

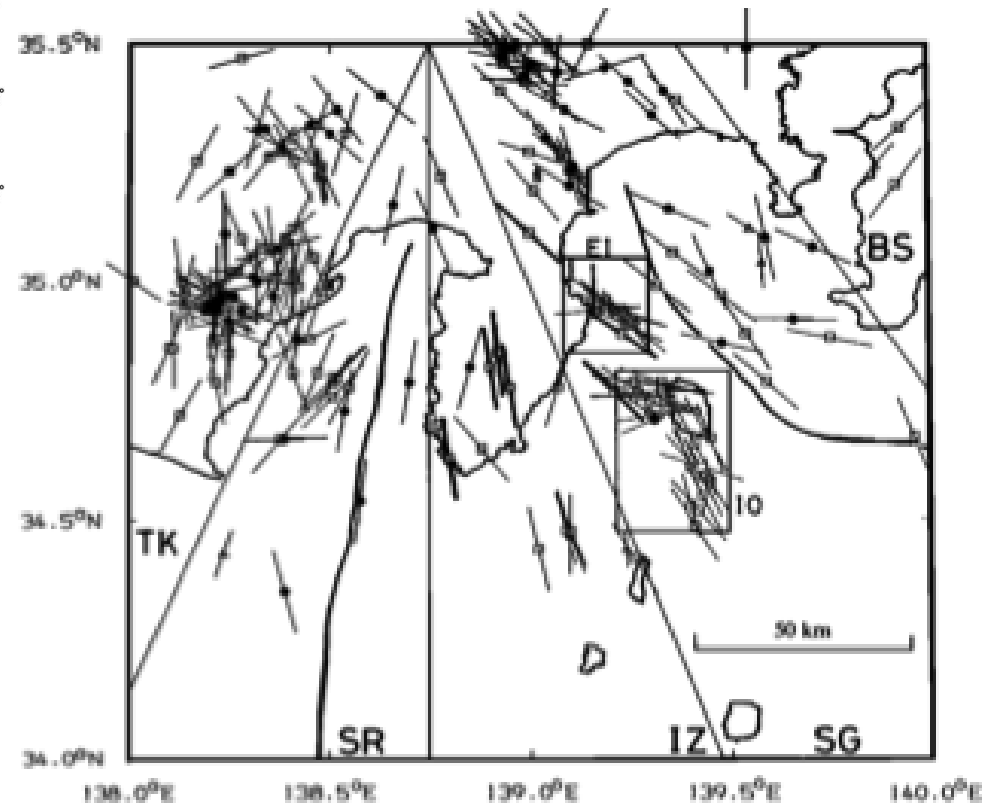
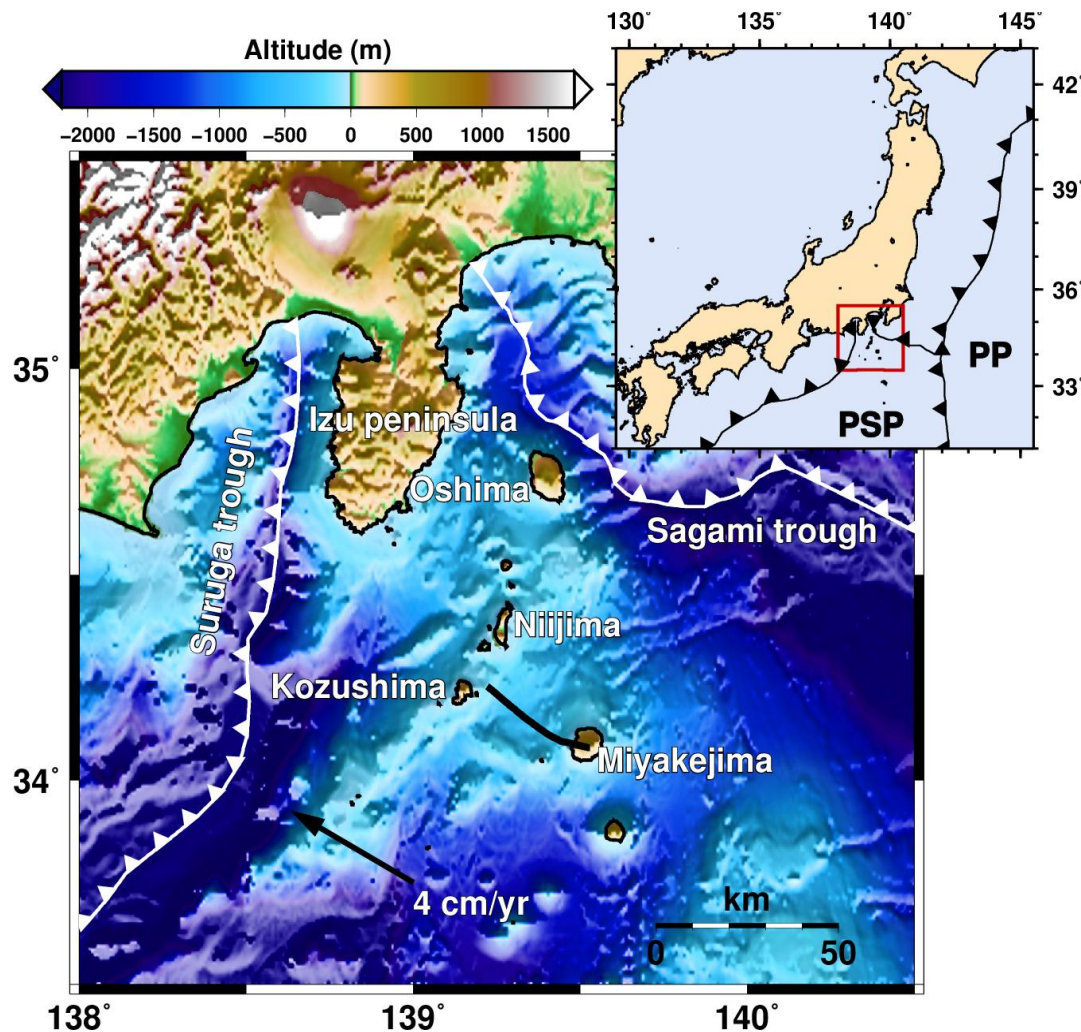
The 2000 Miyakejima dike injection: the mechanics of dike and faulting

Rivalta, E

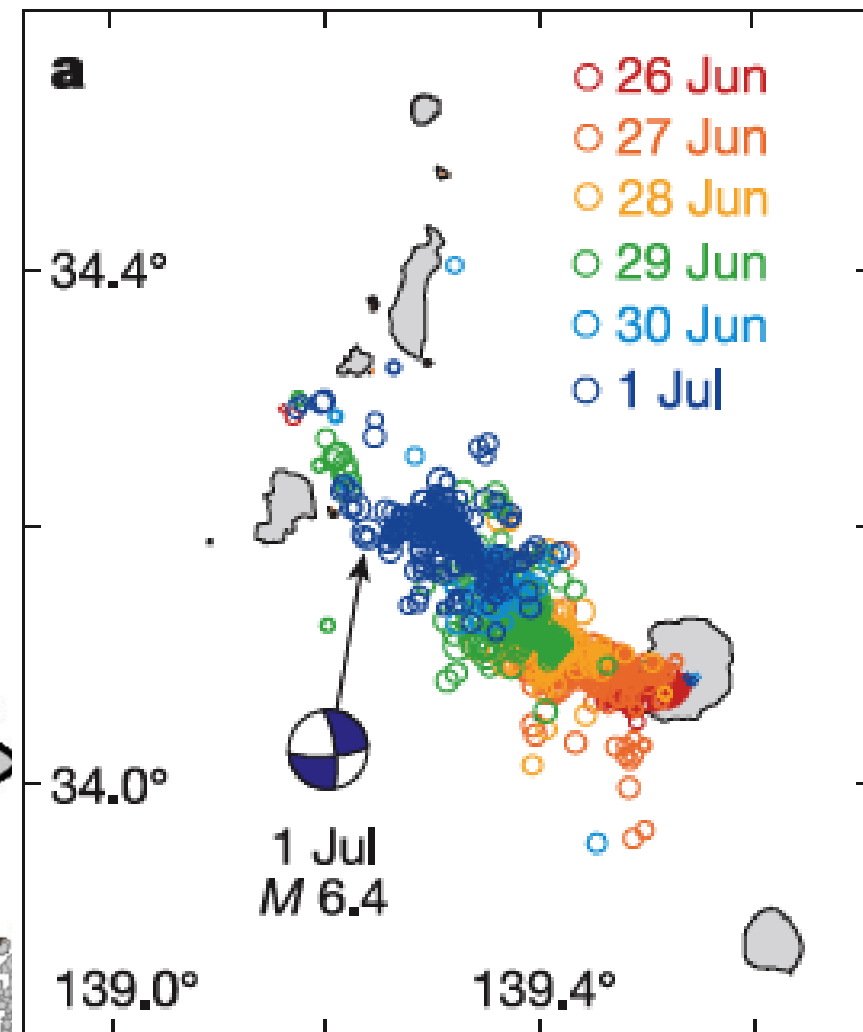
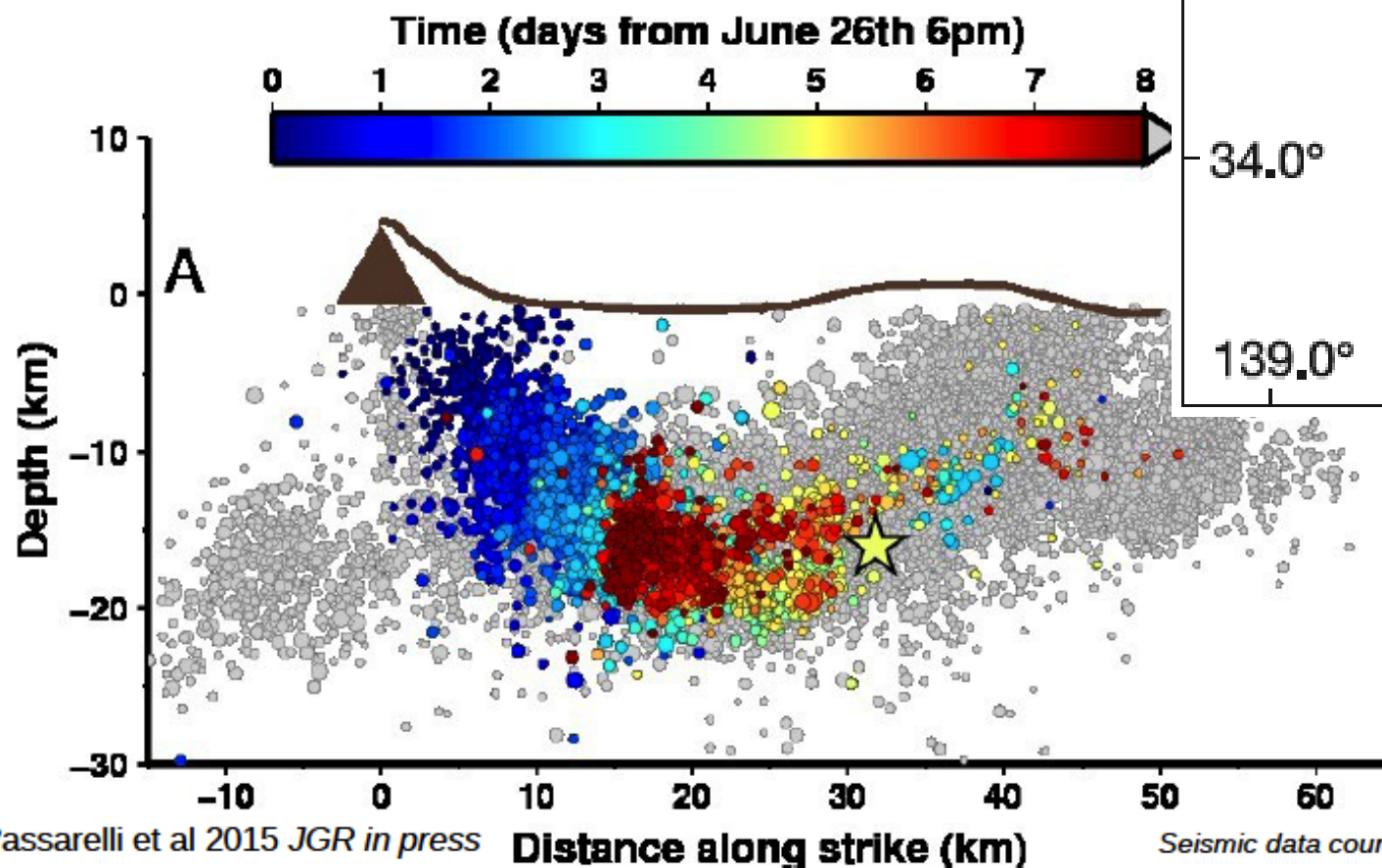
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Luigi Passarelli,
Fabio Corbi,
Camilla Cattania,
Jana Schierjott,
Yosuke Aoki



