



# The POLIS interferometer for ponderomotive squeezed light generation



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POLIS is a suspended interferometer, presently under construction, devoted to the generation of ponderomotive squeezed light and to the study of the interaction of non classical quantum states, of light, and macroscopic objects. The interferometer is a Michelson whose half-meter long arms are constituted by high-finesse cavities, suspended to a seismic isolation chain similar to the Virgo SuperAttenuator. - The mass of the suspended cavity mirrors are chosen to be tens of grams: this value is sufficiently high to permit the use of the well tested Virgo suspension techniques but also sufficiently small to generate the coupling among the two phase quadratures with a limited amount of light in the cavity, of the order of few tens of kW. - In this poster the main features of the interferometer are shown, together with the expected sensitivity and squeezing factor.

### Squeezed State of Light and Sensors

**Minimum Uncertainty States**  $\Delta X_1 \Delta X_2 = 1$

A bright beam ( $\alpha > 0$ ) has the same fluctuation of the vacuum  
Light as 'sensitive' element  
its intrinsic quantum fluctuations  
Determines the final sensitivity

We cannot violate the uncertainty principle  
but  
we can squeeze the quantum fluctuations on one quadrature and 'use' that quadrature as sensitive element

**Squeezed States**

**Coherent State = Displaced Vacuum**  
 $|\alpha\rangle = D(\alpha)|0\rangle$   $[D(\alpha) = \exp(\alpha a^\dagger - \alpha^* a)]$

**Squeezed State**  $|\alpha, \zeta\rangle = D(\alpha)S(\zeta)|0\rangle$   
**Displaced Squeezed Coherent Vacuum**  
 $S(\zeta) = \exp\left(\frac{1}{2}\zeta a^2 + \frac{1}{2}\zeta^* a^{\dagger 2}\right)$   $[\zeta = r e^{i\theta}]$   
Squeezing factor  $r$   
Orientation of the squeezing axis  $\theta$

$\Delta X_1 = \Delta X_2 = 1$   
 $\Delta Y_1 = e^{-r}$   
 $\Delta Y_2 = e^r$   
 $\hat{Y}_1 + i\hat{Y}_2 = (\hat{X}_1 + i\hat{X}_2)e^{-i\theta}$

### Squeezing in Interferometers

C. M. Caves, 'Quantum noise in an interferometer'  
Phys. Rev. D 23 (1693-1708), 1981

Noise in the output as beat between the coherent input beam and the vacuum that enters in the unused port of a beam splitter (dark port of interferometer)

**Vacuum Squeezed in the unused port**

**Noise Reduction (sensitivity improvement)**

Interferometric Gravitational Waves Detectors (IGWD) require a frequency-dependent squeezing quadrature: squeezing angle  $\theta_s = \theta_s(\Omega)$ , with  $\Omega =$  detection frequency

RPN dominates at Low frequencies  
Amplitude squeezed vacuum ( $\theta_s=0$ )  
SN dominates @ High frequencies  
Phase squeezed vacuum ( $\theta_s=\pi/2$ )

### Frequency dependent & independent Ponderomotive Squeezing

**USE OF RADIATION PRESSURE AS SQUEEZING MECHANISM**

Laser Intensity fluctuations  $\leftrightarrow$  test mass motion  
Phase-shift proportional to intensity fluctuations  
**(FREQUENCY DEPENDENT SHIFT)**

Coupling between phase quadrature and amplitude quadrature  
Squeezing  $\xi(\Omega)$  (frequency dependent)

**OPTICAL SPRING FOR FREQUENCY INDEPENDENT SQUEEZING**

Optical Spring modifies the cavity dynamics  
 $\xi(\Omega) \rightarrow \xi$  constant for  $\Omega \ll \Theta$   
optical spring characteristic frequency

gives the frequency independent squeezing band

### What is interesting in ponderomotive squeezing?

**Squeezing generation in MOEMS (Micro-Opto-Electro-Mechanical Systems) - Communication and integrated sensors; on chip devices** OPO integration in the well consolidated silicon technology (mixed technology with KTP and LiNb on Si) is more expensive and does not allow the same integration factor

**Study of the coupling between macroscopic opto-mechanical objects and their quantum mechanical behavior** - Theoretical interest

**Low frequencies and frequency independent squeezing** - GW detectors

**PS is a completely suspended system** - we expect that could be, a regime, a more robust system In long period operation OPO squeezer seems experimentally frequency limited due to losses mechanism in the medium (photo-thermal fluctuations) even if progress in material engineering and dedicate mechanical design promises to overcome these limits.

