



# The Neutron Time-of-Flight facility GELINA at IRMM

*J. Heyse*

*EC – JRC – IRMM*

*Standards for Nuclear Safety, Security and Standards (SN3S)*

*[jan.heyse@ec.europa.eu](mailto:jan.heyse@ec.europa.eu)*

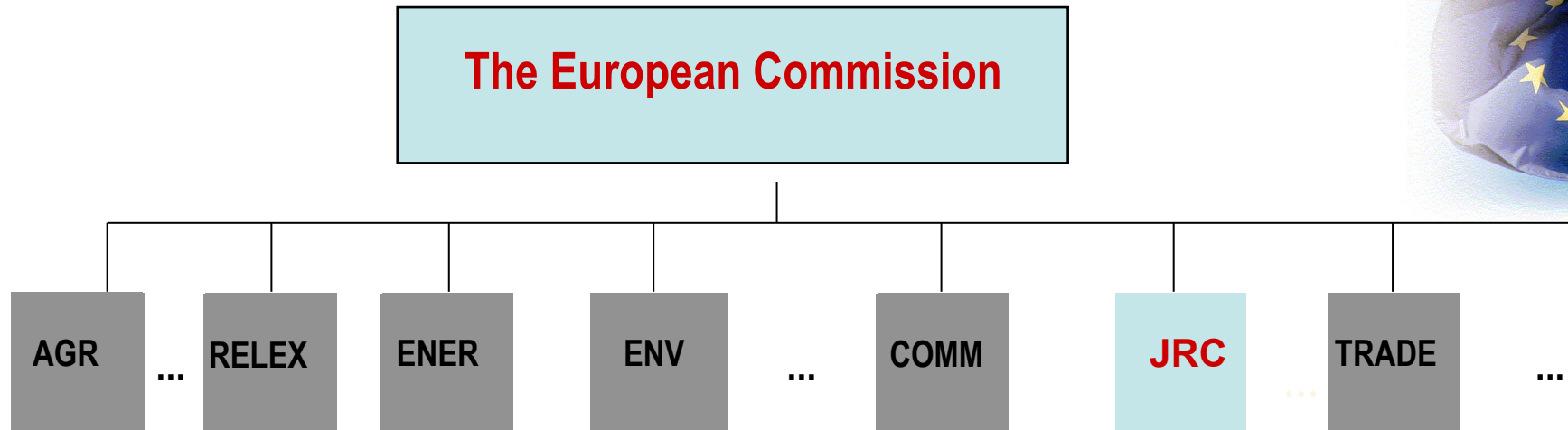
*10 June 2013, Frascati*



- **IRMM**
- **GELINA**
- **Neutron cross section measurements at GELINA**

- **IRMM**
  - **EC – JRC**
  - **Nuclear Data**
- **GELINA**
- **Neutron cross section measurements at GELINA**

# European Commission (EC)



**A research based,  
policy support Institution**

Scientific support of the  
decision-taking process in the EU

# Joint Research Centre (JRC)



7 Institutes in 5 Member States  $\cong$  2700 staff



**IE** - Petten The Netherlands  
-Institute for Energy



**IRMM** - Geel Belgium  
- **Institute for Reference Materials and Measurements**



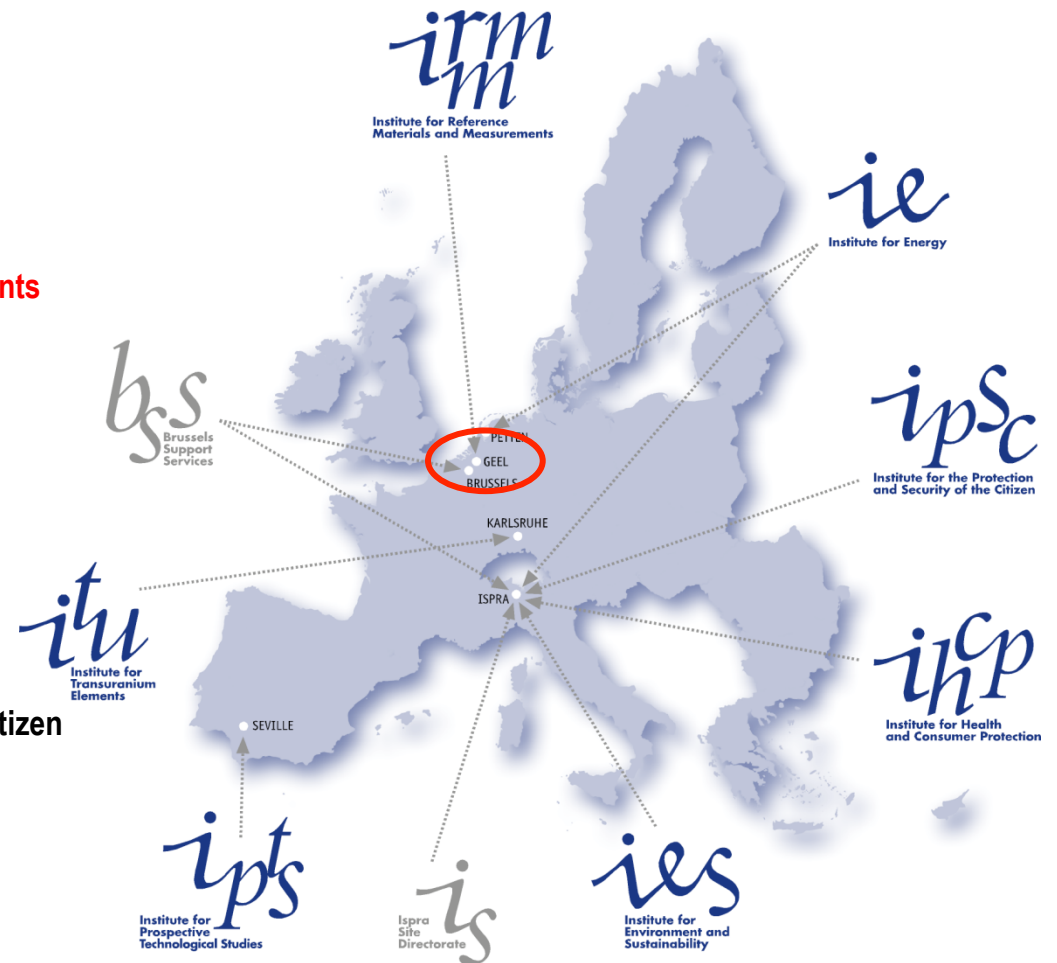
**ITU** - Karlsruhe Germany  
- Institute for Transuranium Elements



