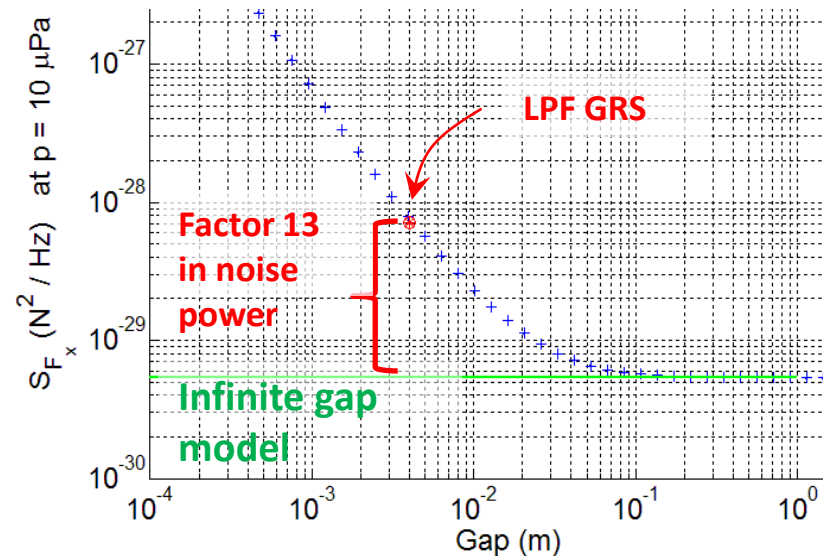
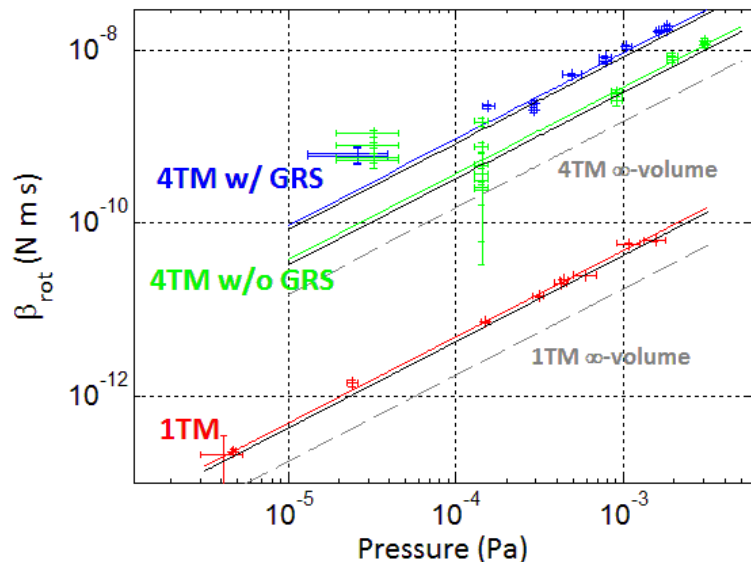
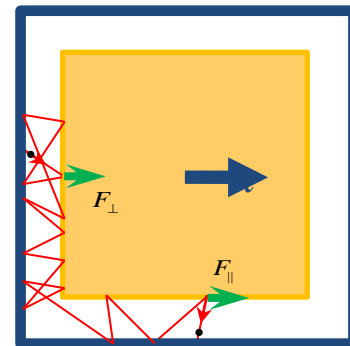


Lightweight TM → test surface forces  
Trento, UW, Firenze / Roma / Napoli, Florida  
Bulk forces (grav + mag) tested separately with LPF

# Noise source: Residual gas impacts

Excess damping + Brownian noise in constrained volume

*PRL*, **103** 140601 (2009) , *Phys Lett A*, **374** 3365 (2010)



## Single TM gas damping noise

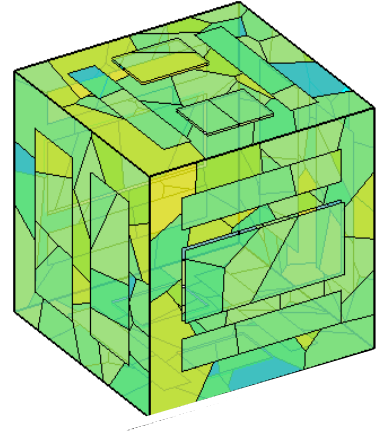
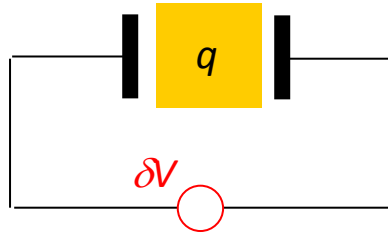
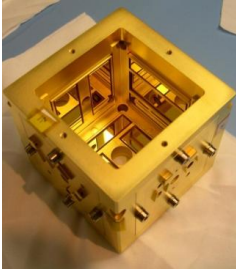
$$S_a^{1/2} \approx 1.8 \text{ fm/s}^2 / \text{Hz}^{1/2} \times \left( \frac{p}{2 \mu\text{Pa}} \right)^{1/2} \left( \frac{m_0}{30} \right)^{1/4}$$

- well modeled and measured
- OK for LISA with 2  $\mu\text{Pa}$
- vent to space  $\rightarrow$  should do much better!

# Noise source: stray electrostatics inside GRS

- Conducting Au-coated shield not truly equipotential (patch effects)
- TM charged randomly by cosmic rays (1/f or worse!)

[Requires periodic or continuous discharge (UV)]



## Largest interaction: TM charge + average residual E field

PRL **108**:181101 (2012)

$$F_x = q \langle E_x \rangle = -q \Delta_x \left[ \frac{1}{C_{TOT}} \left| \frac{\partial C_x}{\partial x} \right| \right]$$

$$\Delta_x \equiv \frac{1}{\left| \frac{\partial C_x}{\partial x} \right|} \sum_{i(TM), j(S)} \frac{\partial C_{ij}}{\partial x} (\delta V_i - \delta V_j)$$

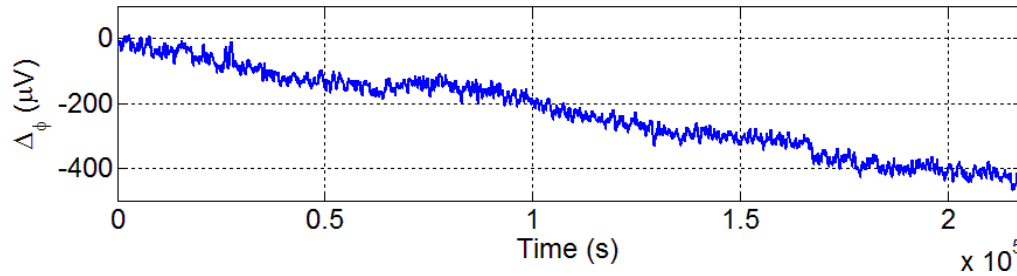
$\Delta_x$ : equiv. single electrode potential

- Measure and compensate average DC field

from  $\Delta \approx 100$  mV intrinsic to better  $\Delta < 1$  mV  
lots of experience in lab, will test on LPF

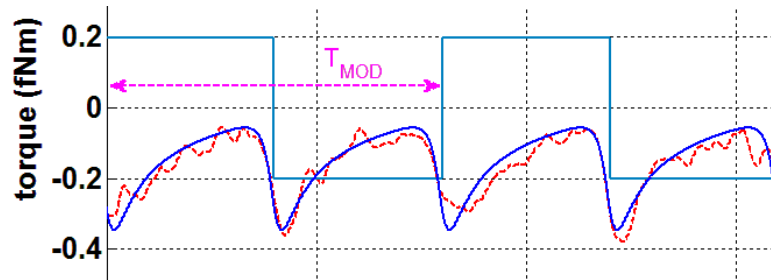
- Need stray potential fluctuations  $< 20\text{-}50 \mu\text{V}/\text{Hz}^{1/2}$

# Lab measurement of stray surface potential fluctuations



$$S_{\Delta_x}^{1/2} < 80 \mu\text{V}/\text{Hz}^{1/2} \text{ at } 1 \text{ mHz}$$

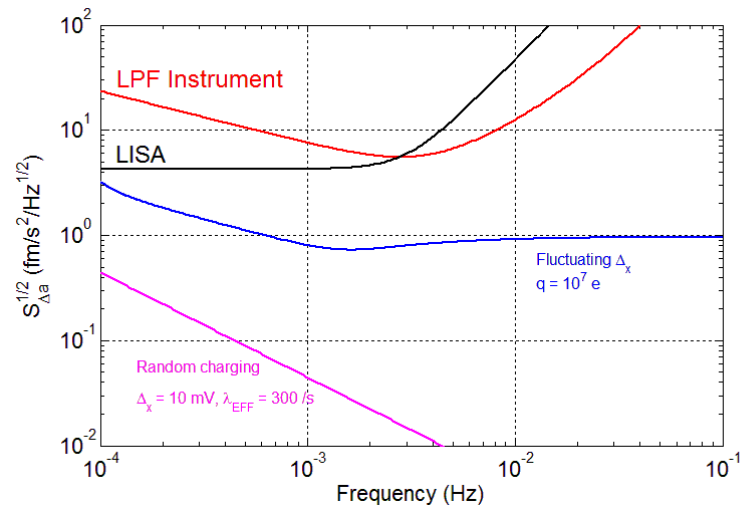
- Single electrode (500 mm<sup>2</sup>) average surface potential noise < 12  $\mu\text{V}/\text{Hz}^{1/2}$



- Upper limits already acceptable for eLISA
- Marginal at 0.1 mHz
- Improving lab measurement

Electrostatic dissipation (thermal noise):

- “Vacuum gap” capacitor: detect  $\delta = 3 \cdot 10^{-7}$
- Thermal contribution  $\approx 1 \mu\text{V}/\text{Hz}^{1/2}$





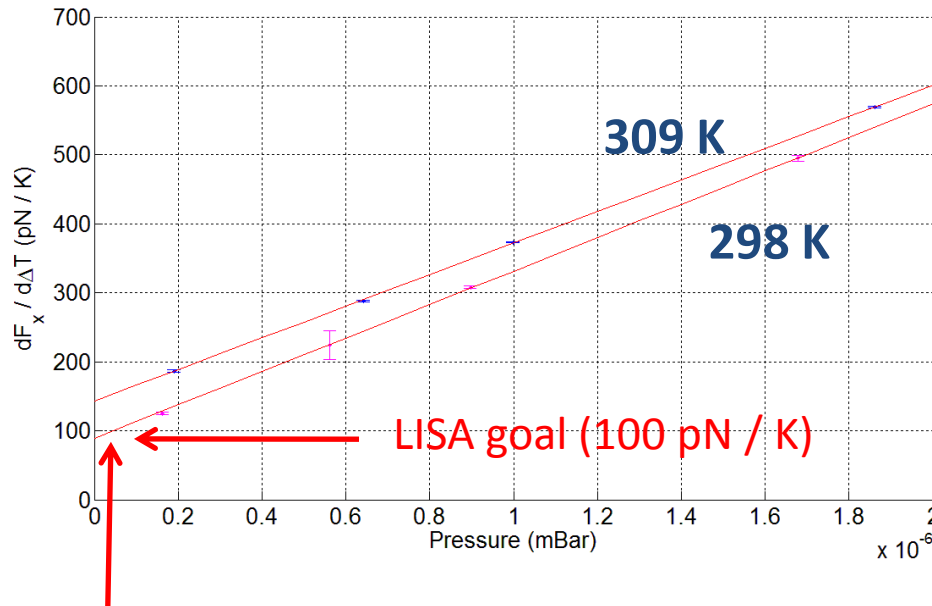
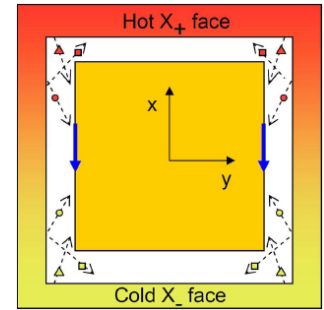
# Noise source: Thermal gradient-induced forces

[PRD, **76** 102003 (2007); CQG, **26** 094012 (2009)]

→ Noise budget:  $dF/d\Delta T \sim 100 \text{ pN / K}$   
 $S_{\Delta T}^{1/2} < 10 \text{ } \mu\text{K / Hz}^{1/2}$

→ Radiometric and radiation pressure effects well modeled

→ Asymmetric outgassing requires measurement (applied  $\Delta T$ )



## Force measurement with EM GRS

- Verify radiometric model (10%)
- Outgassing observed (pre-bake)
  - $p = 0$  data increase faster than radiation pressure  $T^3$
- OK for LPF and LISA