### Polis Optical Parameters

**squeezing factor**  
 $\xi_{min}(\Omega \ll |\Theta|) = \frac{|\delta_7|}{1 + \sqrt{1 + \delta_7^2}}$

**Optical spring resonance**  
 $\Theta^2 \equiv \frac{K_{opt}}{M} = -\frac{4\omega_0^2 \delta_7}{Mc^2} \left( \frac{2F}{\pi} \frac{1}{1 + \delta_7^2} \right)^2$

Fixed the  $\xi$  and  $\Theta$   
key parameters are:  
Input power  $I_0$ , Cavity Finesse  $\mathcal{F}$ , Cavity detuning  $\delta_7$ , Suspended mirrors mass  $M$

**Parameters value optimization** to have  
A large enough squeezing factor and the desired frequency band

**Cavity detuning: trade-off between squeezing value/band**

High level increases band  
Low level increases squeezing

We fix:  $\delta = 0.3 \Rightarrow \xi = 18$  dB and  $\Theta = 2\pi$  kHz

By considering the losses, this assures more than 10 dB of potential squeezing delivered by the interferometer  
It covers the GWD band (but is not vacuum squeezed)

$P_{in} = 2.5$  W  $\mathcal{F} \leq 30$  000

Constrain for the cavity length: inner SAFE diameter  $L = 440$  mm  
Negative stability factors,  $g_i$ , in the cavities with low suspended masses reduce the angular instability  $g_i = -0.76$

Available Radii of Rurvature of the commercial substrates  $RoC_{INPUT} = RoC_{END} = 250$  mm

This value of the RoC assures the maximum spot size,  $w_0$ , on the mirrors with the available commercial radii (large spot  $\Rightarrow$  reduces thermal deformation of the coating)  $w_0 = 0.447$  mm

Gouy phase =  $2.43$  rad =  $0.773493\pi$

well stable cavity:  
avoiding the couplings with thermal deformations or imperfections, mis-match problems and the higher order modes resonance

## Ponderomotive Light Squeezing POLIS project

Project to realize a completely suspended low frequencies ponderomotive squeezer, moving from the pioneers' work made in the LIGO laboratory at the MIT [Corbitt et al. Phys. Rev. A 73 (2 Feb. 2006), p. 023801] and

taking the advantage of the available Virgo Super Attenuator Facility at EGO, SAFE to control the main noises sources in the low frequencies range

### Critical Points

**Ponderomotive Squeezing:**  
large squeezing values without use high laser power and/or very high cavity finesse requires very small suspended mirrors mass

very critical point is the mass suspension

### Chance of success for the project

A relative large mass allows us to use the available well consolidate technologies of Virgo to control the low frequency noise

### higher chance of success

**Low value of mass**

- Large optical Spring resonance (frequency independent squeezing Band)

**High value of mass**

- ease of construction;
- ease to sense and actuate motion;
- use commercial size

Use of SAFE High sensitivity in the low frequency range thanks to better seismic isolation we can choose slightly higher mass:  $M = 10$  g

A standard 25.4 mm mirror in fused silica with a 6.35 mm thickness has a mass of about 7.8 g, while with a 10 mm of thickness it can reach a mass of 11.1 g: It can be suspended with the available technology in Virgo