The 2000 Miyakejima dike

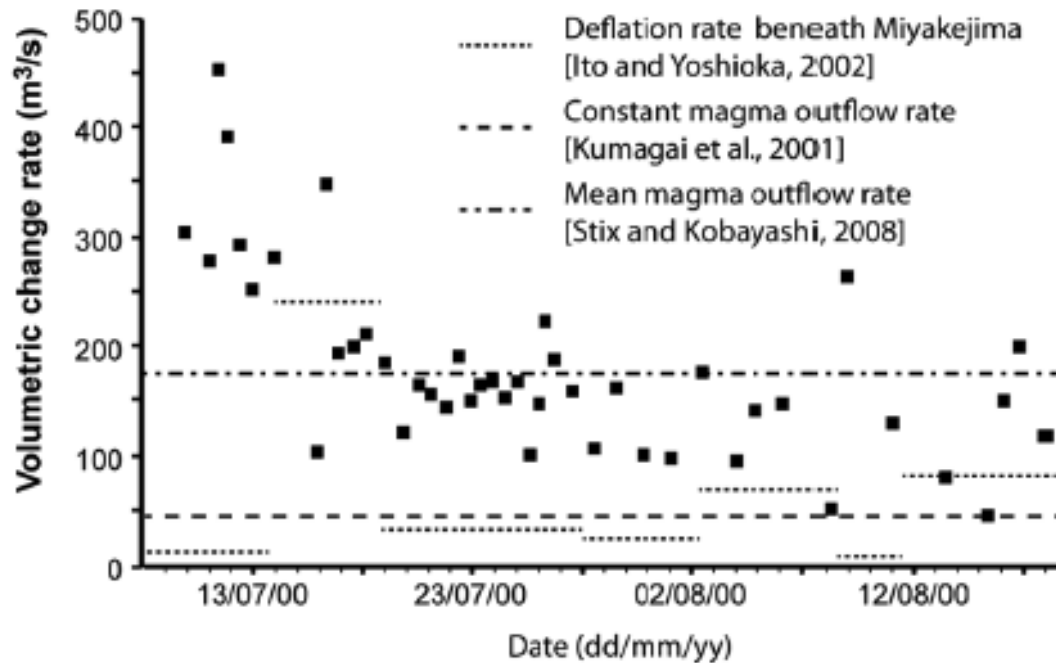
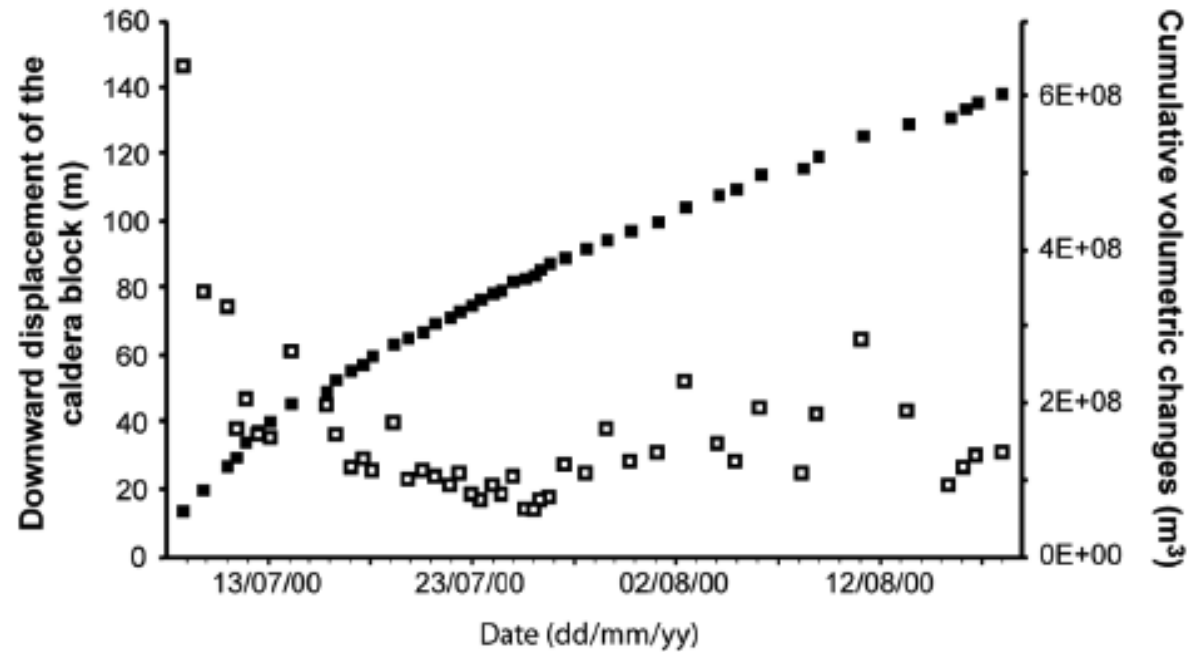


The 2000 Miyakejima dyke



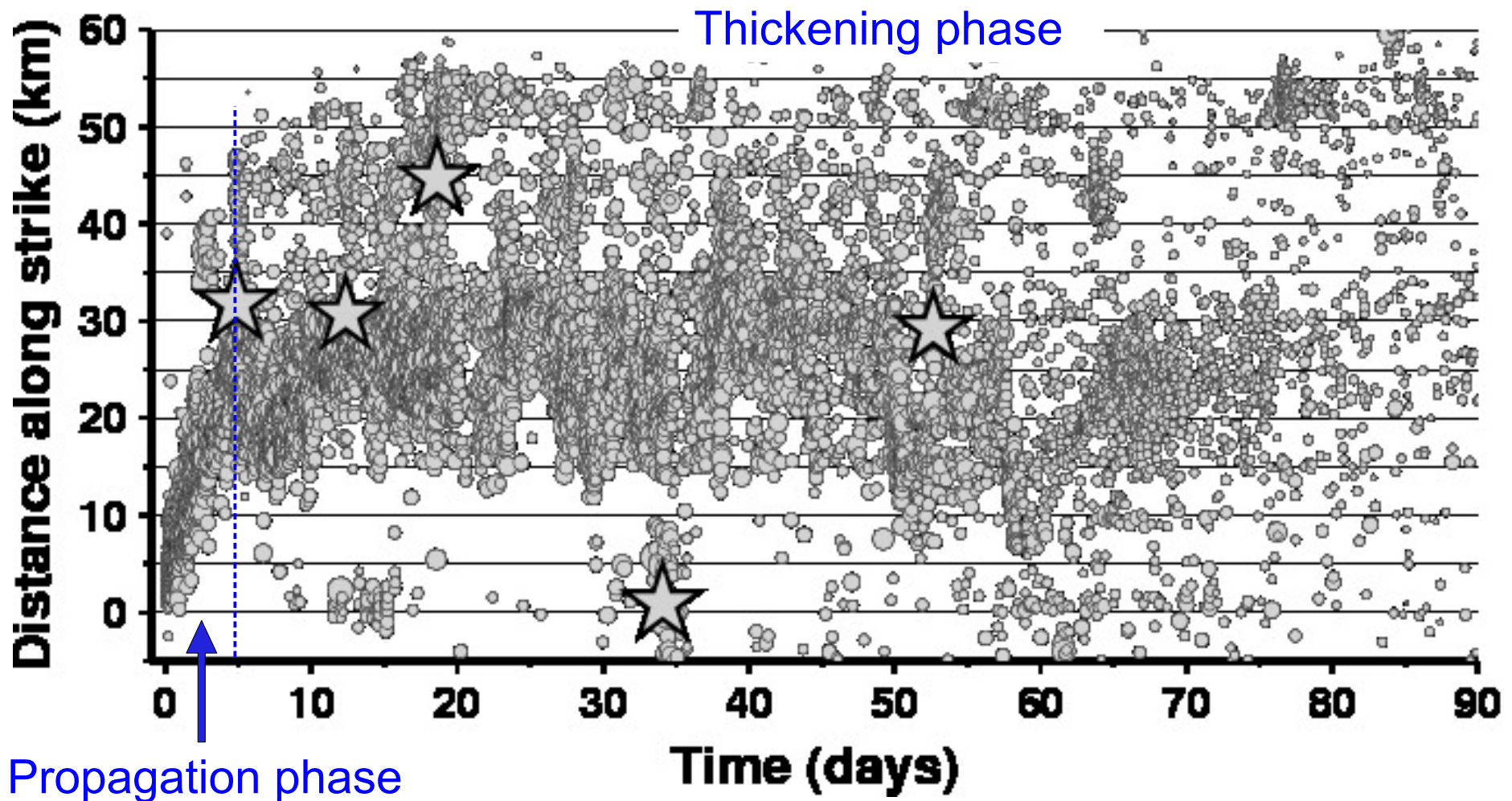
Toda et al., 2002

The dynamics of the caldera



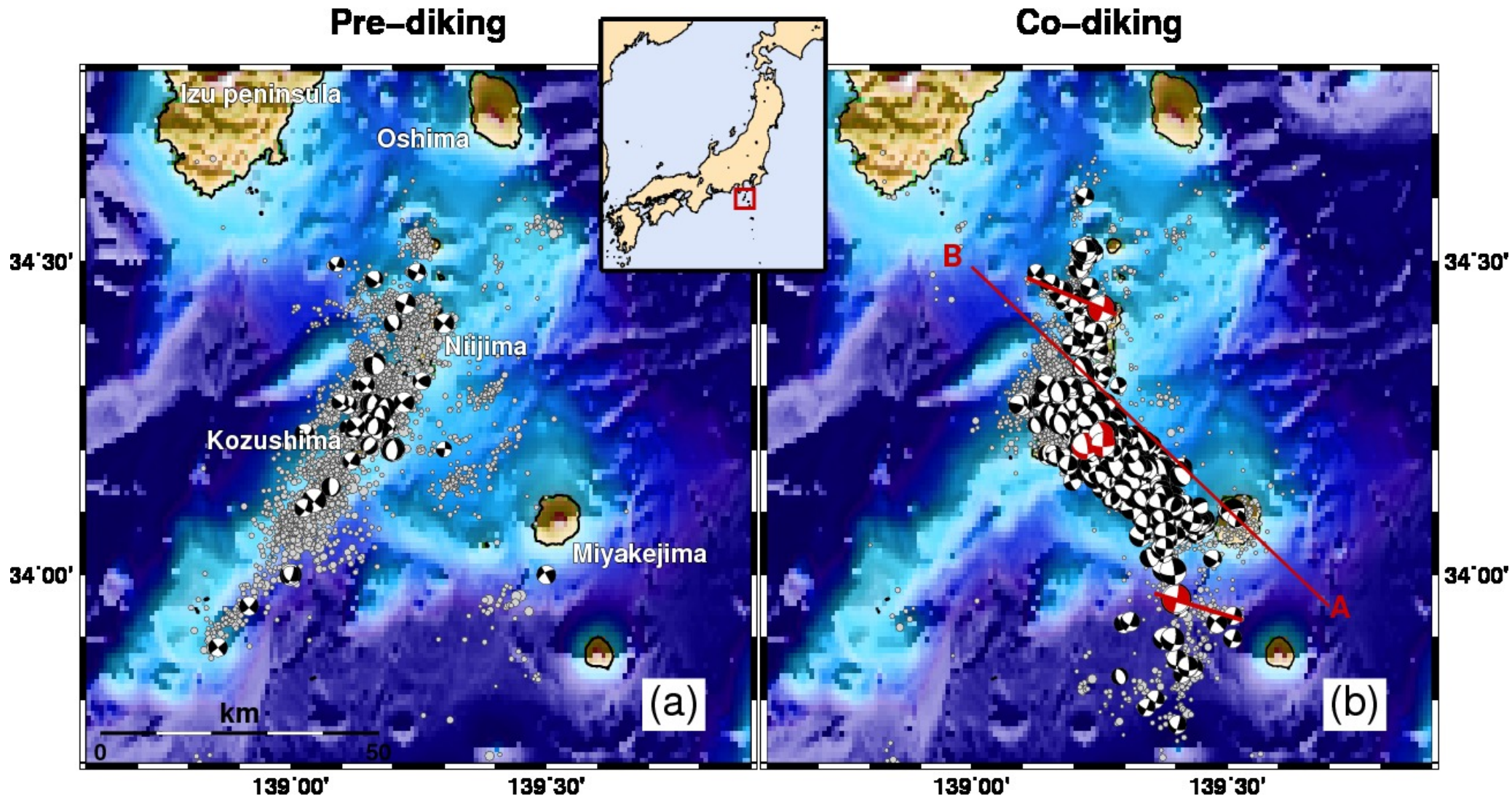
Michon et al., 2011

Motivation: dyke dynamics



- The dike became arrested and did not resume propagation in spite of being abundantly fed. Why?
- What consequences did this have onto the mechanics strain release?

Motivation: faulting patterns



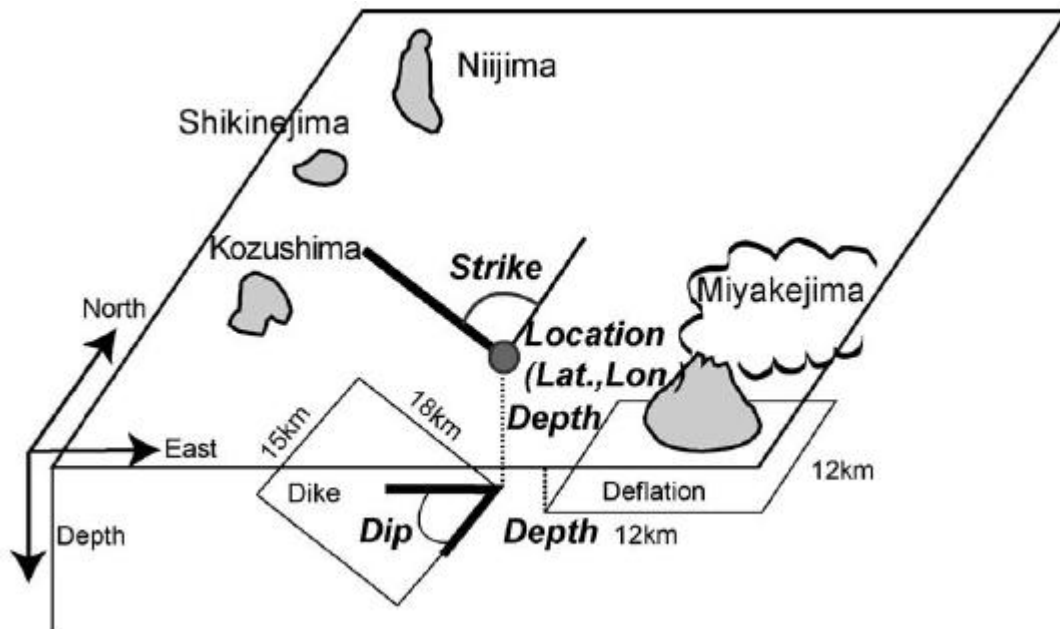
From *Passarelli et al., 2015*. Hypocenters by JMA, $M_l > 1.5$, FMs by NIED, $M_w > 3$

- The co-diking FMs show variability of fault plane orientation. Why?

