



Giroscopi Laser

Applicazione alla metrologia angolare

Nicolò Beverini



RLG project



***Ring Laser Gyroscope for accurate angle metrology
and as demonstrator of self-calibration principle for
Lense-Thirring effect measurements***

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The goal



- **Realization of a mid-scale RL (50 - 90 cm), with a lightweight and stiff structure which can be placed on a precision rotating table -in combination with a precision autocollimator**
- 1) Implementation of an extremely accurate transportable rotational standard for the calibrating the best angular measurement instrument, which resolution today is well beyond the traceability capabilities of most NMIs;
- 2) Realization of a very sensitive gyroscope for the measurement of seismic effects (S-wave phase velocity, Co-seismic rotations), and for the measurements of test mass acceleration in the next generation Earth based gravitational antennas (e.g. Virgo)
- 3) The demonstration of a self-calibration concept leading to the design of a larger rotating RL for geodetic and relativistic experiments, free from the need of extremely difficult dimensional measurements

Filatov's goniometer



Quantum Electronics **30**(2) 141–146 (2000)

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DOI: 10.1070/QE2000v030n02ABEH001675

Development of new methods and means of dynamic laser goniometry

M N Burnashev, D P Luk'yanov, P A Pavlov, Yu V Filatov

Gyrolaser goniometer

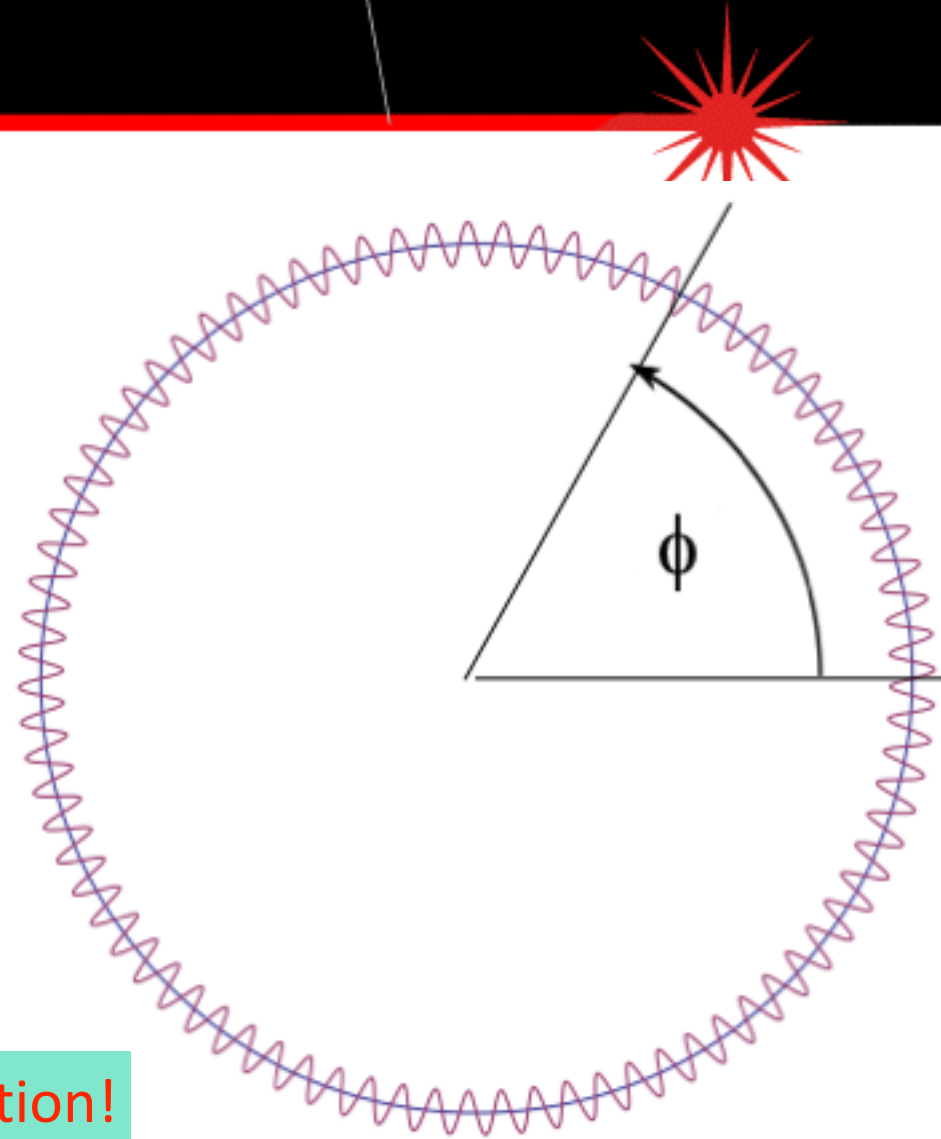
$$f(t) = 4 \frac{A}{\lambda p} \Omega(t) \cos \theta = K \Omega(t)$$

$$N_\phi = \frac{1}{2\pi} \int_{t_0}^{t_1} f(t) dt = \frac{K}{2\pi} \int_{t_0}^{t_1} \Omega(t) dt = \frac{K}{2\pi} \phi$$

$$N_{2\pi} = \frac{1}{2\pi} \int_{t_0}^{t_0+T} f(t) dt = \frac{K}{2\pi} \int_{t_0}^{t_0+T} \Omega(t) dt = K$$

$$\phi = 2\pi \frac{N_\phi}{N_{2\pi}}$$

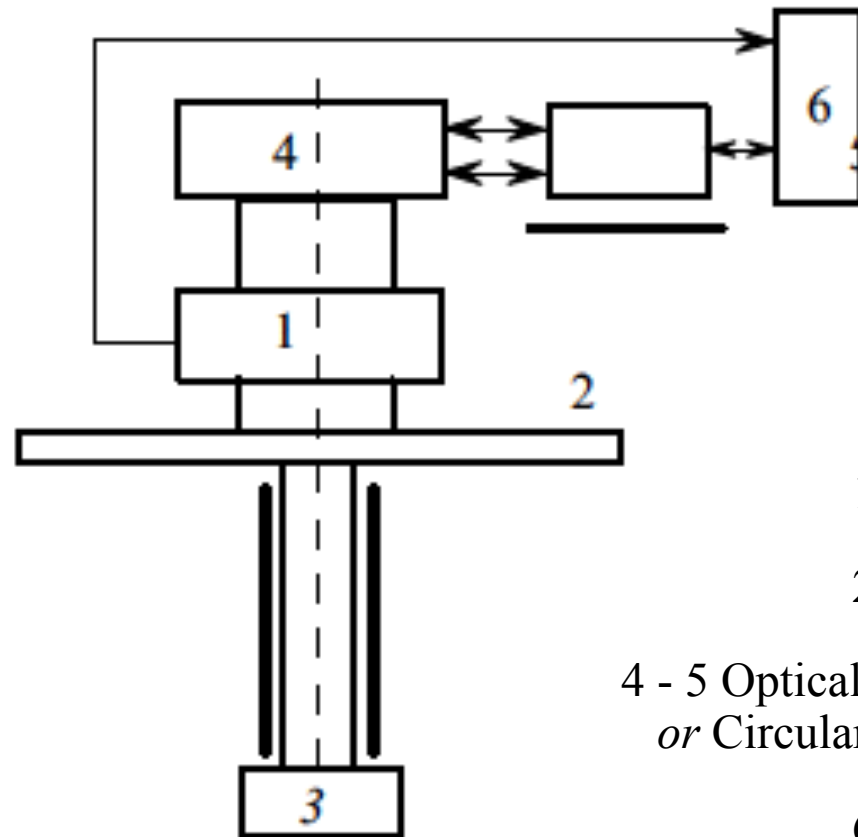
Self-calibration!