**IPSC - IHCP - IES** - Ispra Italy  
- Institute for the Protection and Security of the Citizen  
- Institute for Health and Consumer Protection  
- Institute for Environment and Sustainability



**IPTS** - Seville Spain  
- Institute for Prospective Technological Studies



# Institute for Reference Materials and Measurements (IRMM)



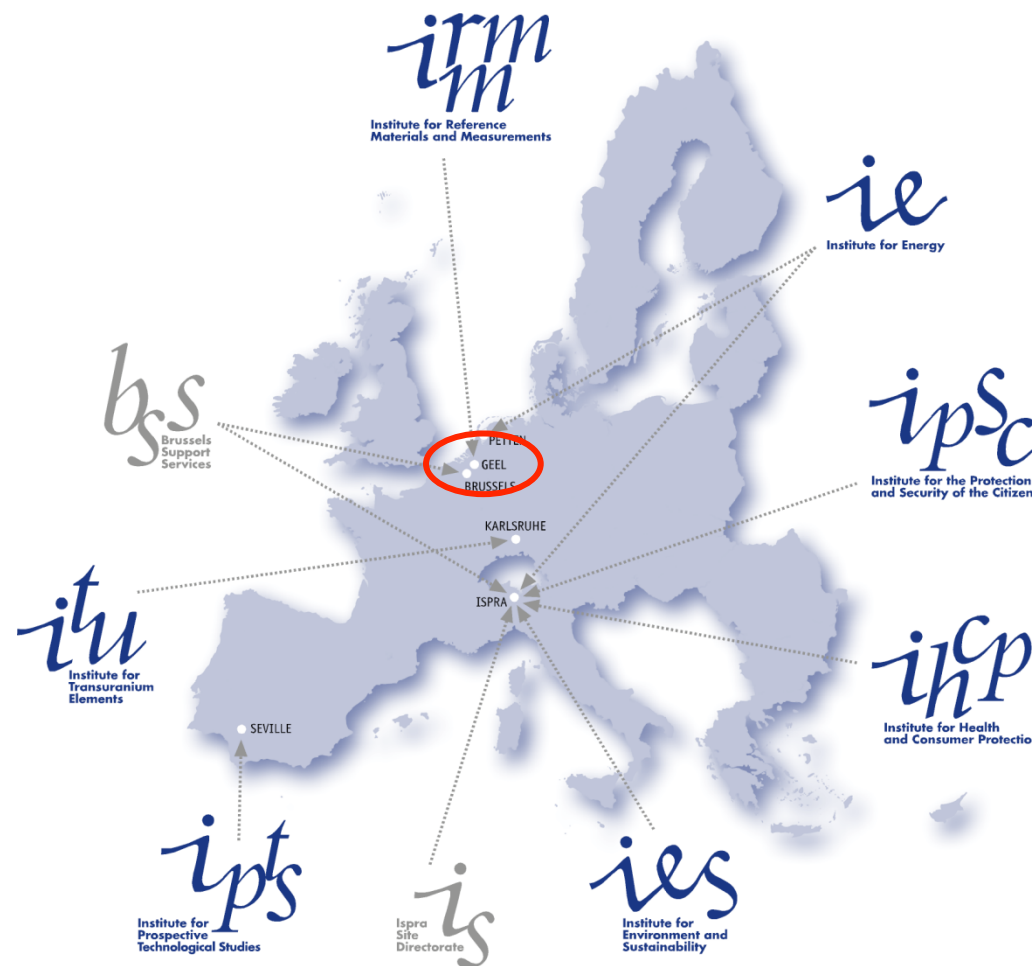
## Mission:

to promote a **common and reliable European measurement system** and to provide science-based advice for EU policies

