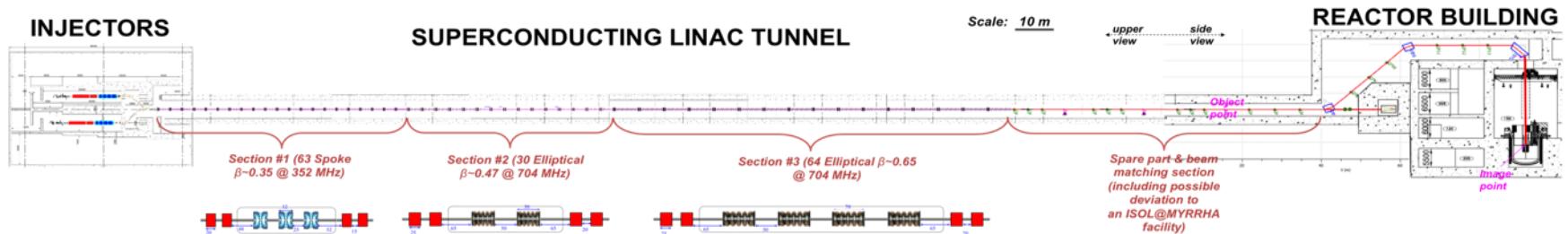


# MYRRHA

Multipurpose hYbrid Research Reactor for High-tech Applications



## MYRRHA: a polyvalent research project around an ADS nuclear reactor

*The fast spectrum Pb-Bi cooled nuclear reactor: subcritical and critical configurations*



STUDIECENTRUM VOOR KERNENERGIE  
CENTRE D'ETUDE DE L'ENERGIE NUCLEAIRE

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Francesco Belloni  
NSP - SCK•CEN



# MYRRHA: multipurpose irradiation facility

Fuel research  
 $\Phi_{tot} = 0.5 \text{ to } 1.10^{15} \text{ n/cm}^2.s$

Material research  
 $\Phi_{Fast} = 1 \text{ to } 5.10^{14} \text{ n/cm}^2.s$   
 (En>1 MeV) in large volumes

## Fission GEN IV



$\Phi = 1 \text{ to } 5.10^{14} \text{ n/cm}^2.s$   
 (ppm He/dpa ~ 10)  
 in medium-large volumes

## Fusion

50 to 100 MWth  
 $\Phi_{Fast} = \sim 10^{15} \text{ n/cm}^2.s$   
 (En>0.75 MeV)

	Challenge	Solution	MYRRHA contribution
Fission	High radiotoxic level waste	Transmutation	ADS demo
Fission GEN IV	Demonstrate concept	Build demonstrators	LFR technology demo Fast spectrum irradiation facility
Fusion	Extreme operating conditions	Material testing & development	Fast spectrum irradiation facility
Fundamental research	Pushing the limits of knowledge	Access to proton beam	Long term experiments with radioactive ion beams (RIB)
Renewable energies	Efficient power electronics	High efficiency transistors (Neutron Transmutation Doped NTD-Si)	Securing NTD-Silicon production
Healthcare	Ageing population	A long term source of medical radioisotopes	Securing radioisotopes production (existing and new ones)

High energy LINAC  
 600 MeV – 1 GeV  
 Long irradiation time



## Fundamental research

## Waste

$\Phi_{th} = 0.5 \text{ to } 2.10^{15} \text{ n/cm}^2.s$   
 (En<0.4 eV)

## Radioisotopes



$\Phi_{th} = 0.1 \text{ to } 1.10^{14} \text{ n/cm}^2.s$   
 (En<0.4 eV)

## Silicon doping



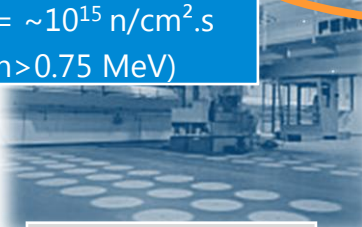
<http://myrrha.sckcen.be/en/MYRRHA/Applications>

# MYRRHA: multipurpose irradiation facility

Fuel research  
 $\Phi_{\text{tot}} = 0.5 \text{ to } 1.10^{15} \text{ n/cm}^2.\text{s}$

## Fission GEN IV

50 to 100 MWth  
 $\Phi_{\text{Fast}} = \sim 10^{15} \text{ n/cm}^2.\text{s}$   
 (En > 0.75 MeV)



Waste

	Challenge	Solution	MYRRHA contribution
Fission	High radiotoxic level waste	Transmutation	ADS demo
Fission GEN IV	Demonstrate concept	Build demonstrators	IFER technology demo Fast spectrum irradiation facility
Fusion	Extreme operating conditions	Material testing & development	Fast spectrum irradiation facility
Fundamental research	Pushing the limits of knowledge	Access to proton beam	Long term experiments with radioactive ion beams (RIB)
		High efficiency transistors	

Challenge

Solution

MYRRHA contribution

Fission

High radioactive level waste

Transmutation

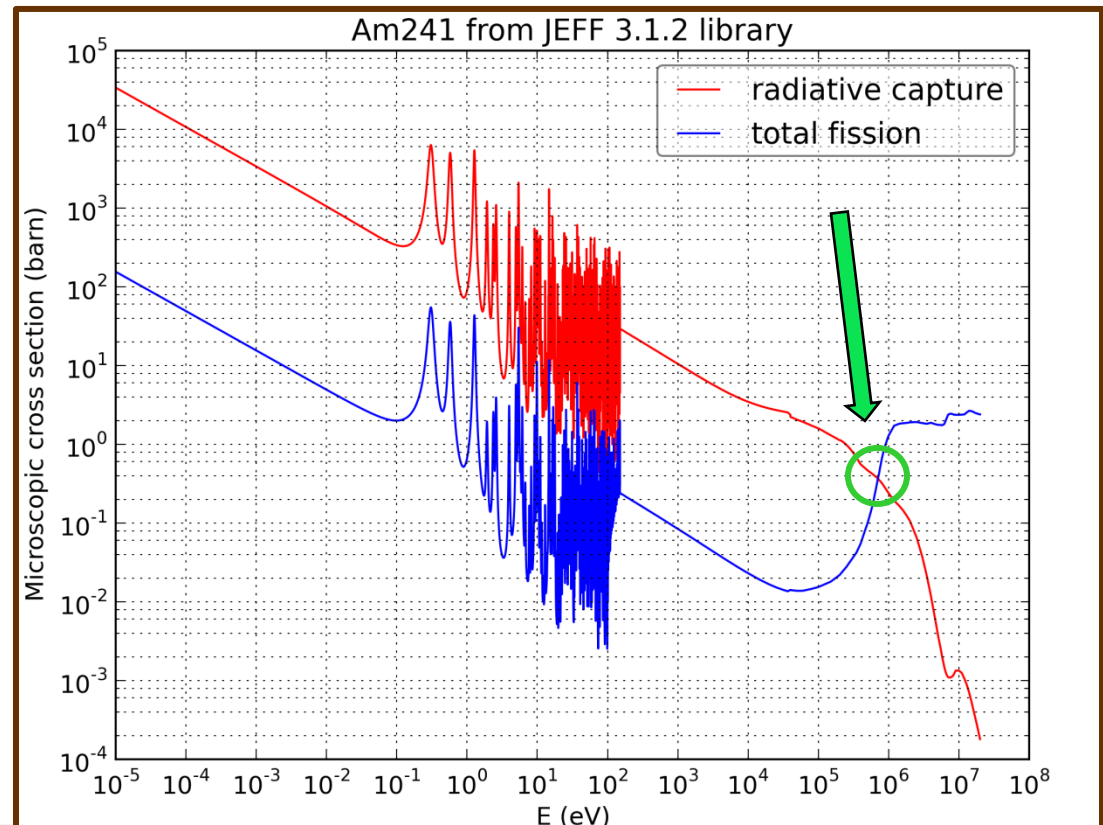
ADS demo

<http://myrrha.sckcen.be/en/MYRRHA/Applications>

# Fast neutrons are fundamental for transmutation

- In order to be transmuted Minor Actinides (MAs) have to be fissioned
- The ratio between fissions and captures is higher at high energy (fast spectrum)
- Increase of fertile fissions: more neutrons available to transmutation

Isotope	PWR	SFR
U-235	0.821	0.807
U-238	0.099	0.194
Np-237	0.014	0.296
Pu-238	0.072	0.711
Pu-239	0.637	0.865
Pu-240	0.003	0.576
Pu-241	0.747	0.873
Pu-242	0.015	0.550
Am-241	0.011	0.233
Am-242m	0.812	0.870
Am-243	0.008	0.334
Cm-242	0.212	0.579
Cm-243	0.847	0.943
Cm-244	0.054	0.479
Cm-245	0.865	0.914



# Critical and subcritical configuration

- The fission reaction chain can be obtained either in critical or subcritical configuration:

$$\phi(x, t) = \frac{p}{K_{\infty} \Sigma_a} \sum_{\substack{n=1 \\ (n \text{ disp.})}}^{\infty} \left[ C_n e^{(K_n - 1)t / \ell_n} + \frac{K_n S_n}{(1 - K_n)} \right] \cos \frac{n\pi x}{a}$$

Fourier's serie

Example 1: solution for a thermal neutron flux in an infinite absorbing slab  
(A. Gandini lectures)

# Critical and subcritical configuration

- The fission reaction chain can be obtained either in critical or subcritical configuration:

$$\phi(x, t) = \frac{p}{K_{\infty} \Sigma_a} \sum_{n=1}^{\infty} \left[ C_n e^{(K_n - 1)t / \ell_n} + \dots \right] \cos \frac{n\pi x}{a}$$

(n disp.)

Fourier's serie

**$K_1 = 1$**   
**CRITICAL**  
**CONFIGURATION**

Example 1: solution for a thermal neutron flux in an infinite absorbing slab (A. Gandini lectures)

# Critical and subcritical configuration

- The fission reaction chain can be obtained either in critical or subcritical configuration:

$$\phi(x,t) = \frac{p}{K_\infty \Sigma_a} \sum_{n=1}^{\infty} \left[ C_n e^{-\lambda_n t} + \frac{K_n S_n}{(1 - K_n)} \right] \cos \frac{n\pi x}{a}$$

(n disp.)