If K could be considered as a constant, the angle should be known with a precision limited only by the noise of the detector



Goniometro laser



1 - Ring Laser

2 - Rotatory table

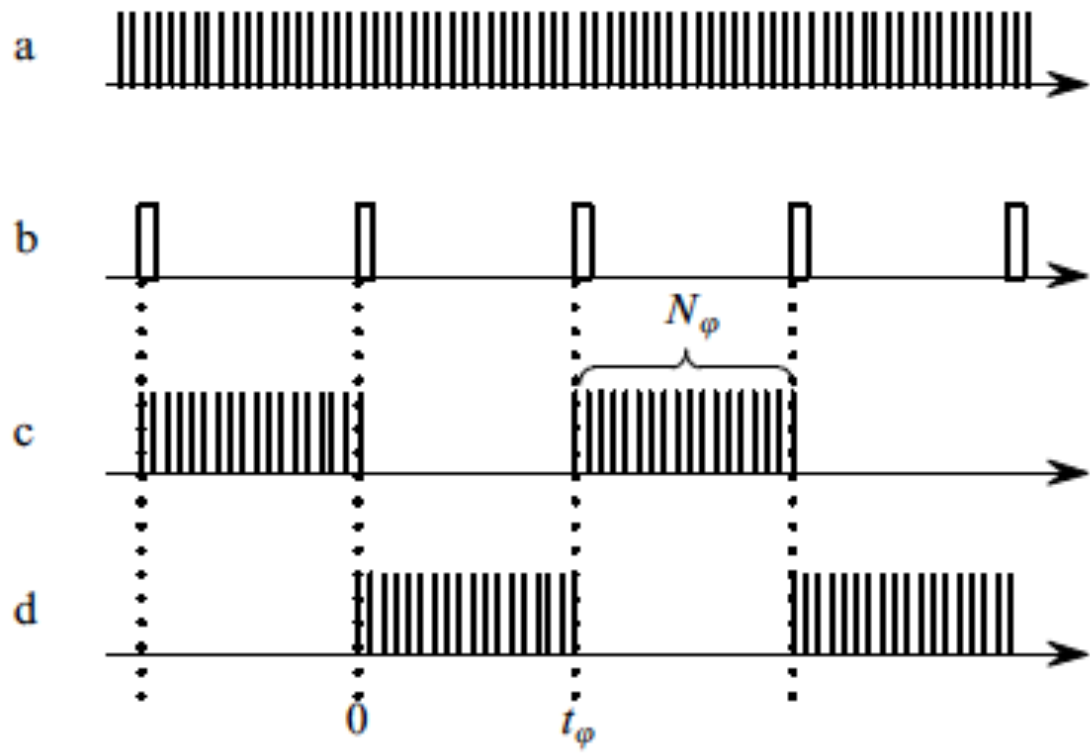
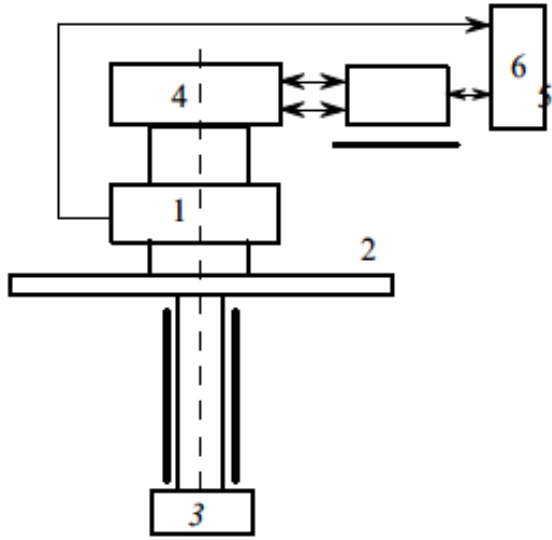
4 - 5 Optical polygon + autocollimator
or Circular encoder disc + reading head