2  $\mu\text{Pa}$



W. J. Weber  
GWADW, May 2013

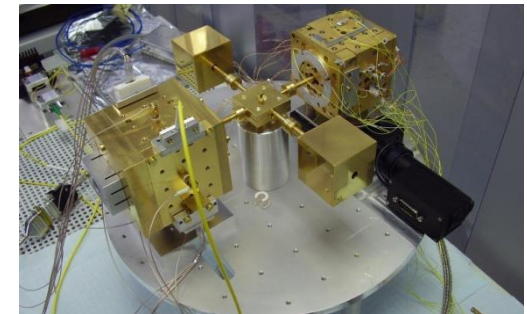
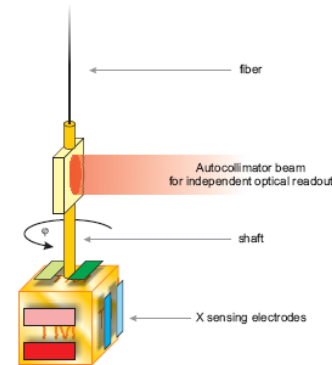
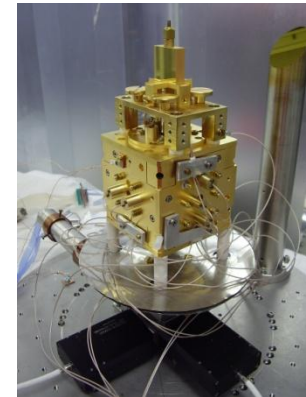
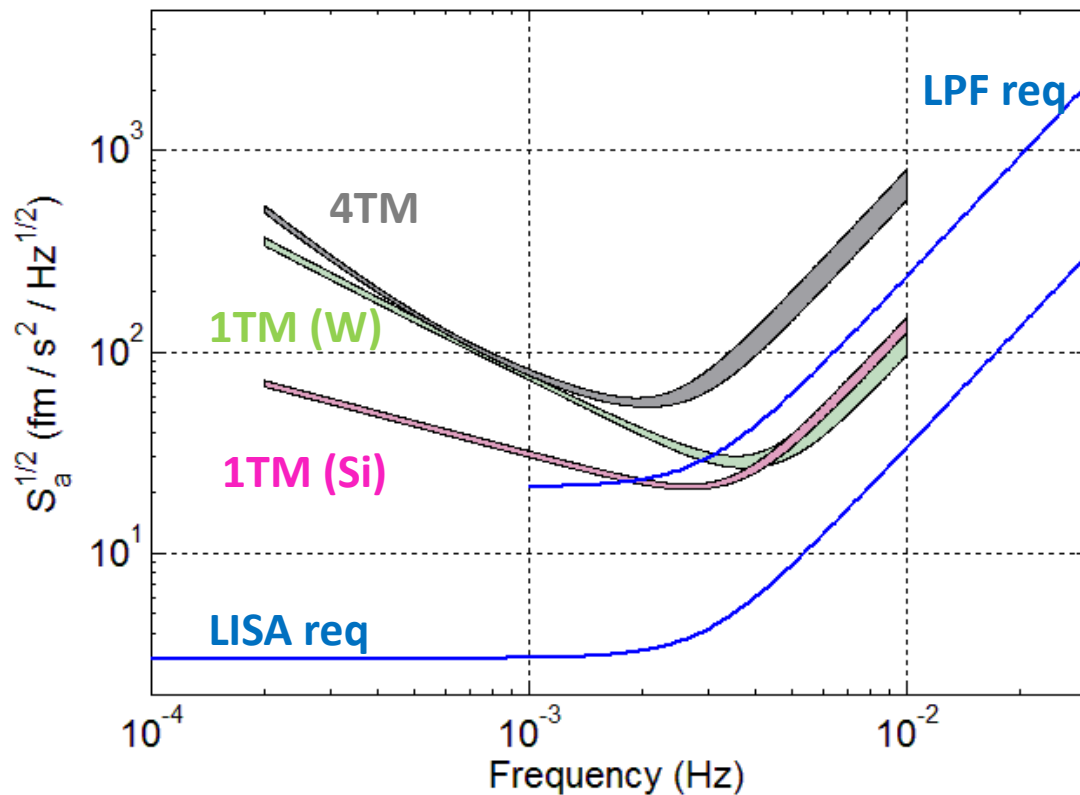


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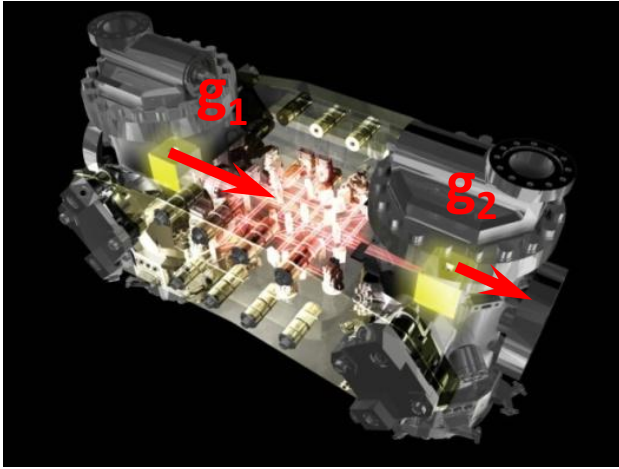


# Torsion pendulum upper limits on GRS force noise: conversion from torque $\rightarrow$ force $\rightarrow$ acceleration

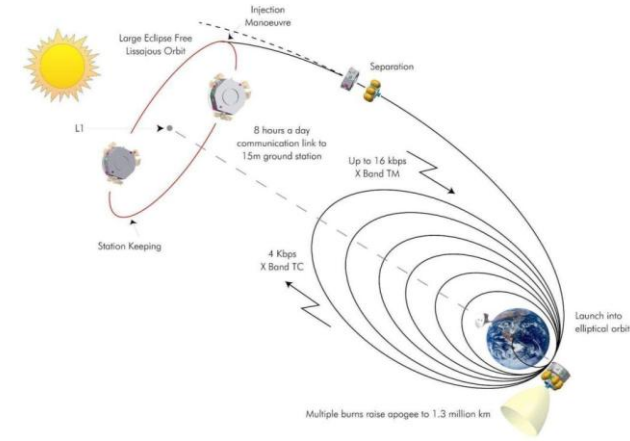


- rule out large class of TM surface disturbances at level of  $30 \text{ fm/s}^2/\text{Hz}^{1/2}$  at 1 mHz
  - within factor 1.5 of LPF goal
  - **bulk forces  $\rightarrow$  LISA Pathfinder**

# LISA Pathfinder: Einstein's Geodesic Explorer (2015)



At L1 Lagrange point

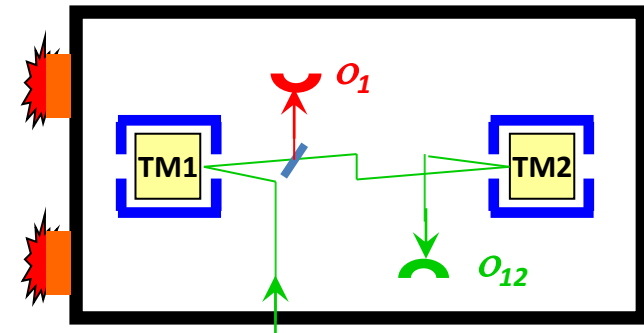


**Compress single eLISA arm to 40 cm inside 1 spacecraft**

**Measure differential TM acceleration**

Test of eLISA GRS and local IFO measurement

- flight heritage for eLISA
- commissioning for eLISA in-flight operations:
  - drag-free, TM uncaging and discharge, calibrations and tuning
- physical model of disturbances for free-falling reference TM



# LISA Pathfinder as differential accelerometer (time domain)

## Newton's Eqns:

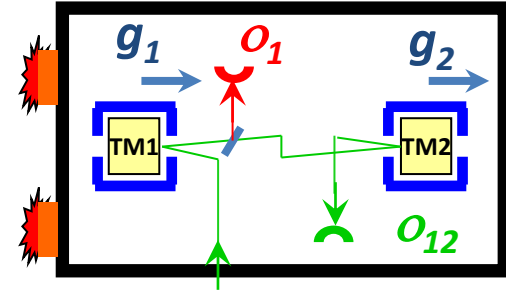
$$m\ddot{x}_1 = mg_1 - m\omega_{1p}^2(x_1 - x_{SC})$$

$$m\ddot{x}_2 = mg_2 - m\omega_{2p}^2(x_2 - x_{SC}) + F_{ES}$$

## IFO Readouts :

$$o_{12} = x_2 - x_1 + n_{12}$$

$$o_1 = x_1 - x_{SC} + n_1$$



## Control

Drag-free:

thrust SC to follow TM1

(null **o1**, 1 Hz BW)

Electrostatic suspension:

force TM2 to follow TM1

(null **o12**, 1 mHz BW)

## IFO Acceleration

$$g_2 - g_1 = \ddot{o}_{12} - F_{ES} + (\omega_{2p}^2 - \omega_{1p}^2)o_1 + \omega_{2p}^2 o_{12}$$

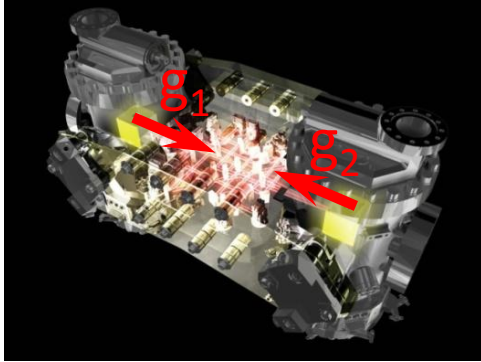
↑ Commanded control forces
 ↑ Elastic coupling

## IFO Noise

$$+ \ddot{n}_{12} + (\omega_{2p}^2 - \omega_{1p}^2)n_1 + \omega_{2p}^2 n_{12}$$

- Produce differential acceleration time series  $\mathbf{g}_2 - \mathbf{g}_1$
- Spacecraft coupling term (stiffness) subtracted (also for LISA)
- Need to measure dynamic parameters: stiffness, actuator calibration, crosstalk

# LPF instrument limit: noisy compensation of DC gravity imbalance



Noise in “DC” force applied to compensate difference in local  $g$

→ **Not present in eLISA!!**

$$F \propto V_{ACT}^2 \quad \rightarrow \quad S_a^{1/2} \approx 2 \Delta g S_{\delta V/V}^{1/2}$$

**Design  
specs**

$$\Delta g < 1.3 \text{ nm/s}^2$$

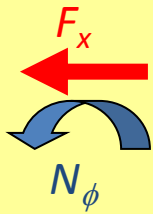


Current **calculations** look better!

$$S_{\delta V/V}^{1/2} < 2 \times 10^{-6} \text{ /Hz}^{1/2}$$



Current measurements 2-3 worse

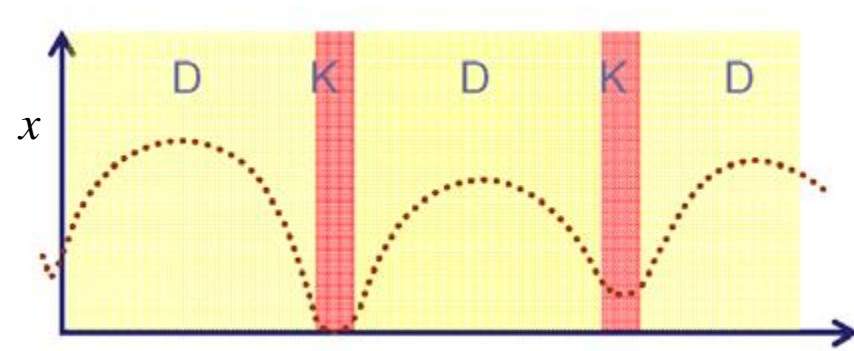


- **Expect  $< 8 \text{ fm/s}^2/\text{Hz}^{1/2}$  at 1 mHz**

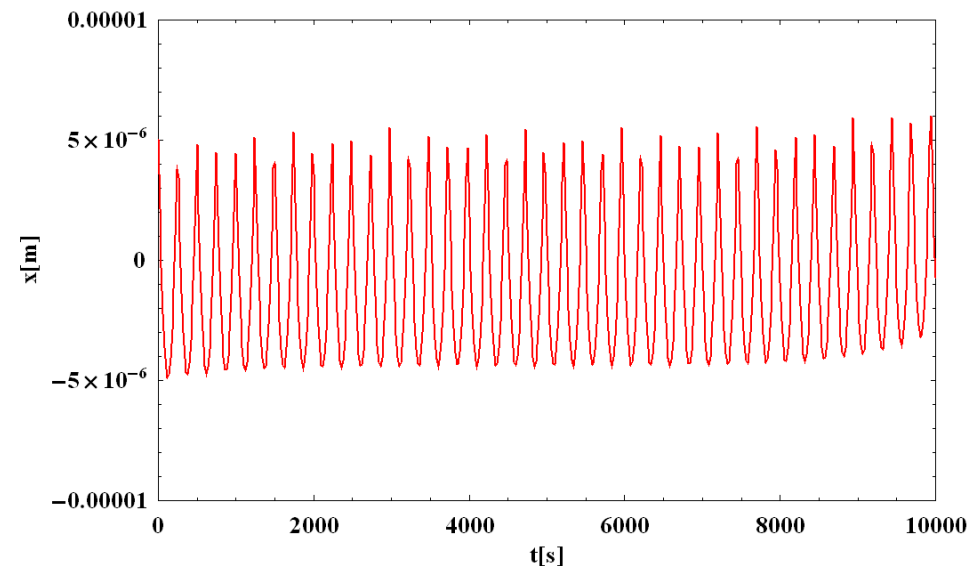
- full analysis complicated by uncorrelated voltage fluctuations,  $\phi$  act

# LISA Pathfinder: avoiding actuation fluctuations with free-fall mode

compensate average DC force imbalance by applying a large impulse followed by free-fall (parabolic flight!)