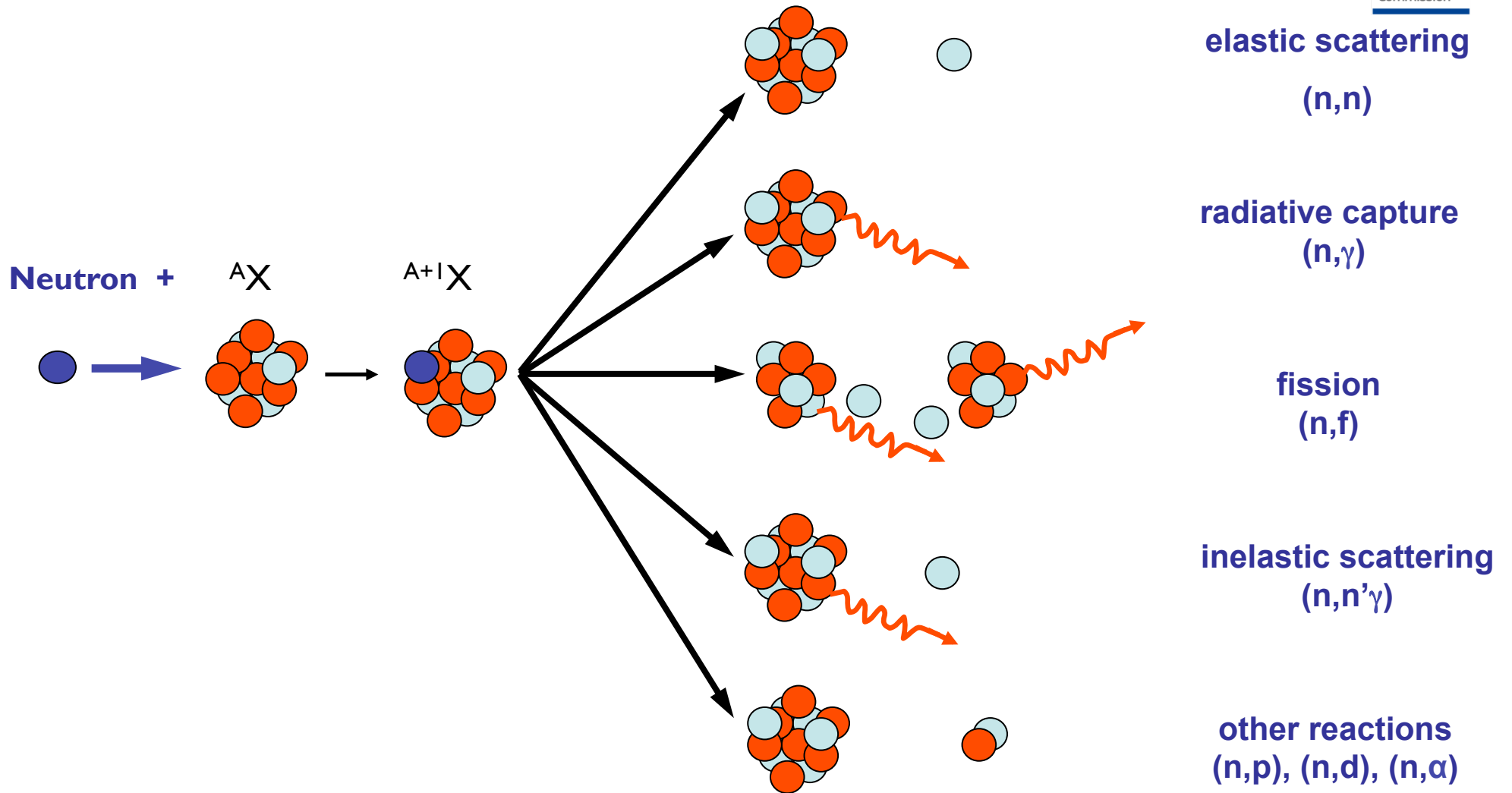
## Four research units:

- Standards for Innovation and Sustainable Development
- Knowledge Transfer and Standards for Security
- Food Bioscience Standards
- Standards for Nuclear Safety, Security and Safeguards (SN3S)

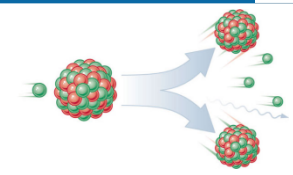
➔ **Nuclear Data**



# Neutron induced reactions



# Reactor calculations



MEASUREMENT

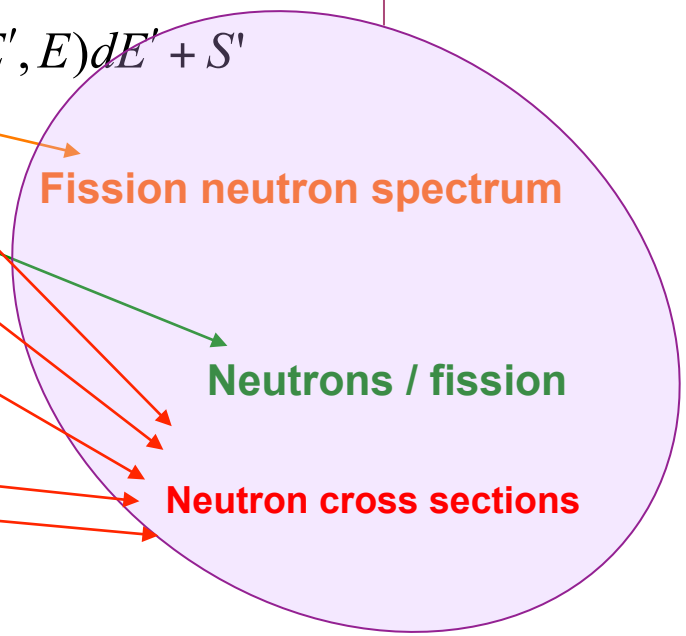
- Boltzmann equation: neutron balance

$$\frac{1}{v} \frac{\partial f}{\partial t} + \Omega \cdot \nabla f + f \sum_i N_i \sigma_{T,i} = S + \int f(E', \Omega') \sum_s (E' \rightarrow E, \Omega' \rightarrow \Omega) dE' d\Omega'$$

$$S = \sum_i N_i \int f(E) \bar{\nu}_i(E') \sigma_{F,i}(E') \chi_{P,i}(E', E) dE' + S'$$