6 - Counter

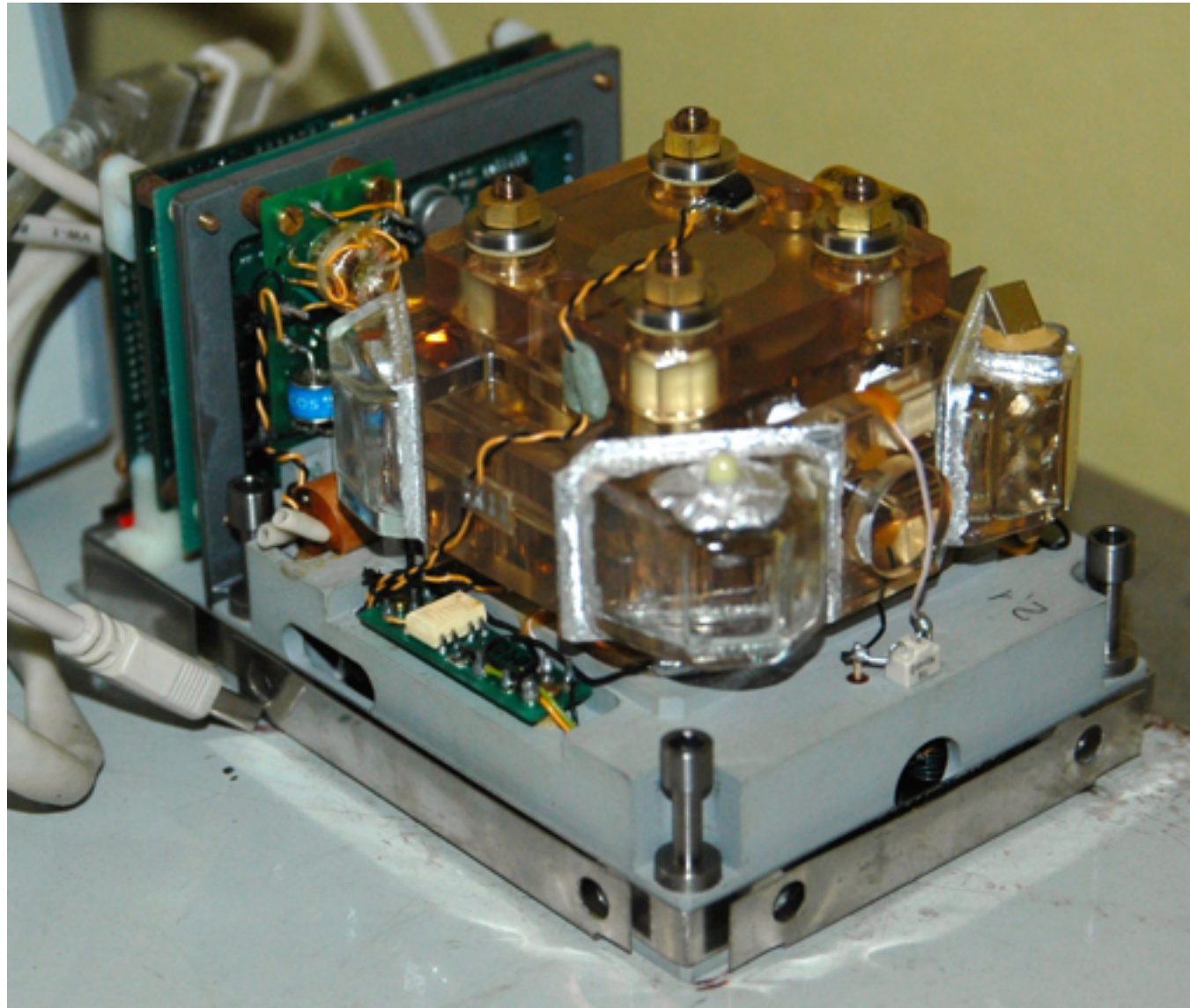
Filatov's goniometer



Goniometro laser



Gyrolaser a prismi



He-Ne Laser gyros



- **Small gyroscopes for navigation**
 - 3- or 4-mirror ring cavity design, with an optical path of the order of 10 – 40 cm
 - Large FSR (comparable with Doppler width)
 - ⇒ *robust transversal single-mode operation*
 - They need of a bias rotation or a dithering to avoid self-locking
- **Large apparatus integral to the ground**
 - Optical path larger than 4 m up to 100 m and more
 - Biased by Earth rotation
 - Small FSR ⇒ *difficult single-mode operation*
 - Seismology, geodesy, length of the day, fundamental physics

Ring laser accuracy



$$f_{Sagnac} = 4 \frac{A}{\lambda p} (1 + k_A) \hat{n} \cdot (\vec{\Omega} + \vec{\Omega}_{\oplus}) + \Delta f_0 + \Delta f_{bs}$$

$$= k_s (1 + k_A) (\Omega \cos \theta + \Omega_{\oplus} \sin \gamma) + \Delta f_0 + \Delta f_{bs}$$

geometrical factor

atomic factor

Earth rotation

(non-reciprocal factor)

zero shift

backscattering

$$N_{\phi} = \frac{1}{2\pi} \int_{t_0}^{t_1} f(t) dt = \frac{1}{2\pi} K \bar{\Omega} + \delta_{\phi}$$

$$N_{2\pi} = \frac{1}{2\pi} \int_{t_0}^{t_0+T} f(t) dt = \frac{1}{2\pi} K \bar{\Omega} + \delta_{2\pi}$$

Linear term: Geometrical factor



$$f = k_s (1 + k_A) (\Omega + \Omega_{\oplus} \sin \gamma) + \Delta f_0 + \Delta f_{bs}$$

- The geometrical factor $A/p \cos \vartheta$ must be kept stable better than 10^{-8} over the measuring time.
 - ⇒ *Linear change smaller than 10^{-8}*
 - For a dilation coefficient of the structure $\approx 10^{-6}/\text{K}$, a temperature stability of 10^{-2} K is required
 - ⇒ *Wobble of the table lower than 10^{-4}*

Linear term: Atomic factor



$$f = k_s (1 + k_A) (\Omega + \Omega_{\oplus} \sin \gamma) + \Delta f_0 + \Delta f_{bs}$$

- The laser action is sensitive to changes of the discharge properties that can produce variation in the laser gain and in the plasma dispersion function.
 - Evolution of the discharge gas composition
 - Stability of the discharge power
- ⇒ Control of the lab temperature, pressure, humidity
- ⇒ Good stabilization of the discharge power and of the laser wavelength
- ⇒ Control of wall outgassing through getter pumps
- ⇒ *Can be quite easily controlled on measurement time $\lesssim 100$ s*

Null-shift



$$f = k_s (1 + k_A) (\Omega + \Omega_{\oplus} \sin \gamma) + \Delta f_0 + \Delta f_{bs}$$

Non-reciprocity in the optical cavity

- *rf* discharge makes negligible asymmetries in the active medium.
- For an ideal ring laser the two counter-propagating laser beams would be identical both in size and in intensity.
- In practice, there have been found quite large differences in the intensities
- Large effect in total reflective prism cavities (*magnetic field effects due to the Verdet coefficient of the prism glass*)
- Also super-mirror cavities exhibit some minute effects (anisotropy in the reflection or birefringence in the super-mirror coating)

Null-shift measured in G-Pisa (1.35 m of side): 10^{-2} Hz

- ⇒ *This null-shift effect can be modeled and taken in account.*
- ⇒ *Diagnostic: relative intensity of the two beams*

Back-scattering



$$f = k_s (1 + k_A) (\Omega + \Omega_{\oplus} \sin \gamma) + \Delta f_0 + \Delta f_{bs}$$

Mirror backscattering couples together the two counter-propagating laser beams through a coupling parameter r : $r = \sum_i r_i \exp(2ikz)$

⇒ *frequency pulling*: $f = \sqrt{f_0^2 - l^2}$ for $f_0 > l$
 $l = r/\pi$ lock-in threshold frequency.

