

# Update on NEG electromagnetic properties characterization at high frequencies

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P.Maurin, G. De Michele, P.Costa Pinto, J.P.Rigaud, S.Dos Santos, M.Taborelli,  
W. Vollenberg

# Overview

- 1 EM material properties measurements in X-band
  - Stainless steel waveguide
  - Copper waveguide
  - 9  $\mu\text{m}$  NEG coated-Cu waveguide
  - 20  $\mu\text{m}$  NEG coated-Cu waveguide
- 2 On the road to high frequencies measurements
  - High frequency measurements
- 3 Summary and future plans

## Use of NEG coating and motivation

- The performance of the CLIC DR is likely to be limited by collective effects due to the unprecedented brilliance of the beams
- Coating will be used in both electron (EDR) and positron damping rings (PDR) to suppress effects like electron cloud formation or ion instabilities
- NEG coating is necessary to suppress fast beam ion instabilities in the electron damping ring (EDR)
- The impedance modeling of the chambers must include the contribution from the coating materials
- A correct characterization of the EM material properties of NEG in a high frequency range is therefore necessary and still widely unexplored

# Material EM properties characterization

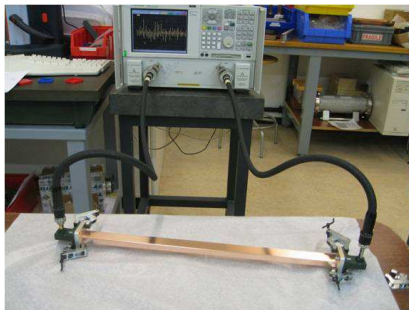
## Waveguide method

The EM properties are determined with the waveguide method, based on a combination of experimental measurements of the complex transmission coefficient  $S_{21}$  and CST 3D EM simulations

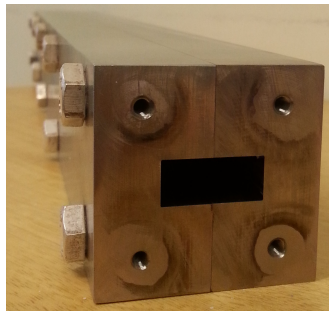
## Measurements in X-band

- An X-band waveguide is connected to a vector network analyzer (VNA) to measure the  $S_{21}$  parameter across the 10 - 11 GHz single-mode band of the WR-90 waveguide
- $S_{21}$  is related to the attenuation due to the material finite conductivity, therefore related to the unknown properties
- The S-parameters can also be obtained numerically from 3D simulations using CST

# Measurements setup and waveguides for testing the method

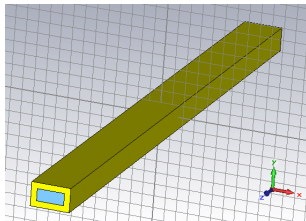
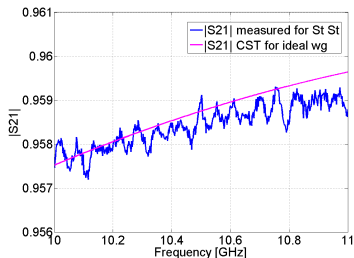


(a) Measurements setup with VNA and a Cu WR-90 waveguide.



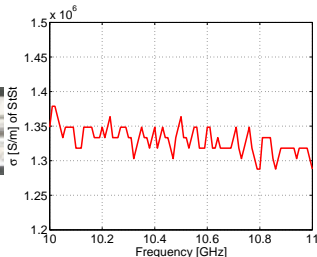
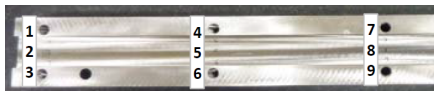
(b) Split-block StSt WR-90 waveguide with vertical cut (interior dimensions of 22.86 x 10.16 mm)

## Benchmark of the method using a well known material: stainless steel 316LN waveguide (1)



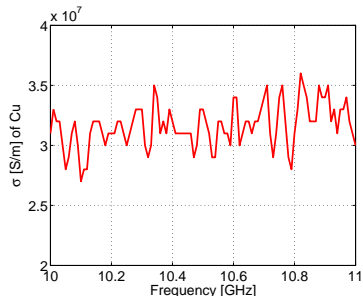
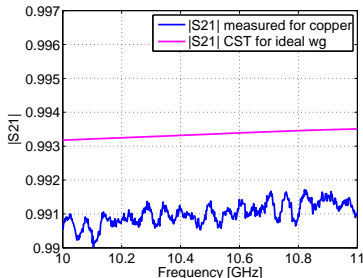
- Measured and simulated  $S_{21}$  for a StSt waveguide (conductivity used in CST simulation  $\sigma=1.35 \times 10^6$  S/m)
- CST assumes no surface roughness. Results in good agreement

## Benchmark of the method using a well known material: stainless steel 316LN waveguide (2)



- Measurements of the Ra roughness parameter along the waveguide were performed (by J.P.Rigaud). Calculating the average,  $R_a = 0.6 \mu\text{m}$ . At 10 GHz,  $\delta = 4.3 \mu\text{m}$ . Surface roughness is not expected to induce significantly higher losses. Extracted StSt conductivity in good agreement with the expected one.

