|   | Laser coupling in capillary tubes with dielectric walls |  |
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# Betatron Radiation in Capillaries for Plasma Acceleration Experiments

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# Summary



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- 2 Electron acceleration in capillaries
  - Wakefield modes in capillaries
  - Betatron Radiation from capillaries
- Laser coupling in capillary tubes with dielectric walls
   Instrumentation and Setup
  - Measurements

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| Bet | atron Radiation | Laser coupling in capillary tubes with dielectric walls |  |
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Quasi-linear wakefield regime

### Betatron Radiation Spectra: X-rays

 $I_0 \sim \times 10^{18} \, W/cm^2, \ \gamma_{max} \sim 1000, \ n_e = 5 \times 10^{17}/cm^3$ 

Acceleration length  $\sim$  5 cm



Spatial distribution of the radiation



Divergence  $\theta_{\beta} \sim \sigma k_{\beta} \sim 3 mrad$ 

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Wakefield modes in capillaries

# Electromagnetic hybrid modes/1



Alessandro Curcio Betatron Radiation in Capillaries Electric field component of the m<sup>th</sup> mode:  $E_{1m} = J_0 (u_m \frac{r}{R_{cap}}) e^{-k_m^{l}z} \cos[\omega_0 t - k_{zm}z]$ Longitudinal wave number of the m<sup>th</sup> mode:  $k_{zm} = \sqrt{k_0^2 - \frac{u_m^2}{R_{cap}^2}}$ Damping coefficient of the m<sup>th</sup> mode:  $k_m^{l} = \frac{u_m^2}{2k_{zm}^2 R_{cap}^3} \frac{1+\varepsilon_r}{\sqrt{\varepsilon_r-1}}$ Group velocity of the m<sup>th</sup> mode:  $v_{g,m} = c\sqrt{1 - (\frac{u_m}{R_{cap}k_0})^2}$ Table lettric field inside the capillance

Total electric field inside the capillary:  $E_L = \sum_m A_m E_{1m}$ 

Expansion coefficient for the m<sup>th</sup> mode of the total electric field:

$$A_m = 2 \frac{\int_0^1 x E_L(x) J_0(u_m x) dx}{J_1^2(u_m)}$$

Wakefield modes in capillaries

# Electromagnetic hybrid modes/2





Laser electric field in the focus of a flat top laser profile:

$$E_L = E_{L0} \frac{J_1(\frac{\nu_3 r}{r_0})}{r}$$

Third zero of the Bessel  $J_1$ :  $\nu_3 = 10.174$ 

Coupling efficiency for the m<sup>th</sup> mode:  $C_m = \frac{4}{J_1^2(u_m)} |\int_0^1 J_1(\frac{\nu_3 R_{capx}}{r_0}) J_0(u_m x) dx|^2$ 

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| Wakefield modes in c | apillaries                           |   |  |

### For a matched flat top profile and linearly polarized laser pulse

Normalized laser vector potential:

 $a = \frac{0.91a_0}{\sqrt{2}} e^{-\zeta^2/2\sigma_L^2} J_0(u_0 \frac{r}{R_{cap}})$ 

The optimal coupling efficiency is obtained when:  $R_{cap}/r_0 \sim 0.35$ 

From the Poisson equation, the continuity equation, and the fluid momentum equation, in the linear ( $a_0 < 1$ ) 3D regime, the scalar wakefield potential comes to be:

$$\Phi(r,\zeta) = -\frac{mc^2 k_p}{2} \int_{\zeta}^{\infty} d\zeta' \sin[k_p(\zeta-\zeta')] a^2(r,\zeta')$$

The corresponding longitudinal wakefield is:

$$E_{z} \sim 0.83 E_{0} \frac{\sqrt{\pi}}{4} a_{0}^{2} \sigma_{L} k_{p} J_{0} (u_{1} \frac{r}{R_{cap}}) e^{-k_{p}^{2} \sigma_{L}^{2}/4} \cos[k_{p} \zeta]$$

The corresponding transverse wakefield is:

$$E_r \sim -0.83 \frac{u_1}{R_{cap}} J_1(u_1 \frac{r}{R_{cap}}) E_0 \sqrt{\pi} a_0^2 \sigma_L e^{-k_p^2 \sigma_L^2/4} \sin[k_p \zeta]$$