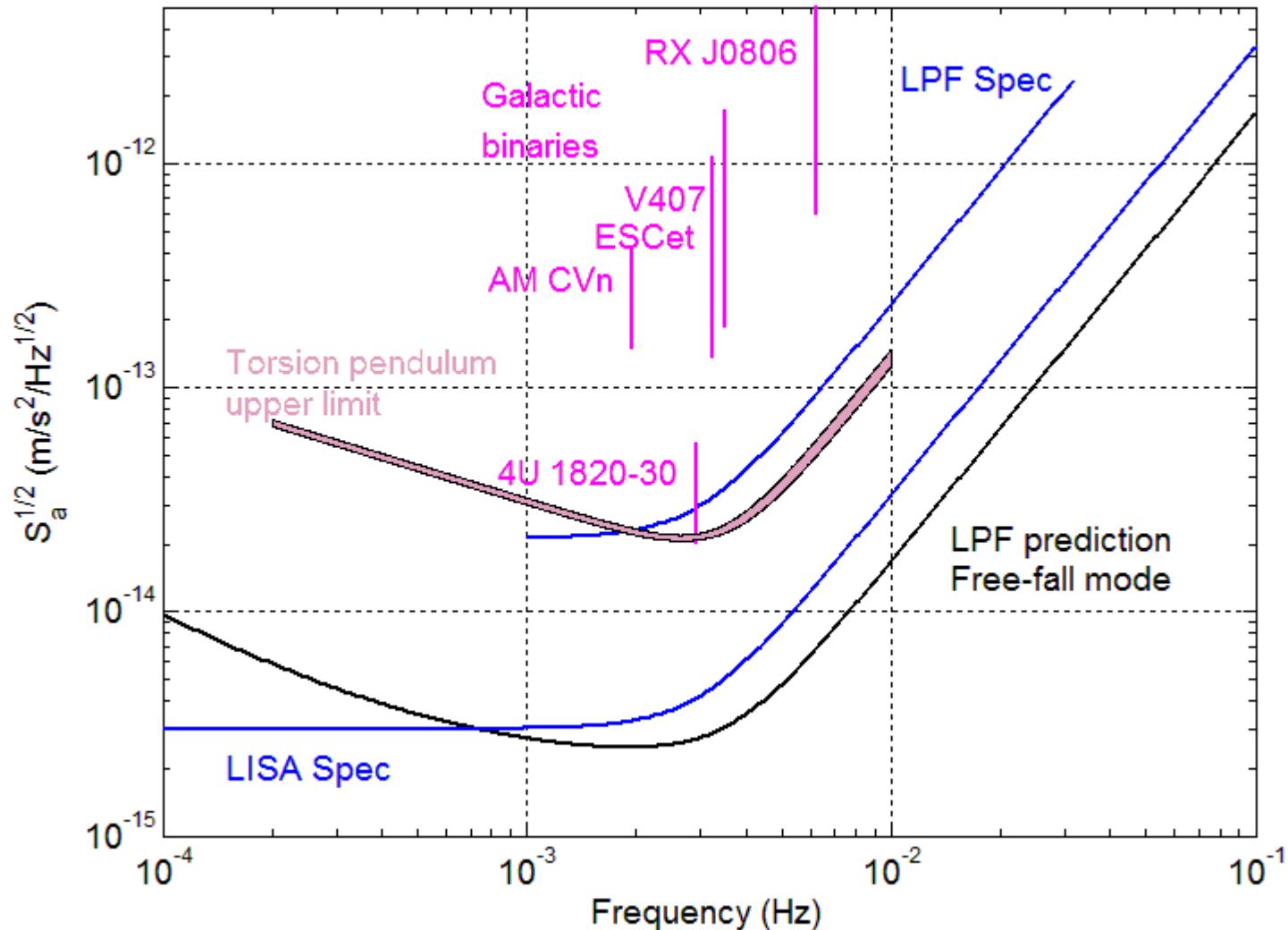


Grynagier, *CQG* **26** (2009) 094007



- Example: Apply 250 x average needed force for 1s, followed by 249 s free-fall
- Keep displacement to 10 micron range
- Throw out data during impulses to measure acceleration noise ***without applied actuation forces***, even to lower frequencies (careful analysis)

# LISA Pathfinder performance prediction in free-fall mode



**LISA Pathfinder should guarantee most of LISA science**

W. J. Weber  
GWADW, May 2013

## LPF also measures

- Measure spacecraft **g** (3 translations and 6 rotations)  
Test gravitational balance to better than  $10^{-10} \text{ m/s}^2$
- Force noise from actuation
- Measure temperature fluctuations down to  $10^{-4} \text{ Hz}$  – and below – and  $dF/d\Delta T$
- Measure magnetic environment and forces from applied B
- Measurement and compensation of average stray E field (nulling  $dF/dq$ )
- Measure low frequency charge fluctuations with long term charge test
- Stiffness / SC coupling / crosstalk measurements

**Create physical model for limits to achieving perfect free-fall**



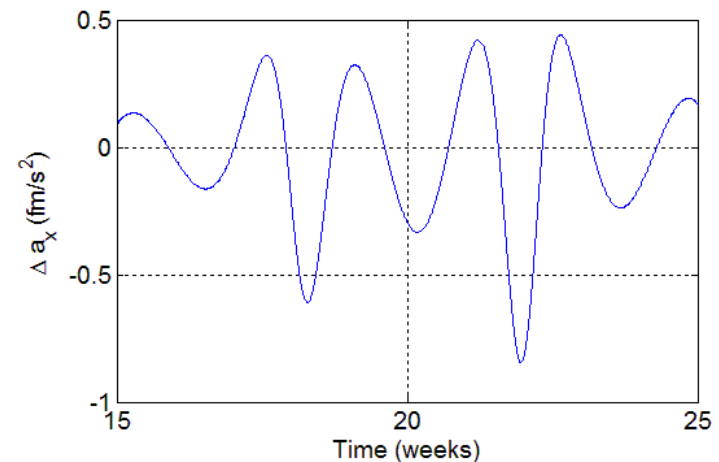
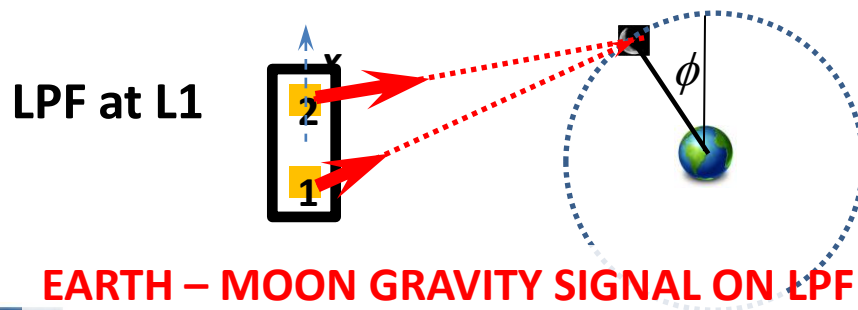
# What will LPF teach about eLISA performance at $10^{-6} - 10^{-5}$ Hz?

- eLISA spec for  $f > 10^{-4}$  Hz → testing too costly at lower frequencies
- Massive black hole merger ( $10^7 - 10^8 M_{\text{SUN}}$ ) science rich at  $10^{-5}$  Hz
- Future GR tests, time-delay need drag-free at  $10^{-6}$  Hz

## LPF

- 1-2 acceleration noise measurements cover  $10^{-5}$  Hz (free-fall mode)
- Dedicated long term measurements of charge (+ T, B-field)
- $\mu\text{Hz}$  – Moon test → extract gravity signal from earth-moon system (2/month)  
→ requires 8-10 x 1 day acceleration measurements over 1 month

→ SNR = 1 requires  $0.5 \text{ pm/s}^2/\text{Hz}^{1/2}$  → same as time delay requirement!



# Improve eLISA GRS by factor 10 – $0.3 \text{ fm/s}^2/\text{Hz}^{1/2}$ at 0.1 mHz?

Starting with same GRS dimensions as eLISA GRS, need:

- $p < 2 \cdot 10^{-8} \text{ Pa}$  (near  $10^{-10} \text{ mB}$ ) [probably ok ... lower outgassing, better bakeout]
- Stray potentials  $< 0.5 \text{ mV}$ , fluctuations  $< 5 \mu\text{V}/\text{Hz}^{1/2}$  on each electrode  
[DC correction ok ... adjust DC correction 1/week]  
[fluctuations ... improve factor 2 electronics, factor 10 stray fields limit]
- Thermal fluctuations  $\Delta T < 2 \mu\text{K}/\text{Hz}^{1/2}$  [maybe OK ... test on LPF]
- Satellite coupling measure to  $200 \text{ pm}/\text{Hz}^{1/2}$  with  $1 \mu\text{N}/\text{m}$  [probably OK, test with LPF]
- Actuation + crosstalk  $2 \text{ ppm}/\text{Hz}^{1/2}$  stability + gravity  $< 0.5 \text{ nm/s}^2$  trans /  $200 \text{ prad/s}^2$  rot  
[measure g on LPF, test FEE on ground]  
[could cure with impulsed actuation, small electrode change]
- Spacecraft gravity fluctuations  $< 10^{-16} \text{ m/s}^2/\text{Hz}^{1/2}$   
[probably analysis only ... won't test at this level on LPF]

- no show stoppers, but not trivial
- Testing a challenge (especially for gravitational fluctuations)
- Surface problems cured with larger mass, larger gaps

W. J. Weber

GWADW, May 2013



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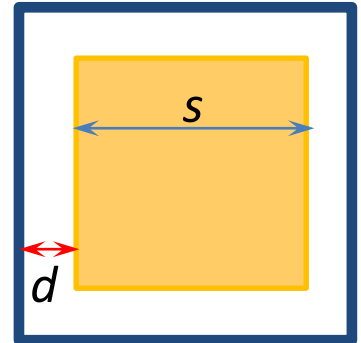
# “Just make the mass bigger and the gaps larger”

- Yes, for many surface disturbances

electrostatic forces  $\sim 1/d, \sim 1/d^2, \text{ or } 1/d^3$

Brownian noise from gas  $\sim 1/d$  for  $d \ll s$

Area  $A \sim s^2$  mass  $M \sim s^3$



- Somewhat for magnetics (for very close sources of field gradient)
- No for gravity (except for closest sources)
- No for actuation noise, most crosstalk
- Larger gaps + larger TM: bigger, heavier,  
harder to actuate, harder to cage

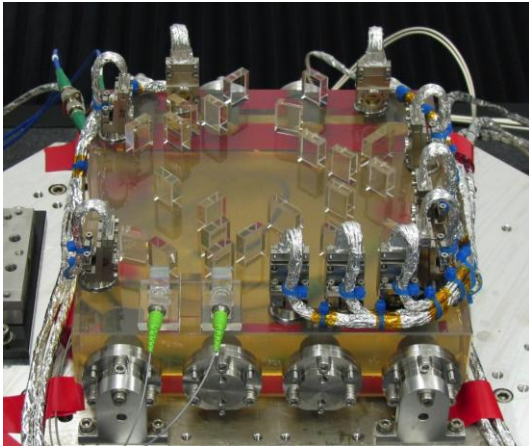
\$\$\$\$

Example: gas damping for DECIGO ( **$4 \cdot 10^{-19} \text{ m/s}^2/\text{Hz}^{1/2}$  at 0.1 Hz**)

100 kg TM, assume  **$d \sim s$**  (no proximity effects)

$$S_a^{1/2} \propto p^{1/2} \frac{A^{1/2}}{M} \propto \frac{p^{1/2}}{\rho^{1/3} M^{2/3}}$$

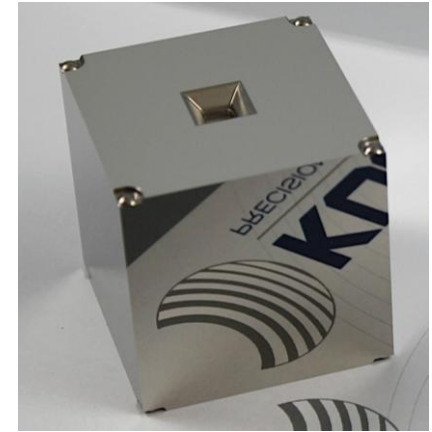
→ need  **$p < 10^{-9} \text{ Pa}$**



Optical bench



Spacecraft + optical bench tests



Uncoated TM

## LPF Launch: July 2015

<https://www.elisascience.org/articles/lisa-pathfinder/lpf-mission>



## STOC Simulations

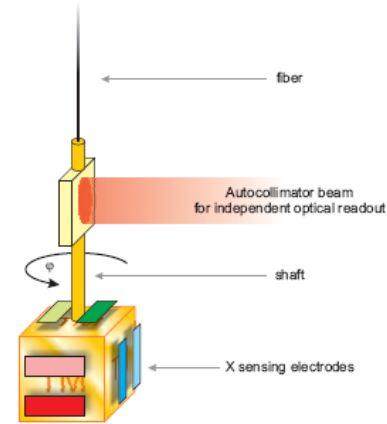
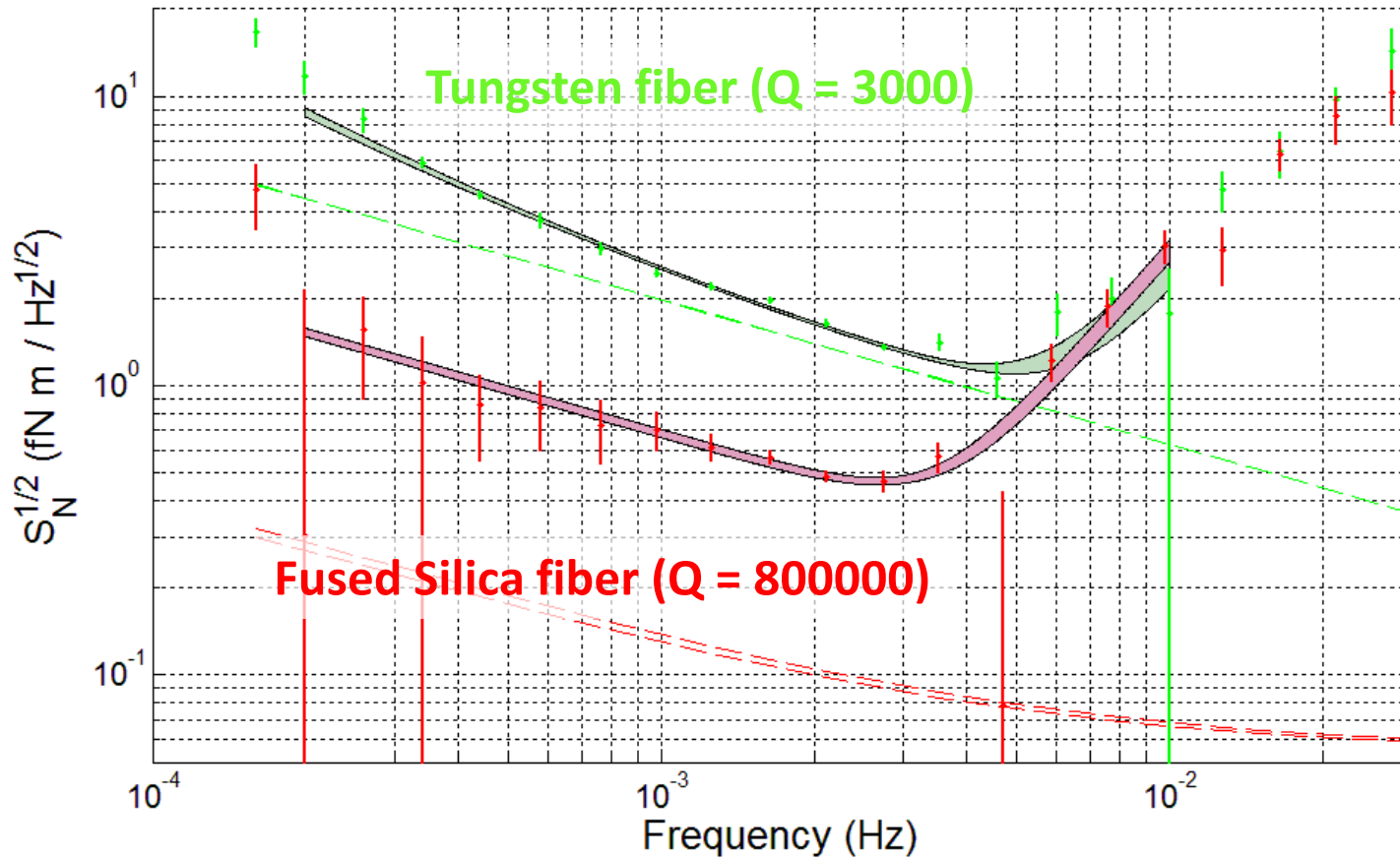