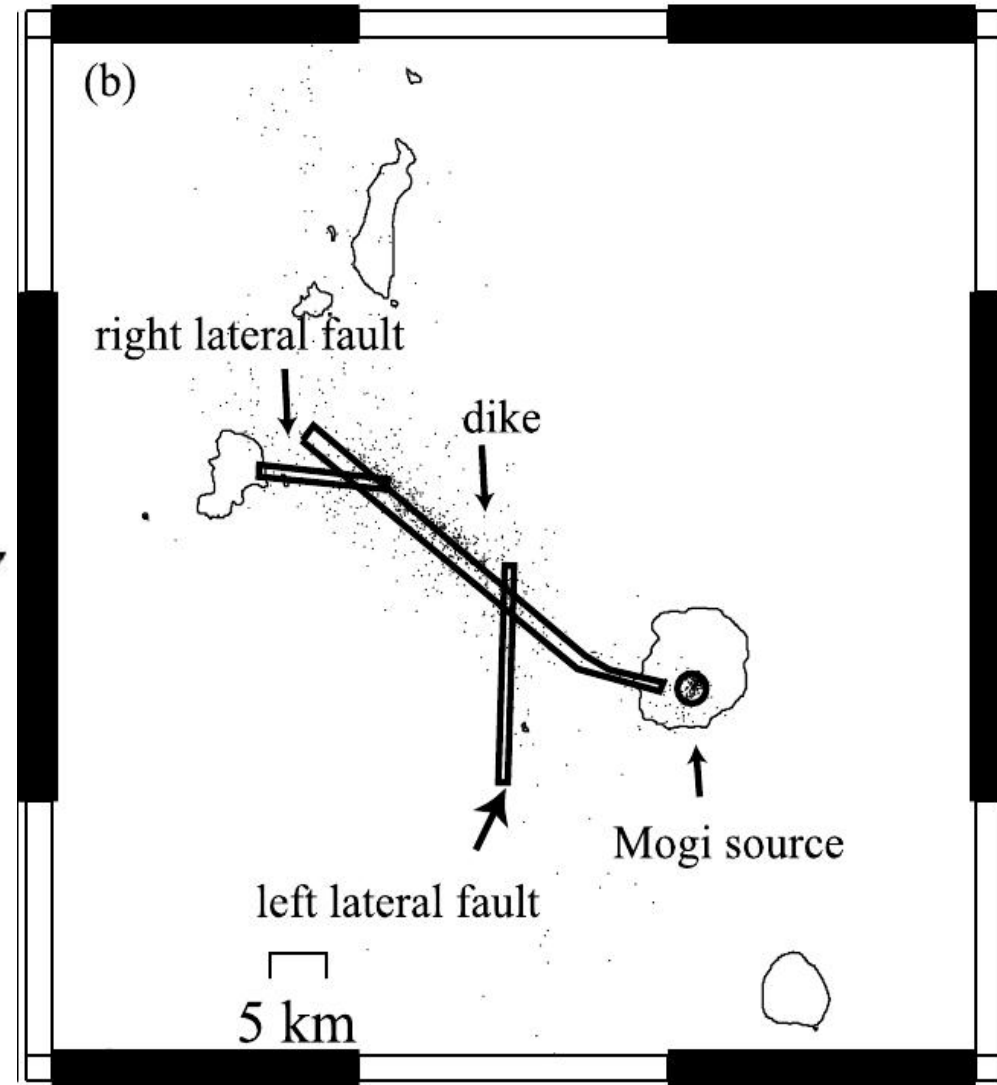
Motivation: deformation

Deformation models span from simple to complex geometries

- Multiple 'slowly moving' shear sources are needed

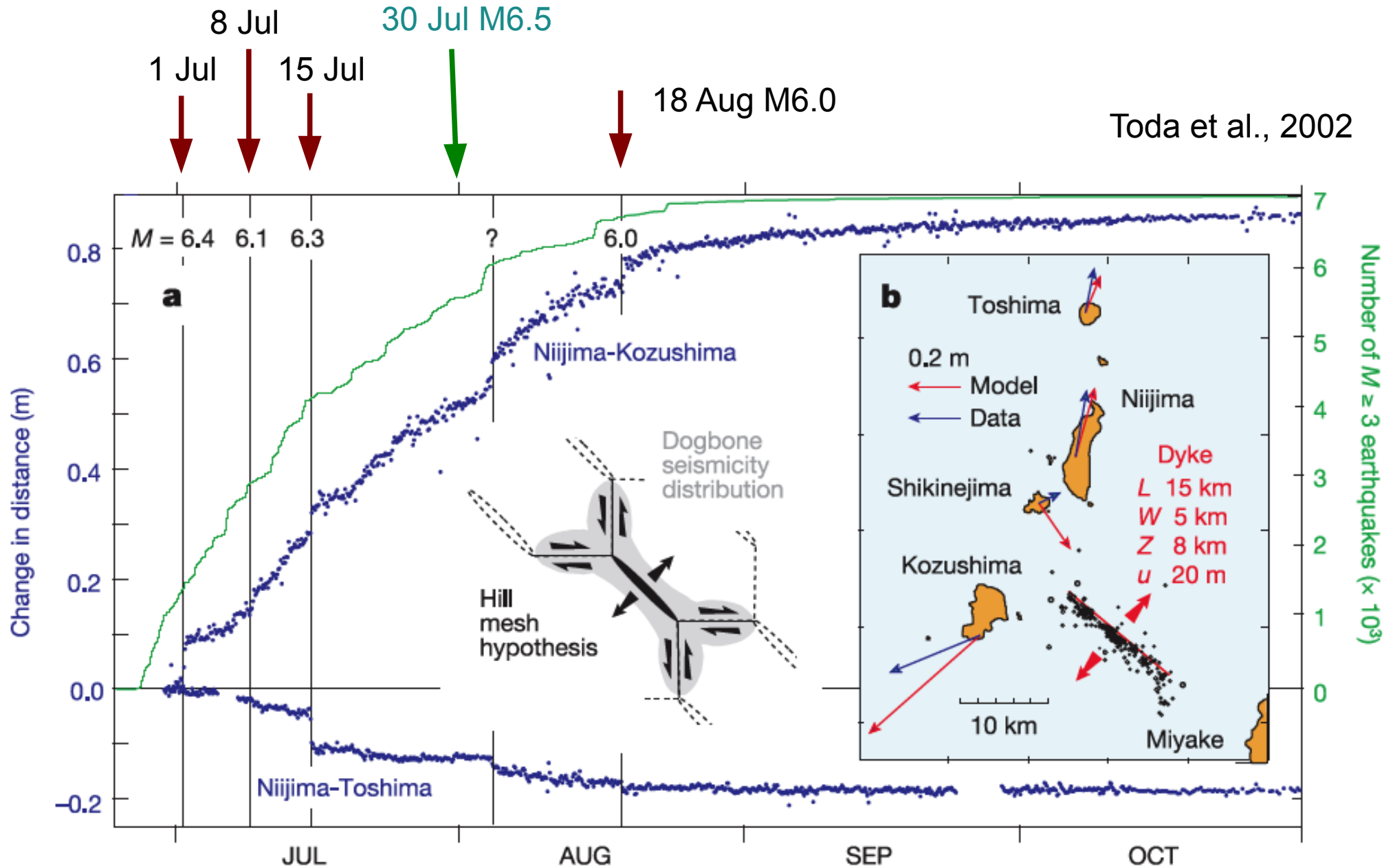


from Ito and Yoshioka 2002.

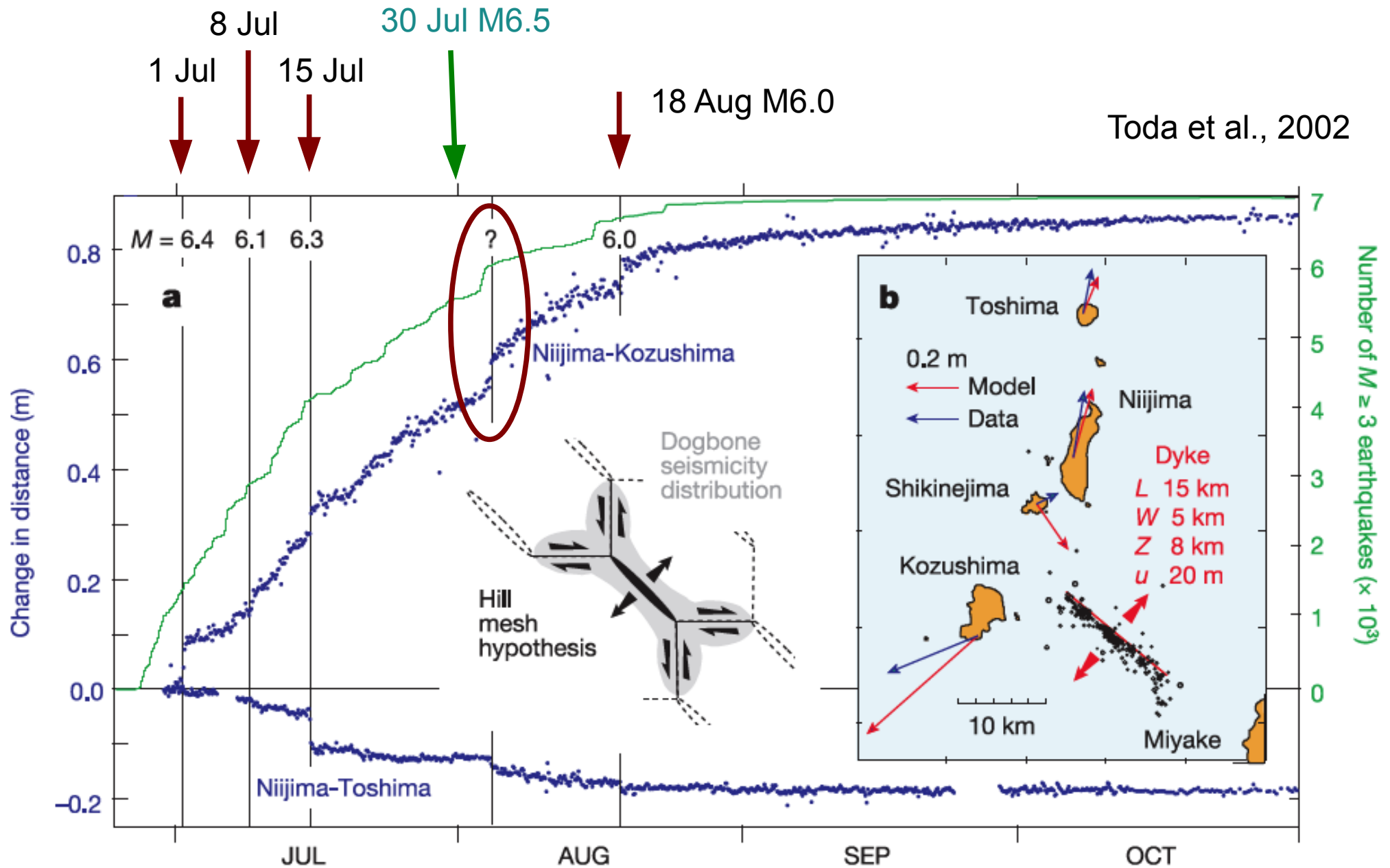


from Ozawa et al., 2004.

Motivation: deformation and seismicity



- The deformation shows unexplained jumps. What is that?



Talk outline

Explore fault-dike interaction for the 2000 Miyakejima dyke
by means of:

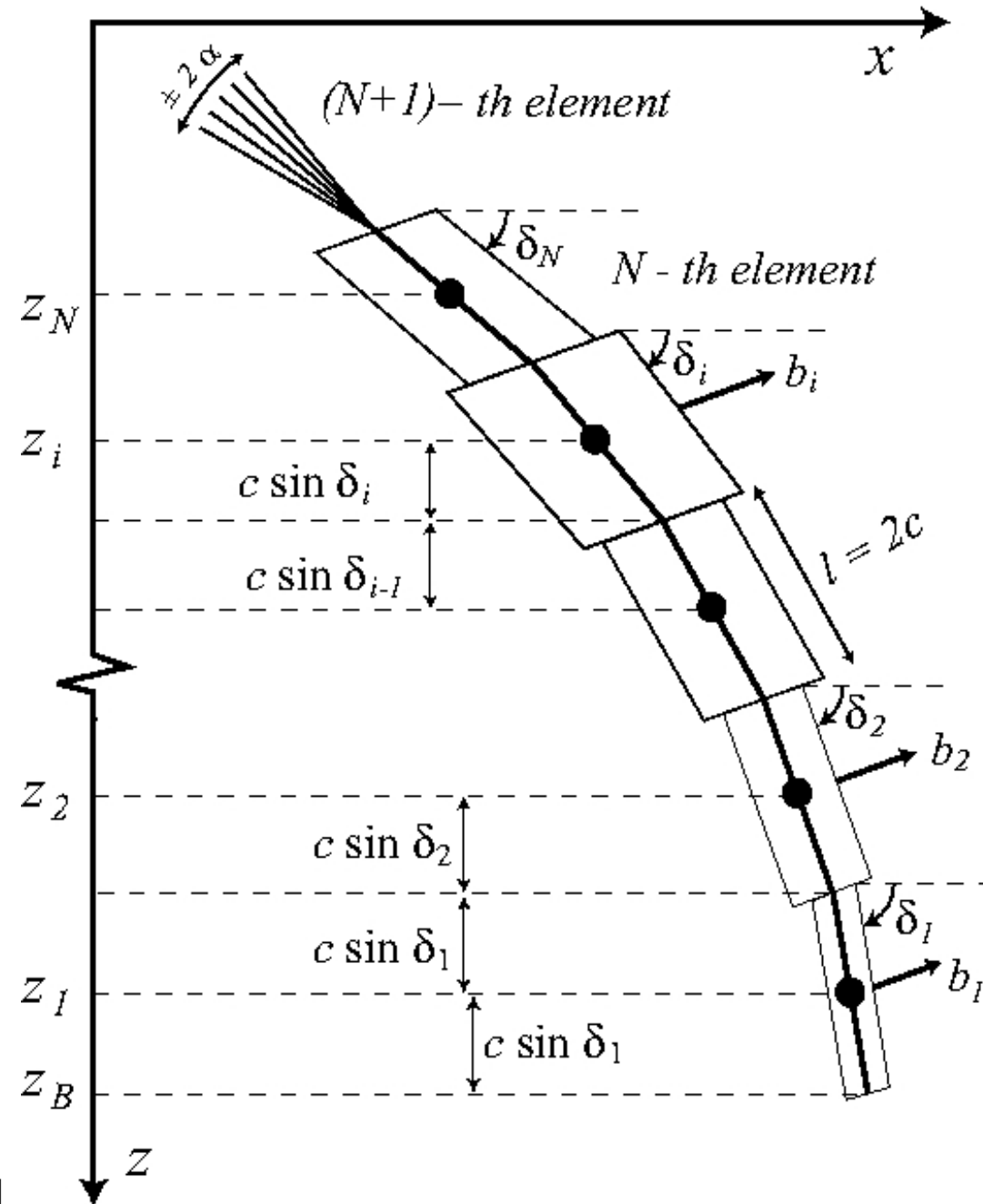
- 1) Numerical and analog mechanical models
- 2) Statistics

Questions:

- 1) What arrested the dike?
- 2) How was the strain released during this dike intrusion?