- By geometry $|r_i| \propto 1/L$
- Moreover, its effectiveness is directly related to the ratio between cavity line-width ($\propto 1/L$) and inversely related to the beams frequency difference ($\propto L$).

r value can vary between $-\sum_i |r_i|$ and $\sum_i |r_i|$ for small perturbations in the ring geometry of the order of λ

If $\Omega \gg \Omega_L$ ($f_0 \gg l$),

$$\Rightarrow f = \sqrt{f_0^2 - l^2} \approx f_0 (1 - l^2/f_0^2) = f_0 - \frac{l^2}{K\Omega}$$

$$l \approx \frac{cs\lambda}{\pi dp} \approx \frac{100}{p} \text{ Hz}$$

Accuracy



$$f = K_1 \Omega + K_0 + \frac{K_{-1}}{\Omega}$$

Primalov and Filatov, Sov. J. QE 7 802 (1977)
Yu.Filatov, *et al.* NATO RTO AG-339 (1999)

K_1 scale factor

K_0 null-shift

K_{-1} back scattering

For $p = 2$ m e $\Omega = 2\pi \cdot 0.1$ Hz:

$$K_1 = 4 \frac{A}{\lambda p} \cos \theta \approx \frac{L}{\lambda} \approx 8 \times 10^5$$

$$f^0 \approx 350 \text{ kHz}$$

$$K_{-1} \approx \frac{l^2}{K_1^0} \approx \frac{(100 \text{ Hz}/2)^2}{8 \times 10^5} = 3 \times 10^{-3} \text{ Hz}^2$$

$$\delta f_{bs} \approx \frac{3 \times 10^{-3}}{2\pi \cdot 10^{-1}} \text{ Hz} \approx 5 \times 10^{-3} \text{ Hz}$$

$$\frac{\delta f_{bs}}{f_0} \sim \frac{5 \times 10^{-3}}{350 \times 10^3} \approx 1.5 \times 10^{-8}$$

Earth rotation effect



$$f = K_1 (\Omega + \Omega_{\oplus} \sin \gamma) + K_0 + \frac{K_{-1}}{(\Omega + \Omega_{\oplus} \sin \gamma)}$$

Correction in K_{-1} is a small correction of a small term

Negligible!

Ω_{\oplus} is well known with high accuracy, but if Ω is not uniform:

$$\begin{aligned} \delta N_{\phi} &= \frac{1}{2\pi} \left(K_1^0 \frac{(\Omega_{\oplus} \sin \gamma + K_0)}{\Omega^0} + \frac{K_0^0}{\Omega^0} + 2 \frac{K_{-1}^0}{(\Omega^0)^2} \right) \int_t^{t+\Delta t} \delta \Omega(t') dt' \\ &= \frac{1}{2\pi} \left(K_1^0 \frac{\Omega_{\oplus} \sin \gamma}{\Omega^0} + \frac{K_0^0}{\Omega^0} + 2 \frac{K_{-1}^0}{(\Omega^0)^2} \right) \langle \delta \Omega \rangle \frac{\phi}{\Omega^0} \end{aligned}$$

First term is the dominant one:

With $L=50$ cm, $K_1 \Omega_{\oplus} \sin \gamma = 40$ Hz, while $K_0 \ll 1$ Hz

$$\delta \phi = 2\pi \frac{\delta N_{\phi}}{N_{2\pi}} \approx \frac{\Omega_{\oplus} \sin \gamma}{\Omega^0} \frac{\langle \delta \Omega \rangle}{\Omega^0} \phi$$

For $\Omega_0 = 2\pi \cdot 0.1$ Hz, an angular accuracy of 10^{-8} rad (0.002") requires $\langle \delta \Omega \rangle / \Omega < 10^{-4}$

Quantum noise



$$\delta\Omega_{shot\ noise} = \frac{c(4L)}{4L^2 Q} \sqrt{\frac{h\nu}{P\tau}} = \frac{c}{LQ} \sqrt{\frac{h\nu}{P\tau}}$$

P output power
 τ measurement time
 Q optical cavity quality factor

$$\delta\phi_{shot\ noise} = \frac{c}{LQ} \sqrt{\frac{h\nu\tau}{P}} \approx 12\text{ nrad} \\ (0.0025'')$$

$L = 50\text{ cm}$
 $\tau = 5\text{ s}$
 $Q = 6,20 \times 10^{11}$
 (cavity losses $\approx 32\text{ ppm}$)
 $P = 10\text{ nW}$