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Laser propagation equation in a plasma medium inside a capillary  $(a_0 < 1)$ :

$$\left(\frac{1}{r^2}\frac{\partial}{\partial r}r^2\frac{\partial}{\partial r}+\frac{\partial^2}{\partial z^2}-\frac{1}{c^2}\frac{\partial^2}{\partial t^2}\right)\overrightarrow{A}\sim k_p^2\frac{n_e}{\gamma n_0}\overrightarrow{A}$$

By the assumption  $\overrightarrow{A} \propto e^{i(kz-\omega t)}$  (neglecting focusing effects):

$$\left(\frac{\partial^2}{\partial r^2} + \frac{1}{r}\frac{\partial}{\partial r} - \left(\frac{u_m}{R_{cap}}\right)^2\right)\overrightarrow{A(r)} = k_p^2 \frac{n_e(r)}{\gamma n_0} \overrightarrow{A(r)}$$

 $\frac{u_m}{R_{cap}} \equiv k_{\perp m} \ u_m = m^{th}$  zero of the Bessel  $J_0$ , the solution of the Schroedinger homogeneous equation

Definition of plasma operator:  $\hat{P} \equiv \frac{n_e}{\gamma n_0}$ 

First order correction to the transverse wavenumber for the m<sup>th</sup> mode:

$$k_{\perp m}^{2'} \sim k_{\perp m}^2 + k_p^2 < EH_{1m} |\widehat{P}| EH_{1m} >, \ k_p = {
m plasma}$$
 wavenumber

Approximated expression of potential vector inside a capillary in a plasma medium:

$$|\overrightarrow{A}\rangle = |\overrightarrow{EH_{11}}\rangle + \frac{k_{p}^{2}}{k_{\perp 1}^{2} - k_{\perp 2}^{2}} < \overrightarrow{EH_{12}} |\widehat{P}|\overrightarrow{EH_{11}}\rangle |\overrightarrow{EH_{12}}\rangle$$

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Developing the normalized vector potential in the capillary modes:

 $a^2 = (\sum_m \overrightarrow{a_m})^2$ 

### We have for the first order wakefield:

$$\Phi(r,\zeta) = -\frac{mc^2k_p}{2} \int_{\zeta}^{\infty} d\zeta' \sin[k_p(\zeta-\zeta')] a^2(r,\zeta') \sim$$
  
$$\sim -\frac{mc^2k_p}{2} \int_{\zeta}^{\infty} d\zeta' \sin[k_p(\zeta-\zeta')] (a_1^2 + a_1a_2)(r,\zeta') \sim$$
  
$$\sim \Phi_1 + \Phi_{12}$$

For a perfectly matched flat top laser profile  $\Phi_{12} \sim 0.1 \ \Phi_1$ 

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The coupling term  $\Phi_{12}$  is an oscillating beating term with wavenumber  $\Delta k_{z2} = k_{z1} - k_{z2}$ , corresponding for most of the real cases to wavelengths of the order of millimeters up to few centimeters. Therefore both the longitudinal and radial wakefields manifest long-range oscillations beside their natural one (that at the plasma wavelength).

Example:

 $R_{cap} \sim 100 \mu m$  $\lambda_0 = 0.8 \mu m$  $\Delta k_{c2} = 628.7 \ m^{-1}$ 

Corresponding to a beating wavelength of  $1 \mbox{\it mm}$ 

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Betatron Radiation from capillaries

### Spectrum modification in case of coupling



 $E_n$  is the irradiated energy. The Matched Coupling corresponds to  $R_{cap}/r_0 \sim 0.35$  while the Not Matched Coupling corresponds to  $R_{cap}/r_0 \sim 0.6$ . The net effect of the coupling can be viewed as a red shift of the critical energy. The decrease of the critical energy in case of coupling is basically due to the decrease of the laser group velocity, namely of the plasma wave phase velocity. In this calculation the coupling with higher modes has been neglected considering a beating wavelength much shorter than the capillary length.