Numerical model

- *Boundary elements* (*Displacement discontinuity method*);
- The *dike propagation* is realized by adding a dislocation element at the tip of the crack and checking if energy release $E >$ fracture energy E_c (if $E < E_c \rightarrow$ stop);
- The direction that *maximizes* the total *energy release* is chosen;



Numerical model: Set-up and assumptions

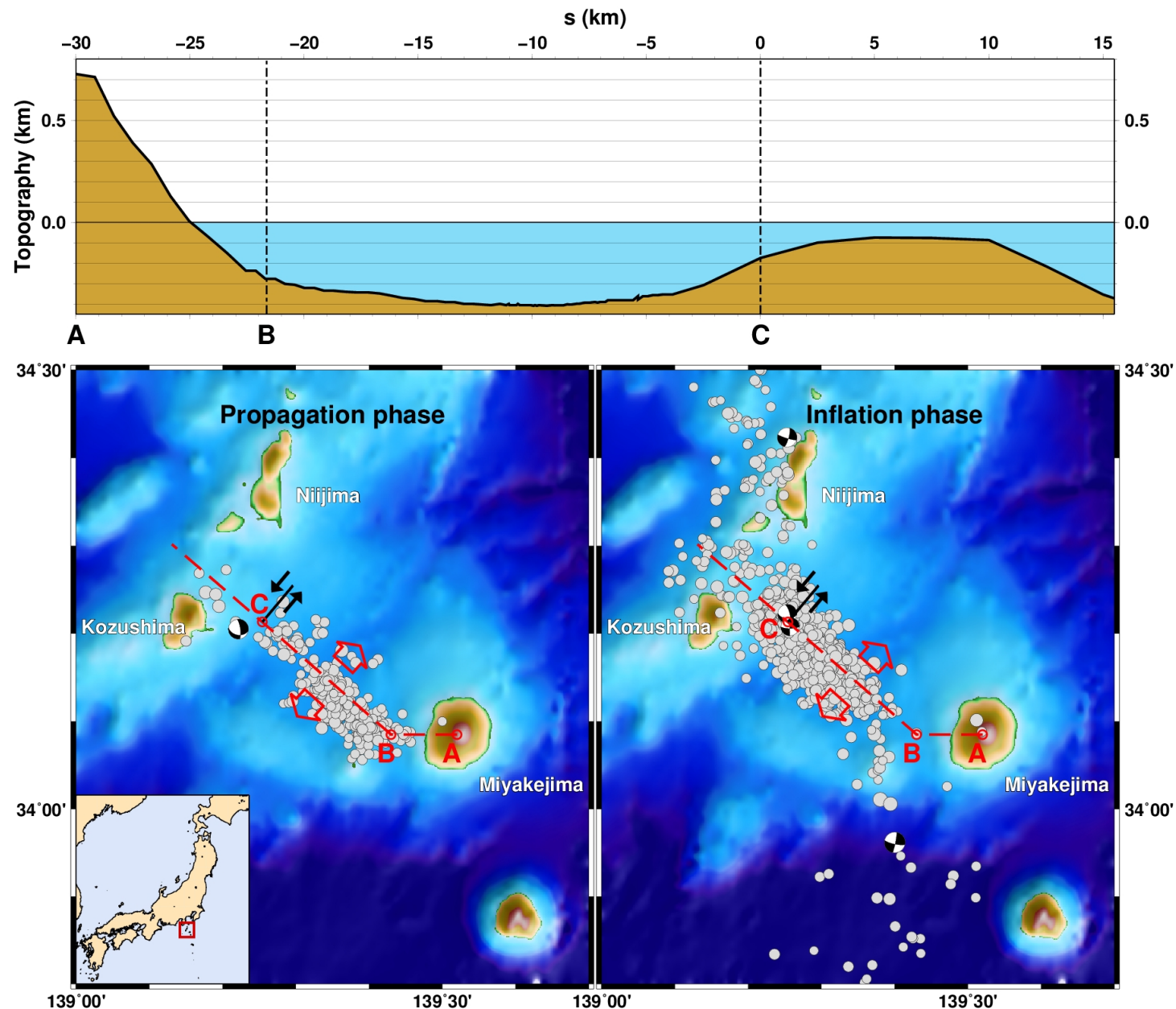
We simulate three scenarios:

1) stress gradient due to topographic load only,

2) dike-faulting interaction only,

3) 1) + 2)

We simulate magma influx by incrementing the dyke volume at each model step.



Numerical model: Parameters and constraints

From *Hughes G. R., 2010, PhD thesis.*

- MECHANICALLY CONSISTENT
DIKE – FAULT GEOMETRY

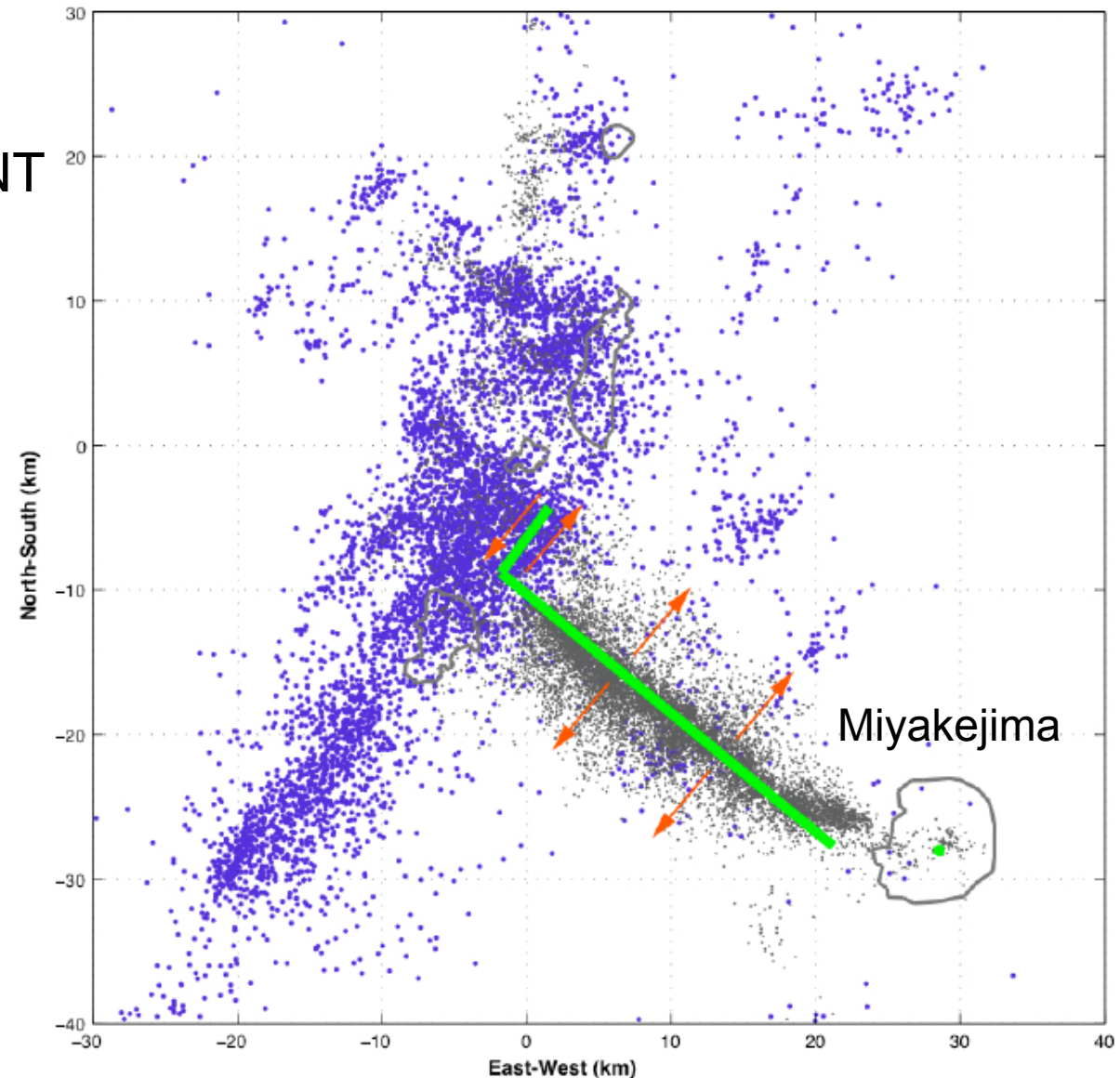
- INVERTED OPENING & SLIP:

End of propagation phase

- DIKE OPENING = 0.82 m
- FAULT SLIP = 0.39 m

End of inflation phase

- DIKE OPENING = 3.4 m
- FAULT SLIP = 4.4 m



Numerical model: Procedure

For each scenario:

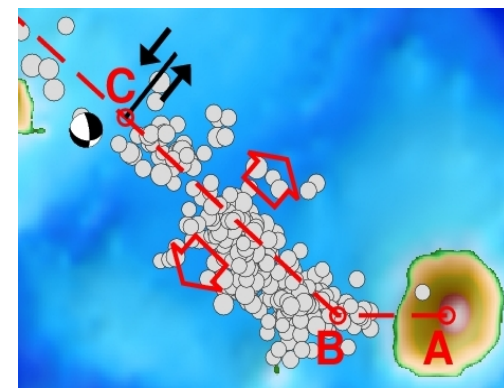
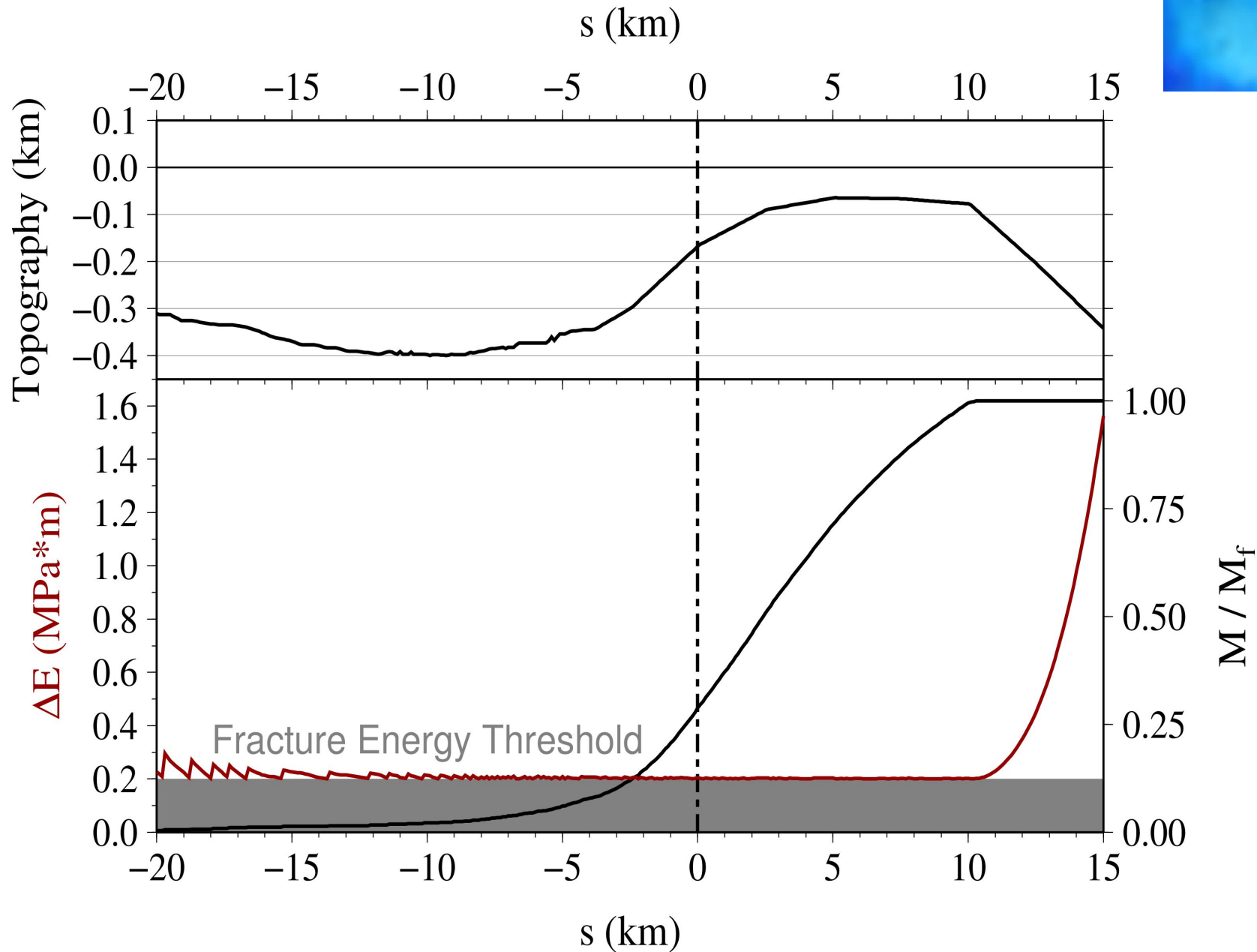
- At every model step, feed dike, add one dislocation element, calculate dike shape and energy release -> if $E > E_c$ accept increment.
- By trial and error, calibrate E_c , (constant) so that the opening at the end of propagation phase is $D_u = 0.82$ m (Hughes, 2010).
- For scenarios 2) and 3), we constrain the interacting dike and fault to have $D_u = 0.82$ m and slip = 0.39 m -> set shear stress pre-loaded on the fault
- Continue to feed the dyke. Check propagation. Stop simulation when either the dike reaches the final opening (3.4 m) or is way beyond the final point.
- For scenarios 2) and 3), obtain shear stress rate for the fault to have a final fault slip of 4.4 m

Numerical model: Model output

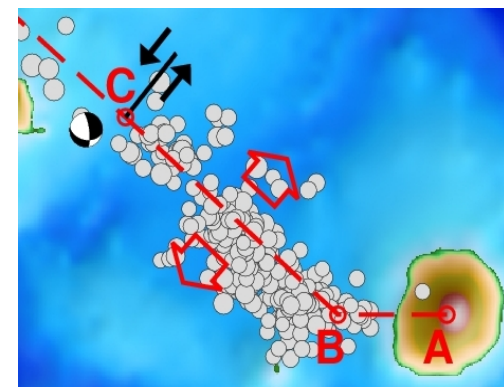
For a given set of parameter values, the model tells us, for each position of the propagating tip:

- How much areal volume has flown into the dyke
 - The cross-sectional shape of the dike (and of the distributed fault displacement)
 - The stress drop on dyke and fault
 - Once the propagation phase has been calibrated, the model reveals if the dyke is going to propagate further or stay arrested.
- > If the model was 3D (future work) we could use the magma influx obtained from the published analyses of the caldera floor dynamics to convert the model steps into time steps. Moreover, we could calculate the expected induced seismicity and deformation.