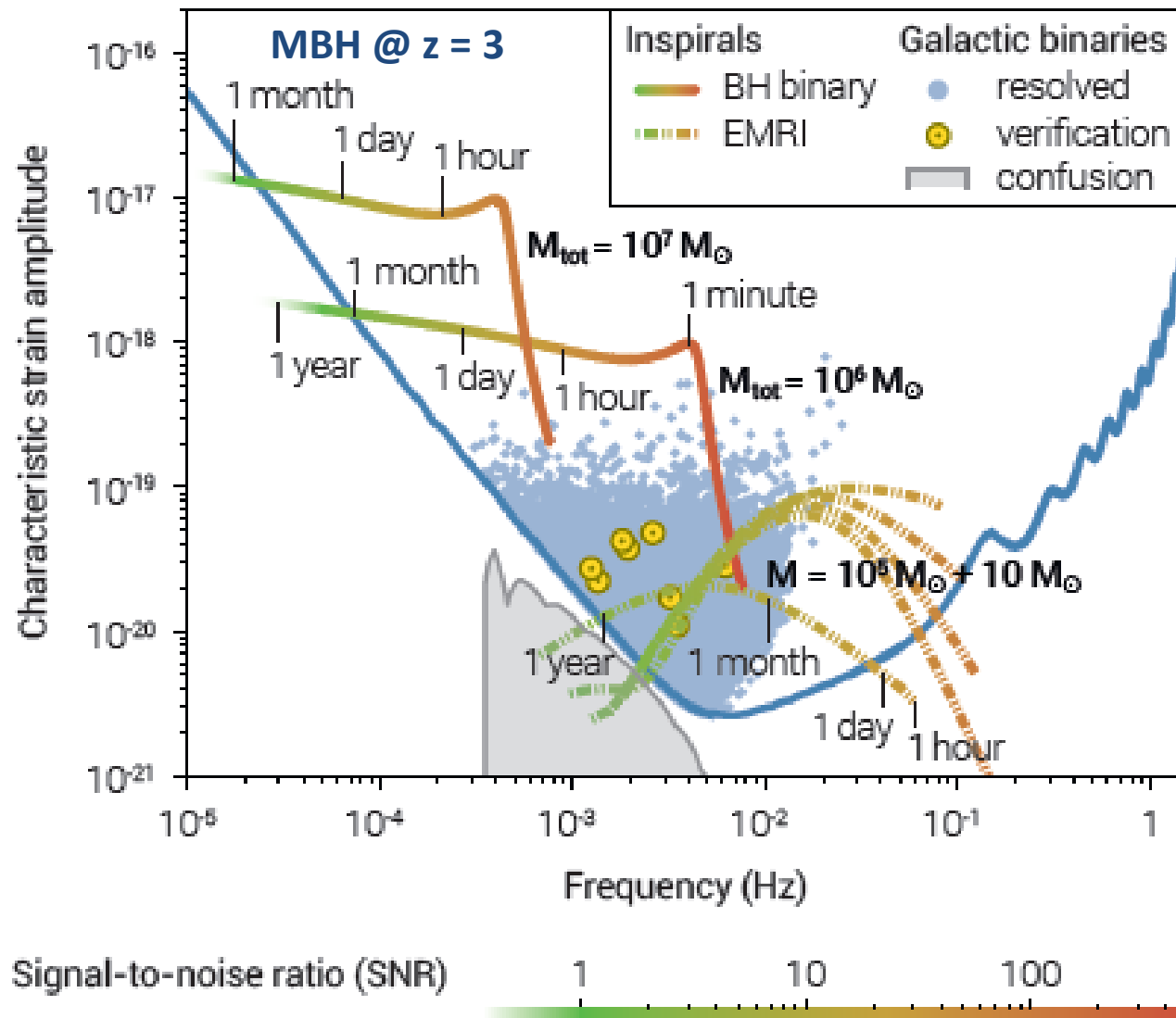
## VEGA (2 launches!)

# Extra stuff

# Overall upper limits on GRS surface force noise:

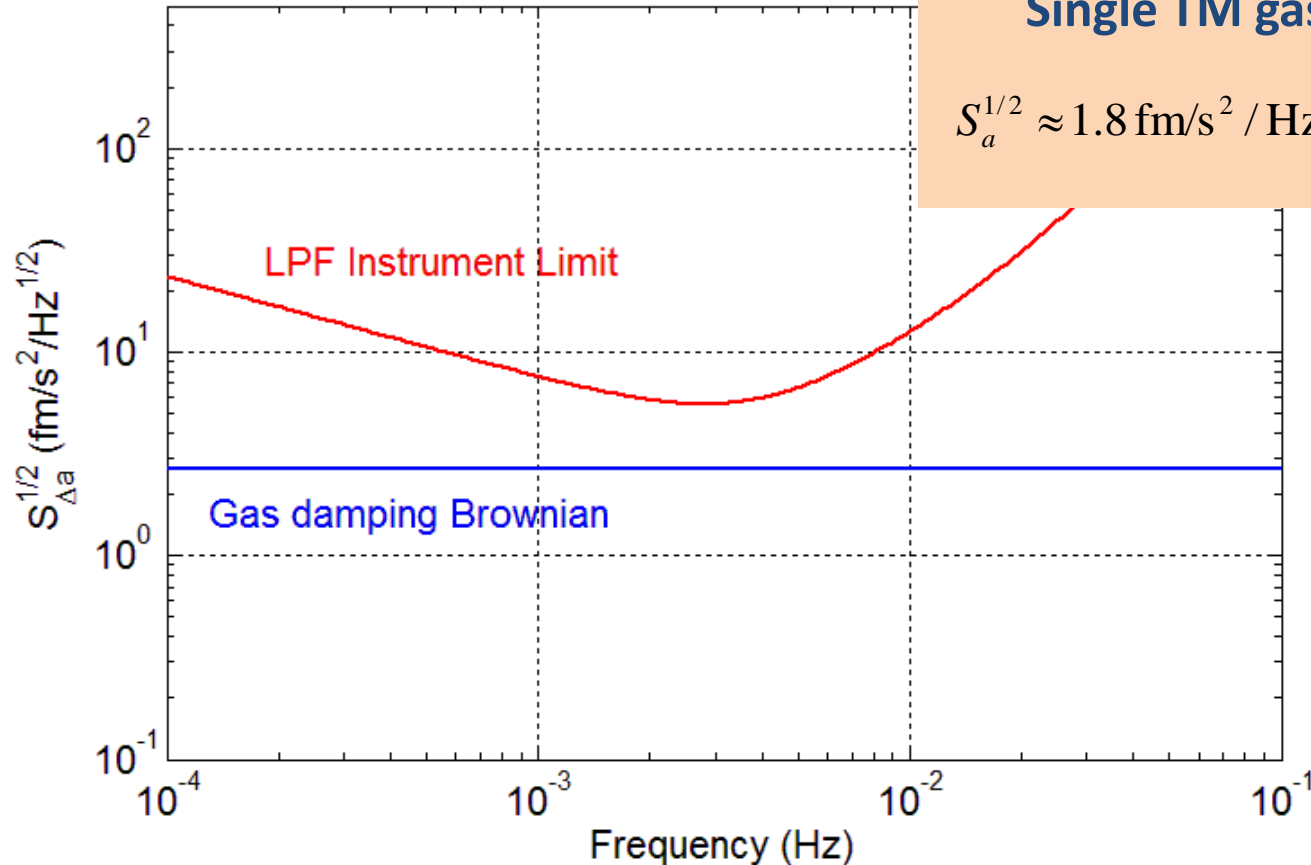
Torsion pendulum noise floor with prototype LPF sensor + electronics





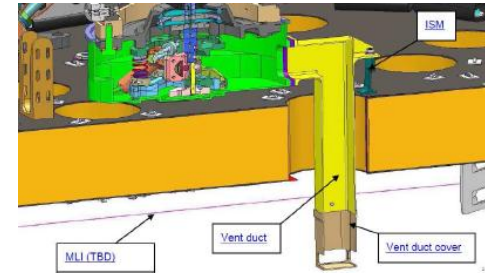


# Noise source: Brownian noise from residual gas

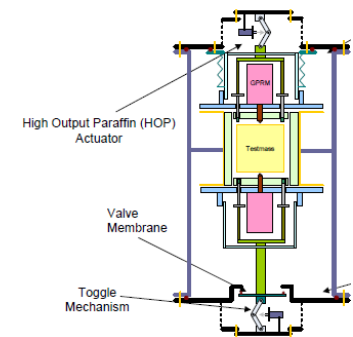


## Single TM gas damping noise

$$S_a^{1/2} \approx 1.8 \text{ fm/s}^2 / \text{Hz}^{1/2} \times \left( \frac{p}{2 \mu\text{Pa}} \right)^{1/2} \left( \frac{m_0}{30} \right)^{1/4}$$



**vent GRS to space**

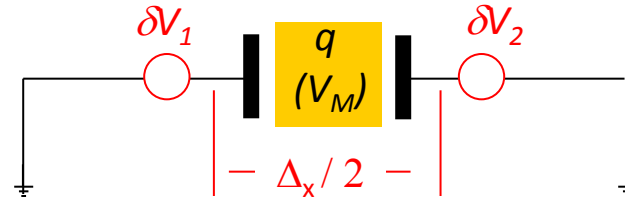


- 2  $\mu\text{Pa}$ : conservative upper limit based on measured gas loads
- worst case: can identify excess with radiometric effect

# Electrostatic interaction between TM charge and average electrostatic field

$$F = \frac{q}{C_{TOT}} \sum_{i(TM), j(S)} \frac{\partial C_{ij}}{\partial x} (\delta V_i - \delta V_j)$$

$$\equiv \frac{q}{C_{TOT}} \left| \frac{\partial C_x}{\partial x} \right| \Delta_x$$



TM charge  $Q$   
Stray potentials  $\delta V$

$$S_F^{1/2} = \frac{\sqrt{2e^2 \lambda_{EFF}}}{\omega C_T} \left| \frac{\partial C}{\partial x} \right| \Delta_x$$

Random charge shot noise  
mixing with DC bias ( $\Delta_x$ )

$$\approx 7 \text{ fN/Hz}^{1/2} \times \left( \frac{\Delta_x}{100 \text{ mV}} \right) \times \left( \frac{\lambda_{EFF}}{300 \text{ /s}} \right)^{1/2} \times \left( \frac{f}{0.1 \text{ mHz}} \right)$$

• need to measure average stray field compensation  $\Delta_x$  to  $<1 \text{ mV}$

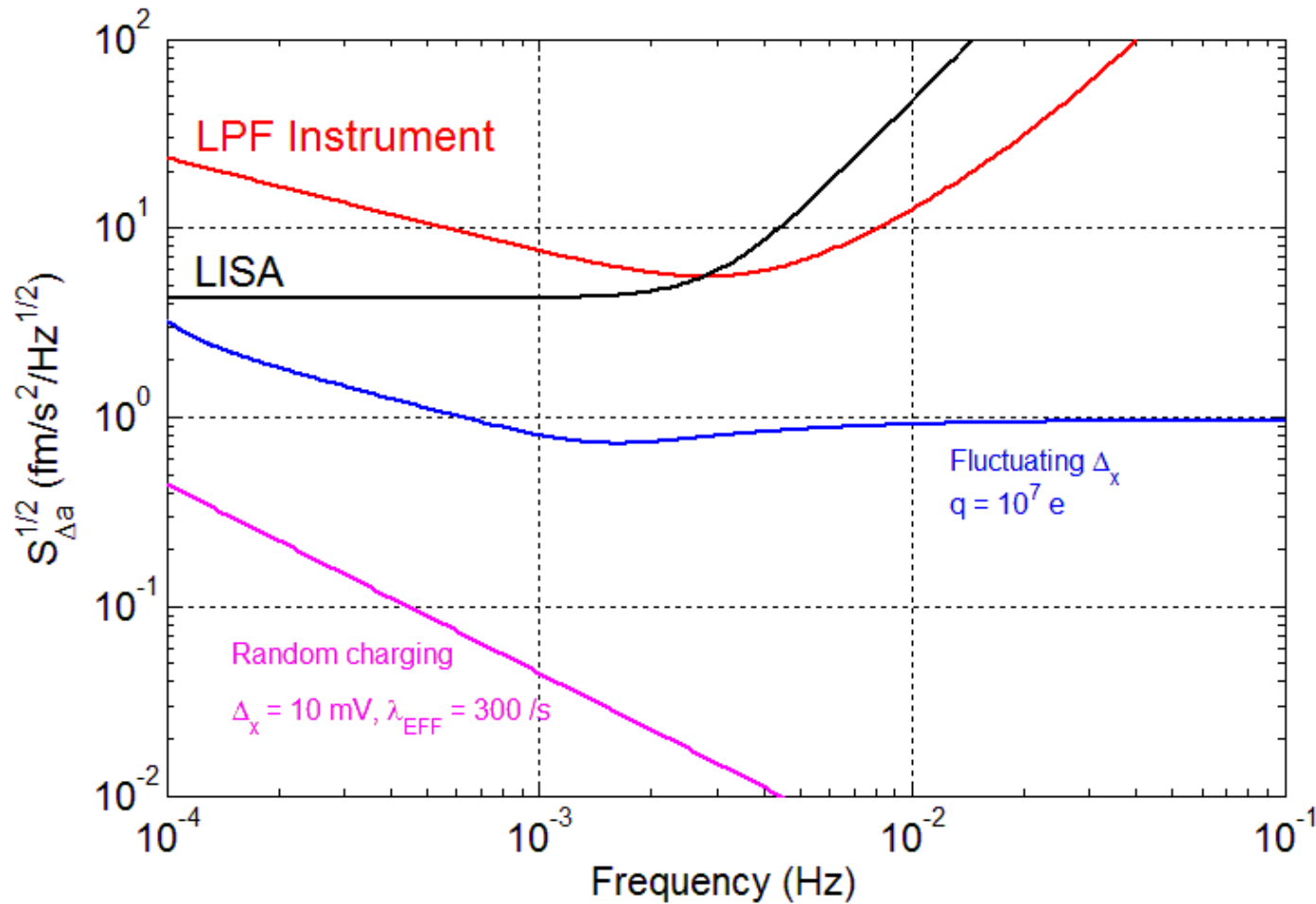
$$S_F^{1/2} = \frac{\langle q \rangle}{C_T} \left| \frac{\partial C}{\partial x} \right| S_{\Delta_x}^{1/2}$$