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Instrumentation and Setup

## Hexapod PI

|  | - 20                                    | 19                                      | Unit   | Tolerance |
|--|---|---|--------|-----------|
|  | for higher resolution<br>and load       | for higher velocity                     |        |           |
| Active axes  | $X, Y, Z, \theta_X, \theta_Y, \theta_Z$ | $X, Y, Z, \theta_X, \theta_Y, \theta_Z$ |        |           |
| Motion and positioning   |   |   |        |           |
| Travel range* X, Y   | ±22.5                                   | ±22.5                                   | mm     |           |
| Travel range* Z  | ±12.5                                   | ±12.5                                   | mm     |           |
| Travel range* 0 <sub>X</sub> , 0 <sub>Y</sub>                                | ±7.5                                    | ±7.5                                    | •      |           |
| Travel range* 0 <sub>Z</sub>   | ±12.5                                   | ±12.5                                   |        |           |
| Single- actuator design resolution   | 0.007                                   | 0.5                                     | μm     |           |
| Min. incremental motion X, Y, Z  | 0.3                                     | 1                                       | μm     | typ.      |
| Min. incremental motion $\theta_{\chi}, \theta_{\gamma}, \theta_{\chi}$      | 3.5                                     | 12                                      | µrad   | typ.      |
| Backlash X, Y  | 3                                       | 1                                       | μm     | typ.      |
| Backlash Z   | 1                                       | 1                                       | μm     | typ.      |
| Backlash 6 <sub>x</sub> , 6 <sub>y</sub>                                     | 20                                      | 15                                      | µrad   | typ.      |
| Backlash 8 <sub>2</sub>  | 25                                      | 25                                      | µrad   | typ.      |
| Repeatability X, Y   | ±0.5                                    | ±0.5                                    | μm     | typ.      |
| Repeatability Z  | ±0.1                                    | ±0.1                                    | μm     | typ.      |
| Repeatability 0 <sub>x</sub> , 0 <sub>y</sub>                                | ±2                                      | ±2                                      | µrad   | typ.      |
| Repeatability 02   | ±2.5                                    | ±2.5                                    | µrad   | typ.      |
| Max. velocity X, Y, Z  | 1                                       | 25                                      | e Vmm  |           |
| Max. velocity θ <sub>x</sub> , θ <sub>y</sub> , θ <sub>z</sub>               | 11                                      | 270                                     | mrad/s |           |
| Typ. velocity X, Y, Z  | 0.5                                     | 10                                      | e Vmm  |           |
| Typ. velocity $\theta_x, \theta_y, \theta_z$                                 | 5.5                                     | 55                                      | mrad/s |           |
| Mechanical properties  |   |   |        |           |
| Stiffness X, Y   | 1.7                                     | 1.7                                     | N/ µm  |           |
| Stiffness Z  | 7                                       | 7                                       | N/ µm  |           |
| Load (base plate horizontal /<br>any orientation)                            | 10/5                                    | 5/2.5                                   | kg     | max.      |
| Holding force, de- energized<br>(base plate horizontal /<br>any orientation) | 100 / 50                                | 15/5                                    | N      | max.      |
| Motor type   | DC gear motor                           | DC motor                                |        |           |
| Miscellaneous  |   |   |        |           |
| Operating temperature range  | -10 to 50                               | -10 to 50                               | °C     |           |
| Material   | Aluminum                                | Aluminum                                |        |           |
| Mass   | 8                                       | 8                                       | kg     | ±5%       |
| Cable length   | 3                                       | 3                                       | m      | ±10 mm    |

Hexapod



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### **Experimental Setup**



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#### Measurements

### Laser Focus at the Entrance



 $w_0 = 26.15 \mu m$ 

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| Managements |   |  |

#### Measurements

### Laser Focus at the Exit

- $\star$  Laser Power :  $\sim$  35  $\pm$  1 mW
- $\star$  Focus diameter : ~ (55.6  $\pm$  7)  $\mu m$
- $\star$  Magnification :  $\sim 1.5$



Fitting Curve:  $a + be^{-(r-c)^2/w_0^2}$  a = 2.85 b = 28.86  $c = 113.54 \mu m$  $w_0 = 27.80 \mu m$ 

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| Measurements |        |   |  |
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## Laser-offset Test

The offset dR is considered in the transverse plane with respect to the laser-capillary axis



Best Coupling



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| Measurements |   |  |

### Laser-misalignment Test

The misalignment  $d\theta$  is considered in the propagation plane with respect to the laser-capillary axis



Best Coupling



 $d\theta = 3.5 mrad$ 







 $d\theta = 8.7 mrad$ 



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### Conclusions e perspectives

\*The propagation of an ultra-short laser in a capillary waveguide has been considered from the point of view of the multimode wakefield structure and the modification in betatron radiation spectra.

 $\star$  We would like to test these methods during the forthcoming experiments of plasma acceleration at LNF.

★ We have tested the coupling of the laser inside a capillary with the help of the Hexapod PI. The coupling with the *EH*11 mode is significantly maintained for an offset of about 30  $\mu m$  and a misalignment of about 5 *mrad*.

|   | Laser coupling in capillary tubes with dielectric walls | Conclusions |
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