1) Only topographic load: Results

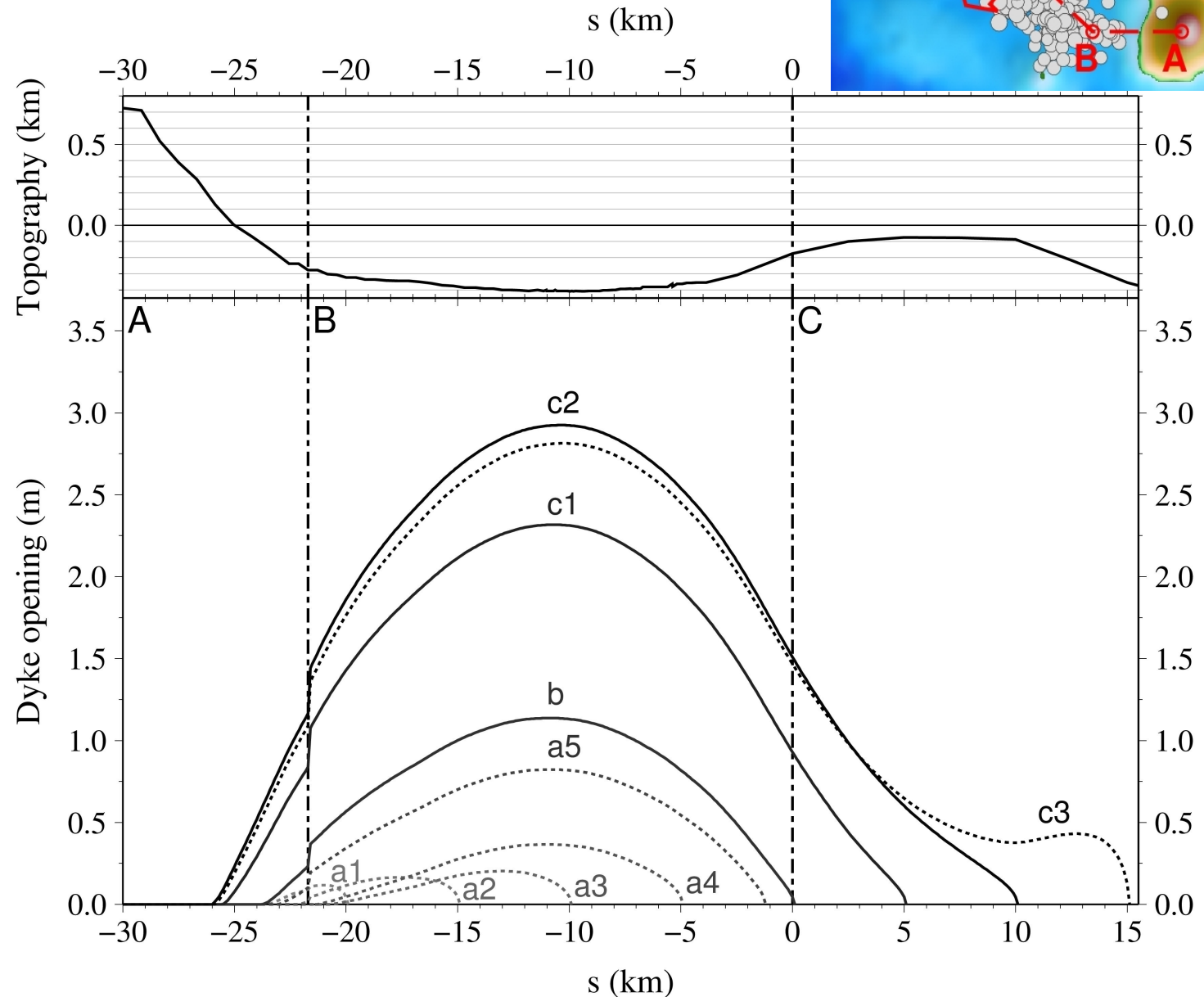


1) Only topographic load: Results

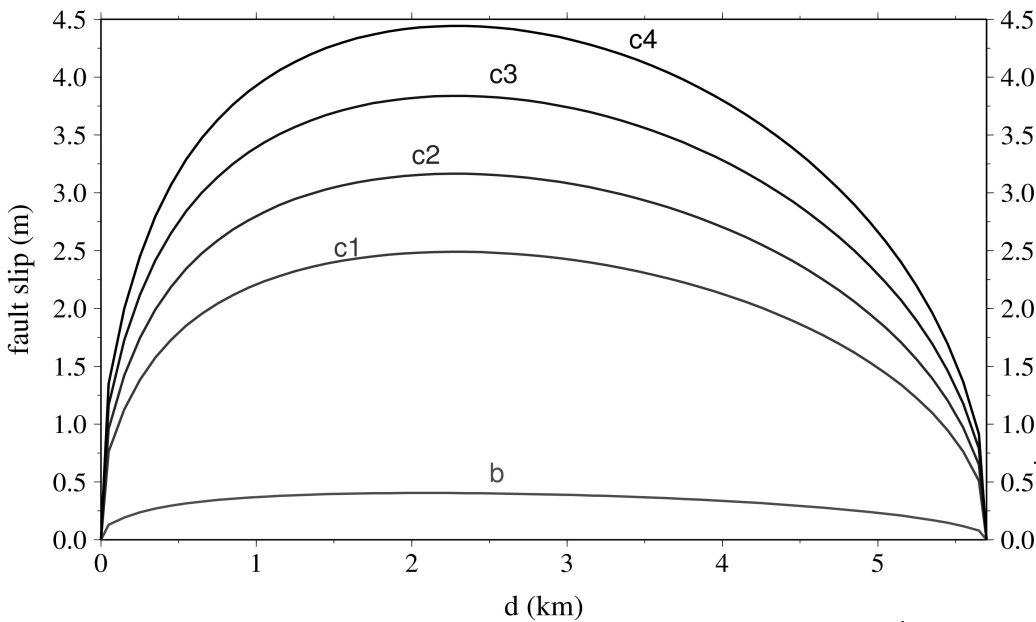
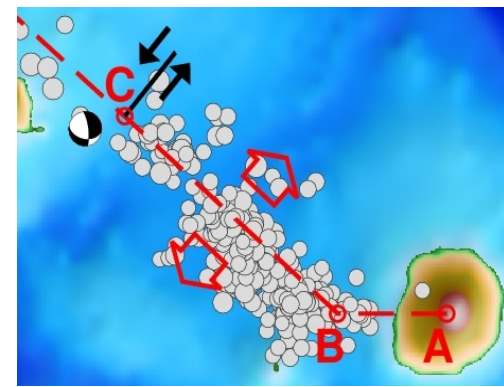


- Dike tip does not stop in C ($s=0$)

- Dike opening does not reach 3.4 m (max opening = 2.9 m)

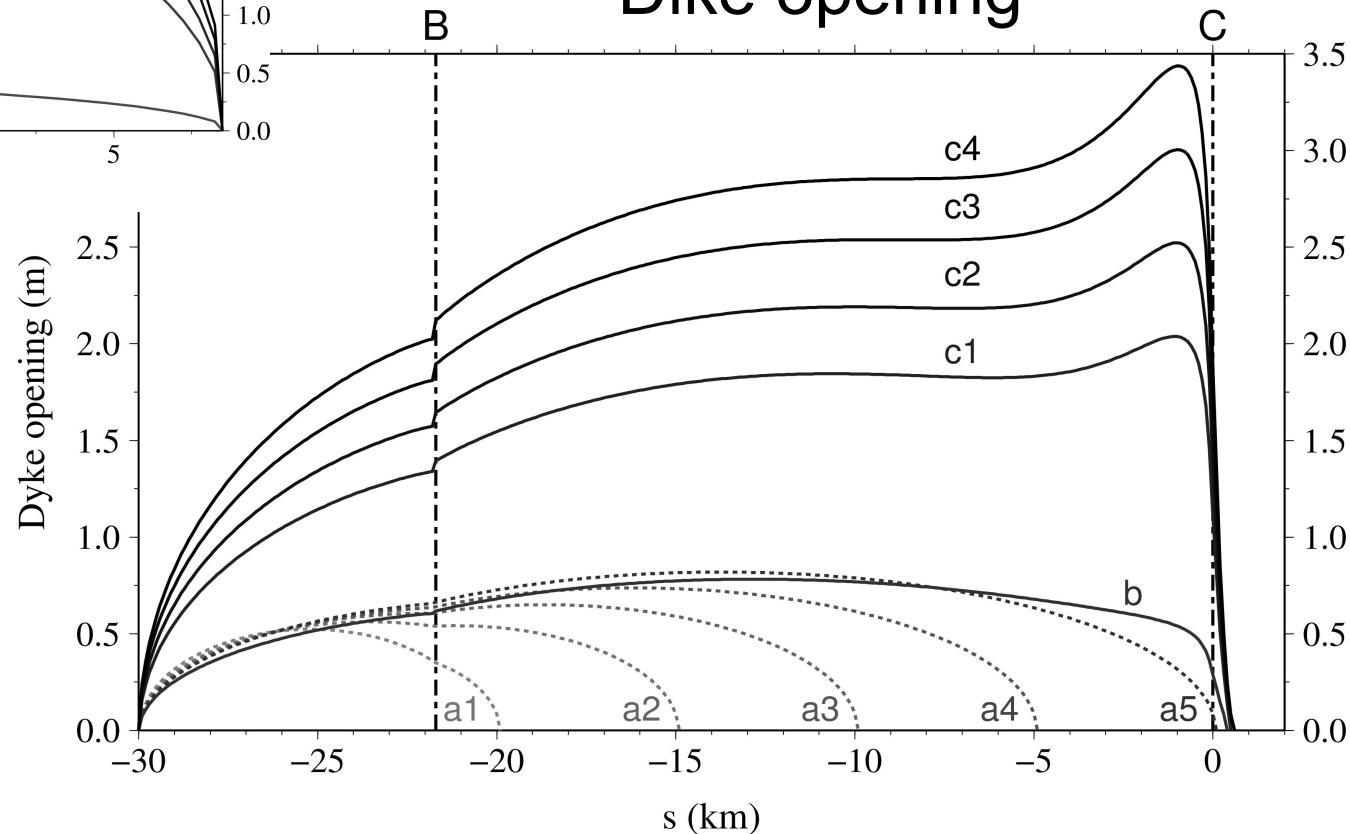


2) Only dike-fault interaction: Results



Fault slip

Dike opening



- Dyke reaches 3.4 m opening without resuming propagation.

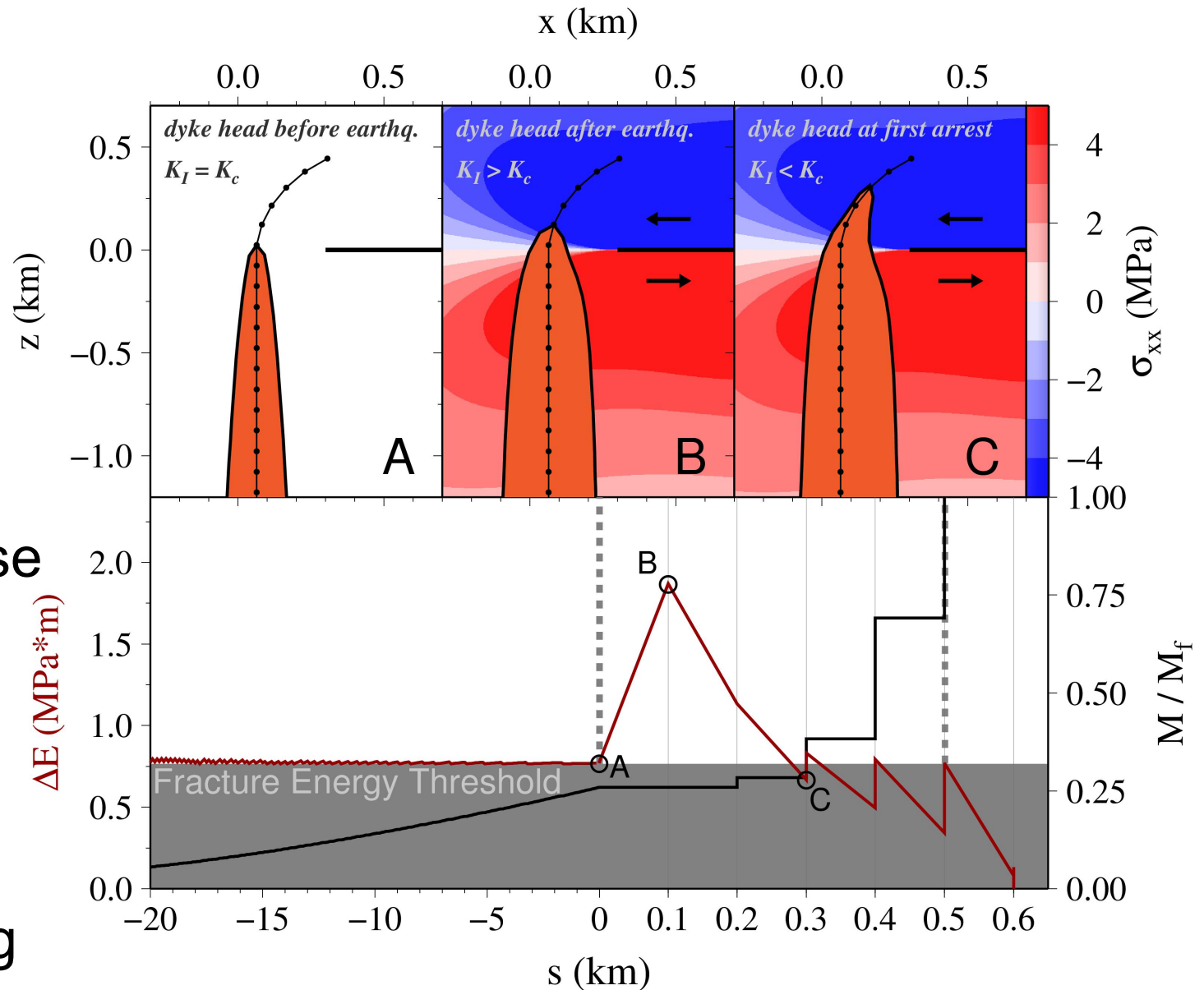
- Dyke inflates along the whole segment.

- Dike propagation with $K=K_r$ ($K_r=175$ MPa*m^{1/2}).