Noisy average “DC” bias ( $S_{\Delta_x}$ )  
mixing with mean charge

$$\approx 1.6 \text{ fN/Hz}^{1/2} \times \left( \frac{\langle q \rangle}{10^7 e} \right) \times \left( \frac{S_{\Delta_x}^{1/2}}{100 \mu\text{V/Hz}^{1/2}} \right)$$

• non-stationary as charge drifts ( $2 \cdot 10^6$  --  $10^7$  charge in one day)

# Interaction between TM charge and stray electrostatic field



[PRL **108**,  
181101 (2012)]

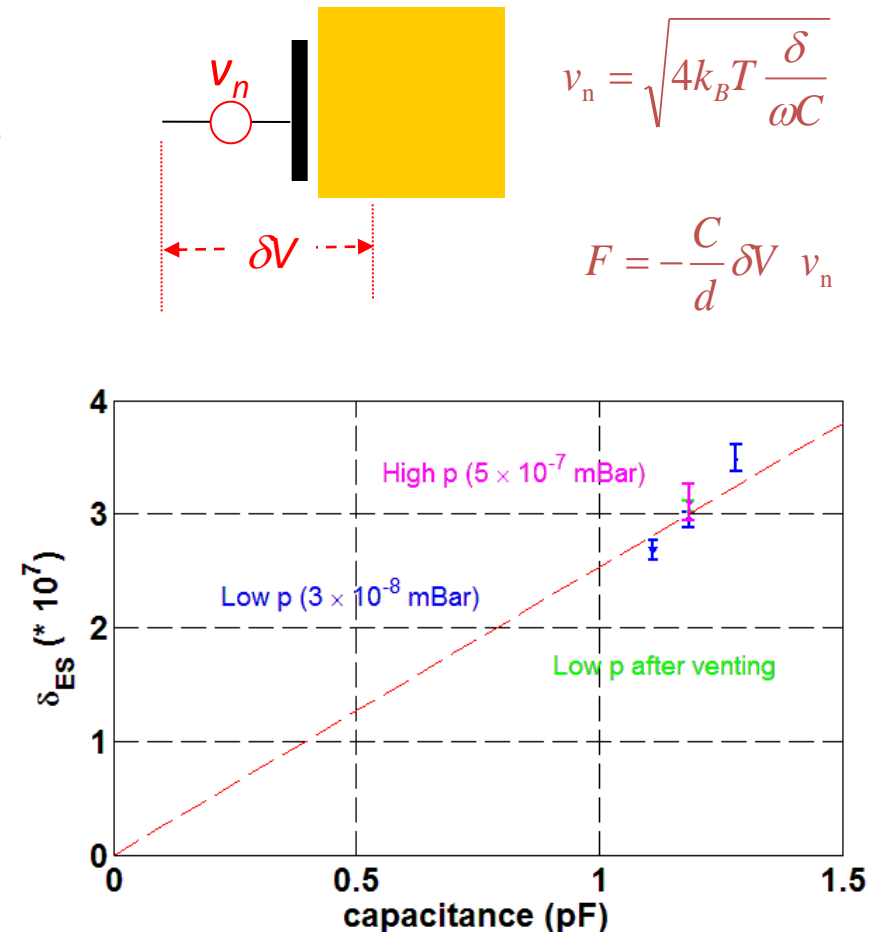
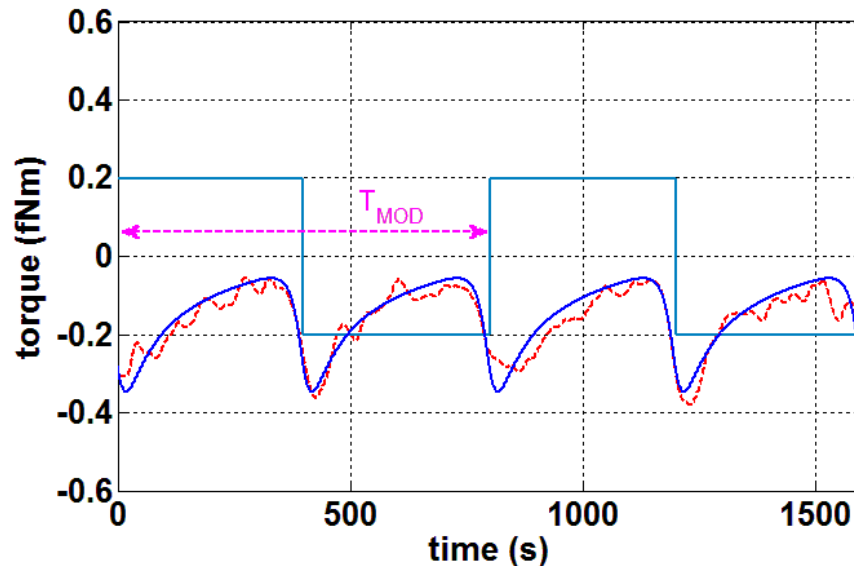
NB noise source proportional to **(1/gap)**

→ even cm size gaps will still require measurement + compensation!

# Force noise from electrostatic dissipation

Thermodynamic voltage noise from surface dissipation mix with DC  $\delta V$  to give force noise

Comparison of measured transient torque with theoretical model for  $\delta = 3 \cdot 10^{-7}$



- Squarewave modulation technique,  $10^{-17}$  Nm transient torque resolution
- Detect loss angle  $\delta \approx 3 \cdot 10^{-7}$  for 2 electrode pairs  $\rightarrow$  small enough for LISA!
- Waveform and distance dependence consistent with  $\delta$  independent of frequency

# Force noise source: interaction of magnetic moment and B field

- Fluctuations in magnetic field:

$$\frac{\chi V}{\mu_0} S_{B_i}^{1/2} \frac{\partial B_{0i}}{\partial x}$$

$$F_x = \vec{m} \cdot \frac{\partial}{\partial x} \vec{B} \quad \longrightarrow \quad \vec{m} = \vec{m}_0 + \frac{\chi V \vec{B}}{\mu_0}$$

- Fluctuations in gradient:

$$\left( m_{0i} + \frac{\chi V B_{0i}}{\mu_0} \right) S_{\partial B_i / \partial x}^{1/2}$$

- Down conversion of field / gradient interaction:  
( $\chi$  frequency dependent, Faraday and skin effect)

$$\frac{\chi(t) V B_i(t)}{\mu_0} \frac{\partial B_i(t)}{\partial x} \approx - \frac{s^3}{\mu_0} \frac{i \omega' \tau}{1 + i \omega' \tau} B_i(\omega') \frac{\partial B_i(\omega - \omega')}{\partial x}$$

Onset (“superconductor limit”)

$$f_{ON} \approx (2\pi\tau)^{-1} \approx \left( 2\pi \frac{s^2 \mu_0 \sigma}{24} \right)^{-1} \approx 450 \text{ Hz}$$

Shielding cutoff from  
vacuum chamber:  
(not including sensor)

$$f_{CUT} \approx 2 \text{ kHz}$$

# LISA Pathfinder Magnetic Measurements

Au/Pt alloy for low susceptibility, low residual moment

Measured EM TM properties

$$\vec{m}_0 \approx 10 \text{ nAm}^2$$

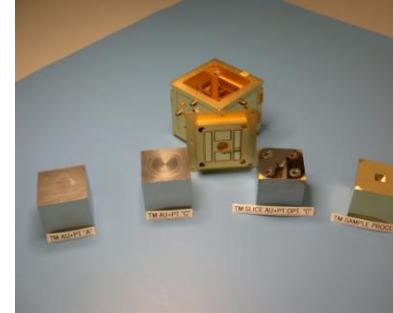
$$\chi \approx 2 \times 10^{-5}$$

Field estimates:

$$|\vec{B}_0| < 1 \mu\text{T}$$

$$\left| \frac{\partial \vec{B}_0}{\partial x} \right| < 12 \mu\text{T/m}$$

$$|\vec{B}_{AC}|_{RMS} < \text{nT/Hz}^{1/2} \text{ to } 1 \text{ kHz}$$



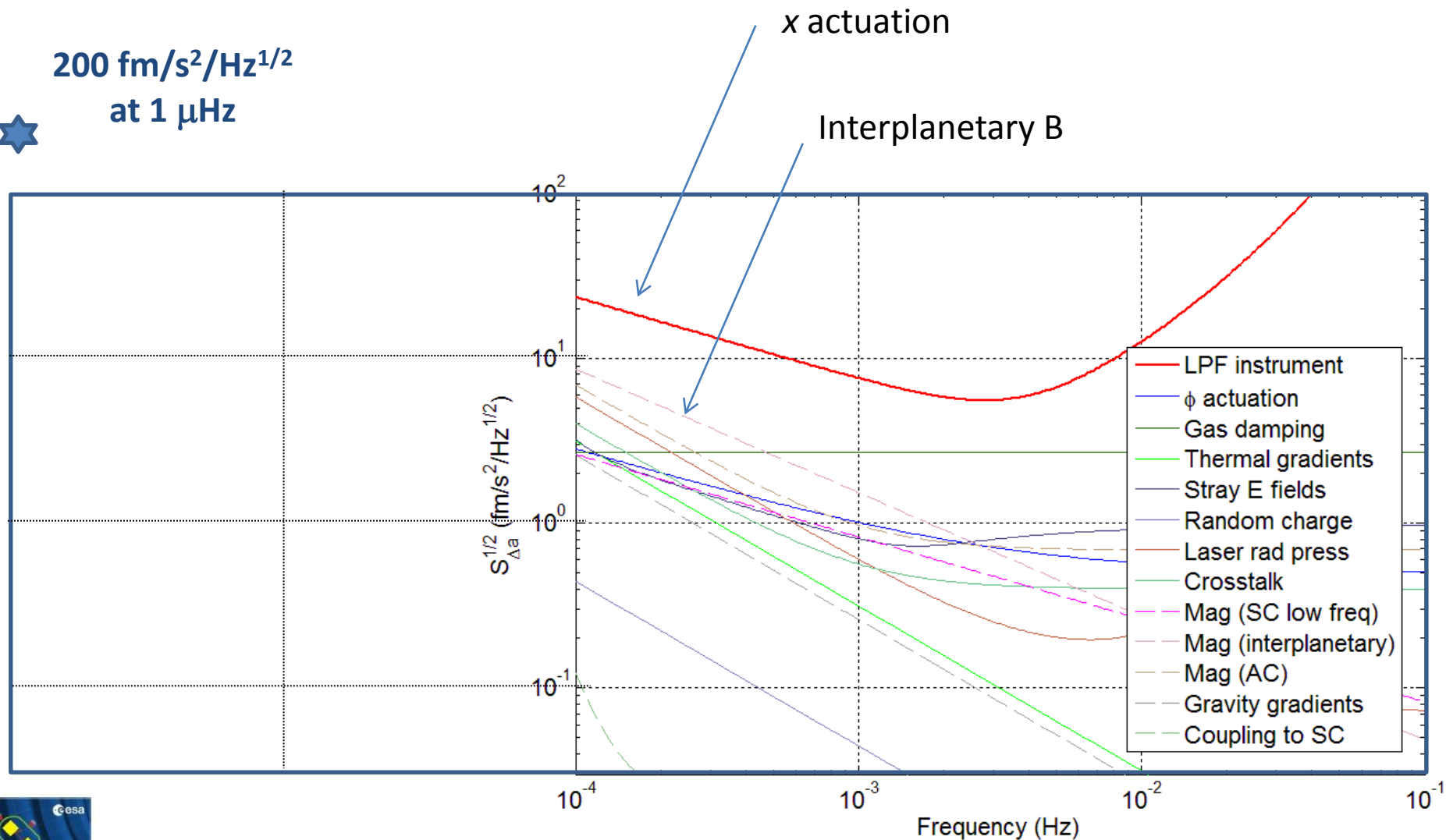
	<b>LISA Pathfinder</b>	S2.ASU.TN.2523 Issue 3 Page 53 of 58
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- Large field gradient due to thermistors mounted on GRS  
→ Should be an order of magnitude lower with demagnetization