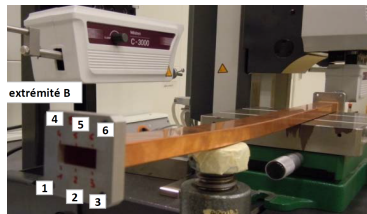
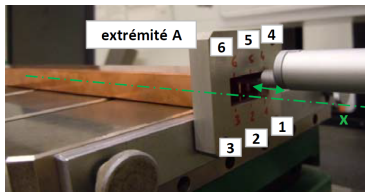
# Benchmark of the method using a well known material: annealed copper waveguide



- 1 Real losses higher than CST prediction for  $\sigma = 5.8 \times 10^7$  S/m ( $\delta = 0.66 \mu\text{m}$  at 10 GHz).  
Theoretical losses for Cu: 0.108 dB/m at 10 GHz. Measured: 0.16 dB/m.
- 2 Extracted  $\sigma_{Cu}$  is lower than the expected DC value, representing a higher-loss waveguide due to roughness effects. CST agrees with this estimated effective conductivity of Cu if roughness is assumed to be  $R_q = 0.4 \mu\text{m}$ .

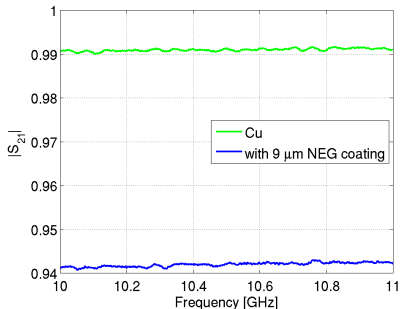
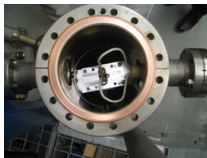
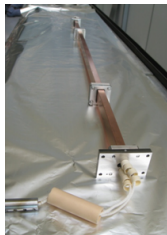


# Roughness measurement on the copper waveguide



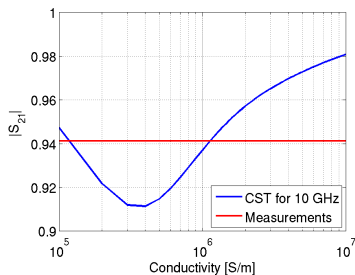
- 1  $R_q$  measurements were performed at the 2 extremities of the waveguide (6 points each) (by J.P.Rigaud)
- 2 Average value of  $R_q=0.3 \mu\text{m}$
- 3 Successful benchmark of the method

# $S_{21}$ measurements for a copper and a 9 $\mu\text{m}$ NEG-coated copper waveguide



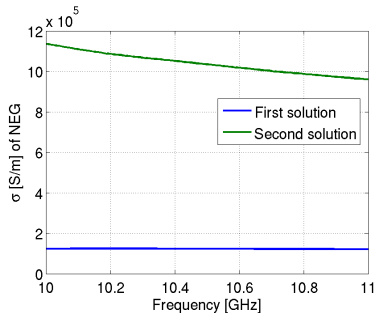
- 1 Coating by *P.Costa Pinto* from TE/VSC group at CERN
- 2 EM interaction with NEG induces more losses

## $S_{21}$ from CST simulations and intersection with measurements- ambiguity in the solution

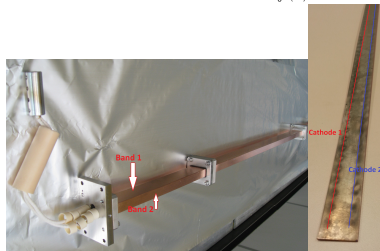
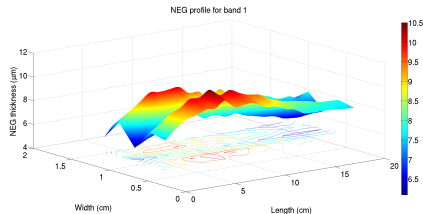


- CST computes  $S_{21}$  at a certain frequency as a function of conductivity (parameter sweep)
- At a certain frequency, intersect CST and measured value to find conductivity. Two possible solutions due to the 2-layers structure

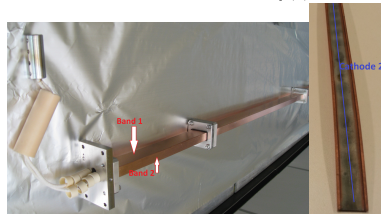
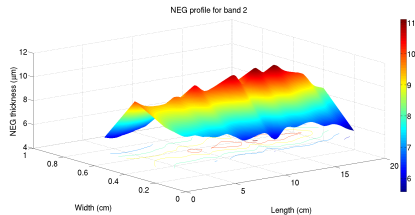
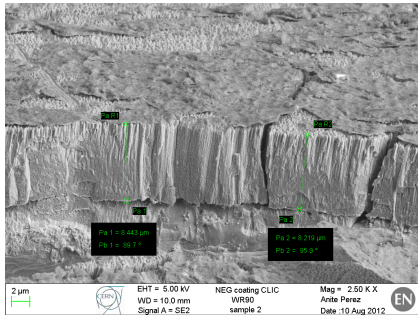
# NEG effective conductivity