- Bateman equation: nuclide inventories

$$\frac{dN_i}{dt} = -\lambda_i N_i - N_i \int \sigma_{a,i} f dE d\Omega + \sum_{j \neq i} \lambda_j p_{j \rightarrow i} + \int \sigma_{a,i \rightarrow j} f dE d\Omega$$

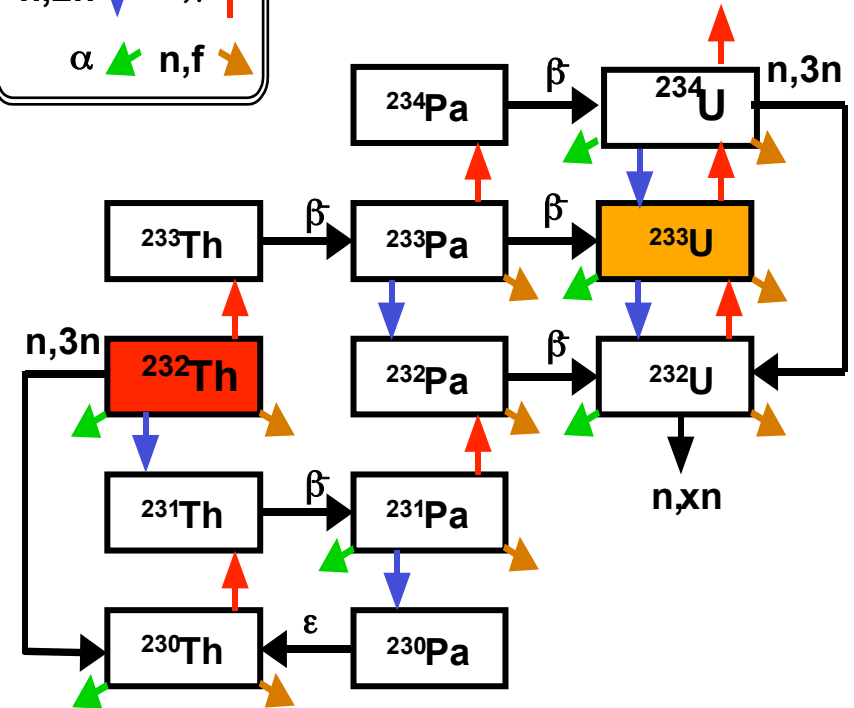
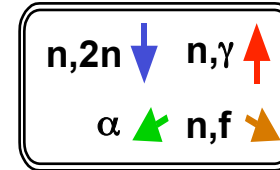




# Nuclear data for reactor technology

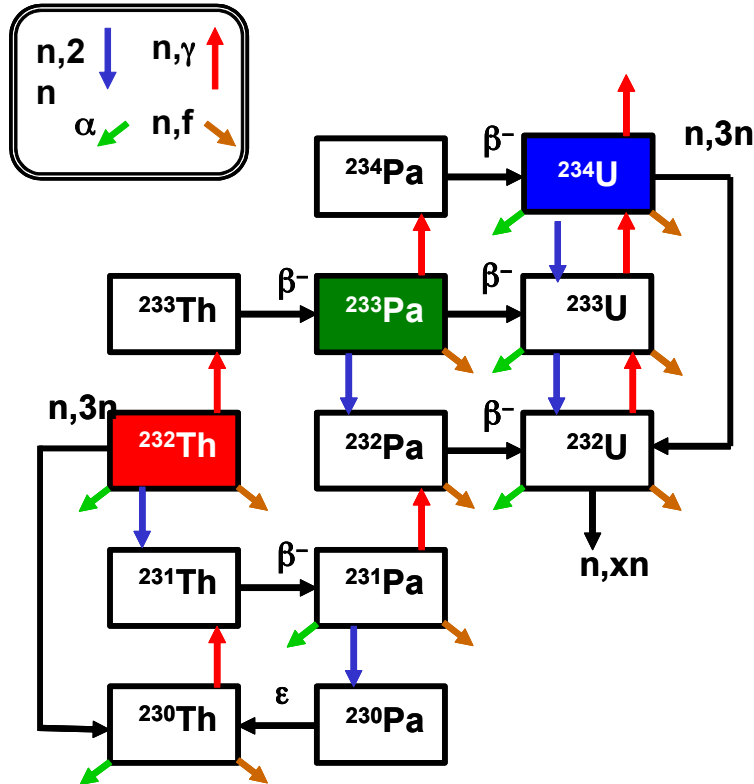


*e.g. Th-U cycle*



- **Nuclear Fuel**  
U, Pu, Th, ...       $(n,f), (n,\gamma), \nu$
  - **Fission Products**  
 $^{103}\text{Rh}, ^{135}\text{Xe}, ^{135}\text{Cs}, ^{149}\text{Sm}, \dots$        $(n,\gamma)$
  - **Neutron absorbers**  
Cd, Hf,       $(n,\gamma)$
  - **Structural Materials**  
Fe, Cr, Ni, Zr, ...       $(n,n), (n,n', \gamma)$
- + Standard cross sections