# Will LPF have the resolution to see the earth-moon signal?

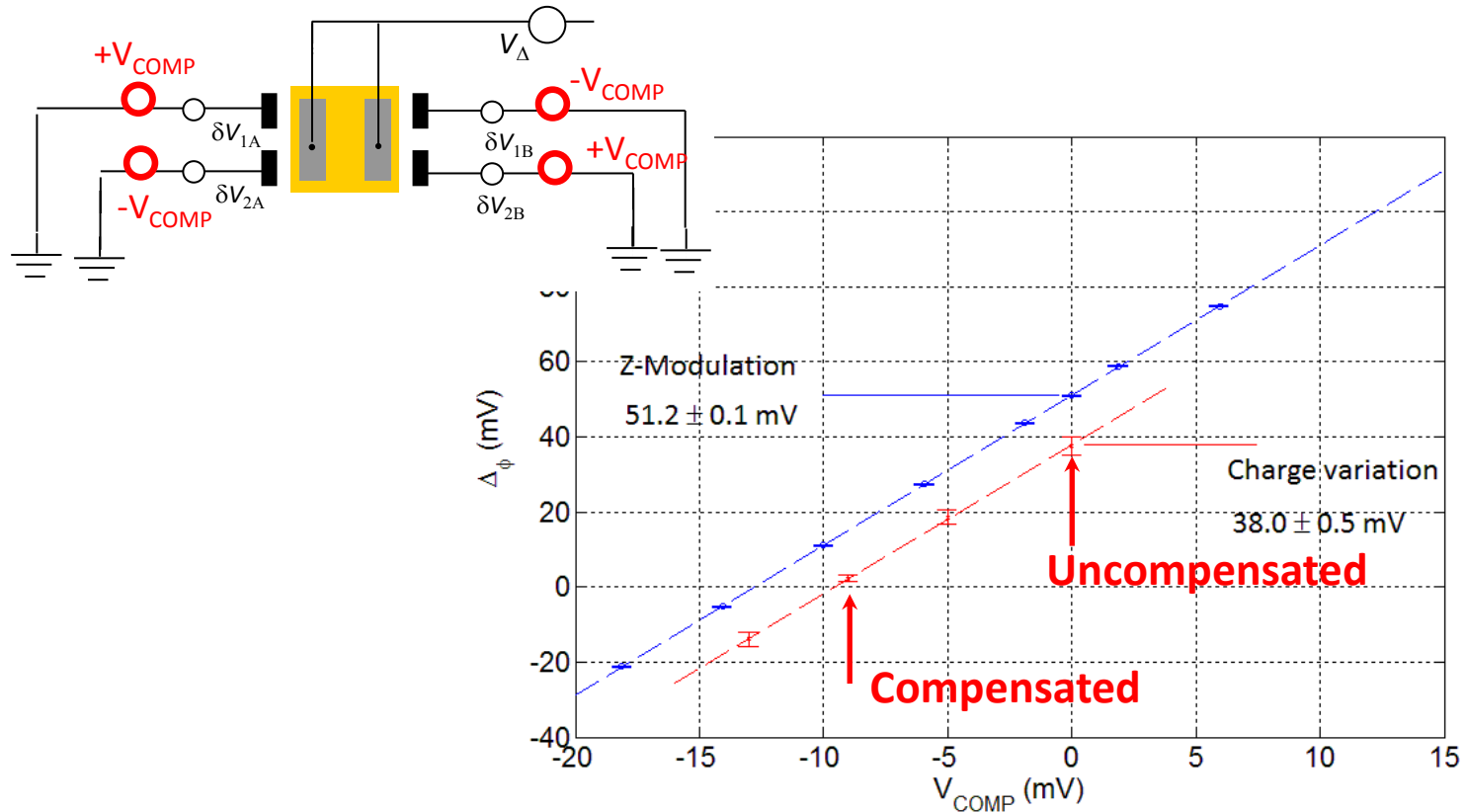
200 fm/s<sup>2</sup>/Hz<sup>1/2</sup>

at 1 μHz



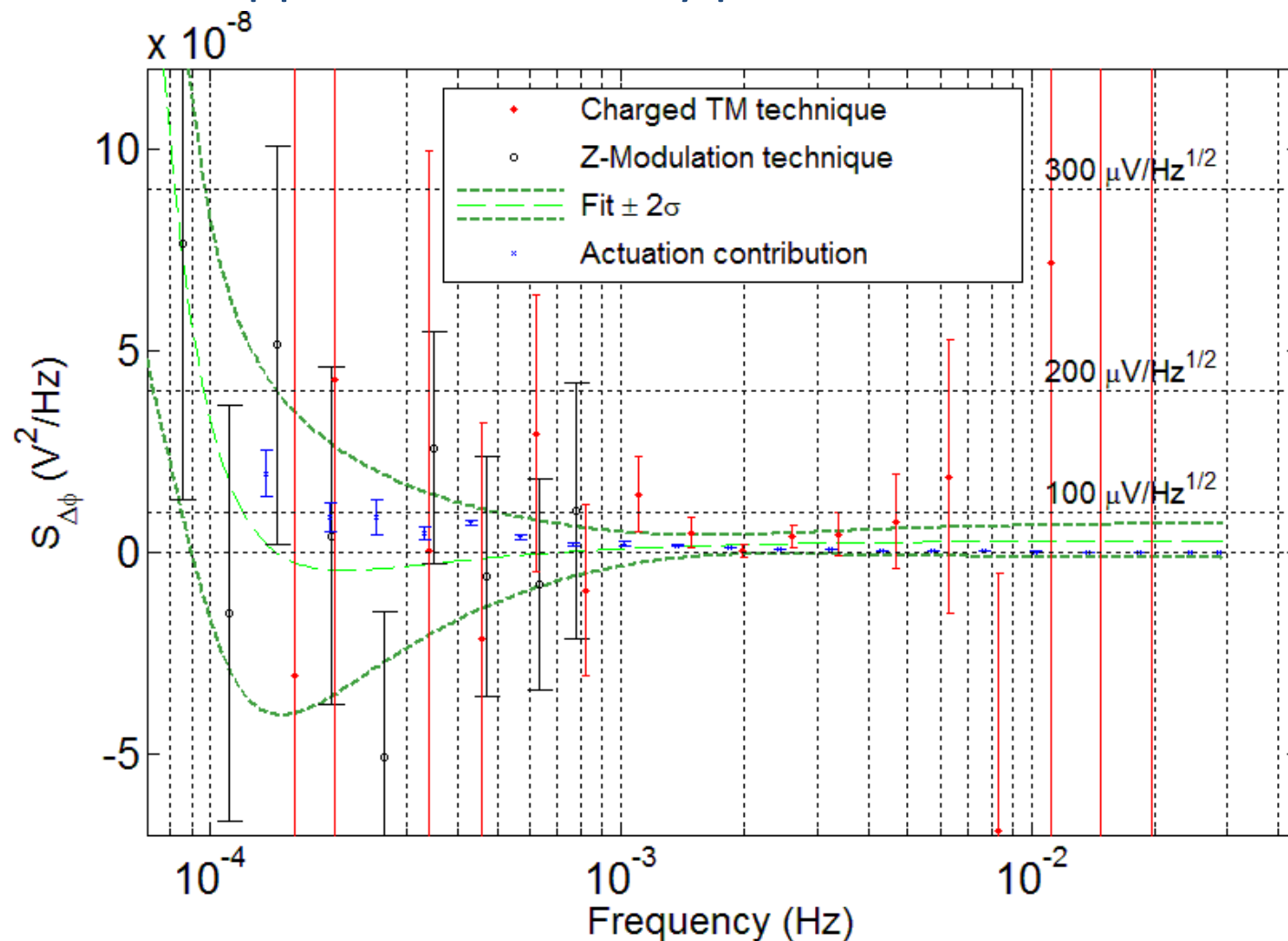


# Experimental verification of stray potential compensation



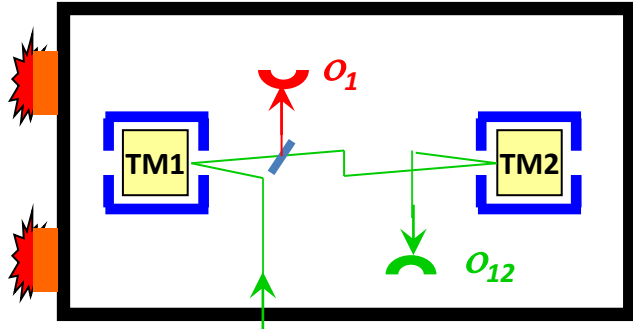
- Measurement of  $dF/dq$  (add charge to TM and measure change in force)
- Measure and compensate typical 100 mV imbalance to  $< 1$  mV
- Need to measure by varying charge (not same as changing  $V_{TM}$  with applied voltages)
- Observed drifts small (order several mV in 1 month)  $\rightarrow$  periodic remeasurement

# Experimental upper limits on stray potential fluctuations



- consistent with sensor electronics noise fluctuations
- no excess noise from surface potential fluctuations
- **upper limit for 5 cm<sup>2</sup> surface:  $<12 \mu V/Hz^{1/2}$  at 1 mHz**

# LISA Pathfinder as differential accelerometer



Closed loop noise in differential IFO signal  $o_{12}$

*Differential  
force noise  
(for LISA)*

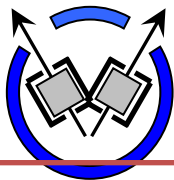
*Coupling to satellite "jitter"  
(can be tuned to zero)*

*Baseline stability  
(Zerodur)*

$$o_{12}(\omega) = \frac{-1}{\omega^2 - (\omega_{2p}^2 + \omega_{ES}^2)} \left\{ \underbrace{(g_2 - g_1)}_{\text{Differential force noise (for LISA)}} + \underbrace{\left( n_1 + \frac{F_{SC}}{M\omega_{DF}^2} \right) [\omega_{2p}^2 - \omega_{1p}^2]}_{\text{Coupling to satellite "jitter" (can be tuned to zero)}} - \underbrace{n_{12}(\omega^2 - \omega_{2p}^2)}_{\text{IFO readout noise}} + \underbrace{\delta x \omega_{2p}^2}_{\text{Baseline stability (Zerodur)}} \right\}$$

*IFO readout noise*

**LPF Instrument Noise**  
*(include x force actuation noise)*



**LISA**

$$a_{res} = \underbrace{g}_{\text{Differential force noise (for LISA)}} + \omega_p^2 \left( x_n + \frac{F_{str}}{M\omega_{DF}^2} \right)$$

W. J. Weber  
GWADW, May 2013

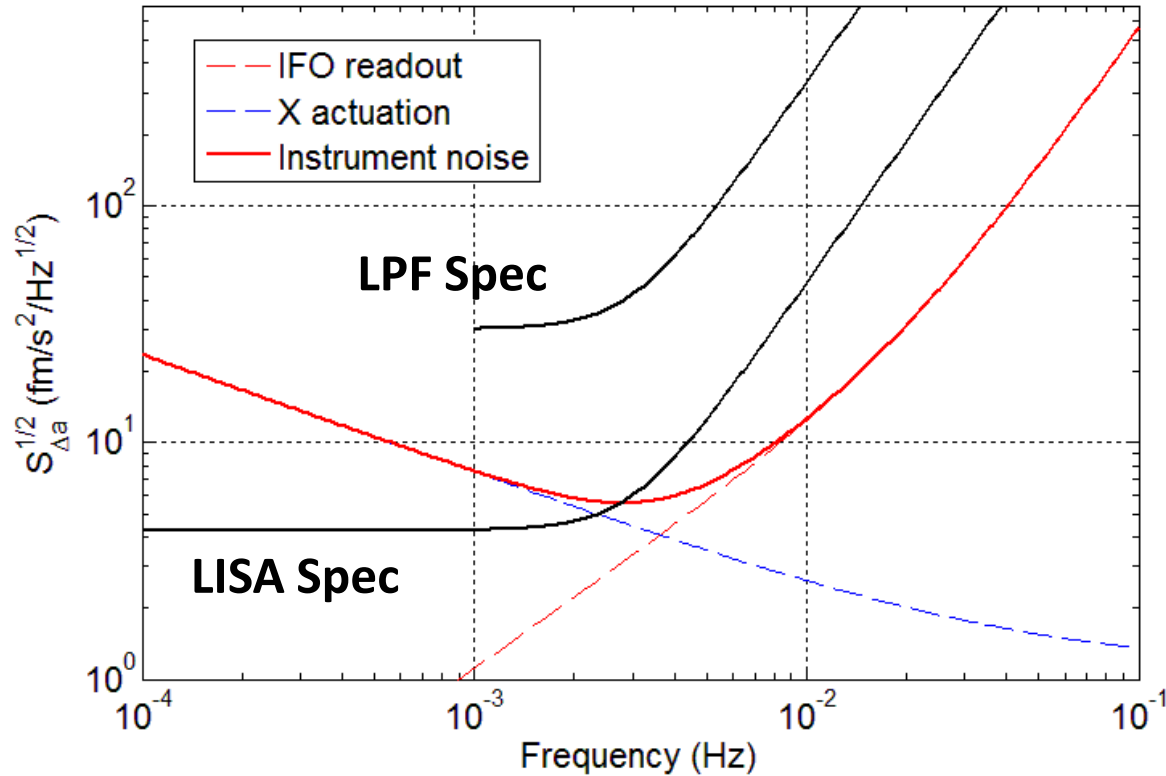


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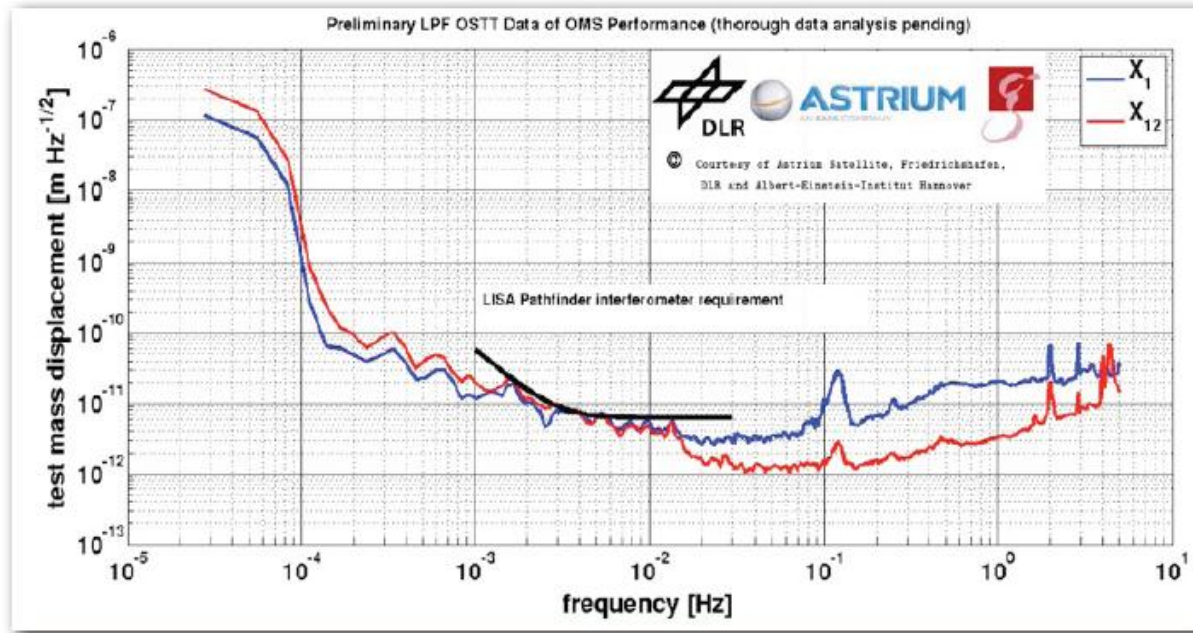
# LISA Pathfinder as differential accelerometer for LISA TM