**$K_1 < 1, S > 0$   
SUBCRITICAL  
CONFIGURATION**

Fourier's serie

Example 1: solution for a thermal neutron flux in an infinite absorbing slab (A. Gandini lectures)

# Intrinsic safety of the ADS

Example 2: Spherical reactor, two energetic groups of neutrons, static solution  
(A. Ottonello, Master thesis)

$$\left\{ \begin{array}{l} \Phi_1(r) = \frac{1}{r} \sum_{n=1}^{\infty} \frac{s_n}{D_1} \frac{\left(\frac{n\pi}{R}\right)^2 - \delta}{\left[\left(\frac{n\pi}{R}\right)^2 - \alpha\right] \left[\left(\frac{n\pi}{R}\right)^2 - \delta\right] - \xi\gamma} \sin \frac{n\pi r}{R} \\ \Phi_2(r) = \frac{1}{r} \sum_{n=1}^{\infty} \frac{\gamma s_n}{D_1} \frac{1}{\left[\left(\frac{n\pi}{R}\right)^2 - \alpha\right] \left[\left(\frac{n\pi}{R}\right)^2 - \delta\right] - \xi\gamma} \sin \frac{n\pi r}{R} \end{array} \right.$$

$\Phi_1$ : thermal neutron flux  
 $\Phi_2$ : fast neutron flux

source off  $\longrightarrow$  reactor off !!

Easy power control



# ADS reactor: rather a *necessity* than a *virtue*

- On the contrary a big load of MAs can jeopardize the control of a critical reactor because of:

- 1) Reduced delayed neutron fractions,  $\beta$  (due also to the reduction of  $^{238}\text{U}$ ) and reduced margin to prompt criticality ( $\rho = \beta$ )

$$\psi(\mathbf{r}, t) = \psi_0(\mathbf{r}) \sum_{m=0}^M A_m e^{\omega_m t}$$

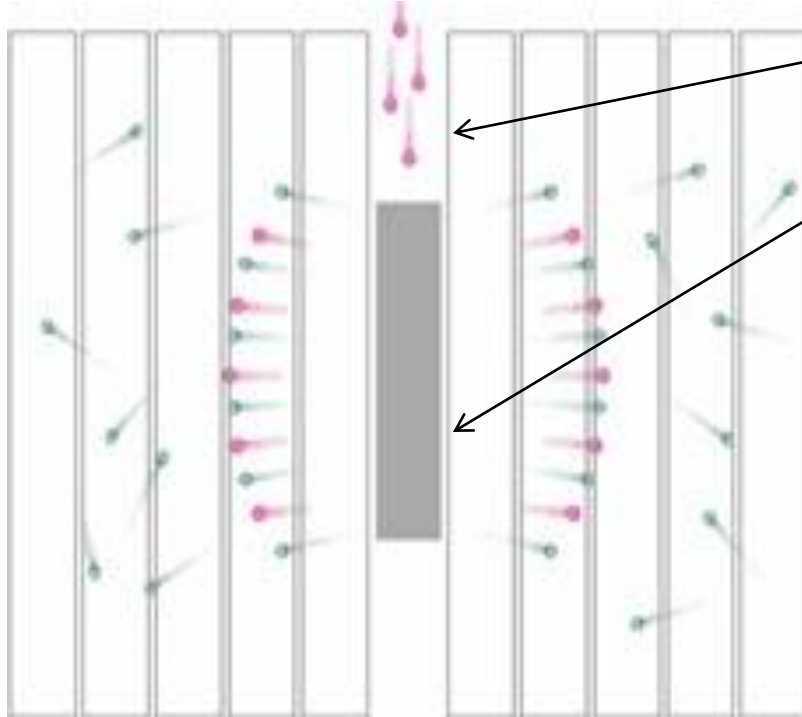
Characteristic period of the reactor

- 2) Doppler feedback reduced with increasing amount of MAs

The ADS can transmute big loads of MAs without losing safety and this solution is needed for heavily MA loaded core (>10%)

# Neutron source by spallation reaction

## Spallation



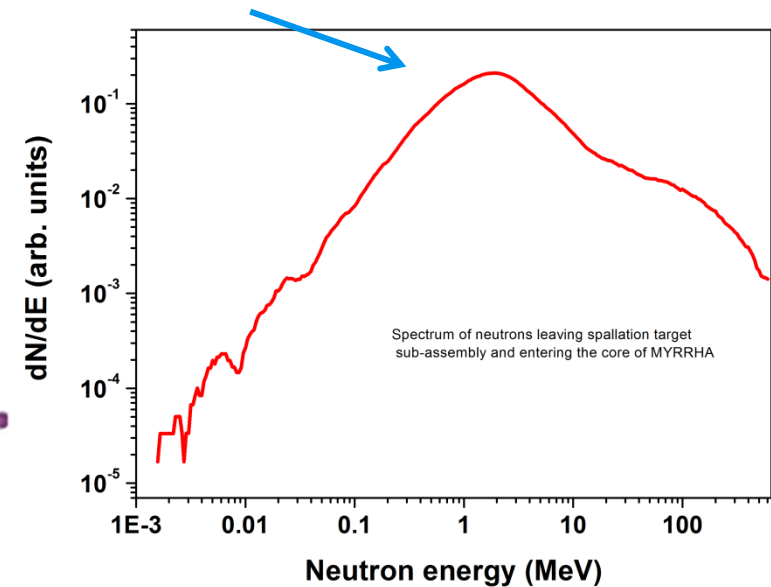
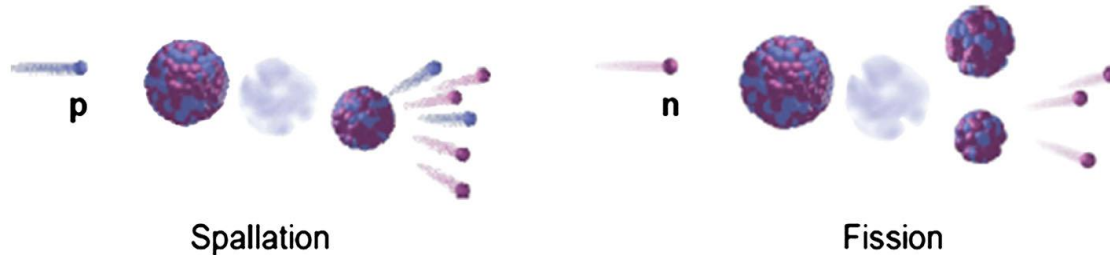
Incoming protons at 600 MeV

Spallation target (HM)

15 neutrons / proton

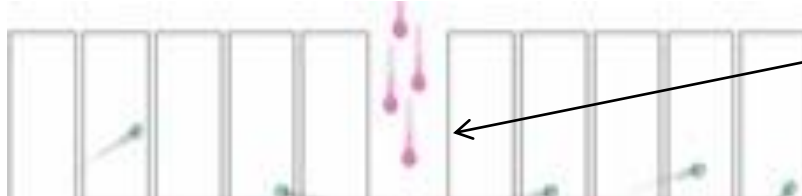
Spectrum: conventional fast spectrum (Max energy at 2 MeV) + a 3% neutrons tail towards the impinging protons energy

## Spallation + Fission



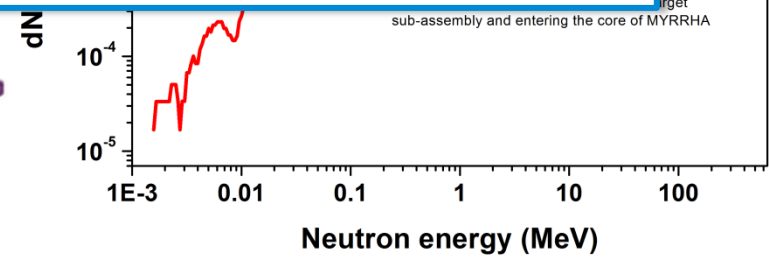
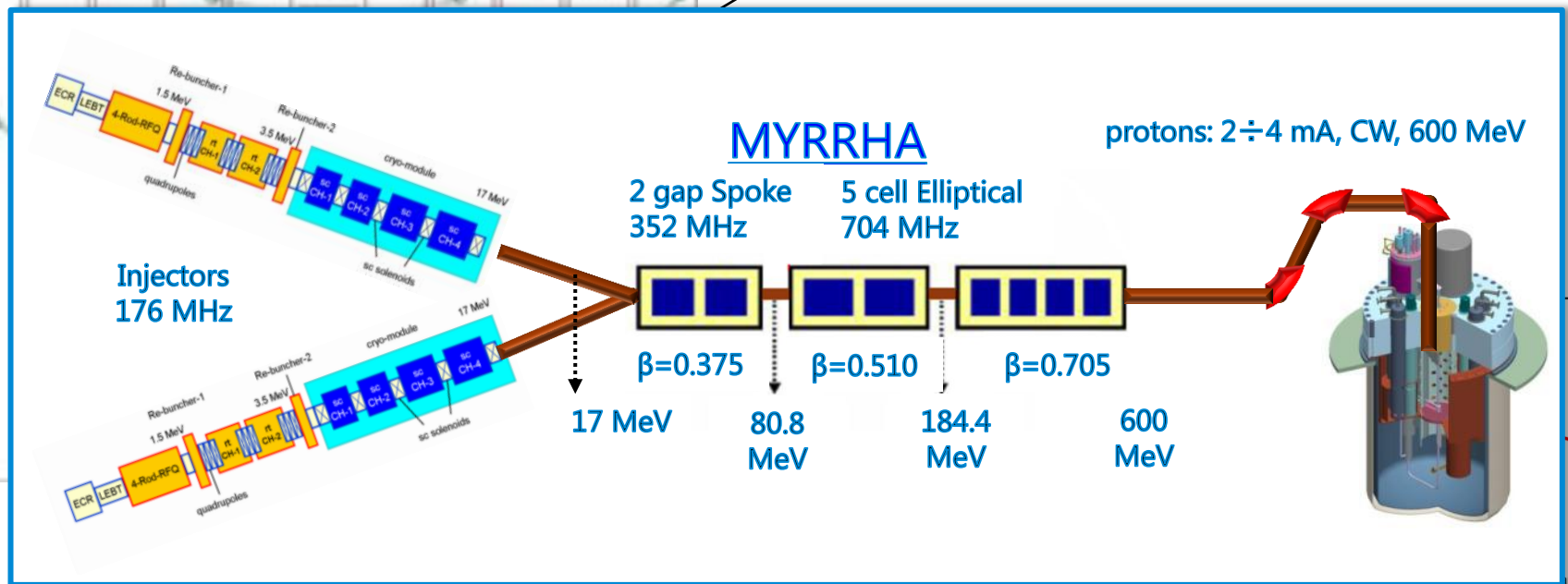
# Neutron source by spallation reaction