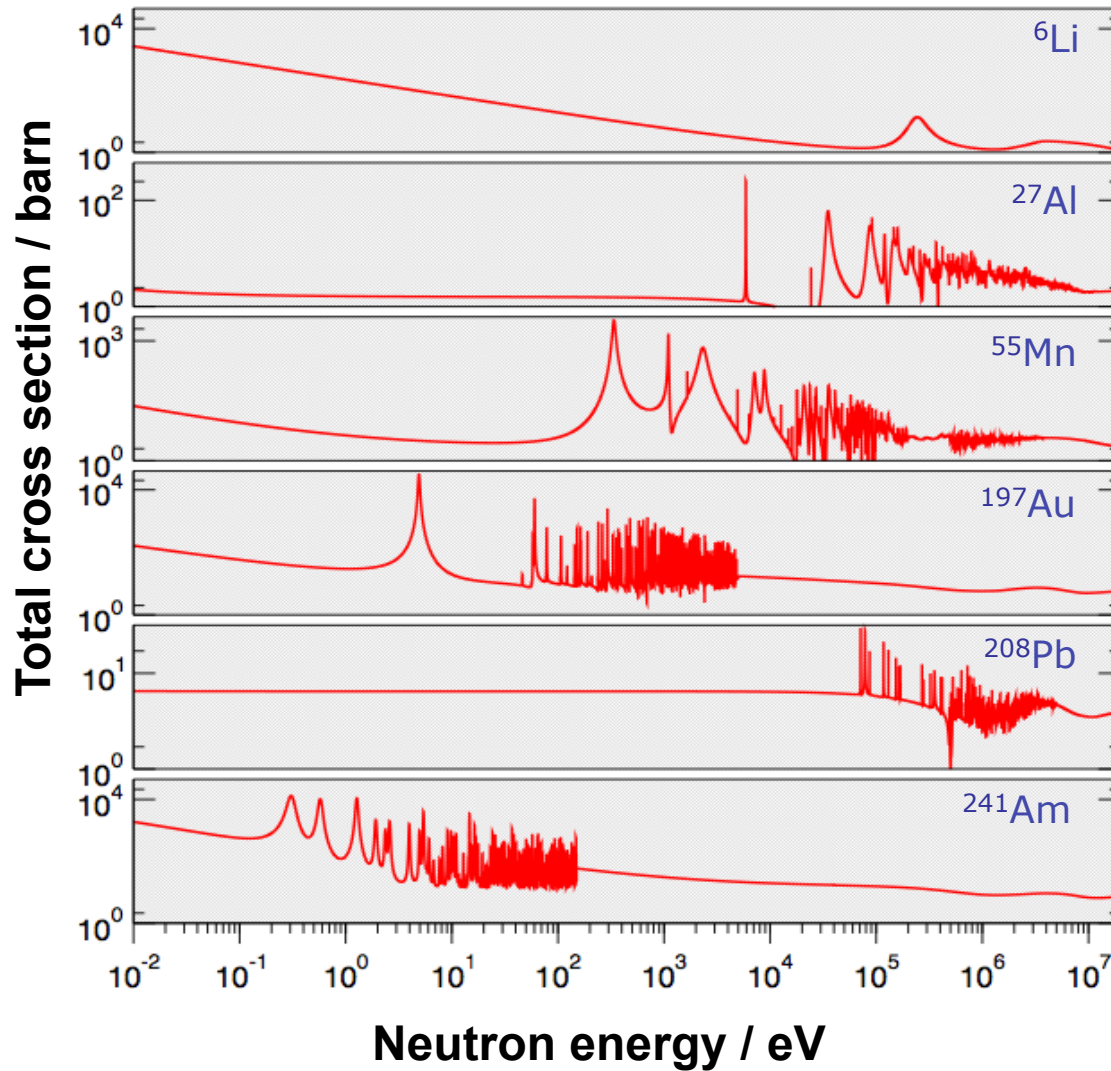
# Thorium – Uranium fuel cycle



Nuclide	Reaction	Accuracy (%)
$^{232}\text{Th}$	total	3
	(n, $\gamma$ )	1-2
$^{233}\text{Pa}$	(n, f)	20
$^{234}\text{U}$	(n, f)	3
$^{236}\text{U}$	(n, f)	5