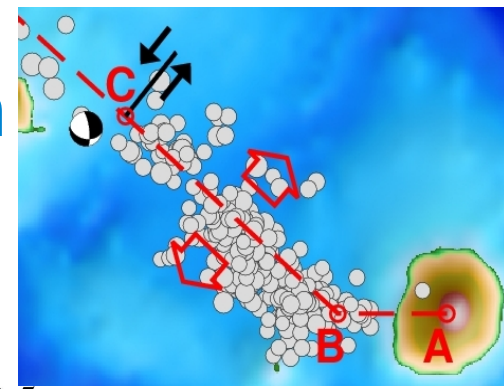
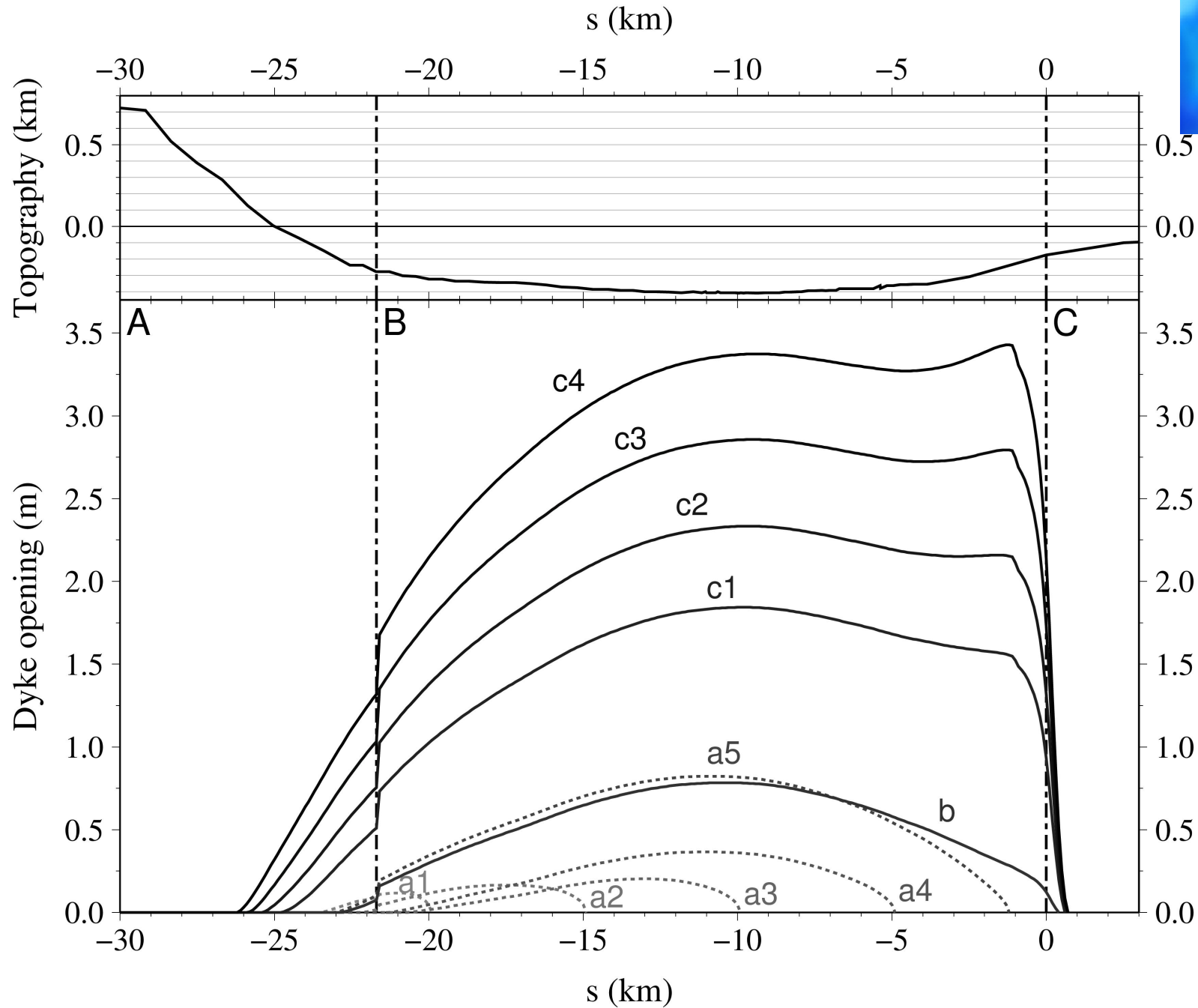
- Dike tip stops close to point C ($s=0.5$).

- Dike reach 3.4 m opening.

- Dike inflates along the whole segment.

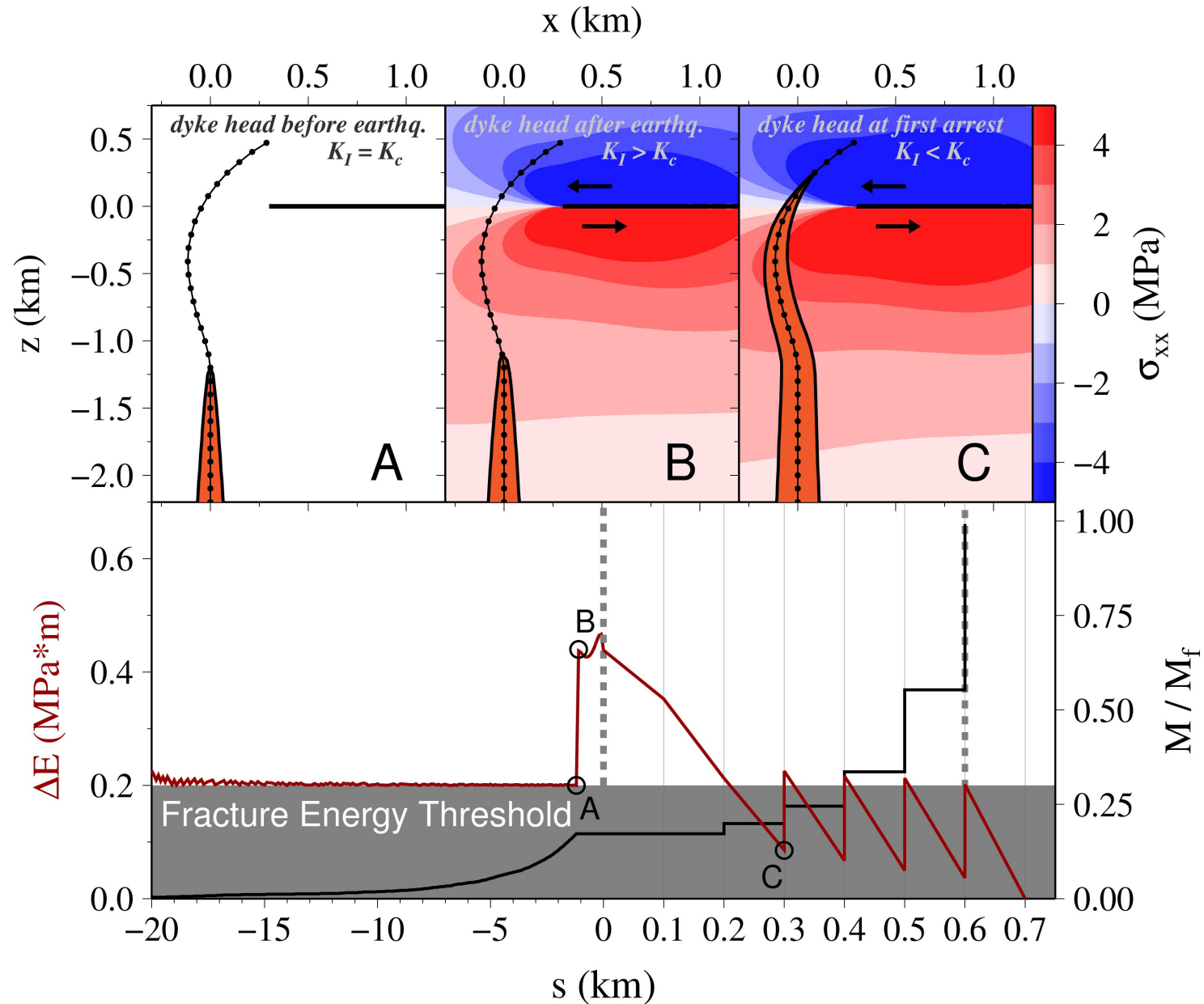


3) Topography and dike-fault interaction



3) Topography and dike-fault interaction

- Dike tip stops close to point C ($s=0$)
- Dike inflates and reaches 3.4 m opening without resumming propagation
- Dike opening concentrates on B-C





lens cap) (photo courtesy of P Delaney). In (b), magma front (*arrow*) extends slightly beyond the intersection of the fault zone with the dike; crack followed by magma continues beyond top of photo. A small amount of magmatic material has infiltrated the fracture zone. (Lens cap has been moved to the opposite side of the dike.)

Rubin, 1995

Mechanical model: conclusions

- The numerical model shows that interaction with the pre-existing fault system explains efficient dyke arrest provided that:

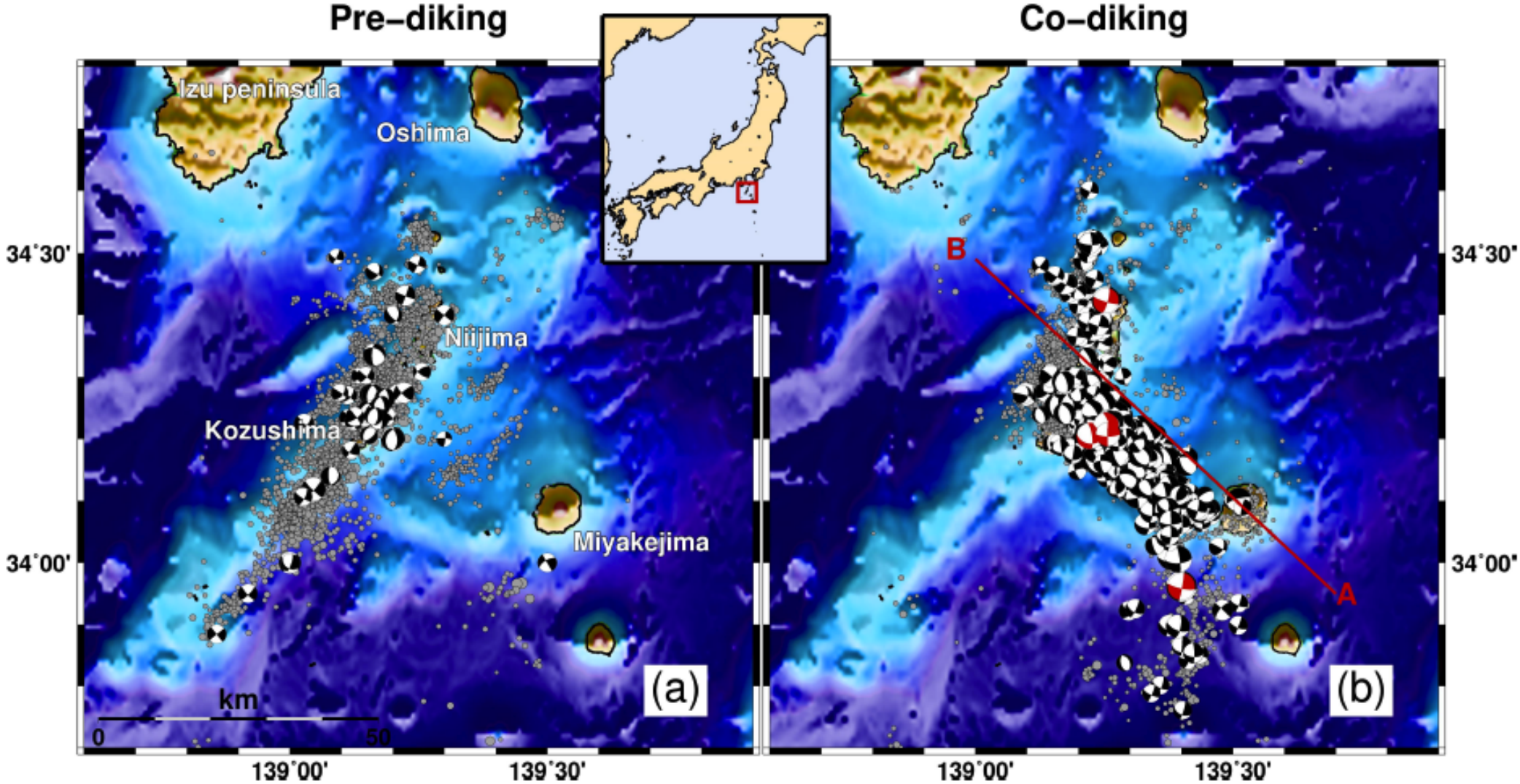
- 1) The fault was pre-loaded (-> a dyke does not get itself arrested by inducing faulting)

- 2) A shear stress rate was active on the fault (-> additional pre-loaded faults and asperities breaking one after another)