## Spallation



Incoming protons at 600 MeV

Spallation target (HM)

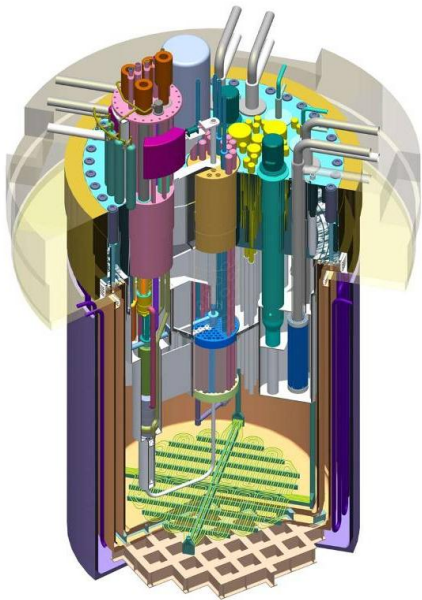


# Reactor design rationale

Objectives	Requirements	Choices
Flexible Fast Spectrum Irradiation facility	<ul style="list-style-type: none"> <li>• <math>1.10^{15}</math> n/cm<sup>2</sup>s (&gt;0.75 MeV) in large volumes</li> </ul>	<ul style="list-style-type: none"> <li>• small spallation target</li> <li>• LM cooling</li> </ul>
	<ul style="list-style-type: none"> <li>• availability (65%)</li> <li>• flexibility</li> </ul>	<ul style="list-style-type: none"> <li>• pool-type</li> <li>• in-vessel storage</li> <li>• FA manipulation beneath core</li> <li>• in-vessel inspection &amp; repair</li> <li>• IPS manipulation above core</li> <li>• Replaceability</li> <li>• HLM cooling</li> </ul>
	<ul style="list-style-type: none"> <li>• no high temperatures required</li> </ul>	<ul style="list-style-type: none"> <li>• LBE cooling (<math>T_m = 123</math> ° C)</li> </ul>

# Design History of the MYRRHA reactor

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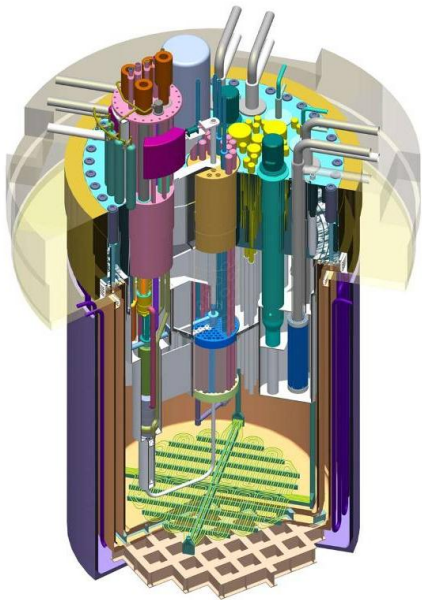


Draft 2

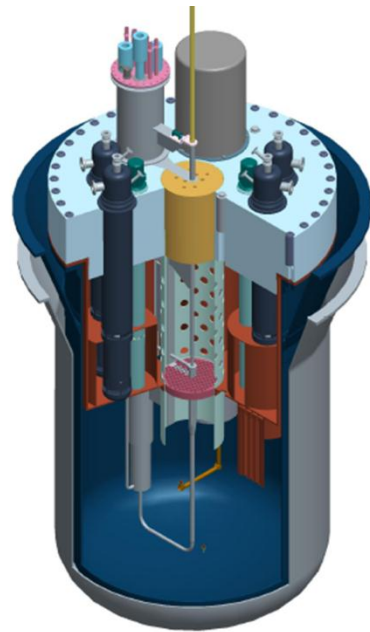
2005



# Design History of the MYRRHA reactor



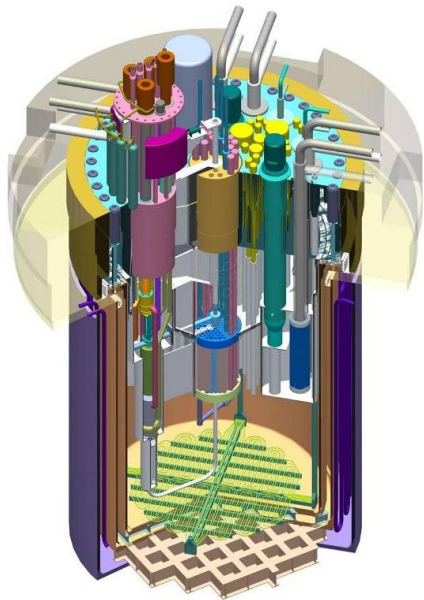
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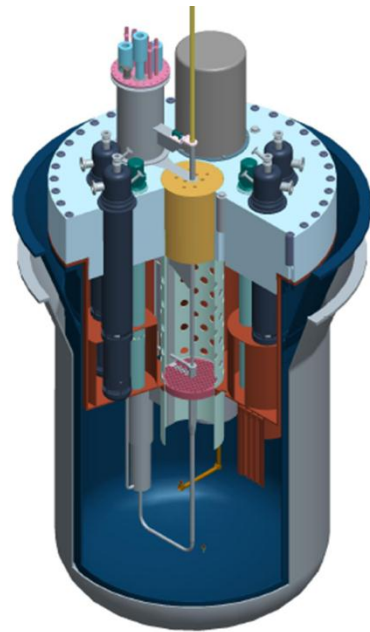
XT-ADS  
2009



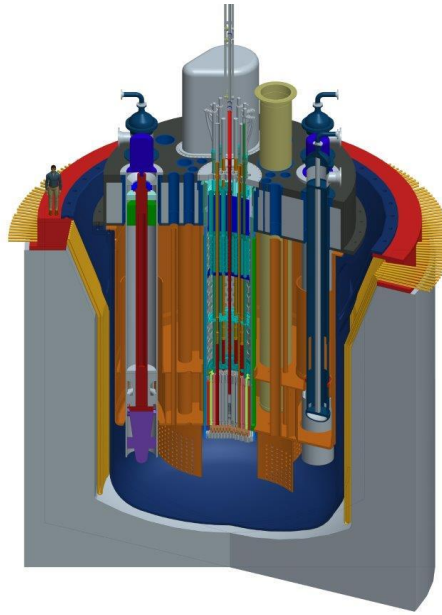
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2005



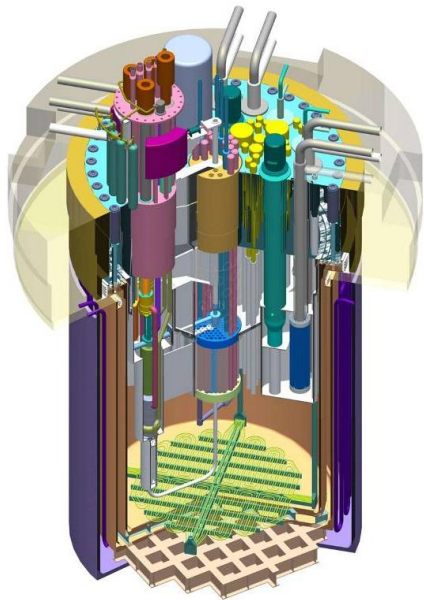
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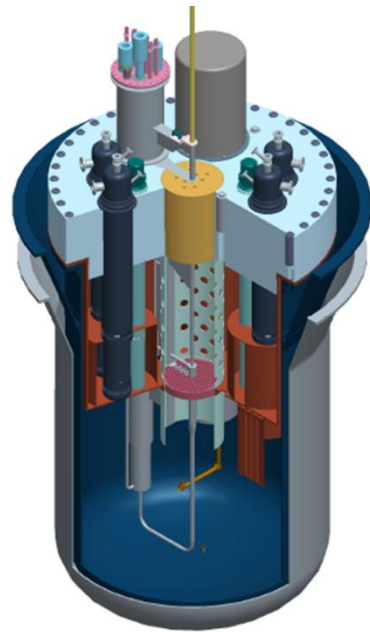
FASTEF  
(**CDT Result**)  
2012