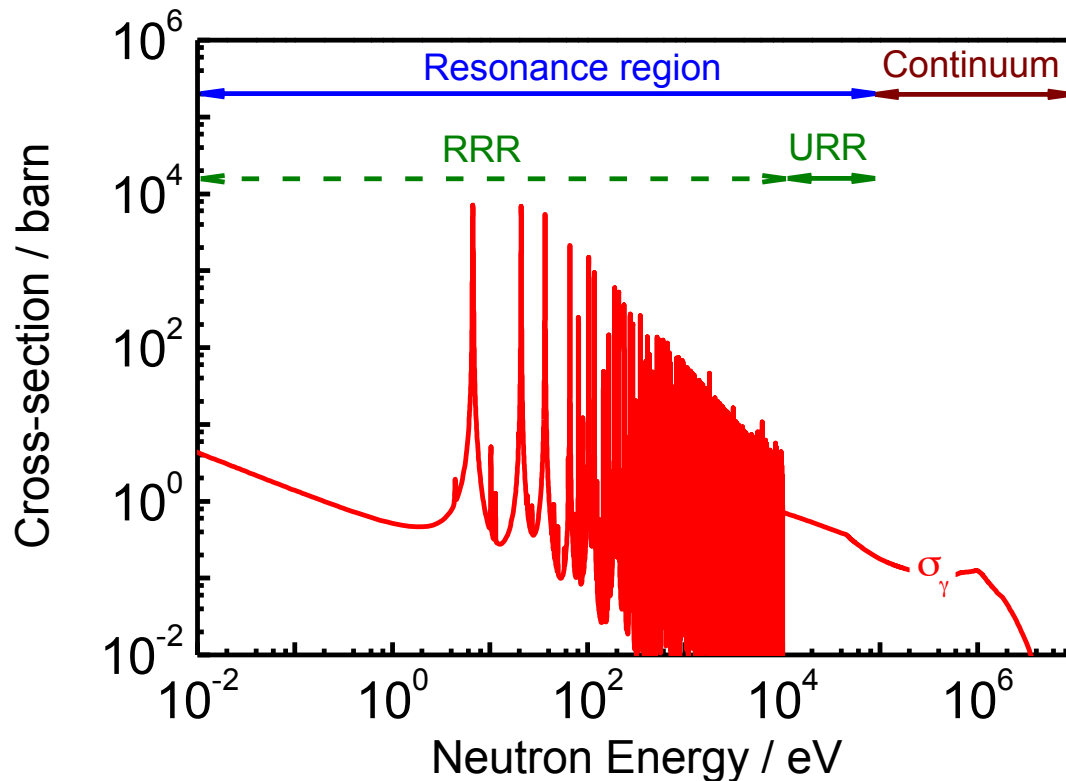
- 2 % uncertainty on  $\sigma_\gamma$  for  $^{232}\text{Th}(n, \gamma) \Rightarrow$  1% uncertainty on  $^{233}\text{U}$  production rate
- 10 % uncertainty on  $\sigma_\gamma$  for  $^{232}\text{Th}(n, \gamma) \Rightarrow$  30% uncertainty on proton current to operate ADS with a  $k_{\text{eff}} \approx 0.97$

# Cross section



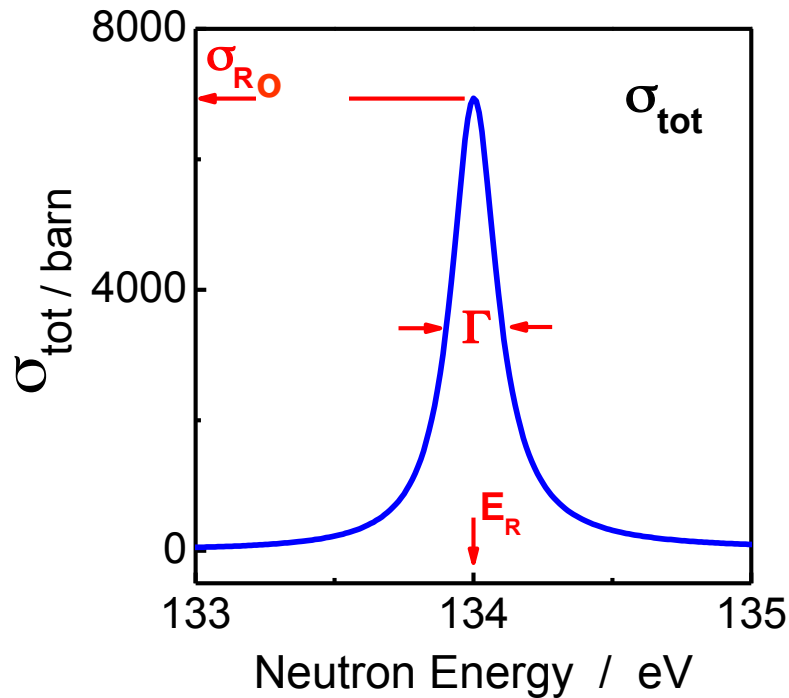
**Resonances appear at energies, which are specific for each nuclide**

# Neutron Induced Reactions



- **Resonance Region** :  $D > \Gamma$ 
    - **Resolved Resonance Region**  
 $\Delta_R < D$
    - **Unresolved Resonance Region**  
 $\Delta_R > D$
  - **Continuum** :  $D < \Gamma$   
(fast, high energy)
- $\Gamma$  : level width  
 $D$  : level distance  
 $\Delta_R$  : **resolution**