Moreover macroscopic masses reduce the thermal noise

### SAFE and Polis

resonance frequency of the SAFE first stage = 40 mHz

Suspended optical bench in place of the Virgo suspended mirror

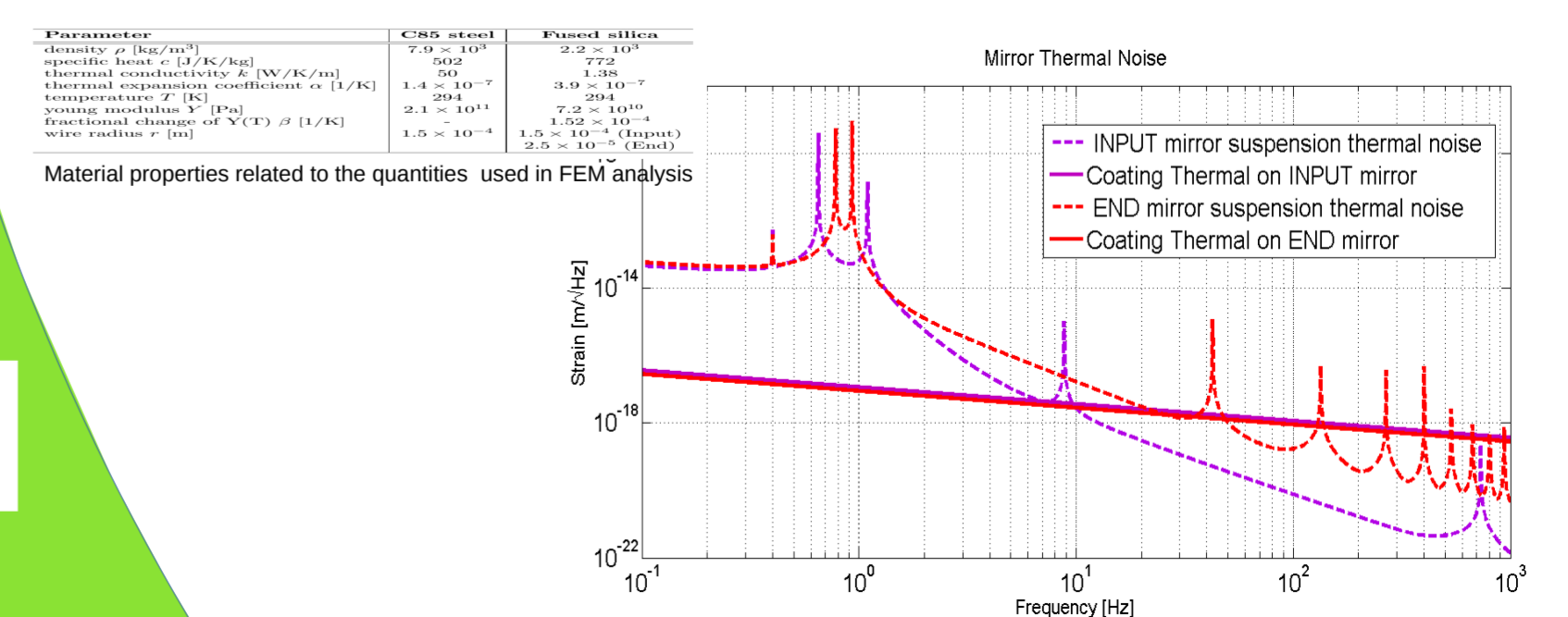
### Polis Interferometer expected noise

Maximum equivalent interferometer noise on the differential mode in order at least to reach the non-squeezed noise level.

The three curves for the equivalent noise of the interferometer are shown. In case of 7 db of squeezing, taken as realistic value due to losses, the interferometer sensitivity limit is  $10^{-15}$  m/sqrt(Hz) @ 10 Hz and  $10^{-17}$  m/sqrt(Hz) @ 100 Hz. These requirements can be fulfilled by careful design of the interferometer.

With our choice of parameters the FEM simulations predict a suspension and coating thermal noise below the expected squeezing value at low frequencies. They are expected to be the major source of fundamental noises in the 10-20 Hz frequency region.

The expected noise is within the requirements, as shown in figures



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FRONTIER DETECTORS FOR FRONTIER PHYSICS  
13<sup>th</sup> Pisa Meeting on Advanced Detectors

24-30 May 2015 - La Biodola, Isola d'Elba (Italy)