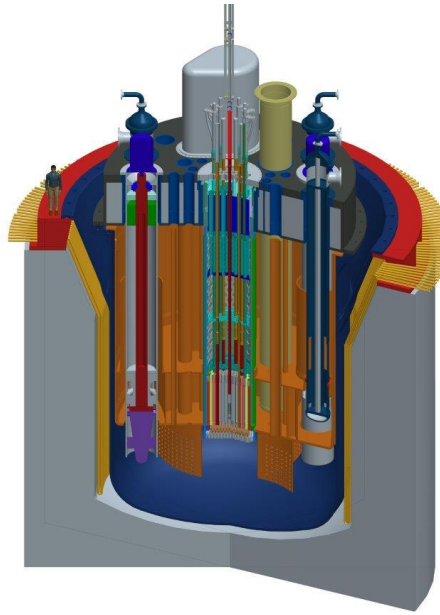
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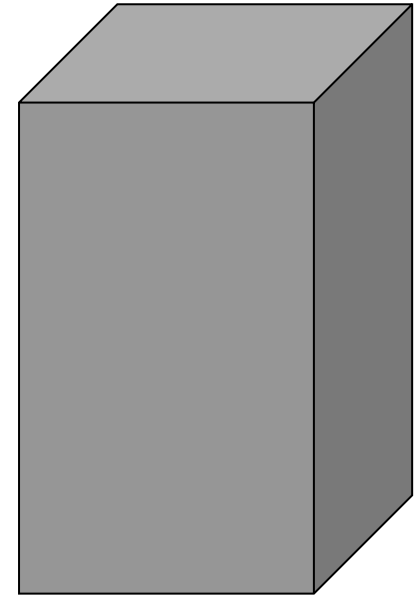
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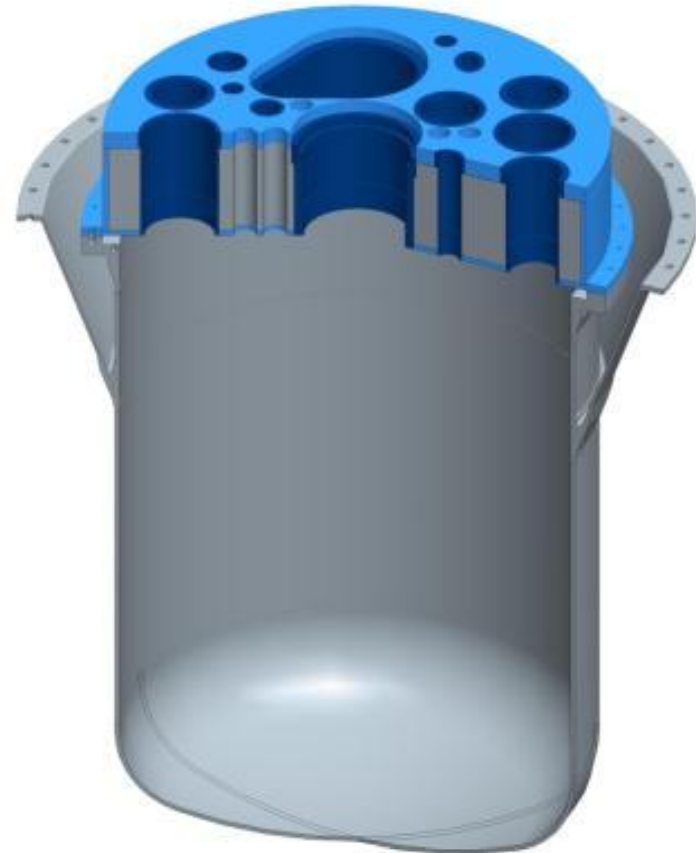
Rev. 1.6  
2014



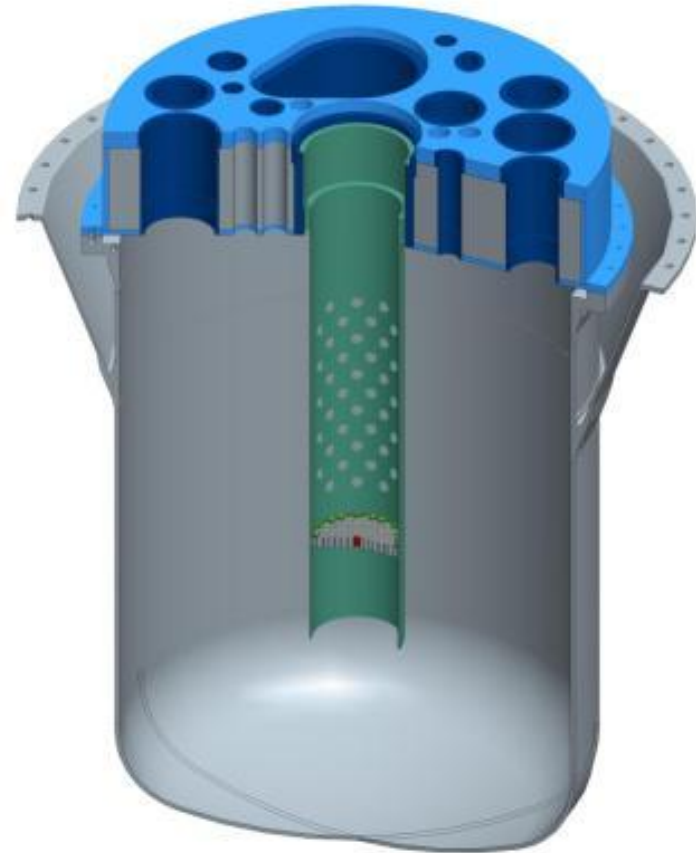
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- Diaphragm
  - IVFS
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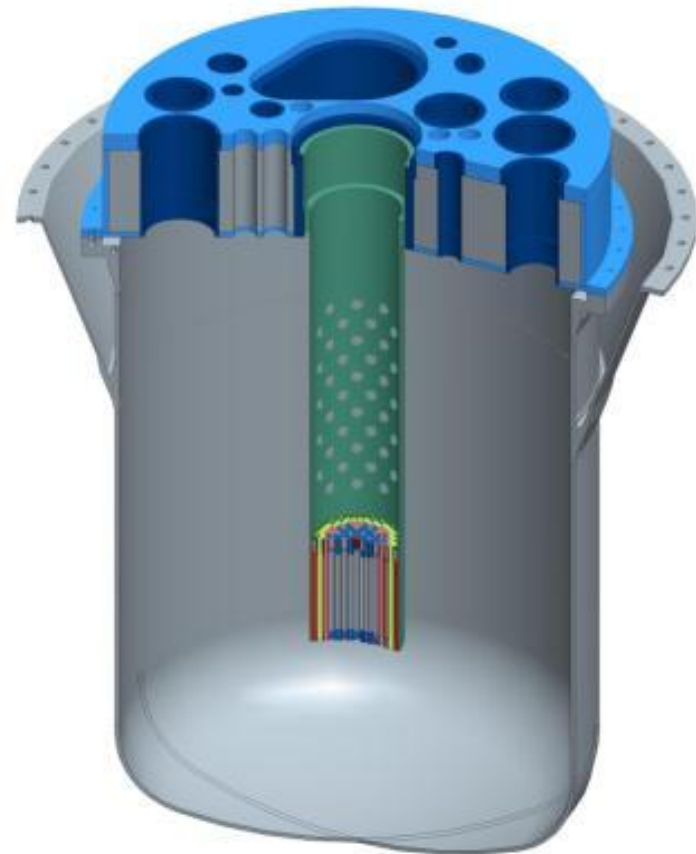
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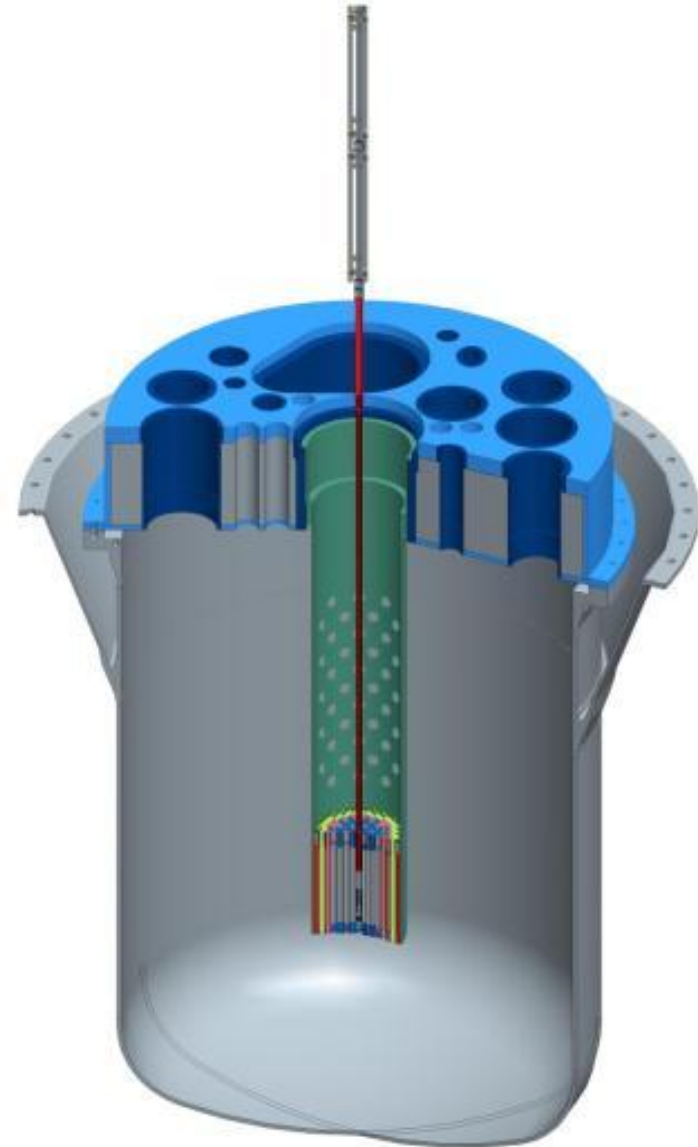
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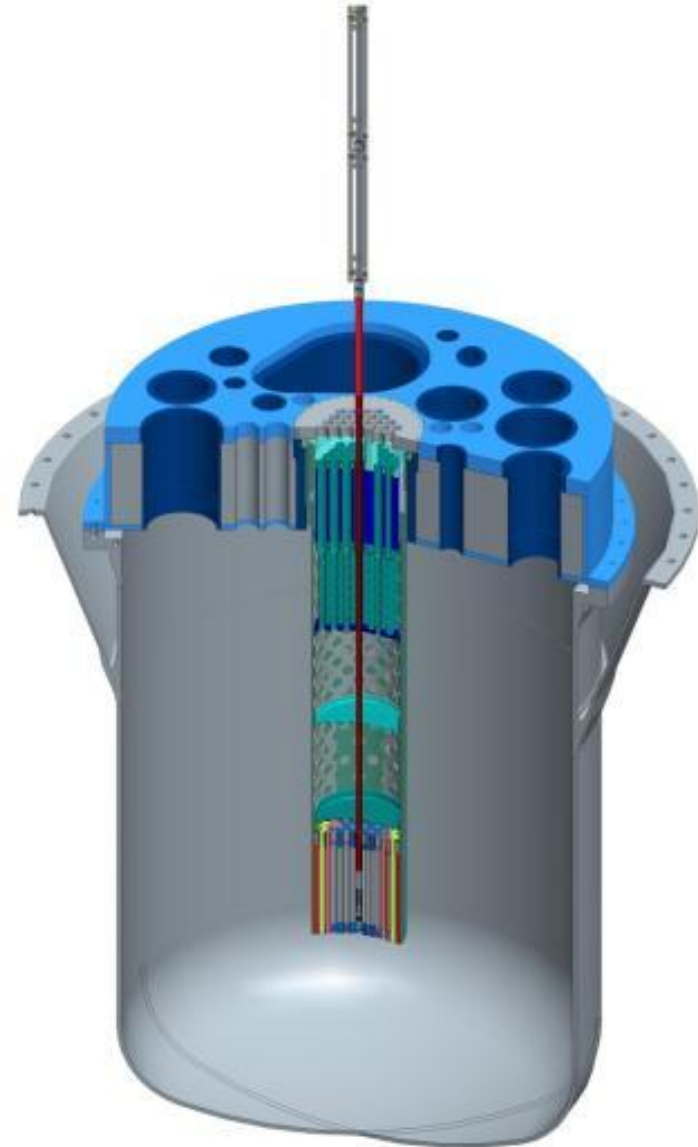