ABRS Air-Bearing Direct-Drive Rotary Stage

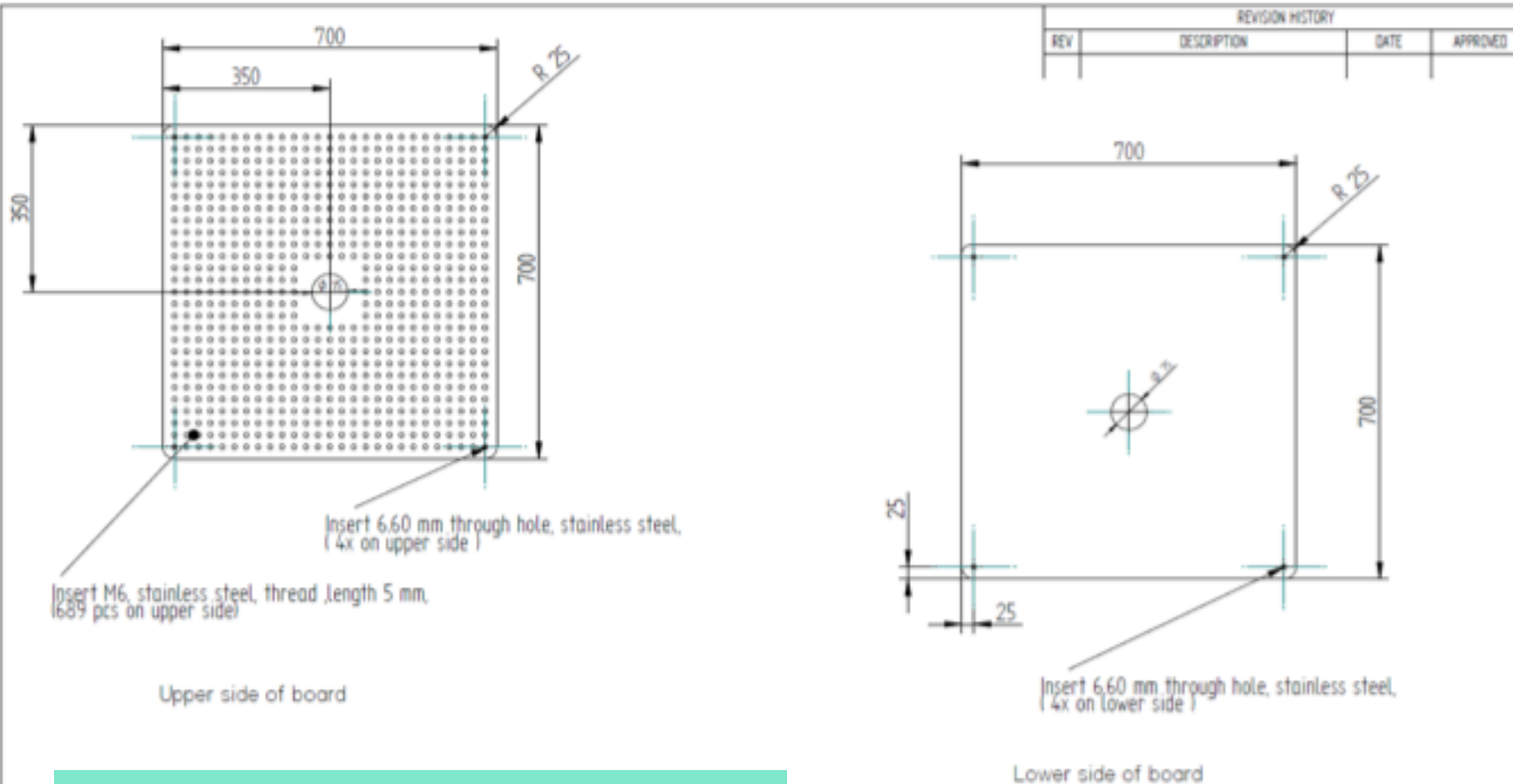




Resolution ⁽¹⁾	0.174 μ rad (0.036 arc sec)	
Fundamental Encoder Resolution	18,000 lines/rev	
Max Speed ⁽²⁾	500 rpm	
Accuracy ⁽³⁾	<1 arc sec	
Bidirectional Repeatability	<1 arc sec	
Max Load ⁽⁴⁾	Axial	97 kg
	Radial	51 kg
	Tilt	45 N-m
Axial Error Motion (Synchronous)	<100 nm	
Radial Error Motion (Synchronous)	<250 nm	
Tilt Error Motion (Synchronous)	<2.4 μ rad (<0.5 arc sec)	
Axial Error Motion (Asynchronous)	<20 nm	
Radial Error Motion (Asynchronous)	<20 nm	
Tilt Error Motion (Asynchronous)	<0.2 μ rad (<0.04 arc sec)	