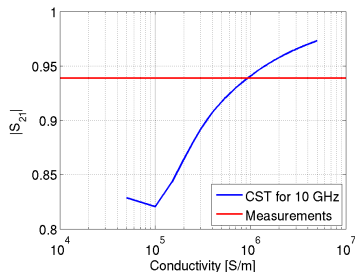
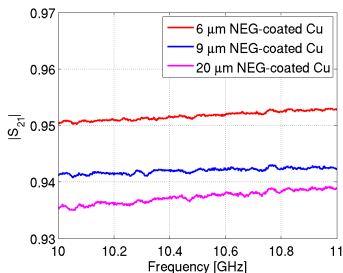
- First solution gives a stable but too low value of  $1.2 \times 10^5$  S/m
- Non uniform coating from XRF (by *M. Malabaila*)



# NEG effective conductivity

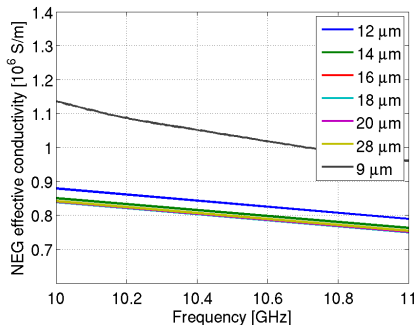


## $S_{21}$ measurements in a 20 $\mu\text{m}$ NEG-coated Cu



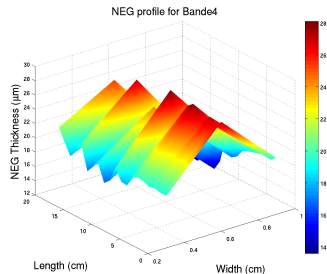
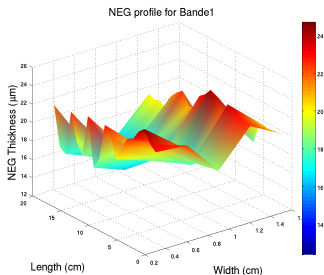
- One solution over this conductivity scan
- To accept the first solution,  $\sigma_{NEG} < 10^4$  S/m

## NEG effective conductivity for 9 and 20 $\mu\text{m}$ coating



- Measurements with two different waveguides give close results. Indication to accept this second solution  $10^6 \text{ S/m}$  (in agreement with measurements of NEG resistivity, see *S.Calatroni talk*)
- Frequency dependent behavior. But still low frequencies to see relaxation effects. Very non uniform coating also in this case that could explain this behavior (see *S.Calatroni talk*)

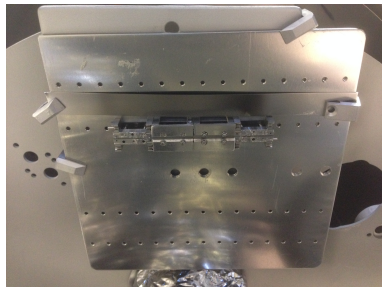
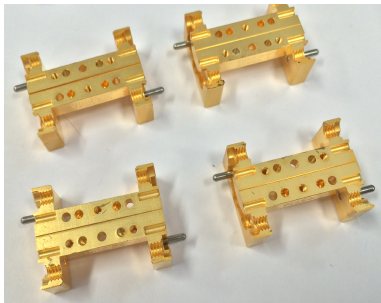
# XRF profile analysis



- Variation of profile between 12 and 28  $\mu\text{m}$

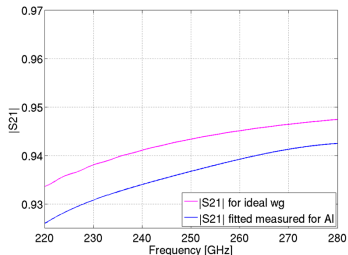
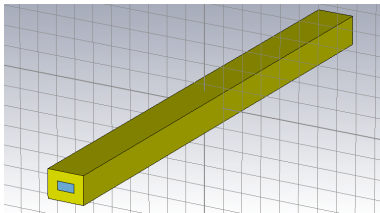


# Preparation for measurements with WR3.4 220-330 GHz and WR1.5 500-750 GHz waveguides from VDI



- WR3.4: 0.864 x 0.432 mm, WR1.5: 0.381 x 0.191 mm
- Challenging coating due to the very small aperture (*by W.Vollenberg*)

## $S_{21}$ measurements with Al gold plated WR3.4 waveguide



- Comparison of measured  $S_{21}$  for a WR3.4 Al gold plated waveguide and simulated with CST Al waveguide

## Conclusions

- Successful benchmark of the waveguide method in X-band
- Investigate the effect of non uniform coating
- Promising beginning for the high frequency measurements
- October 2014: measurements at VDI of Al (gold plated) NEG-coated waveguides (WR 3.4 and WR 1.5) at 220-330 GHz and 500-750 GHz