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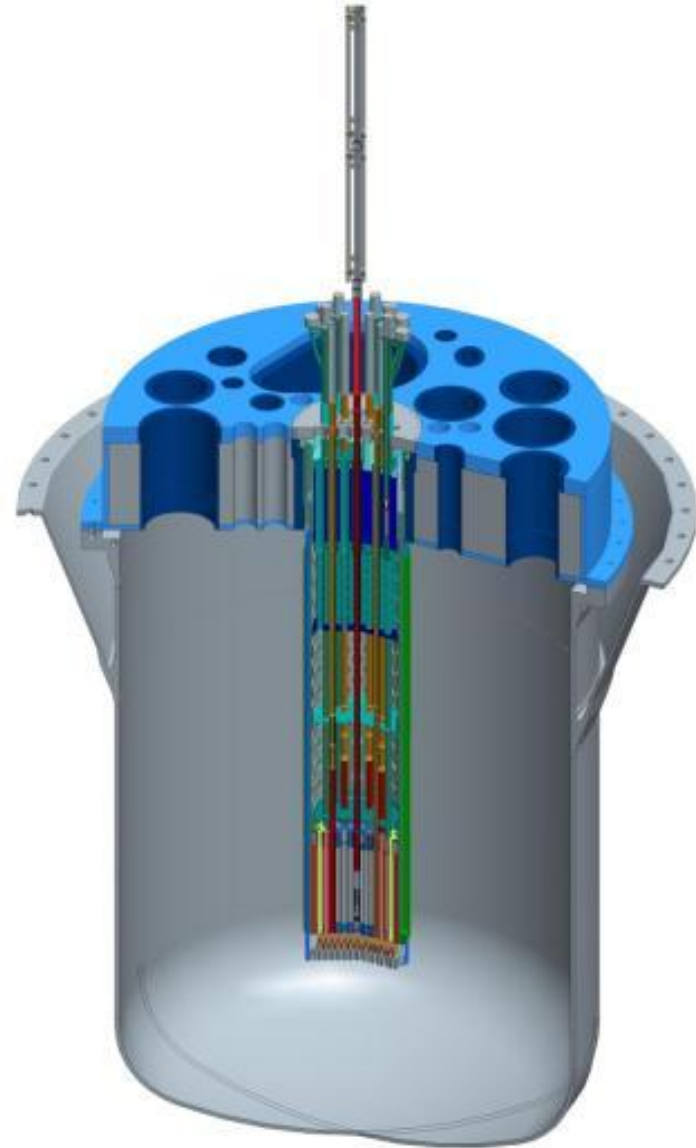
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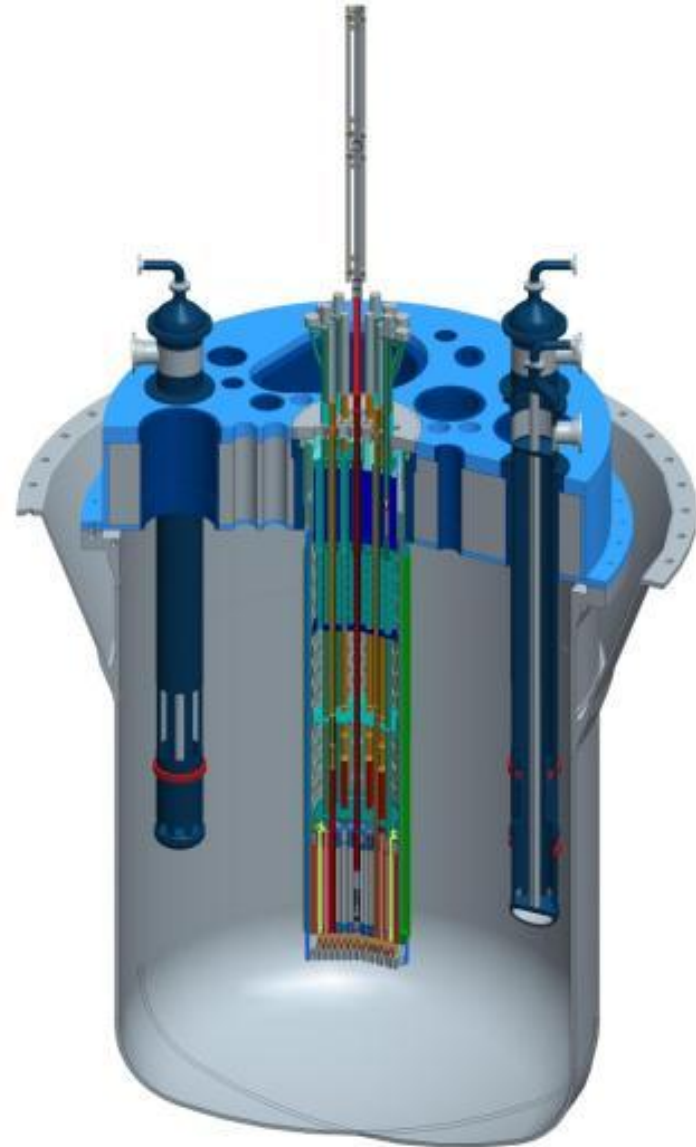