Width	300 mm
Tabletop Diameter	278.1 mm
Height	110 mm

Basamento in fibra di carbonio

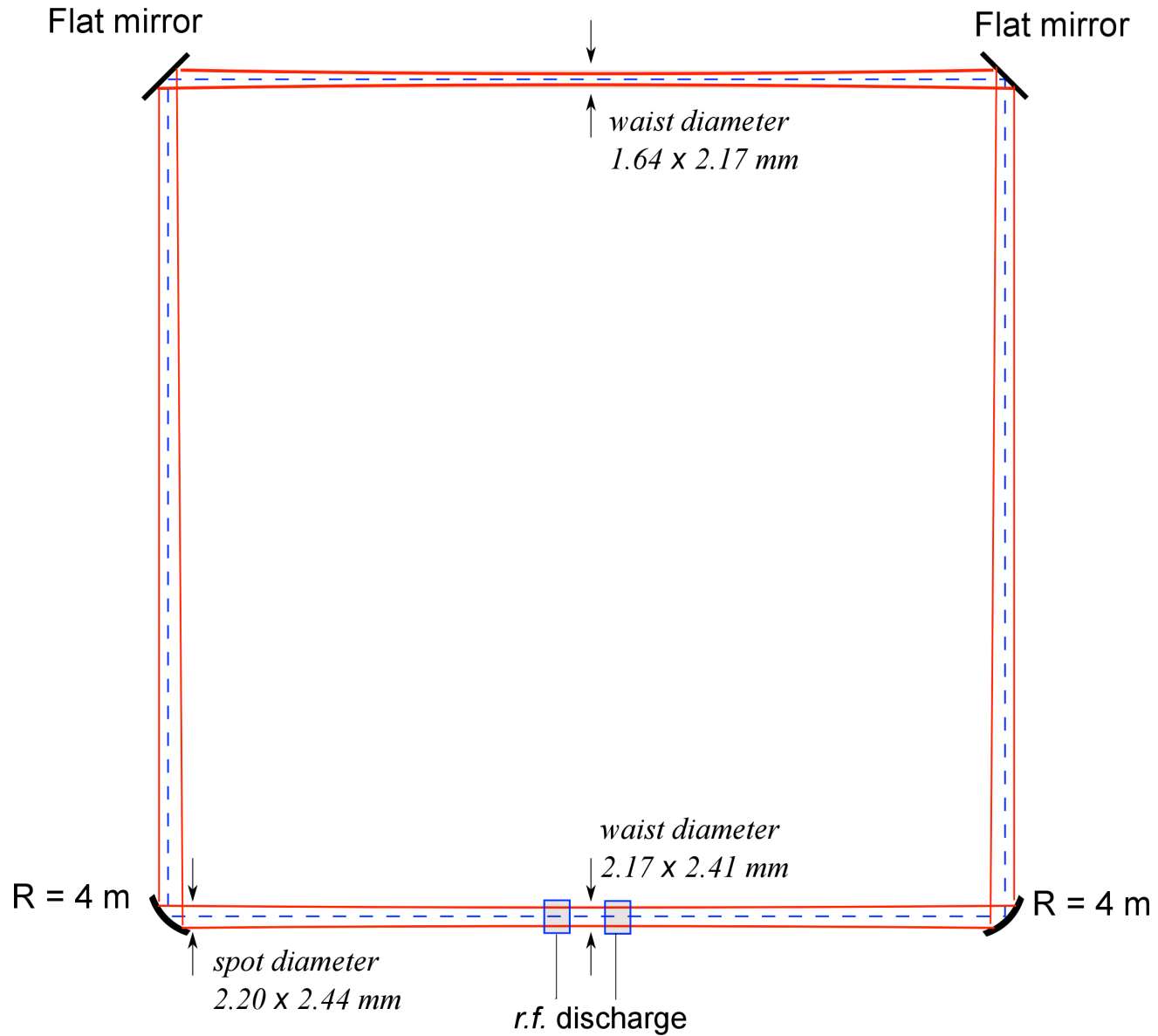


Dimensioni: 700x700x100 mm
 Peso ~12 kg

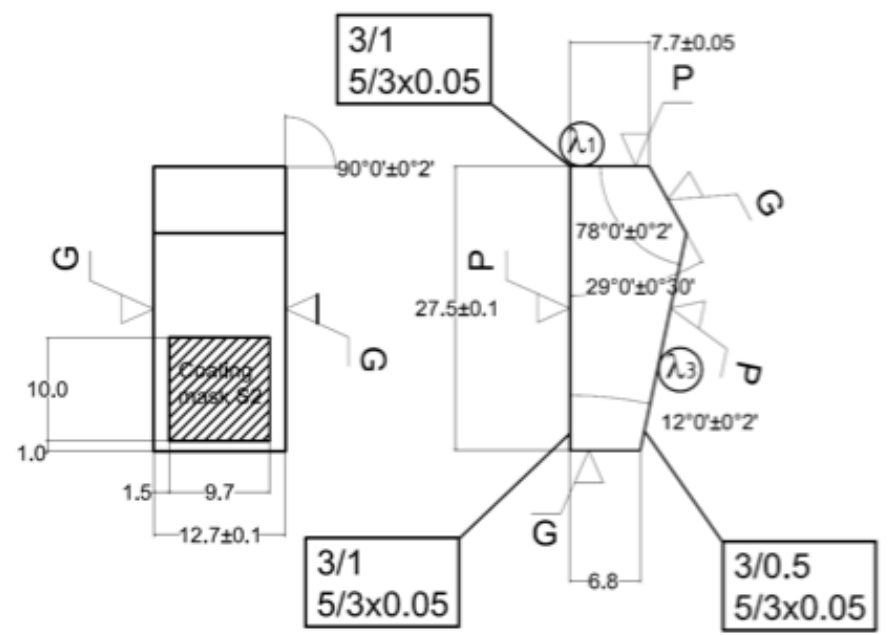
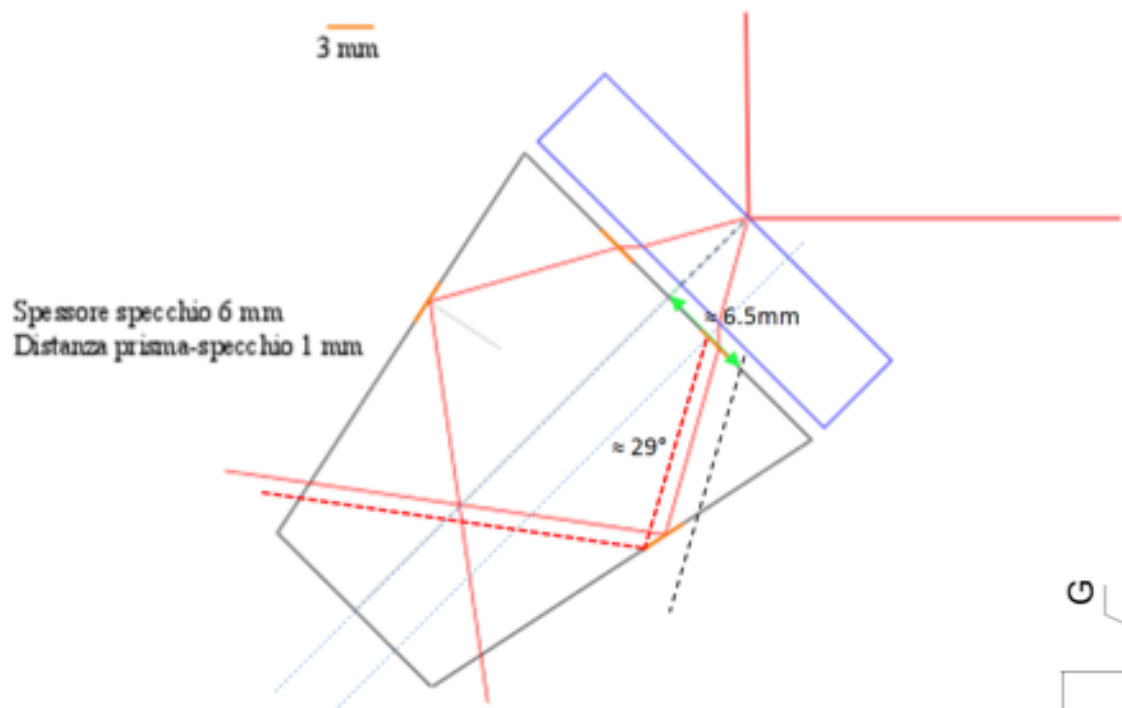
REVISION HISTORY			
REV	DESCRIPTION	DATE	APPROVED

	NAME	DATE	CarbonVision GmbH Carbon Fiber Breadboards TITLE CAI-700x700x100-25-1-SP1418
DRAWN	Schlosser	11/2014	
CHECKED			
ENG APPR			
MGR APPR			SIZE A3 DWG NO 100.176 REV NC FILE NAME: 001%_CAI-700x700x100-25-1-SP1418 UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN MILLIMETERS ANGLES °XX'X 2 PL. XXXX 3 PL. XXXXX SCALE WEIGHT SHEET 1 OF 1