# Resonance structure



- Cross sections as a function of  $E_n$  reveals a resonant structure
- Breit-Wigner shape :

$$\sigma_{\text{tot}} \sim \frac{1}{(E_n - E_R)^2 + (\Gamma/2)^2}$$

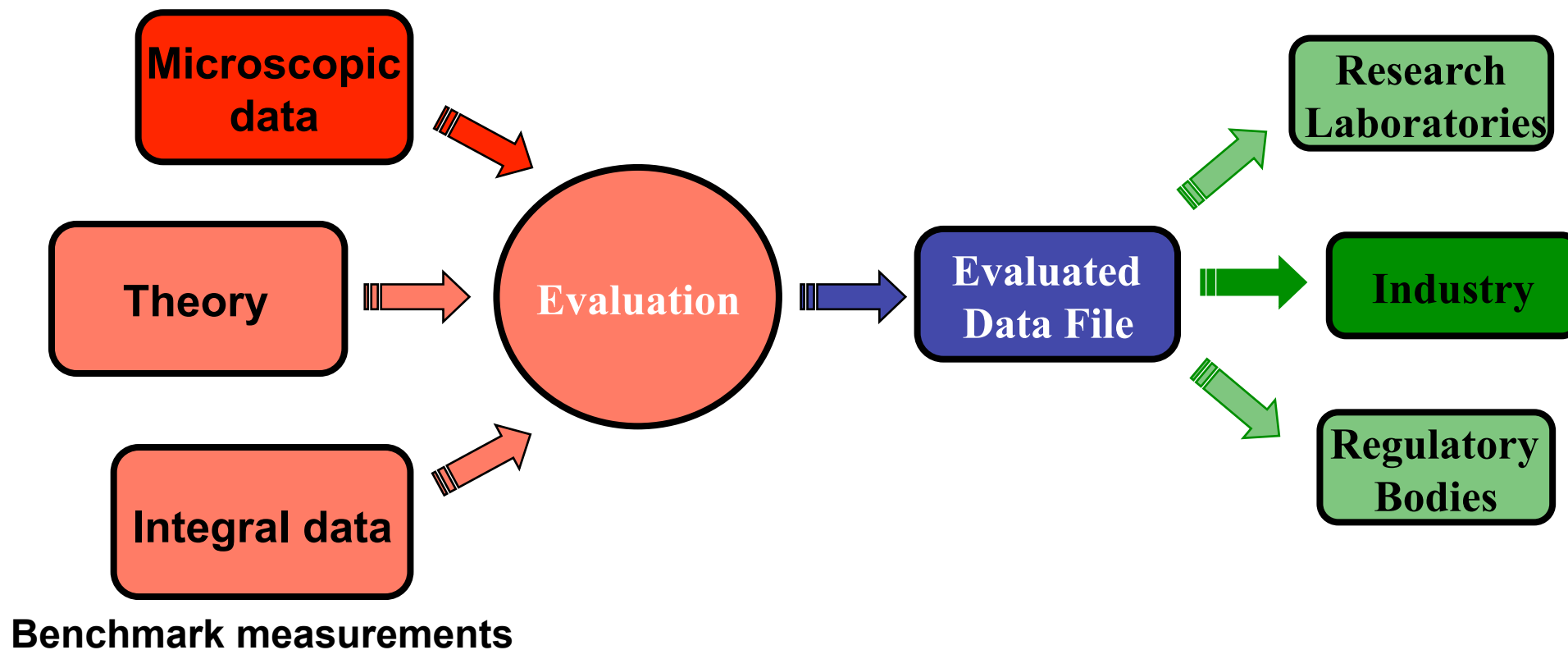
- $E_R$  resonance energy
- $\Gamma$  total width
- $\Gamma_n, \Gamma_\gamma$  partial widths
- $\Gamma = \Gamma_n + \Gamma_\gamma + \dots$

$(E_r, J^\pi, \Gamma_n, \Gamma_\gamma, \dots)_j$  can not be predicted by theory

Determination of RP requires a combination of complimentary experimental data

⇒ TOF-facility GELINA

# Cross sections result of evaluation process





- IRMM
- **GELINA**
  - **Neutron production**
  - **Time of flight facility**
- Neutron cross section measurements at GELINA