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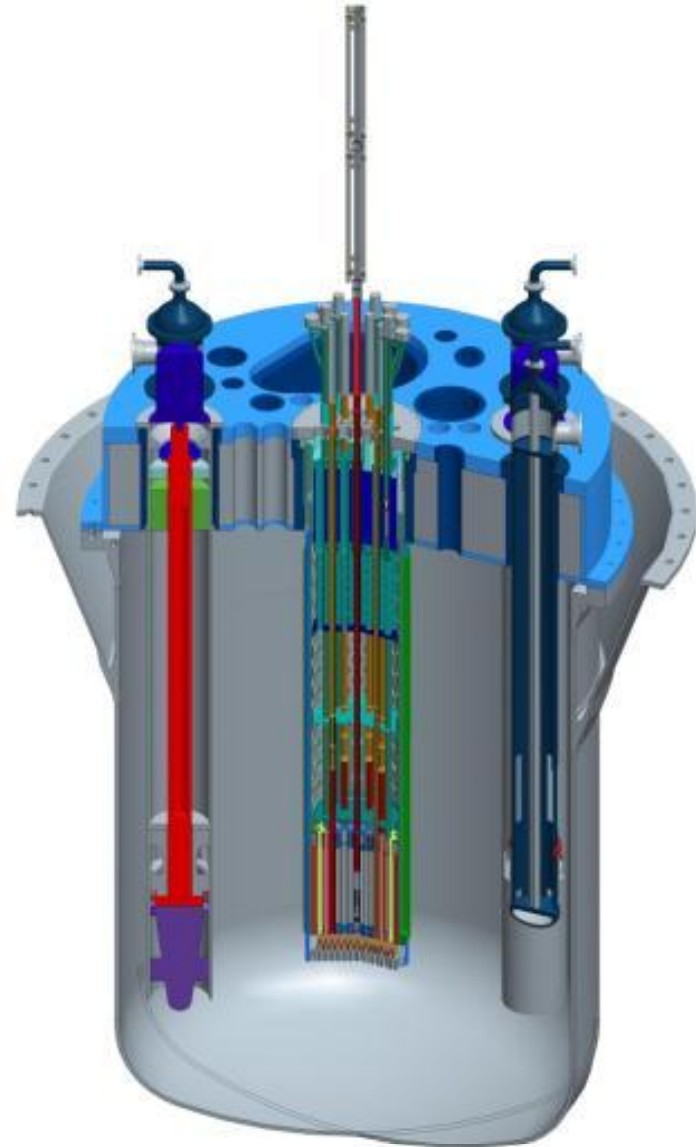
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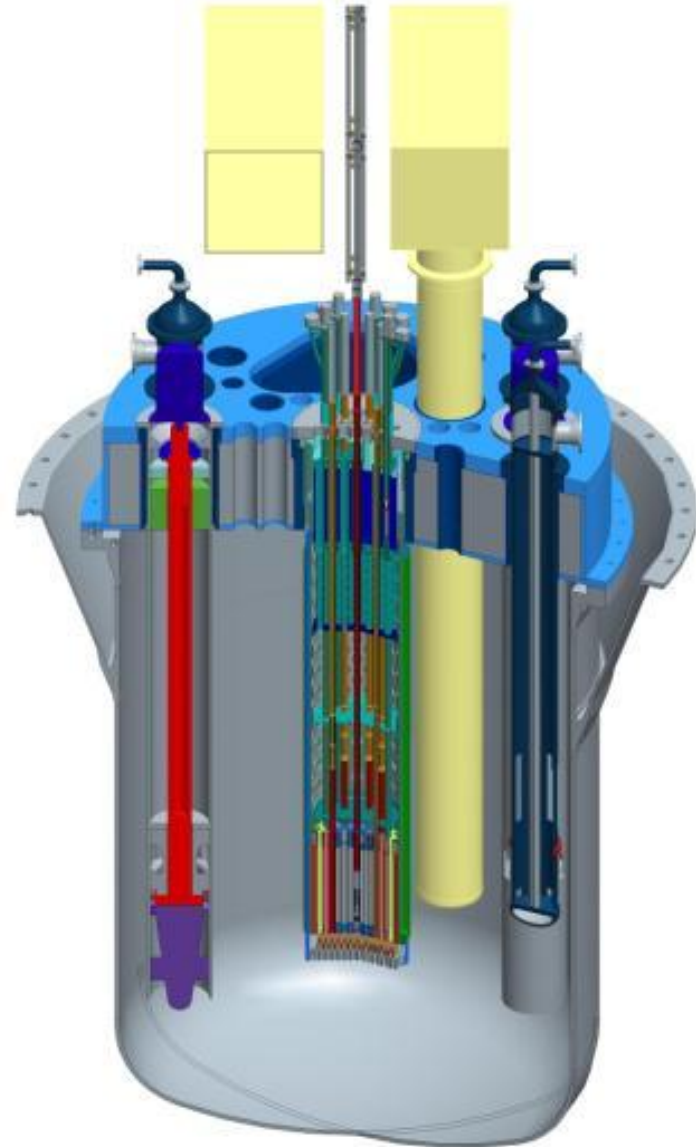
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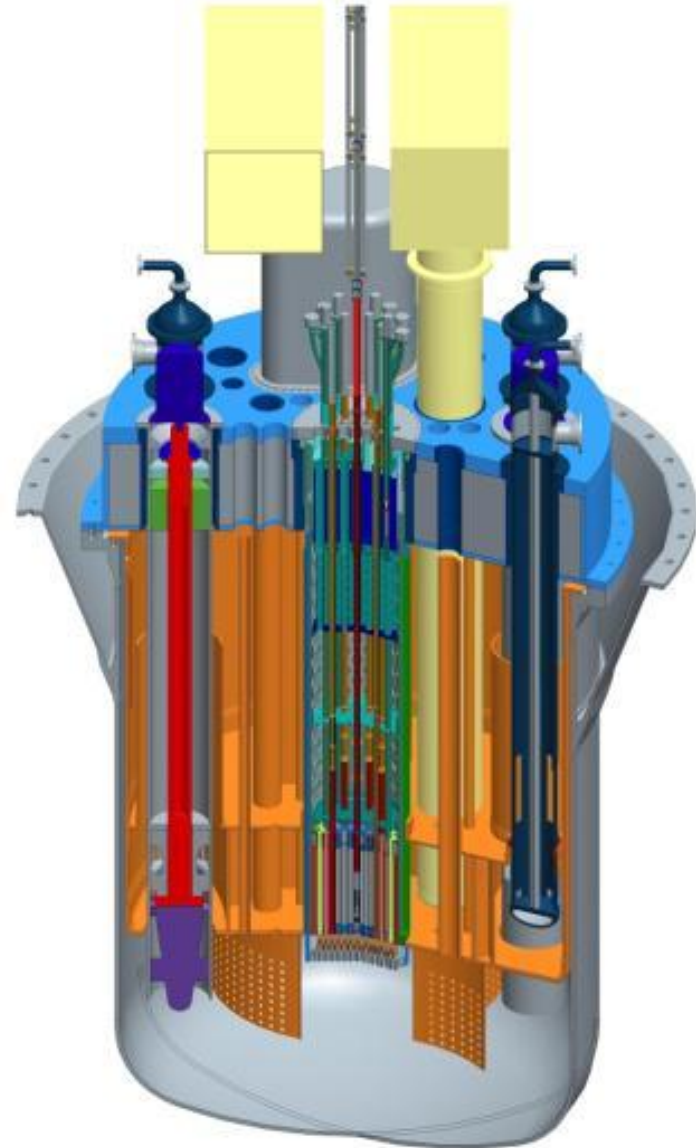
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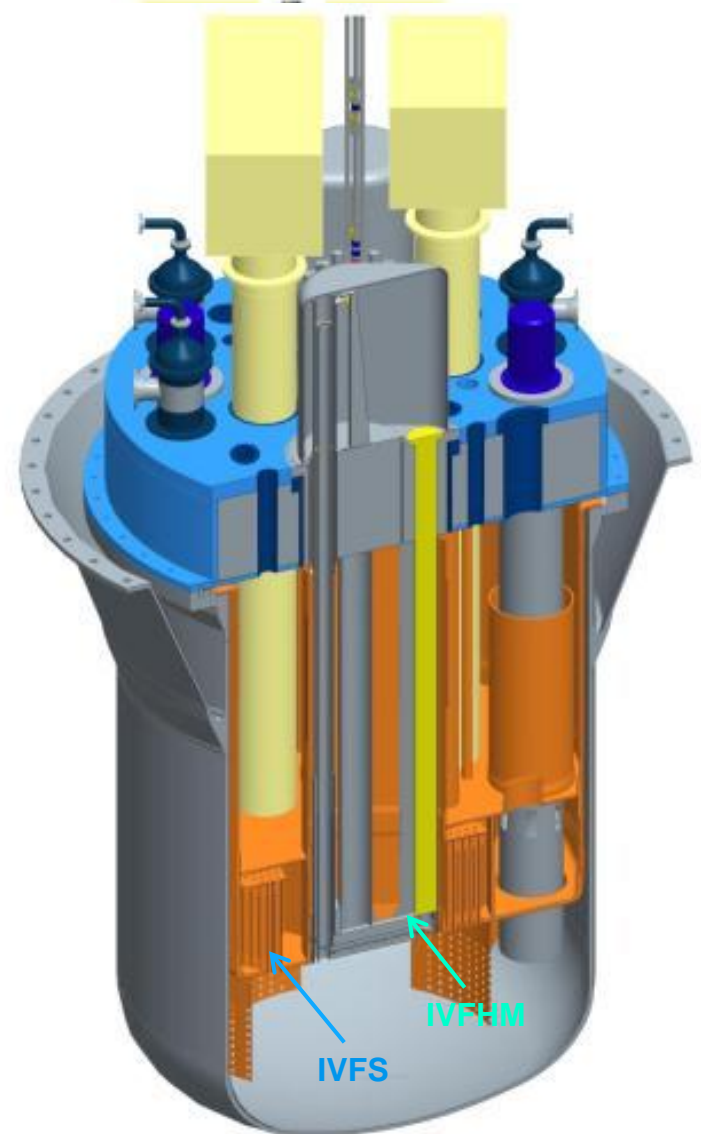
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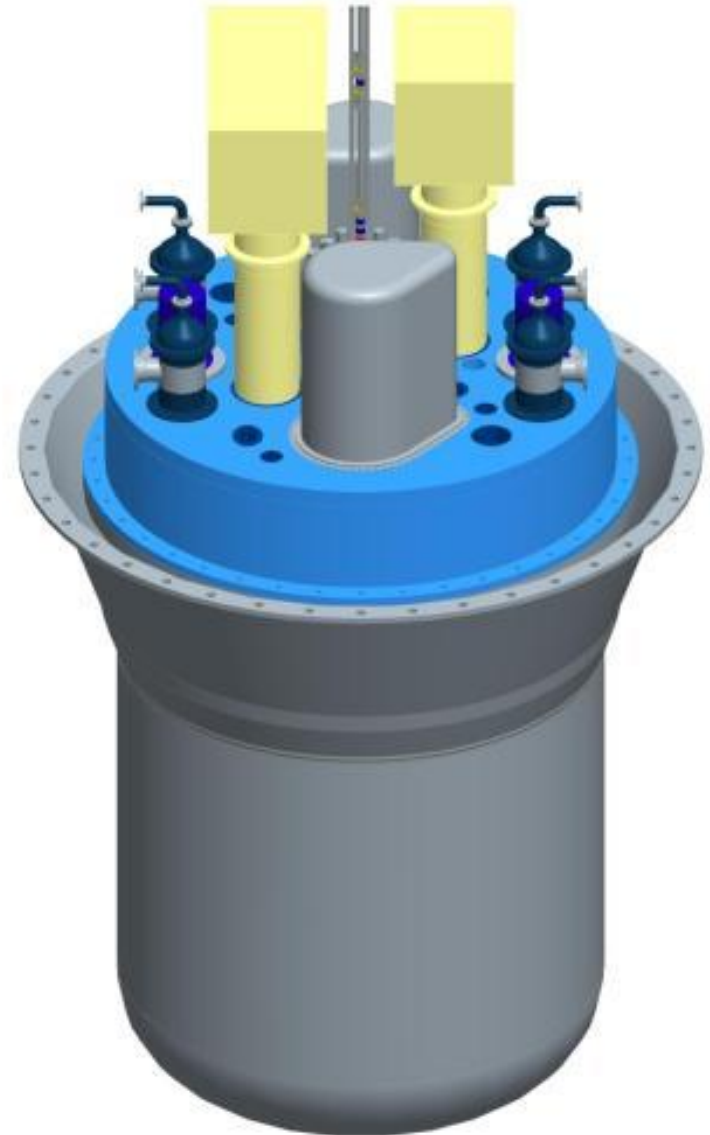
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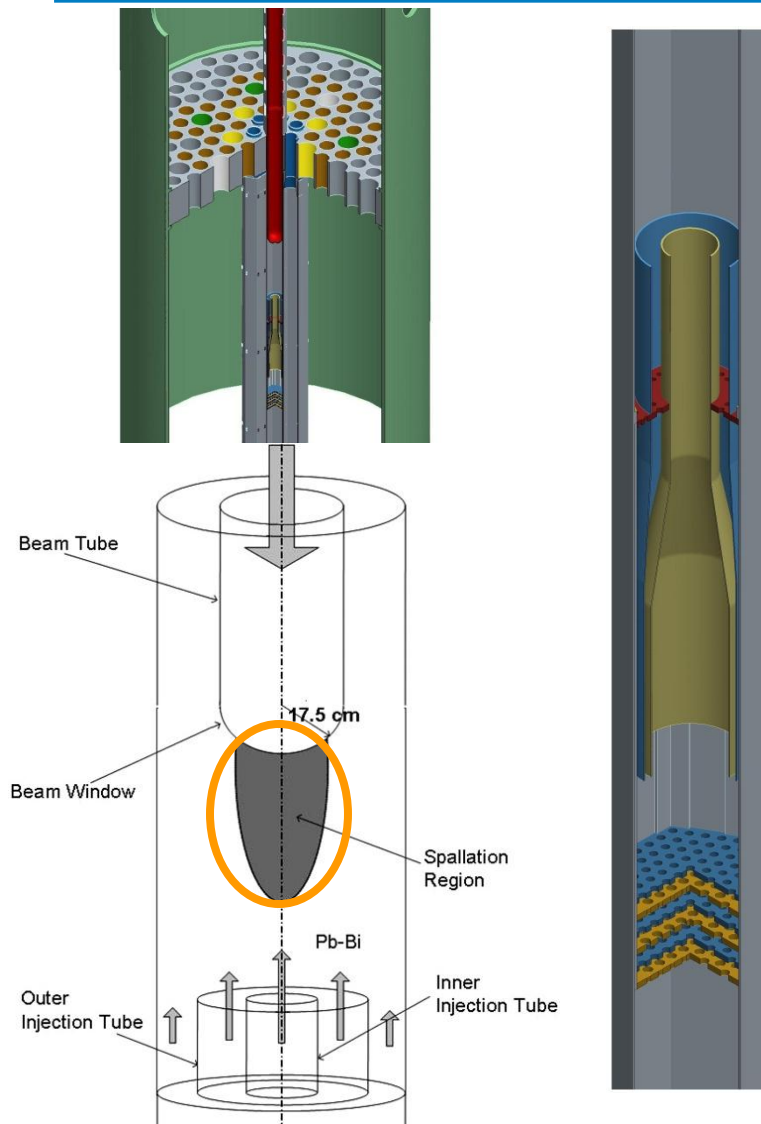