## acceleration noise: Instrument performance



# Verification of LPF Optical Metrology

## OSTT - TOQM OMS longitudinal sensitivity



- Milestone: first performance demonstration of a FM OB.
- This OB is now baseline for flight (3OB).
- ASD test reports released: S2-ASD-TR-3152, TR-3155

LISA Symposium 2012

LISA Pathfinder Flight Hardware

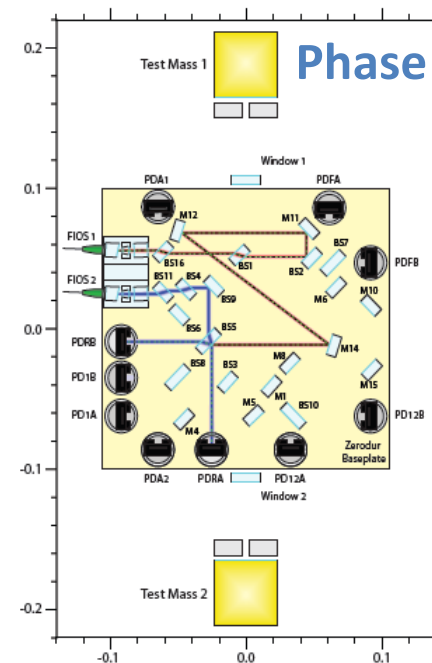
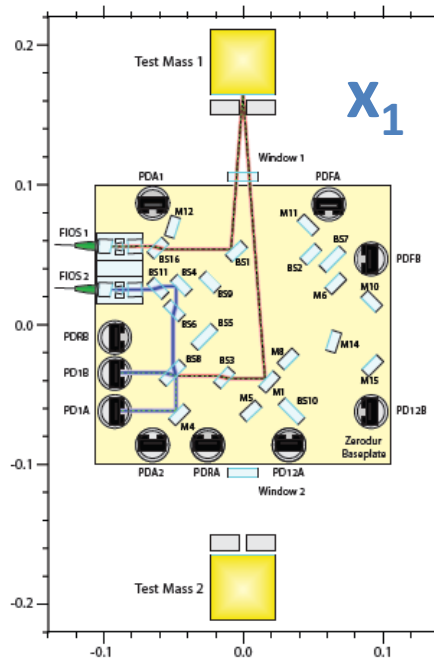
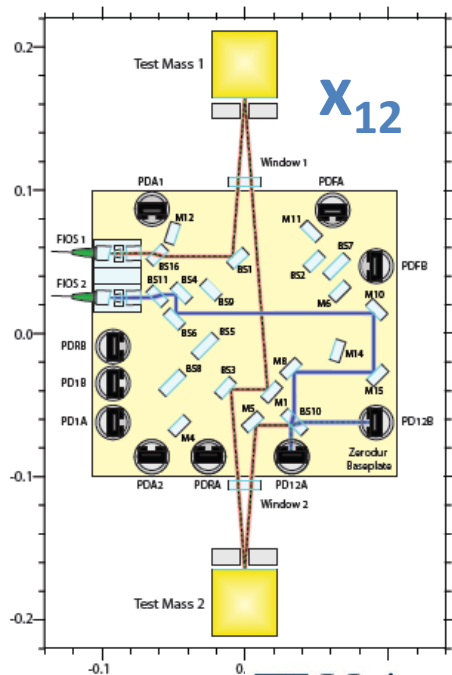
Felipe Guzmán



- Necessary displacement sensing achieved across whole LPF band

# LPF Hardware for LISA: optical metrology

- ( $x_{12}$ ) Differential TM displacement at  $6 \text{ pm/Hz}^{1/2}$  level (3-30 mHz)
- ( $x_1$ ) TM1 to spacecraft displacement – LISA local TM measurement
- Auxiliary IFO for phase and frequency noise correction
- Audio-frequency heterodyne Mach-Zehnder interferometer with waveform digitizing phasemeter
- High stability Zerodur optical bench, monolithic construction





# The micro-Newton thrusters

- Cold gas developed for Gaia better than requirements
- Now selected as baseline in place of FFFPc



Date 14/09/2012

Ref SRE-PN/18234-12/CGM

From C. García Marirrodiga (SRE-PN)

Visa T. Passvogel (SRE-P)

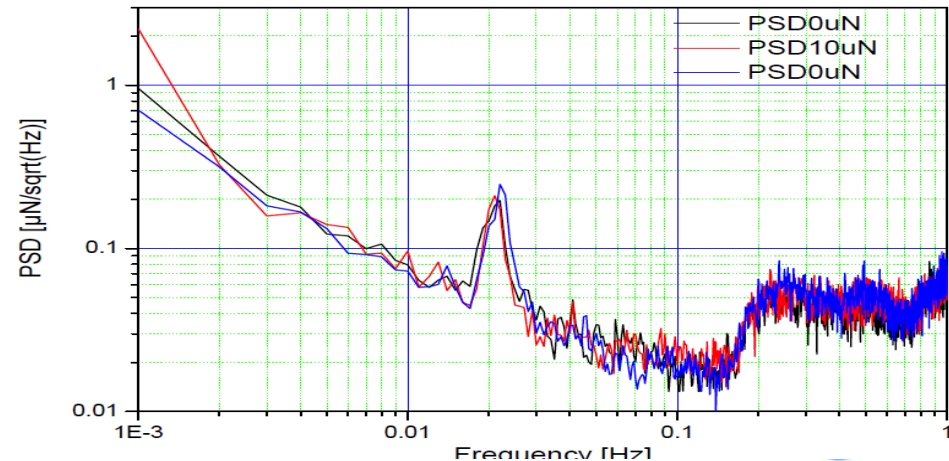
To LISA Pathfinder MPSR Board:  
R. Schmidt (DG-I)  
W. Veith (TEC-Q)  
C. Stavrinidis (TEC-M)  
A. Tobias (TEC-S)  
M. McCaughrean (SRE-S)  
G. Saccoccia (TEC-MP)

Copy A. Giménez Cañete (D/SRE)  
P. McNamara (SRE-SA)  
S. Vitale (University of Trento)  
E. Bachem (DLR)  
B. Sanders (TNO)  
LPF Project Team & MPS support

**Subject: Decision on the change of Micro-Propulsion System baseline for LISA Pathfinder**

In November 2011 the LISA Pathfinder Micro-Propulsion System Review (MPSR) Board reviewed the status of the Caesium FEEP development tests and of the alternative Cold Gas system. The Board recommended (cf. Board Report DG-IR/2011/109/KL) continuing the testing of the FEEPs on unit and assembly level (TUVT and TAET respectively). In parallel, as a backup, the Board recommended to proceed with and complete the design work for the cold gas system, and to initiate the procurement of the long lead items. The overall status should be presented to the Board not later than April 2012. Such report was released in due time by the LPF Project (cf. SRE-PN/17498-12-GR), including the criteria to reach a decision on the MPS for LPF.

This memorandum summarizes the status reached at the present time, and introduces the LPF Project decision to select the cold gas micro-propulsion system as baseline and to discontinue further development work of the FEEP system within the context of the LISA Pathfinder project.

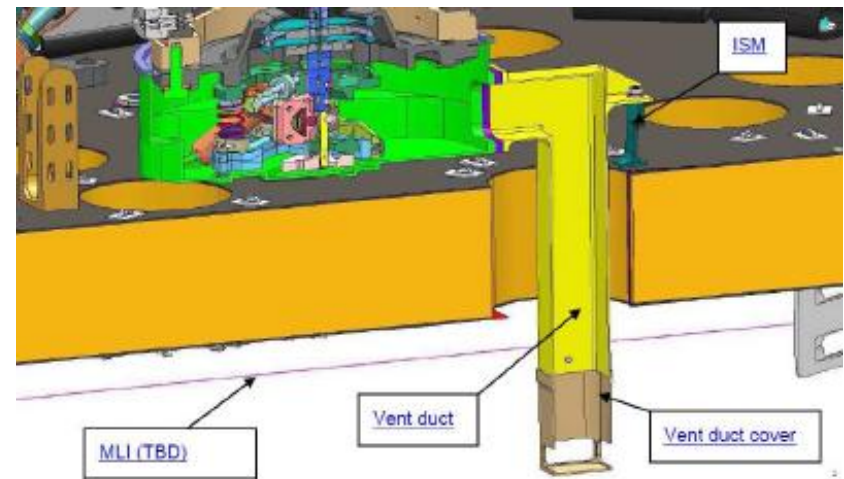
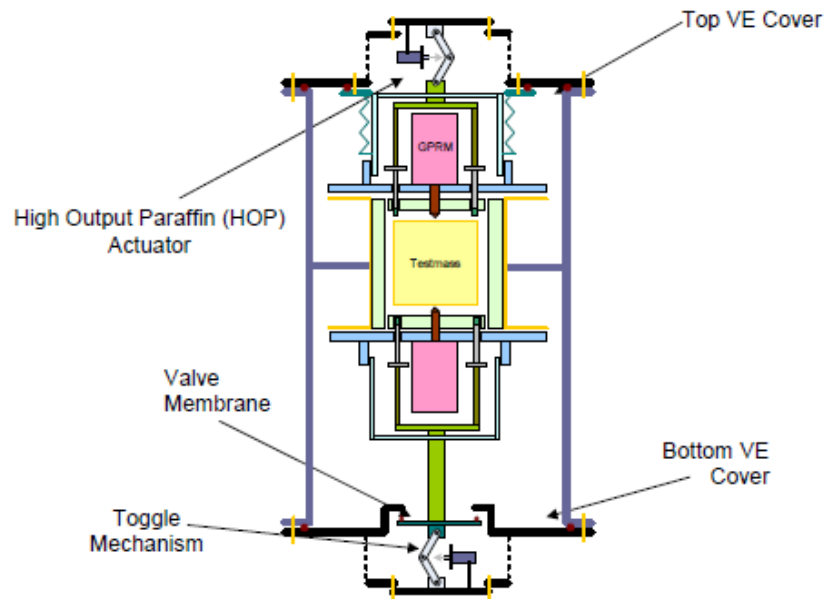




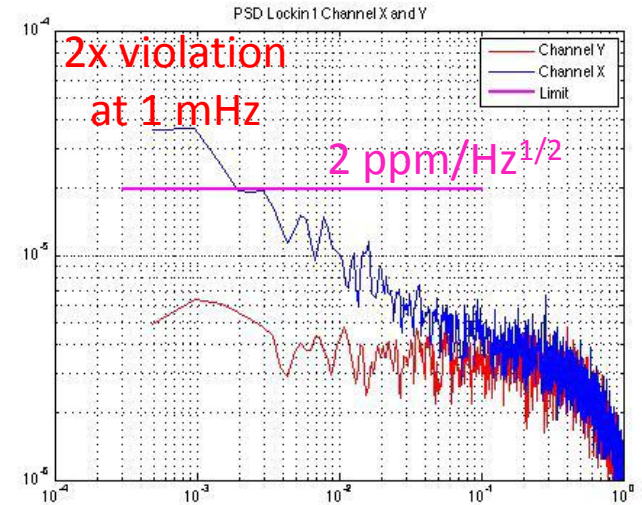
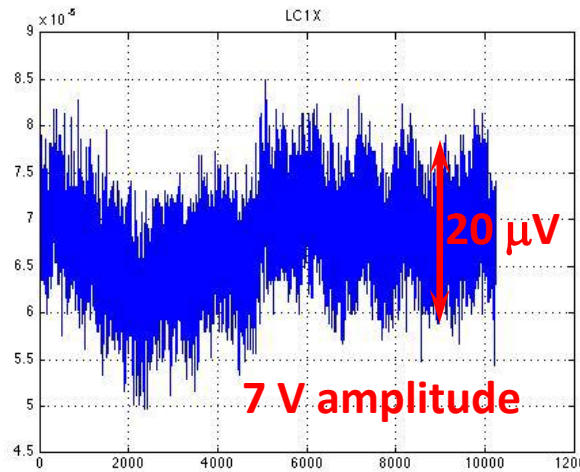
# New LPF vacuum strategy: vent to space



- Replace getter pumps – low pumping speed – with high conductance (15 l/s) duct to space
- Requirement 2  $\mu\text{Pa}$
- Gas load measurements indicate significantly lower



# Actuation fluctuations: experimental limits with FM FEE



- Actuation fluctuations from 3-15 ppm/Hz<sup>1/2</sup> (x channels 3-7 ppm /Hz<sup>1/2</sup>) at 1 mHz
- Typical power increase with 1/f at lower frequencies

→ Gives roughly 7 fm/s<sup>2</sup>/Hz<sup>1/2</sup> at 1 mHz with 0.65 nm/s<sup>2</sup> grav imbalance