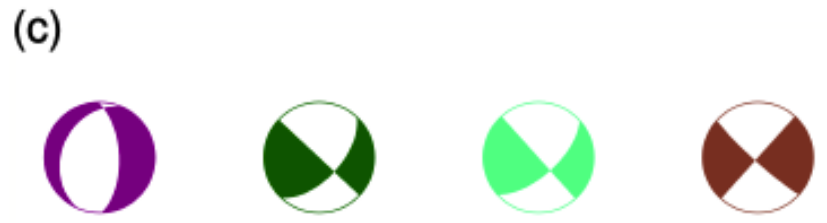
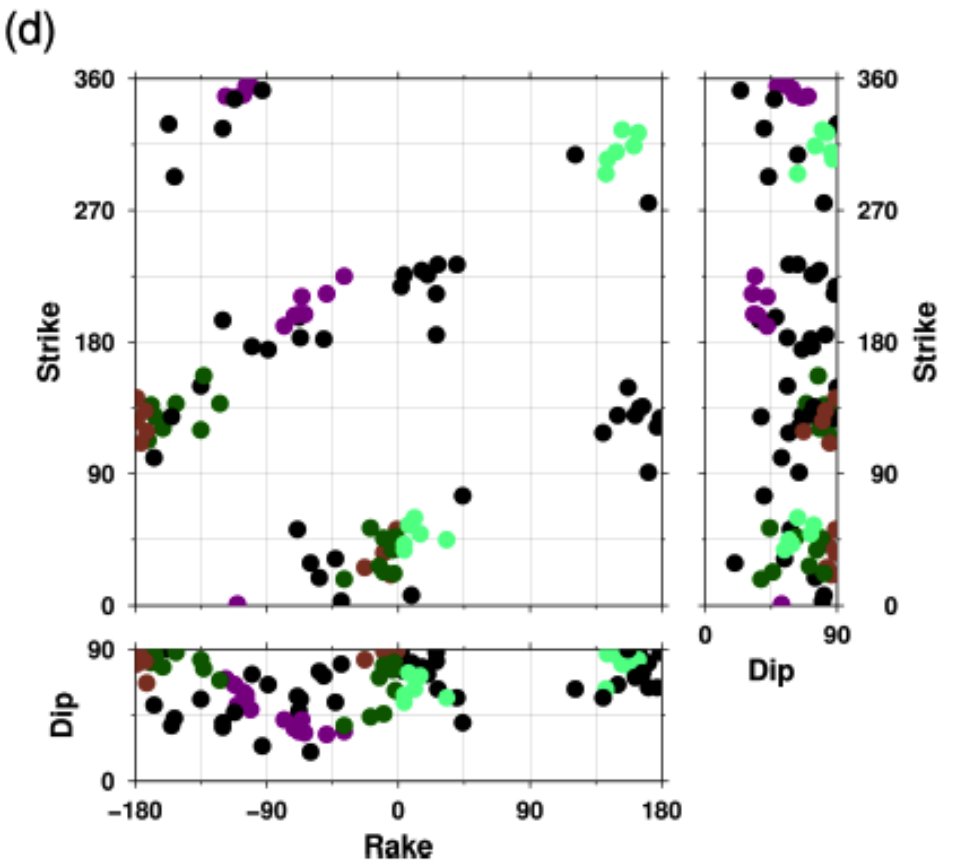
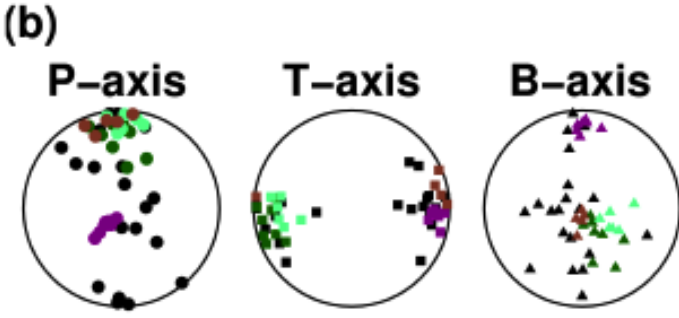
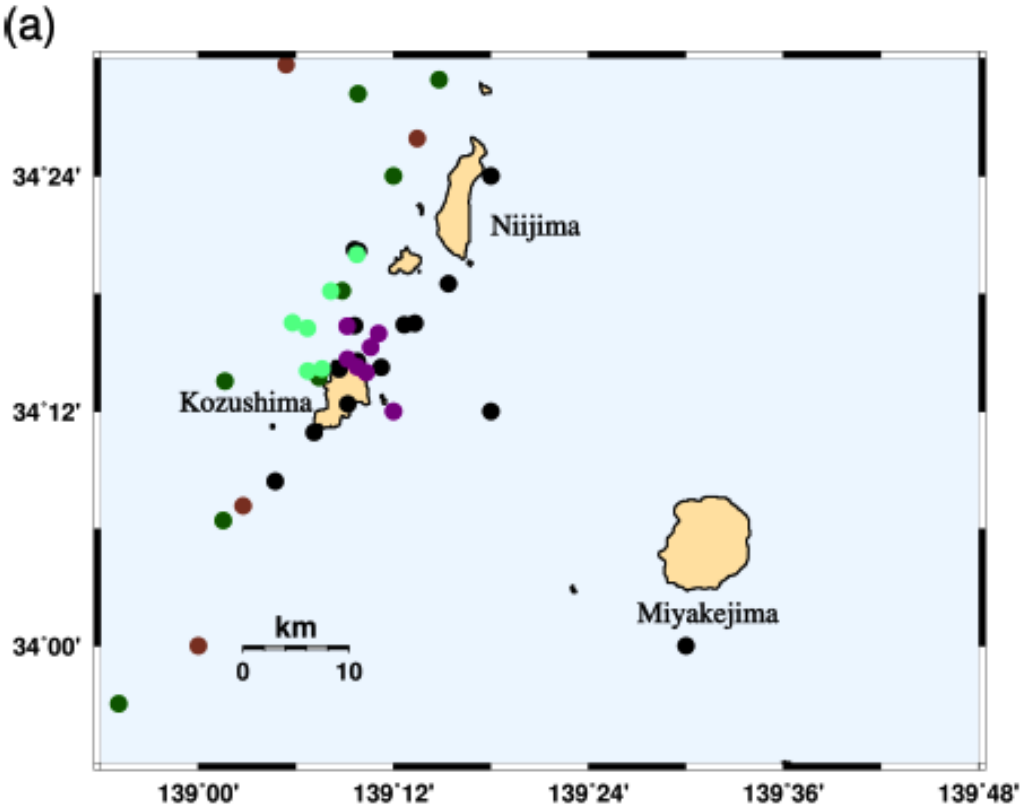
- 3) The topographic load is necessary to explain the 'confined' opening of the dike, and the propagating cloud of seismicity

- 4) Fracture energy values $\sim 0.2-1 \text{ MJ m}^{-2}$ (equivalent to $\sim 100-200 \text{ Pa m}^{1/2}$) and areal inflow rate \sim are consistent with the other parameters

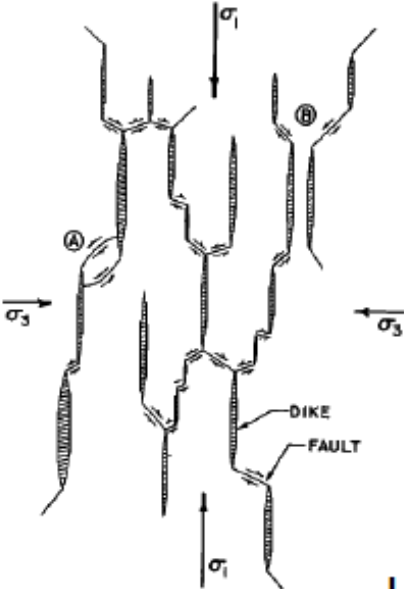
Focal mechanisms



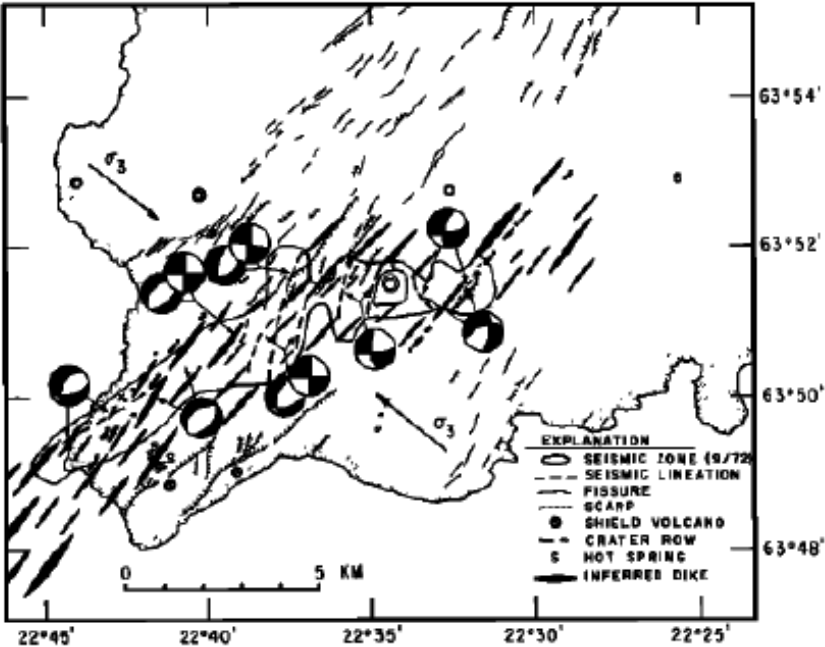
Focal mechanisms: pre-diking



Focal mechanisms: previous models



Hill, 1977



(a) Strike-slip:
horizontal σ_1 , horizontal σ_3

A diagram illustrating strike-slip faulting. It shows a central fault with two blocks of rock on either side. Red ellipsoids represent stress axes: a large horizontal one for σ_1 and a smaller horizontal one for σ_3 . Black circles with shaded quadrants represent focal mechanism solutions, showing slip along the fault.

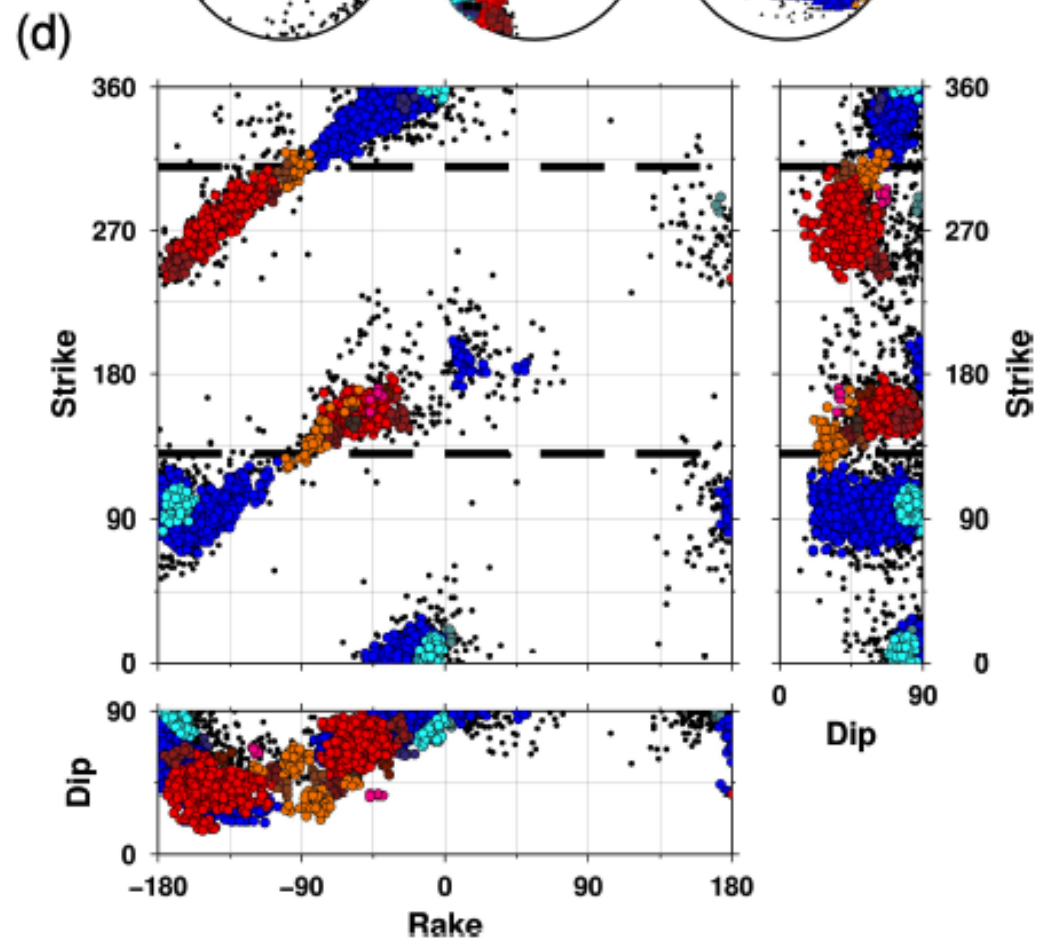
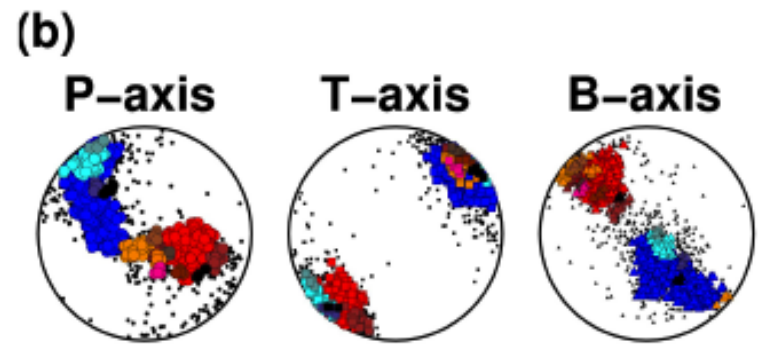
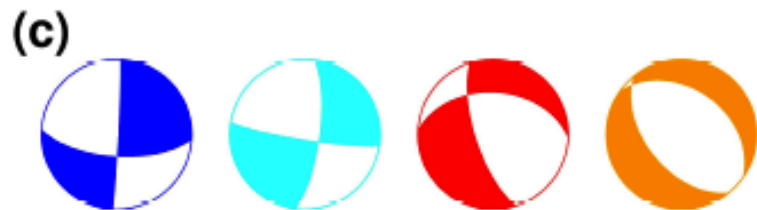
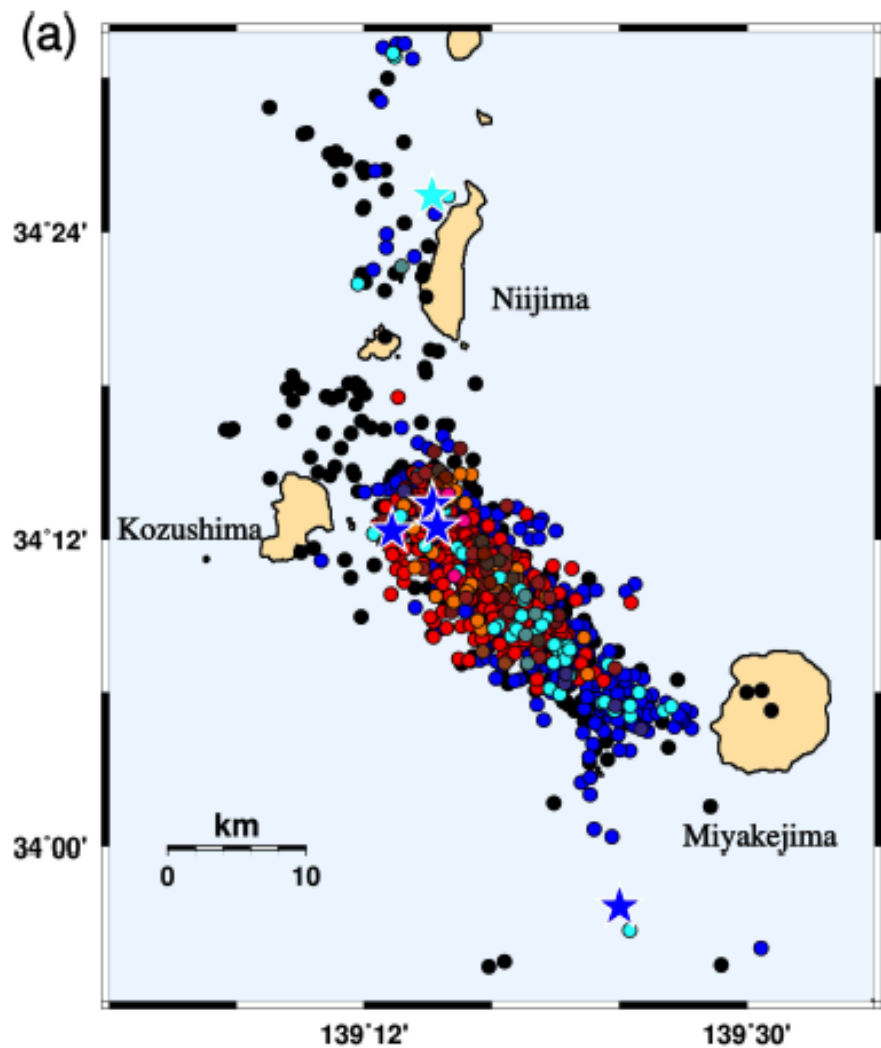
Passarelli et al 2015 submitted JGR