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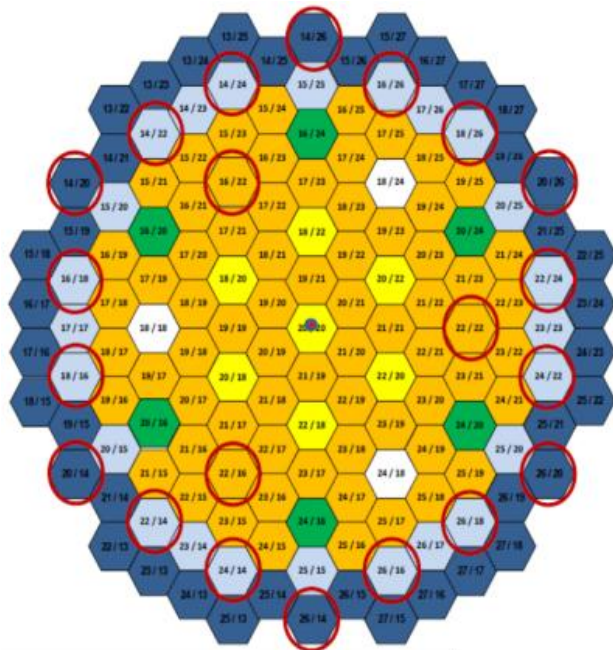


# Spallation target window in the reactor core



- Produces about  $10^{17}$  neutrons/s at the reactor mid-plane to feed subcritical core
- Fits into a central hole in core
  - Compact target
  - Remove produced heat
- Accepts megawatt proton beam
  - 600 MeV, 3.5 mA  $\rightarrow$   $\sim$ 2.1 MW heat
  - Cooling of window is feasible
- Material challenges
  - Preferential working temperature: 450 – 500° C
  - Service life of at least 3 full power months (1 cycle) is achievable

- 151 positions
- 37 multifunctional plugs



- 69 FAs
- 7 (central) IPS
- 6 CR (buoyancy)
- 3 SR (gravity)
- 24 "inner" Dummy (LBE)
- 42 "outer" Dummy (YZrO)
- 151 S/As

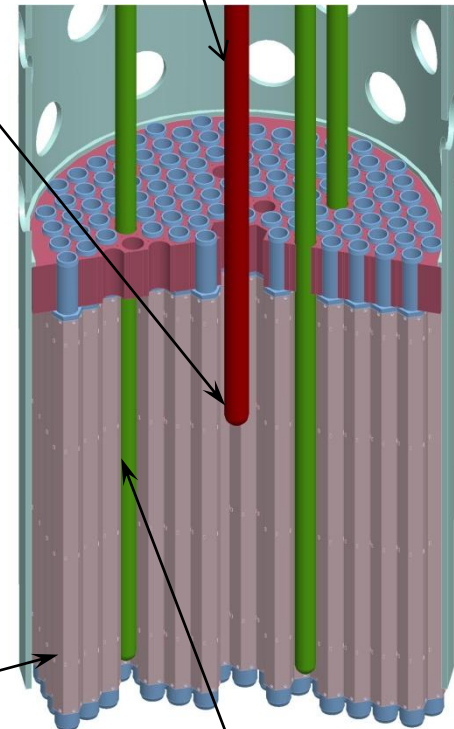
○ Additional positions available for inserts from the top (21/37)

**Both critical and subcritical configuration:**

- **Critical: 100 MWth**
- **Subcritical 85 MWth ( $k_{eff} \sim 0.96$ )**

**Spallation target**

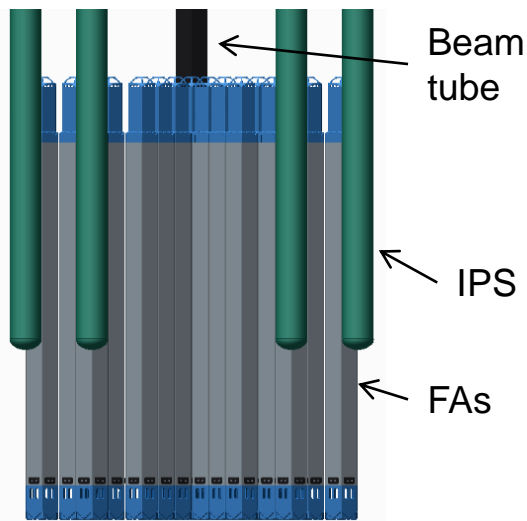
**Beam tube**



**Fuel Assemblies**

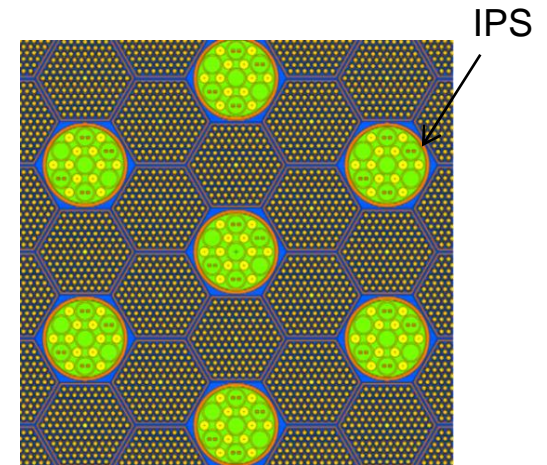
**IPS**

# IPS: Material Irradiation Performances for FR Reactors



Subcritical			
IPS	Total flux, $n/(cm^2s)$	Fast flux ( $> 0.75MeV$ ), $n/(cm^2s)$	Radiation damage, DPA/FPY
1	$2.64 \times 10^{15}$	$4.20 \times 10^{14}$	22.3
2	$2.72 \times 10^{15}$	$4.29 \times 10^{14}$	23.0
<b>3</b>	<b><math>2.75 \times 10^{15}</math></b>	$4.29 \times 10^{14}$	<b>23.1</b>
4	$2.72 \times 10^{15}$	$4.18 \times 10^{14}$	22.5
5	$2.70 \times 10^{15}$	<b><math>4.35 \times 10^{14}</math></b>	22.7
6	$2.68 \times 10^{15}$	$4.23 \times 10^{14}$	22.8

Critical				
Sample n°	IPS in Chan [0 0 0]		IPS in Chan [2 0 0]	
	dpa/FPY	$\Phi_{tot}$ ( $n/cm^2s$ )	dpa/FPY	$\Phi_{tot}$ ( $n/cm^2s$ )
8	18.1	$2.38E+15$	16.2	$2.12E+15$
7	23.0	$2.85E+15$	20.7	$2.54E+15$
6	25.9	$3.19E+15$	23.3	$2.85E+15$
5	27.5	$3.37E+15$	24.5	$3.02E+15$
4	27.2	<b><math>3.39E+15</math></b>	24.5	<b><math>3.03E+15</math></b>
3	25.7	$3.23E+15$	22.9	$2.89E+15$
2	22.3	$2.92E+15$	19.9	$2.62E+15$
1	17.3	$2.50E+15$	15.5	$2.23E+15$