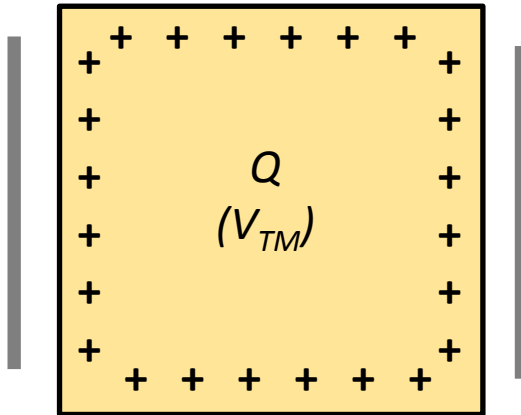
W. J. Weber  
GWADW, May 2013



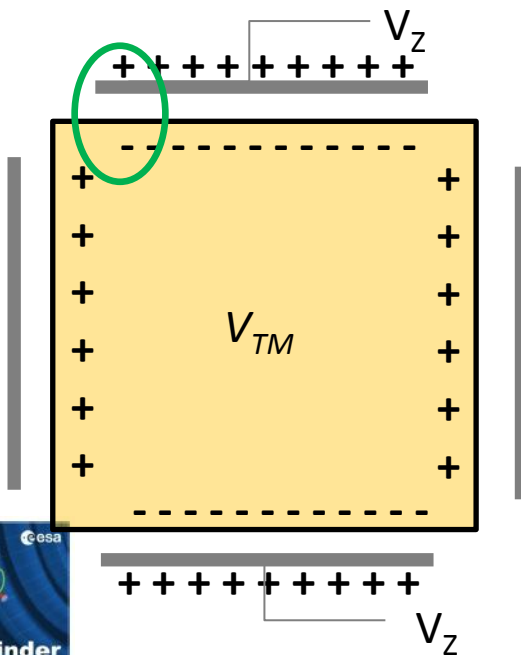
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# Difference between Q-modulation and $V_z$ modulation techniques



$$\frac{\partial F_x}{\partial Q} = -\frac{1}{C_{TOT}} \left| \frac{\partial C_x}{\partial x} \right| \Delta_x$$



$$\frac{\partial F_x}{\partial V_z} = -\frac{4C_z}{C_{TOT}} \left| \frac{\partial C_x}{\partial x} \right| \Delta_x + \sum_{\alpha(Sz), \beta(TM)} \frac{\partial C_{\alpha, \beta}}{\partial x} (\delta V_\alpha - \delta V_\beta)$$

- In addition to modulation TM potential, introduce large field gradient at borders of z electrodes
  - amplifies shear force that is not relevant for TM charge

W. J. Weber

GWADW, May 2013



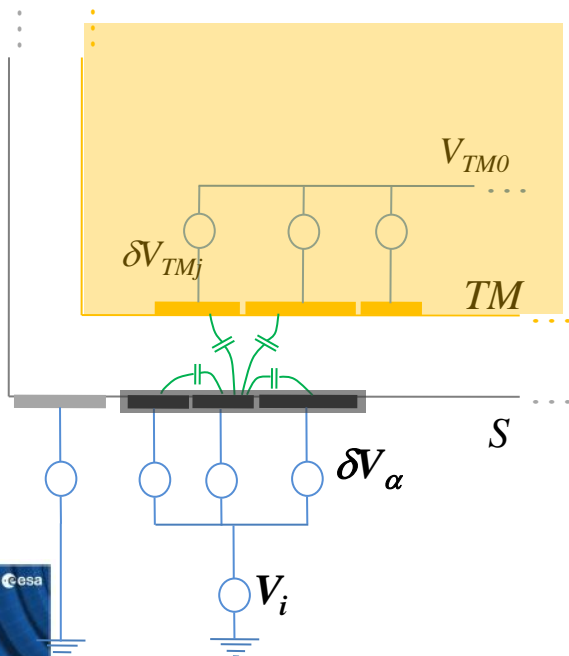
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# Electrostatic forces and possibility of compensating with applied voltages

$$F_x = \frac{1}{2} \sum_{\alpha, \beta < \alpha} \frac{\partial C_{\alpha, \beta}}{\partial x} (V_\alpha - V_\beta)^2$$

$$V_{TM} = \frac{Q}{C_{TOT}} + \frac{\sum_i C_i V_i}{C_{TOT}}$$



**Forces proportional to:**

$$(\delta V_\alpha - \delta V_\beta)^2$$

Individual domain potential differences

$$Q^2$$

charge stiffness

$$(V_i - V_{TM})^2$$

Electrode voltage fluctuation (FEE)

$$Q\Delta_x$$

Interaction charge and average field

**Ideally:**

- Want  $dF/dQ$ ,  $dF/dV_i$ ,  $dF/d\delta V_\alpha = 0$
- Would require all conductors at same potential

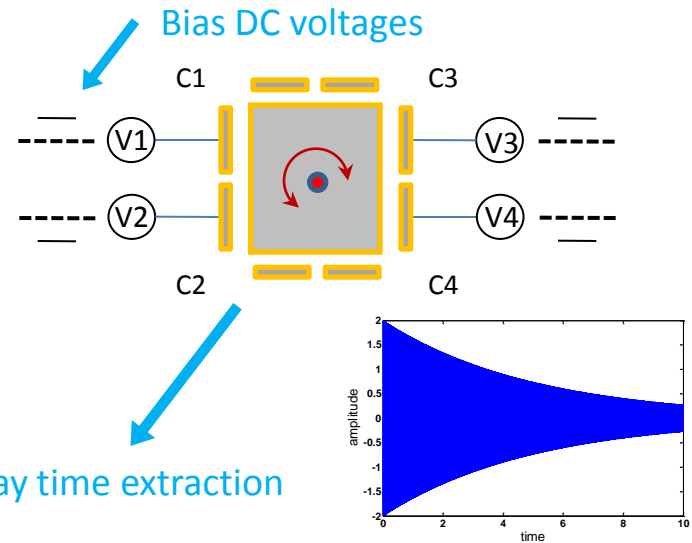
**We can:**

- apply DC voltages at will (up to 5 V)
- change TM charge (using UV)

# 2.1 Measurement with ringdown tech (2010~2012)

**Object:** A LPF flight model, Au-coated electrodes, 4 mm capacitive gap along x

**Tech1:** measure pendulum amplitude decay as a function of electrode voltages



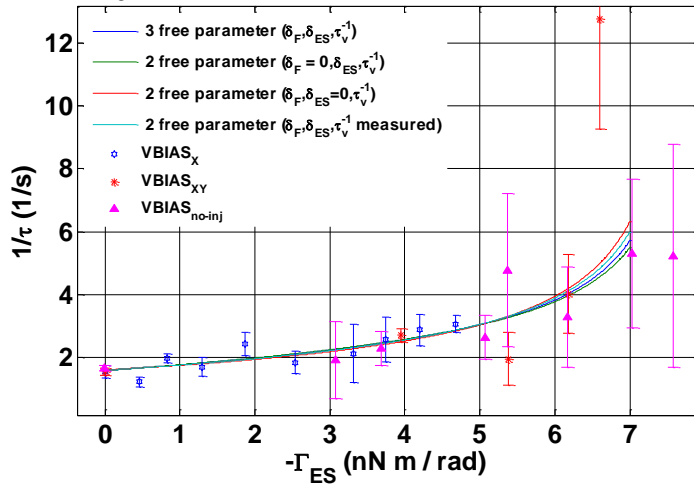
Decay time extraction

$$\frac{1}{\tau_{\text{exp}}} = \frac{1}{\tau_v} + \frac{1}{\sqrt{I}(\Gamma_F + \Gamma_{\text{ES}})} \cdot (\Gamma_F \cdot \delta_F - \Gamma_{\text{ES}} \cdot \delta_{\text{ES}})$$

Viscous damping  
 $\times 10^{-8}$

fiber damping

Electrostatic damping

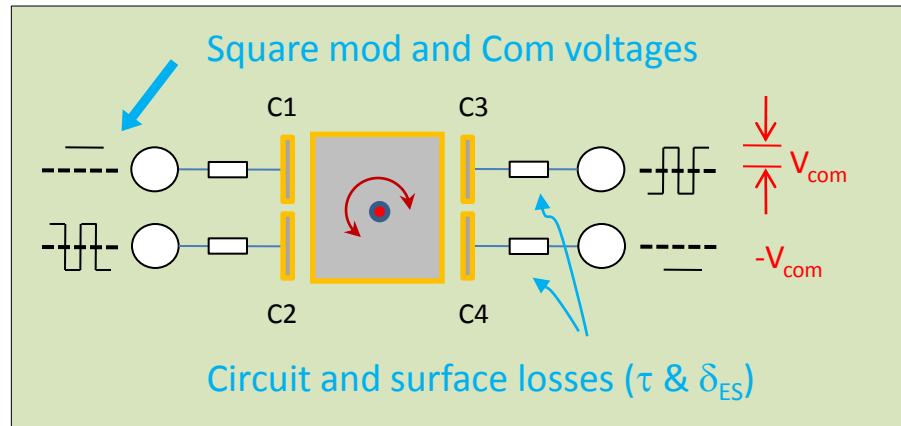


Fit condition	$\delta_{\text{ES}}$ ( $10^{-7}$ )	$\delta_F$ ( $10^{-7}$ )	$1/\tau_v$ ( $10^{-8}$ /s)	$\chi^2$	Remark
3 free parameters	7.6 (7.5)	-4 (12)	1.1 (1.6)	1.2 (20 DOF)	Physical
Assuming $1/\tau_v$ only from gas	4.5 (1.3)	8.7 (.4)	0.43	1.2 (21 DOF)	Physical
Assuming $\delta_{\text{ES}}=0$	--	16 (.03)	-.5 (.3)	1.2 (21 DOF)	Not physical

**Result:** upper limit of  $\delta_{\text{ES}}$   $1.5 \cdot 10^{-6}$ .

## 2.2 Measurement with modulation tech (2011~2012)

**Tech2:** Perfect Square Wave modulation, which gives constant torque proportional to  $V^2$ . However delays due to lossy elements cause force transients proportional to delta at every square wave transition \*



Ideal SW to one diagonal pair

$$V_{MOD} = \sum_{j, odd} \frac{4V_M}{j\pi} \sin(\omega_M t)$$

Compensation voltages to the other pair

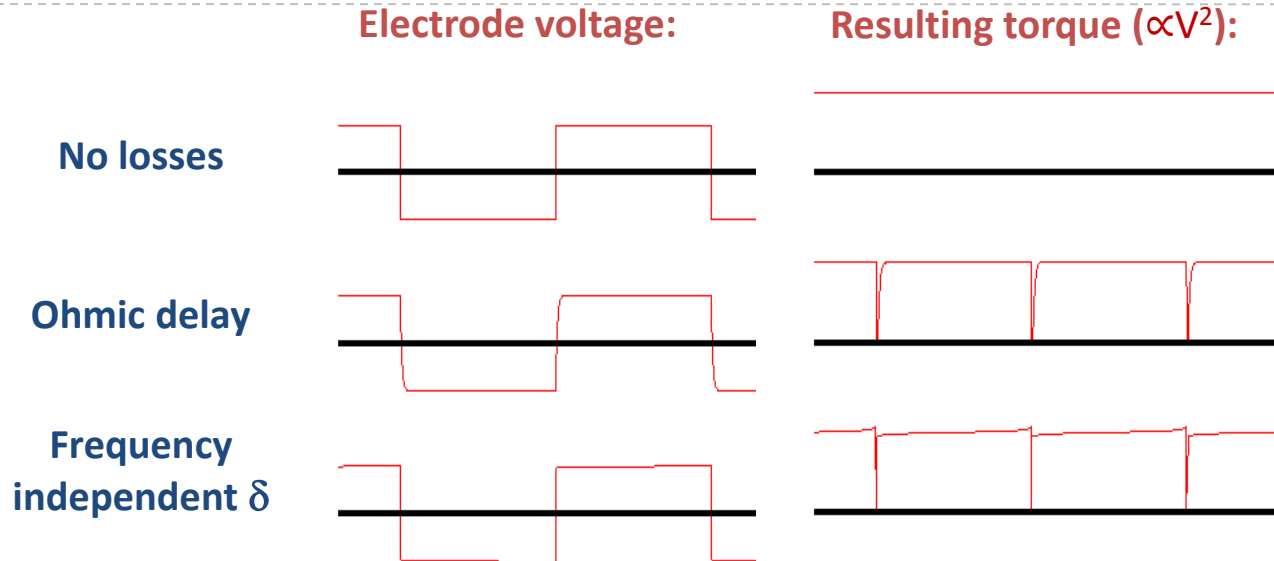
$$N_{DC} \equiv \frac{\partial C}{\partial \phi} V_{COM}^2$$

Huge DC torque cancelled  
Small transient torque left

- $\pm V_{com}$  and out of phase square wave applied to diagonal pairs, to avoid the change of TM potential
- enable to measure circuit loss and surface loss  $\tau$  &  $\delta_{ES}$  together
- Huge DC torque ( $\sim 10^{-10}$  N m) cancelled, small transient torque left ( $\sim 10^{-17}$  N m  $\leftrightarrow$   $\delta_{ES} \sim 10^{-7}$ ) for losses extraction

\* L. Carbone et al, 6th Amaldi, Japan, 2005

## 2.3 Illustration of measured signal



- 2f signal (+ other even harmonics)
- Nearly “Dirac  $\delta$ -function” for ohmic delay (all cosine)
- Longer lived signal for frequency independent  $\delta_{ES}$  (both sine and cosine)

$$\begin{aligned}
 \frac{-N_{2f}}{N_{DC}} &\approx \left[ \delta_{ES} \cdot \left(\frac{4}{\pi}\right)^2 \frac{2}{\pi} \left( \sum_{j, \text{odd}} \frac{\ln j(j+2)}{j(j+2)} \right) + 8f_M \tau \right] \cos(2\omega_M t) + \left[ \delta_{ES} \cdot 1 \left(\frac{4}{\pi}\right)^2 \right] \sin(2\omega_M t) \\
 &\qquad \qquad \qquad \approx 0.681 \qquad \qquad \qquad = 1 \\
 \frac{-N_{4f}}{N_{DC}} &\approx \left[ \delta_{ES} \cdot \left(\frac{4}{\pi}\right)^2 \frac{2}{\pi} \left( \sum_{j, \text{odd}} \frac{\ln j(j+4)}{j(j+4)} - \frac{\ln 3}{3} \right) + 8f_M \tau \right] \cos(4\omega_M t) + \left[ \delta_{ES} \cdot \frac{2}{3} \left(\frac{4}{\pi}\right)^2 \right] \sin(4\omega_M t) \\
 &\qquad \qquad \qquad \approx 0.574 \qquad \qquad \qquad \approx 0.67
 \end{aligned}$$