(b) Normal faulting:
vertical σ_1 , horizontal σ_3

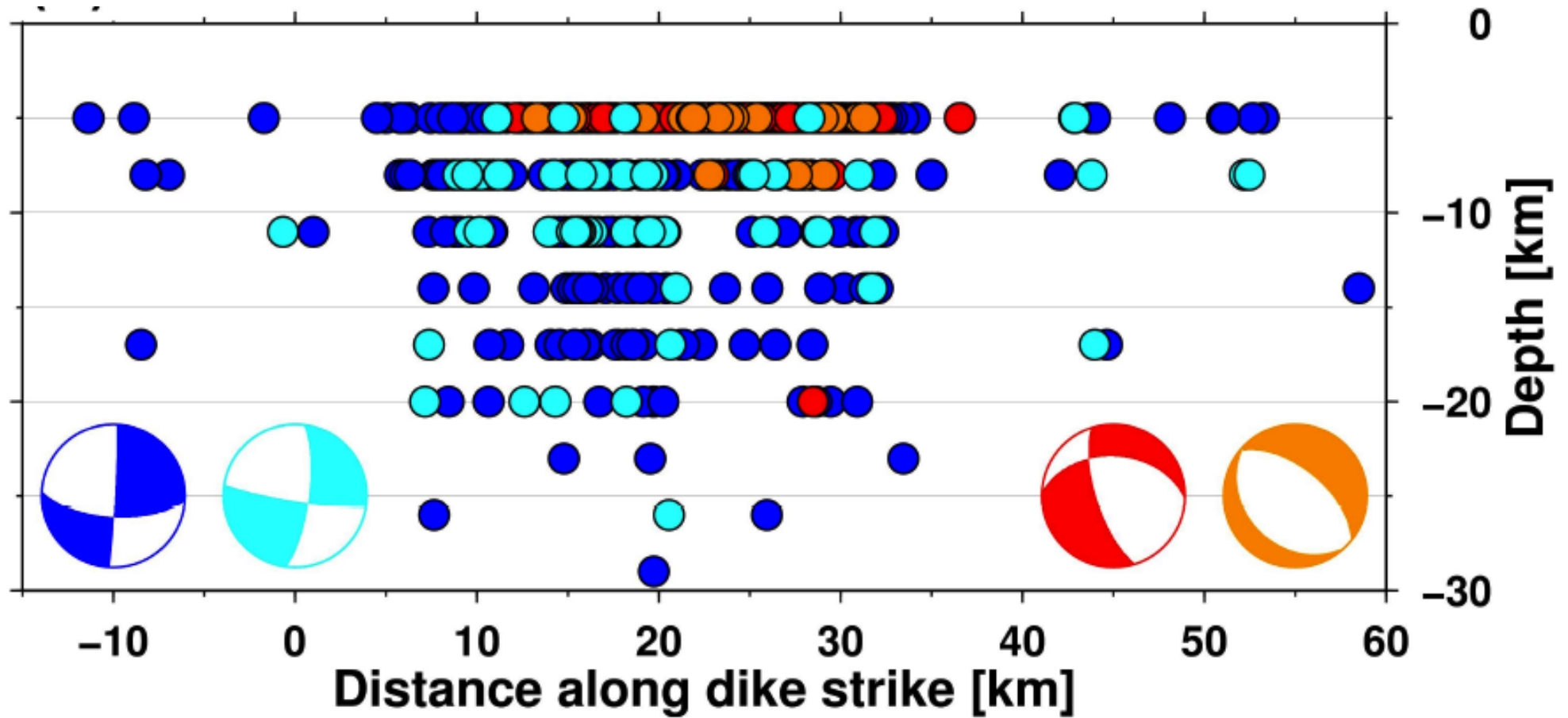
Cross-section:
surface

A diagram illustrating normal faulting. It shows a central fault with two blocks of rock on either side. Red ellipsoids represent stress axes: a large vertical one for σ_1 and a smaller horizontal one for σ_3 . Black circles with shaded quadrants represent focal mechanism solutions, showing slip along the fault. A cross-section labeled 'surface' shows the fault dipping downwards from the surface.

Focal mechanisms: co-diking

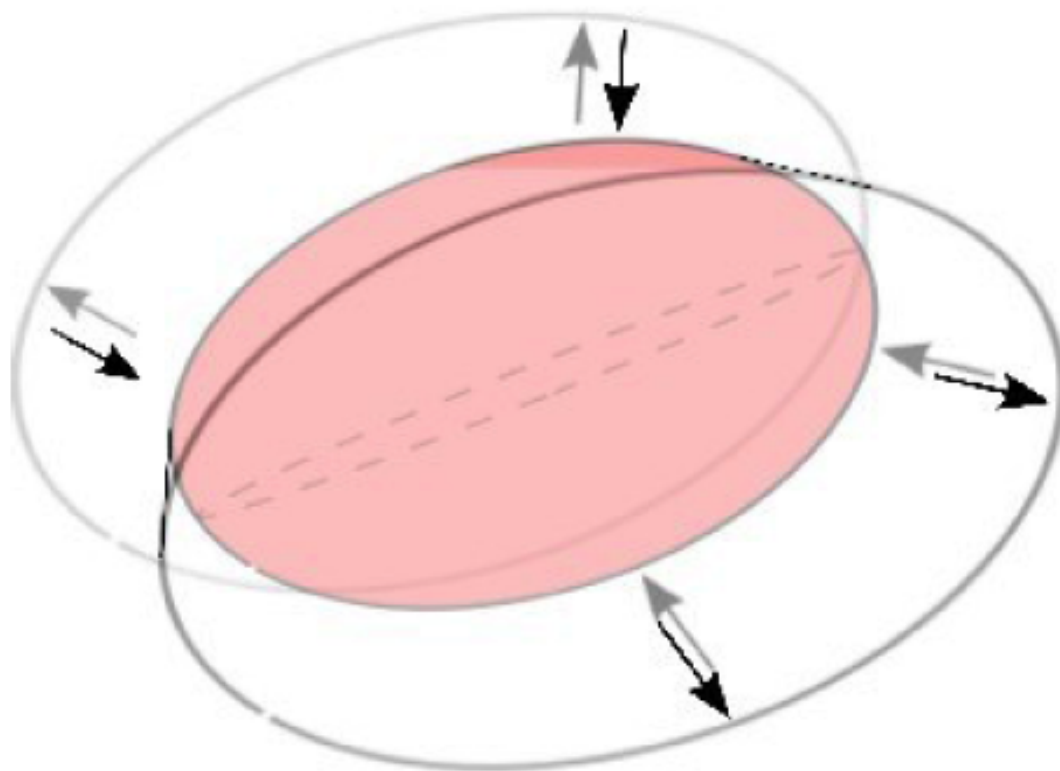


Focal mechanisms: depth

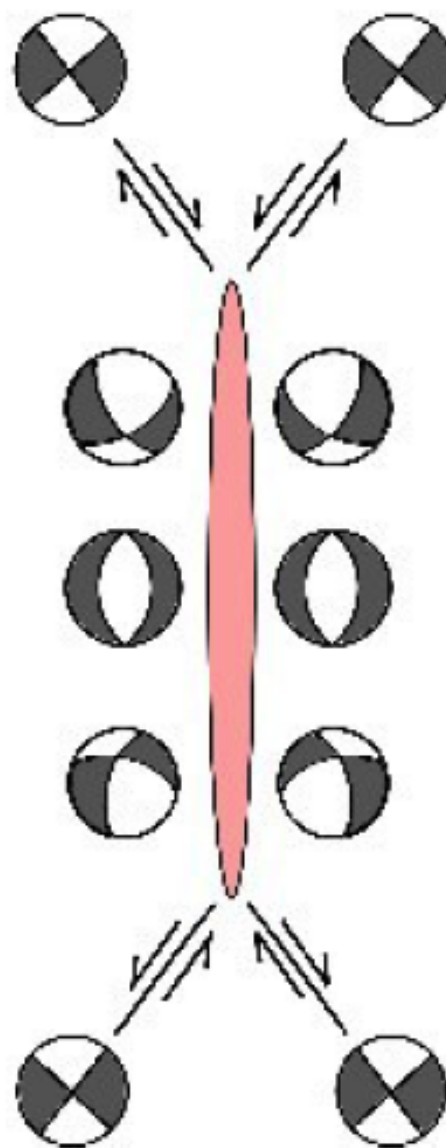


Focal mechanisms: depth

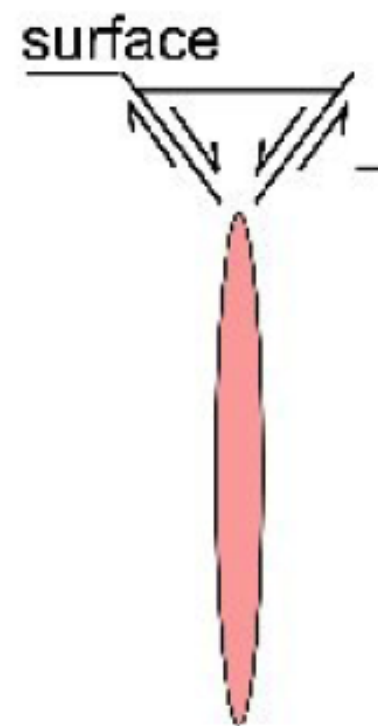
a) perspective



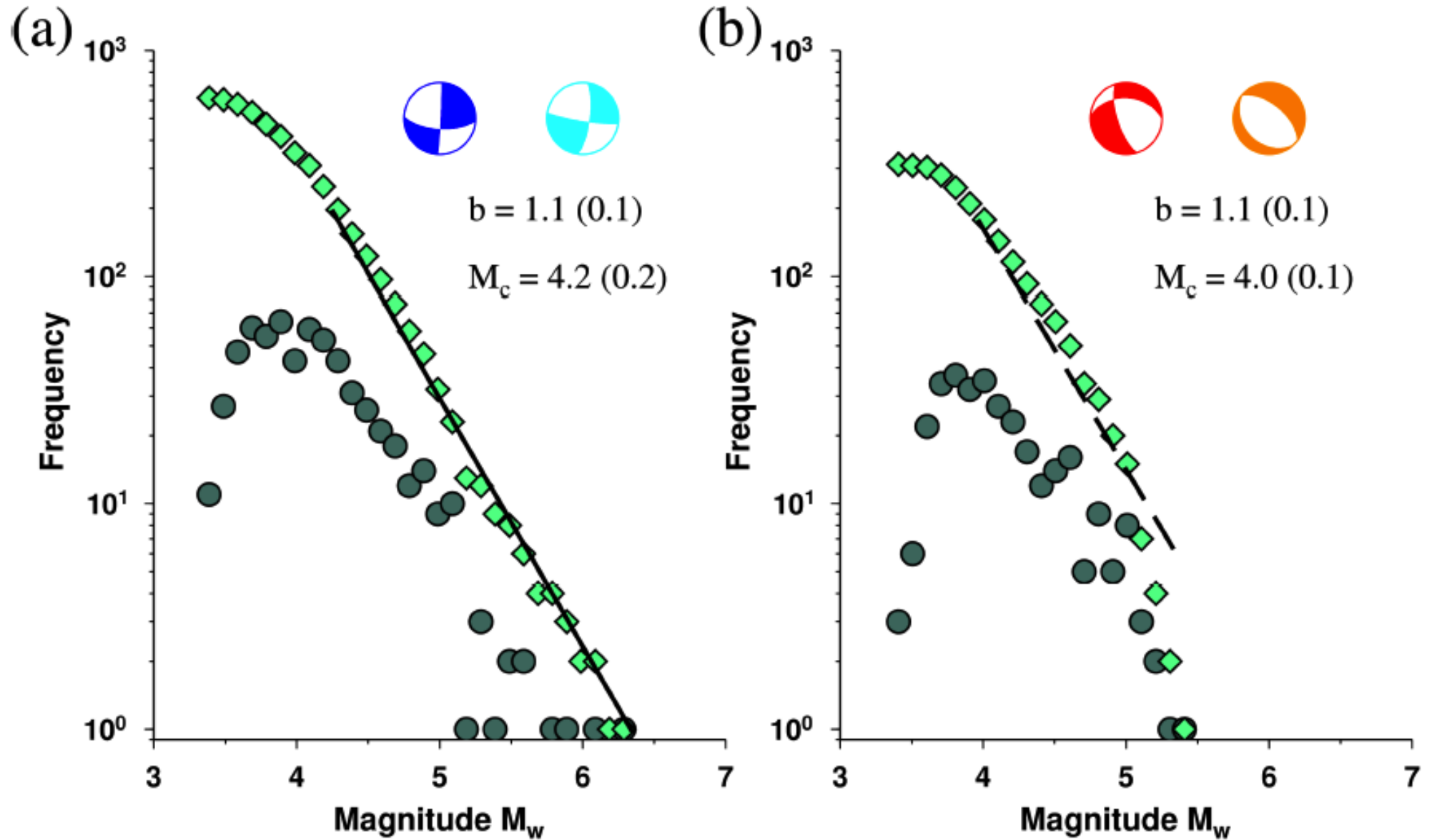
b) top view



c) front view



Focal mechanisms: statistics



Focal mechanisms: statistics

Seismic b -values in volcanic areas have large variability.

Influenced by:

State of stress:

- Stress (Scholz, 1968, Schorlemmer, 2005),
- Thermal stresses
- Pore pressure (Wyss, 1973)

Material heterogeneities:

- Fracture density (Mogi, 1962)
- Material rheology (Amitrano, 2003, Bean et al., 2013)
- Limited thickness of competent rock layers (Becker et al., 2012)

Analog model