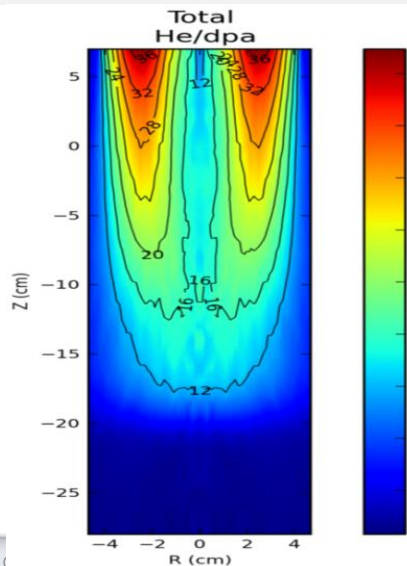
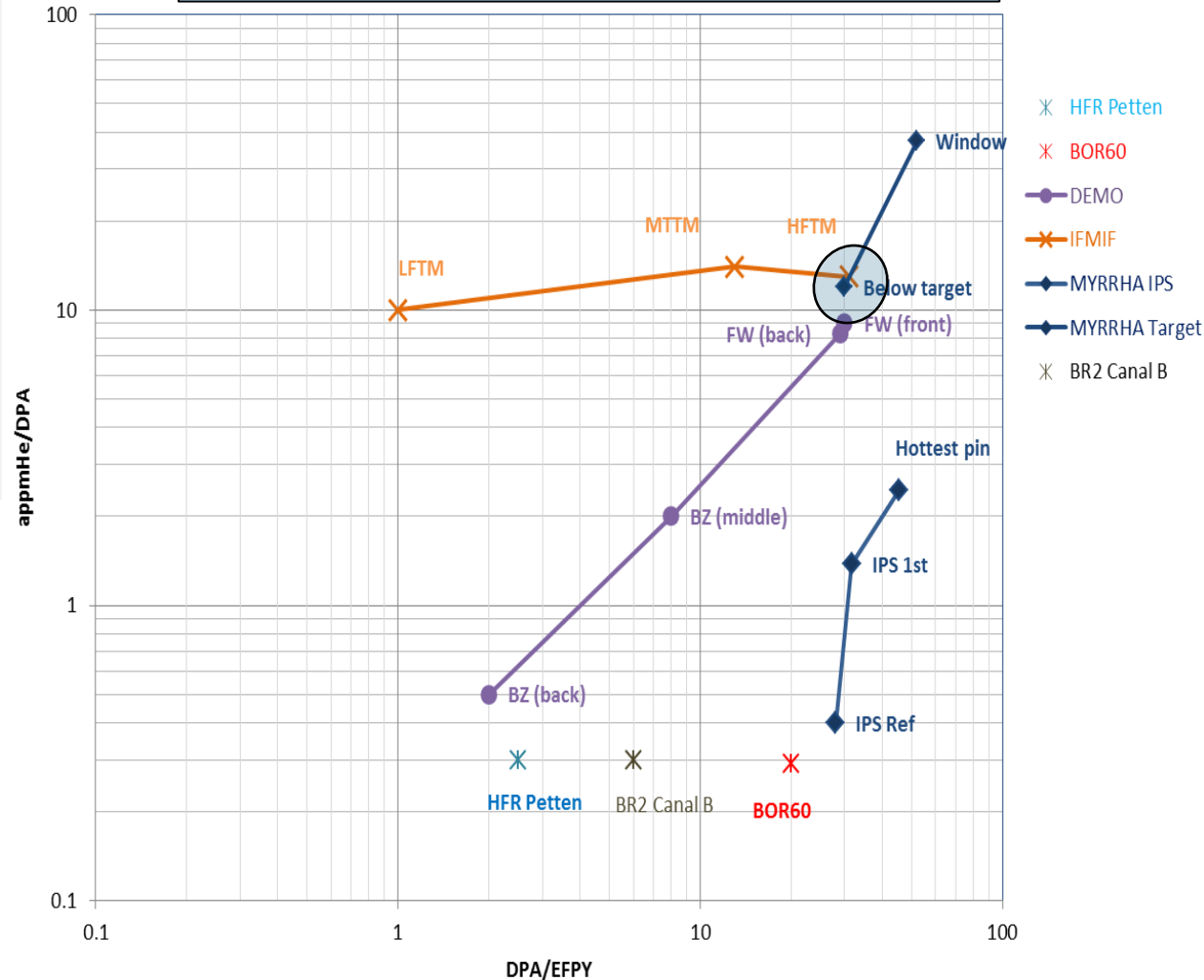




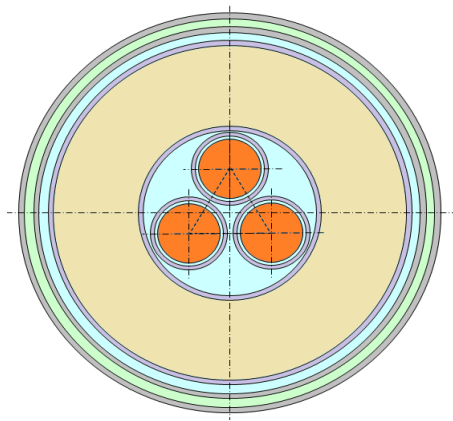
# MYRRHA-IFMIF for fusion materials

- In sub-critical ADS-mode:
  - high appmHe/dpa ratio,
  - close to the target window
- Volume of 1 lt with appmHe/dpa (Fe)  $\sim 12$ , close to the spallation target
- ➔ Useful volume
  - 30 lt** with range from 5 to 20 appmHe/dpa
- ➔ (Pre-)selection of materials for fusion application

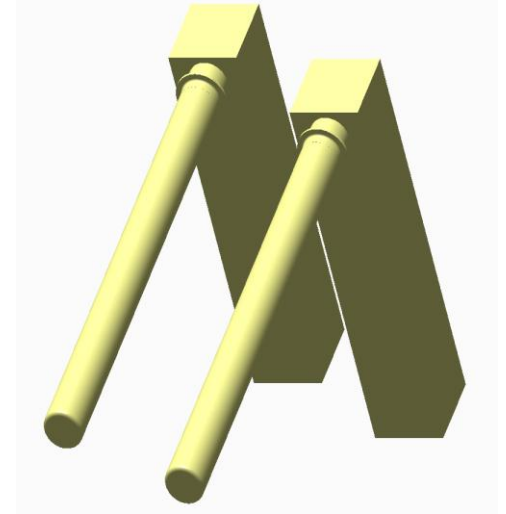
Estimated damage induced in DEMO and proposed irradiation conditions in IFMIF and MYRRHA-IFMIF



# Irradiation at low energy neutron flux: Silicon Doping



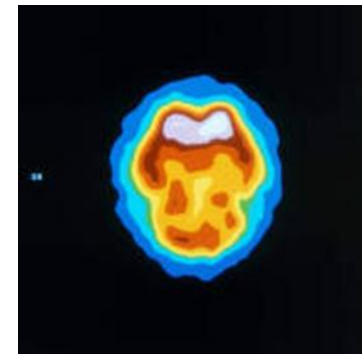
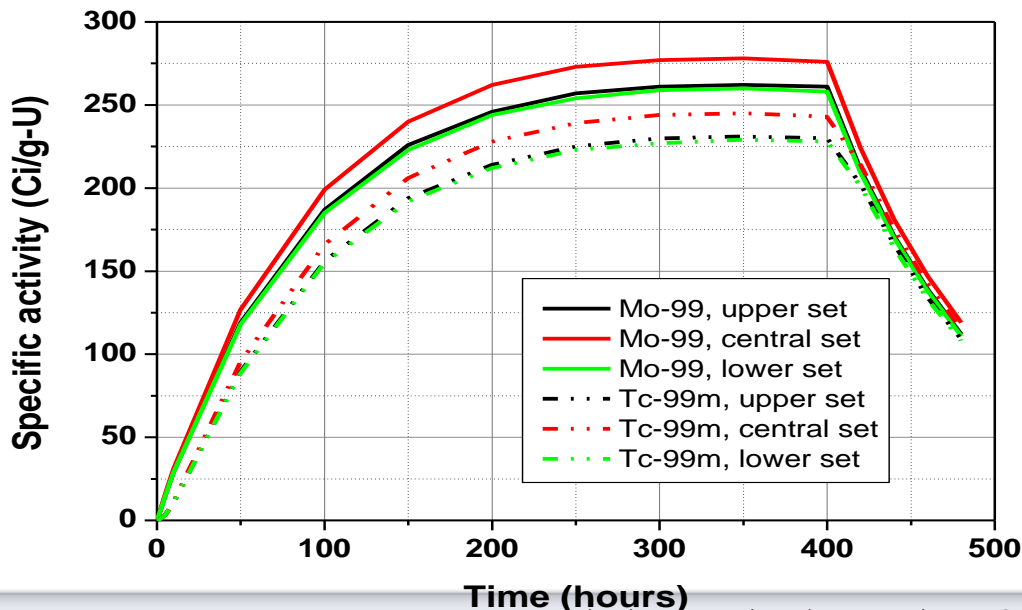
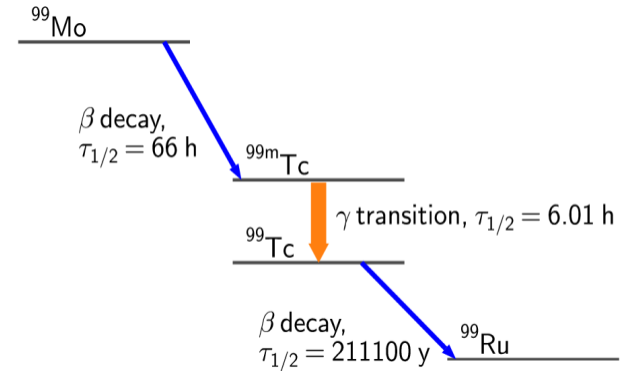
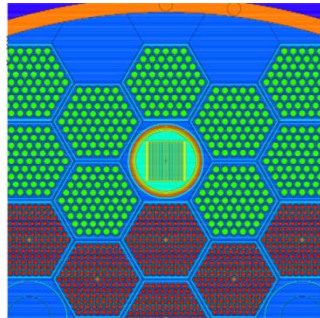
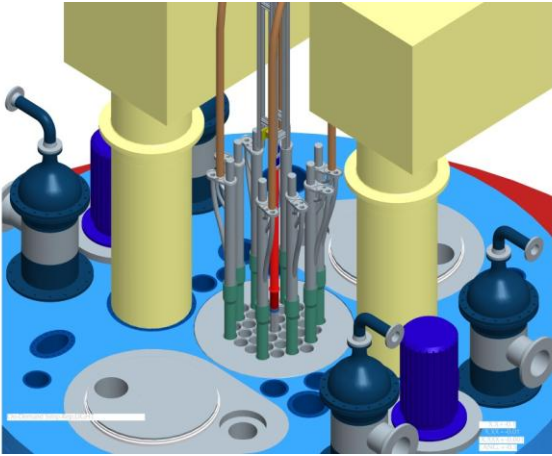
- Moderator (BeO)
- Si ingot (dia. 8 inch)
- water (coolant)
- Cadmium screen
- Stainlesssteel (AISI 316L)
- Aluminum Alloy (5754)



- Production:  $n$  (thermal) + Si  $\rightarrow$  P doped silicon (N-type)
- Silicon ingots are:
  - Huge: 8" in diameter
  - High: 200/250 mm
  - Massive: 10 to 35 Kg per ingot
- Raw material: Si (monocrystalline)



# Radioisotope (Mo-99) production capability



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