Optical cavity design



Prisma di ricombinazione



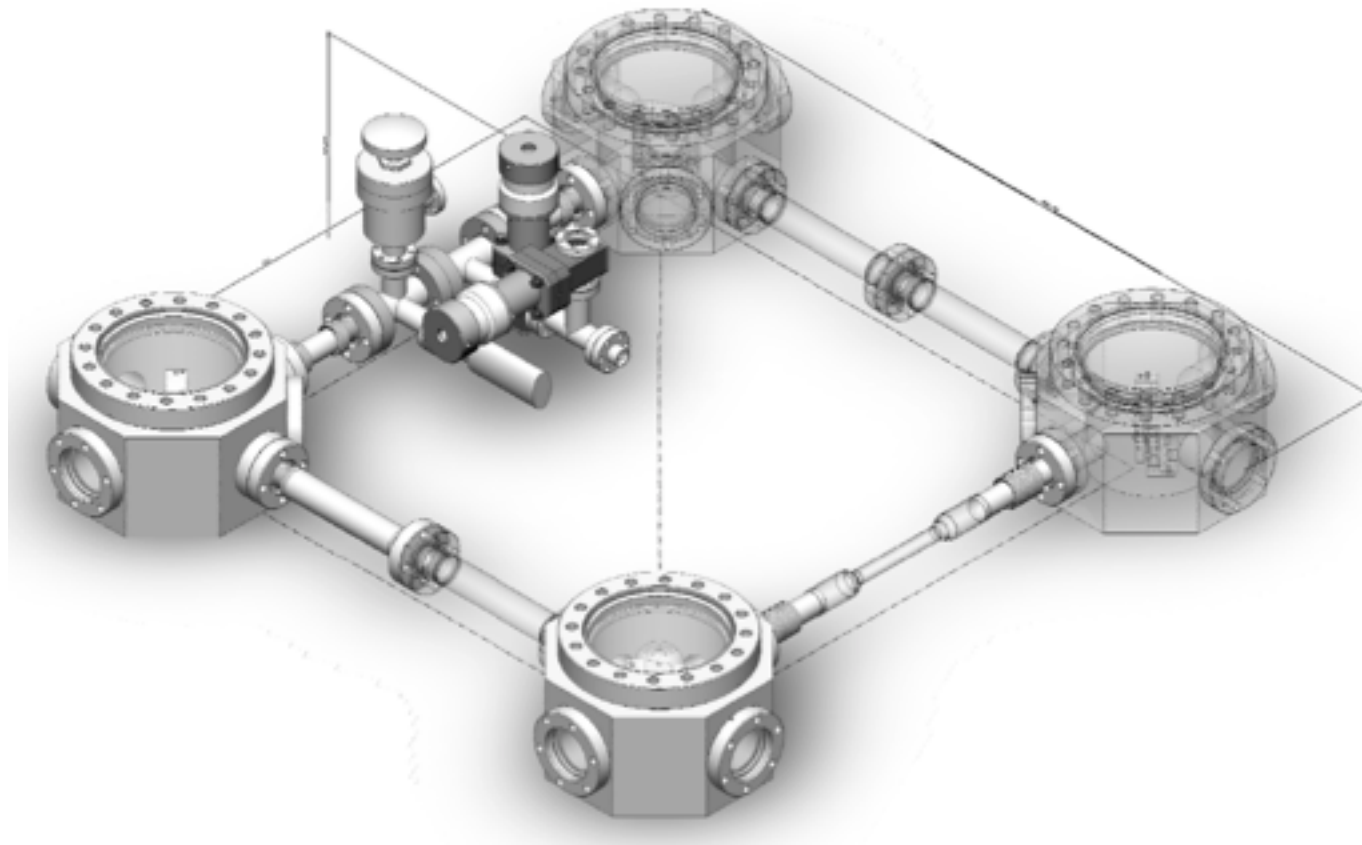


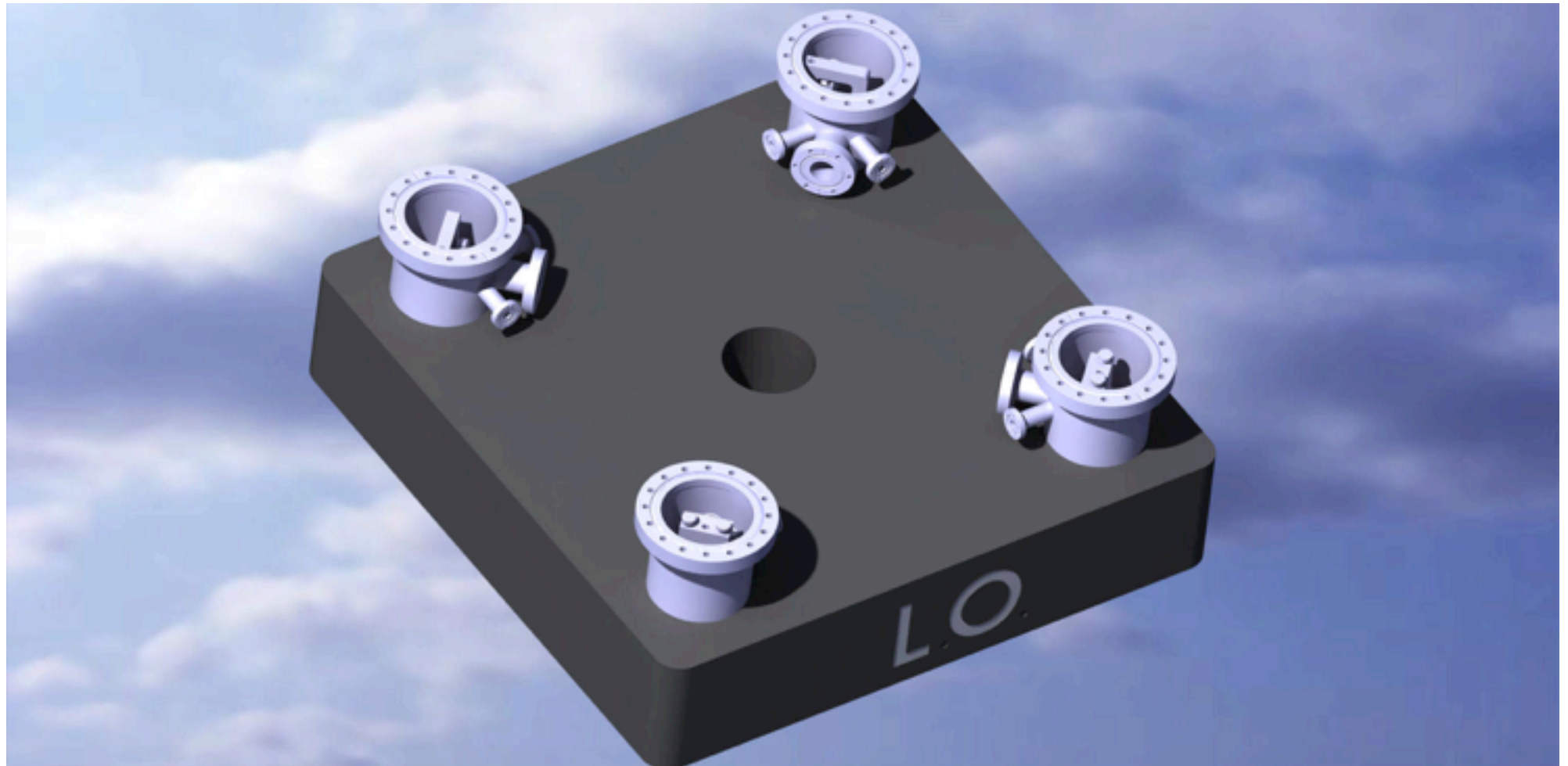
L m	f @ .1 Hz kHz	f Earth* Hz	FSR MHz	optical cavity Q^{\wedge}	q. noise nrad $\sqrt{\tau}^{\$}$	$\Delta\phi$ b. s. nrad
0,11	77,3	9,0	682	$1,36 \times 10^{11}$	268	8650
0,50	351,3	40,8	150	$6,20 \times 10^{11}$	12,1	20
0,90	632,4	73,4	83	$1,12 \times 10^{12}$	5,42	1,9
1,35	948,6	110,1	56	$1,68 \times 10^{12}$	1,65	0,04

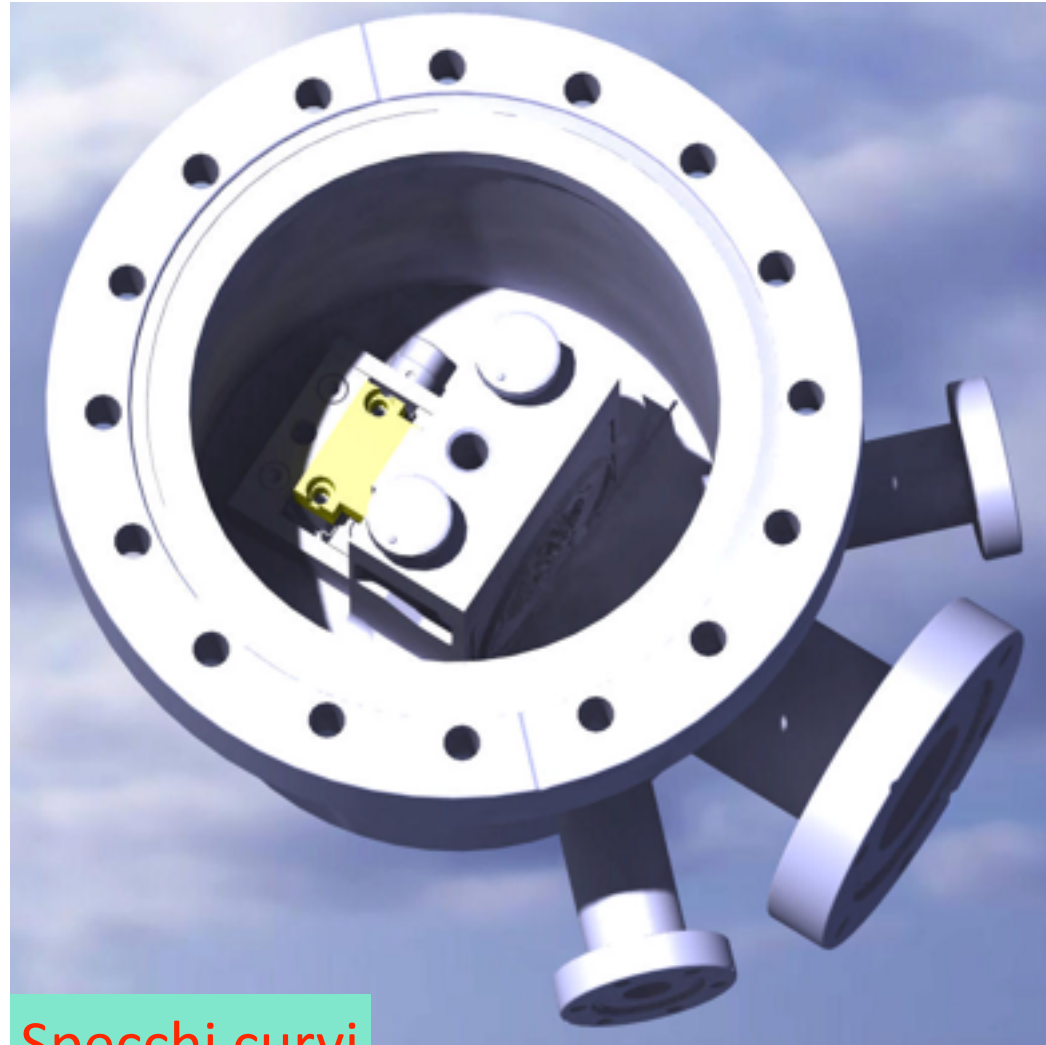
* Calculated for the latitude of Turin ($45^{\circ}04'$)

\wedge Estimated total cavity losses 32 ppm

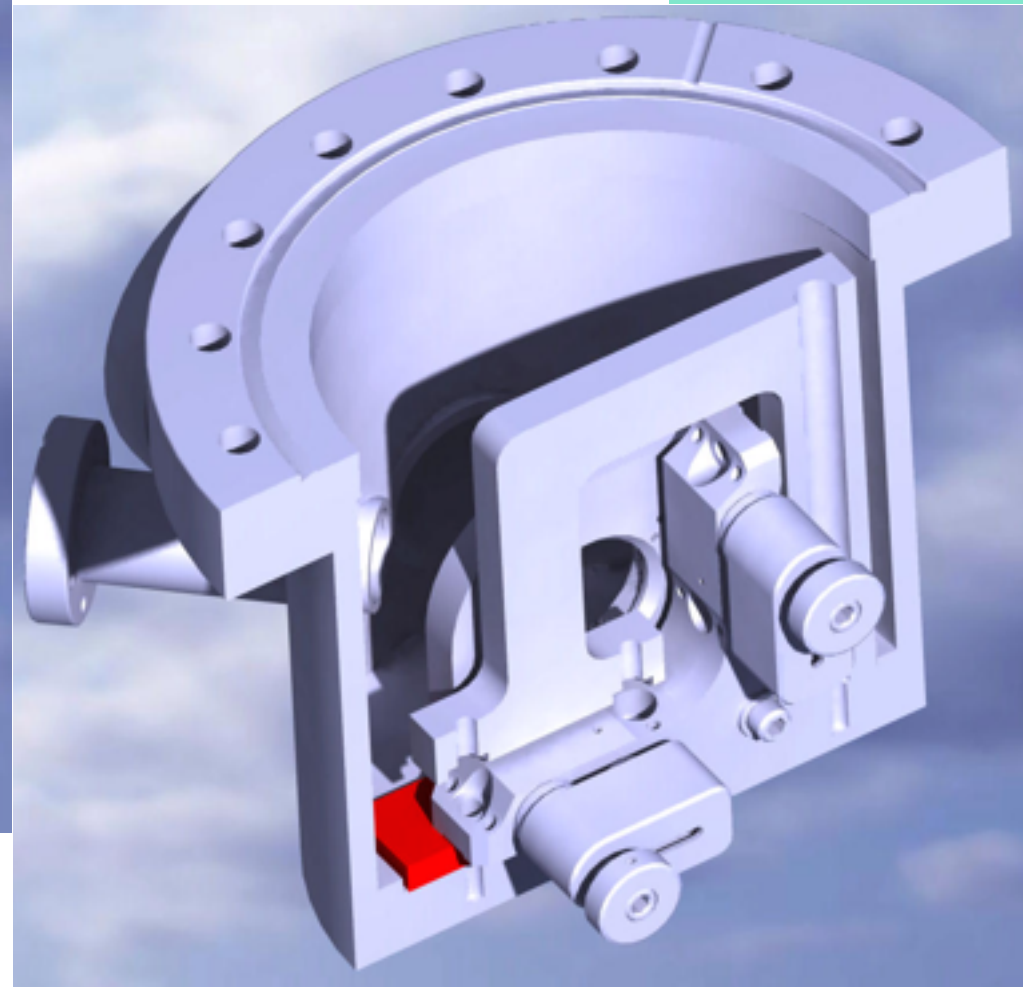
$\$$ $\tau = 5$ s







Specchi curvi



Specchi piani