# JRC – IRMM : neutron facilities



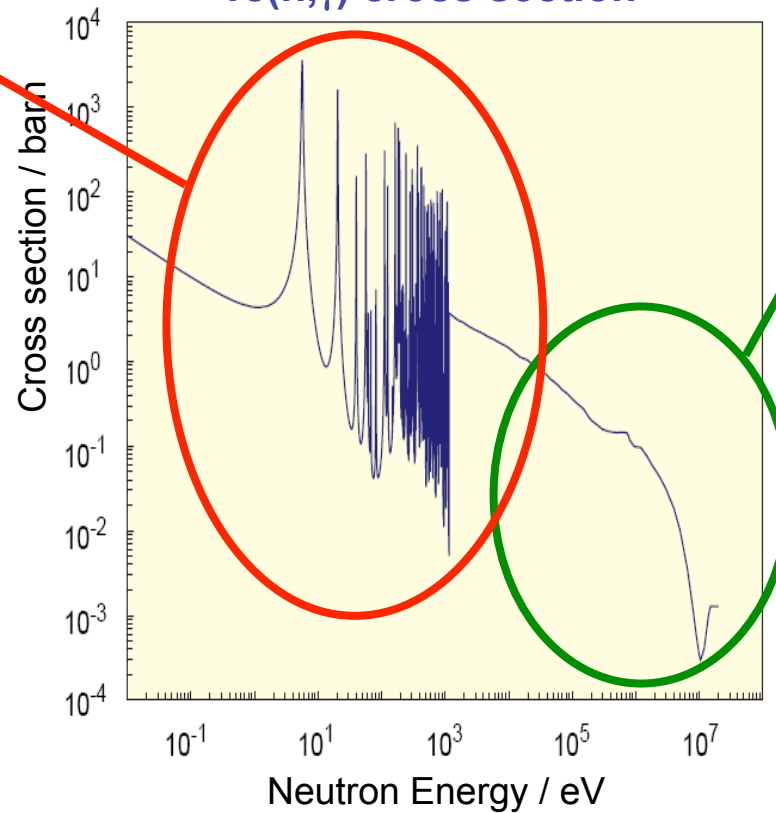
**GELINA**



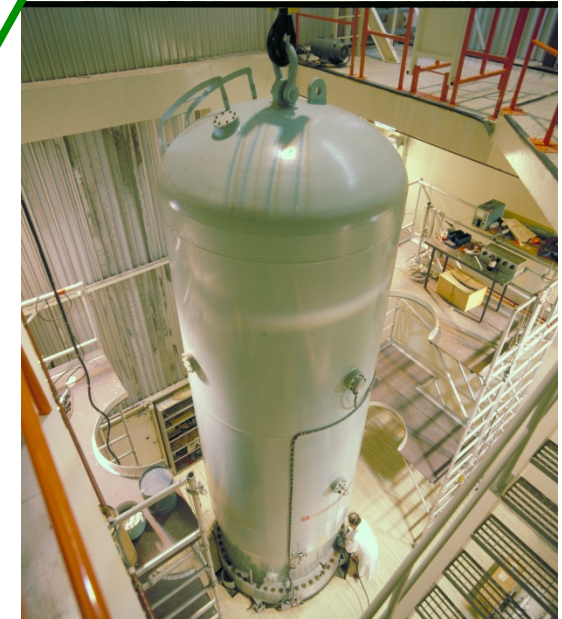
**White neutron source  
+  
Time-of-flight (TOF)**

**$\sim 3.4 \cdot 10^{13}$  n/s  
(integrated)**

$^{99}\text{Tc}(n,\gamma)$  cross section



**Van de Graaff**

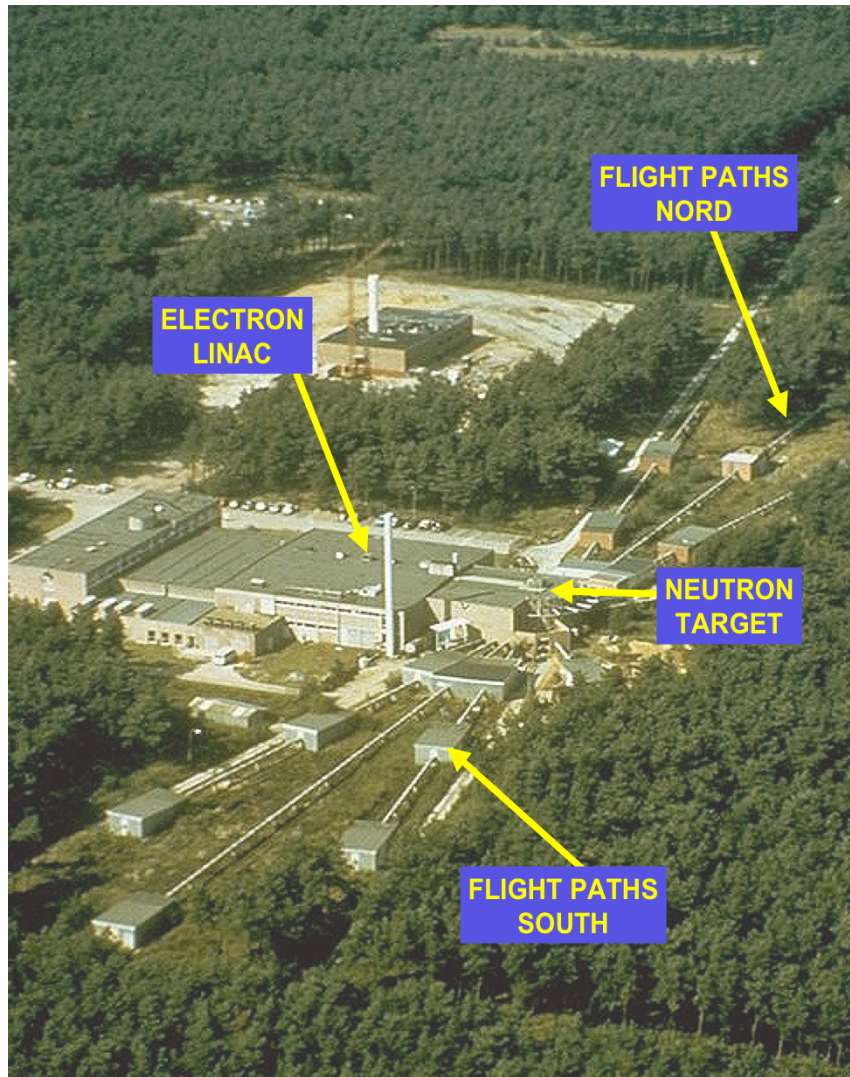


**Mono-energetic neutrons  
(cp,n) reactions**

**$\sim 10^6$  n/s/cm<sup>2</sup>  
(10 cm from target)**

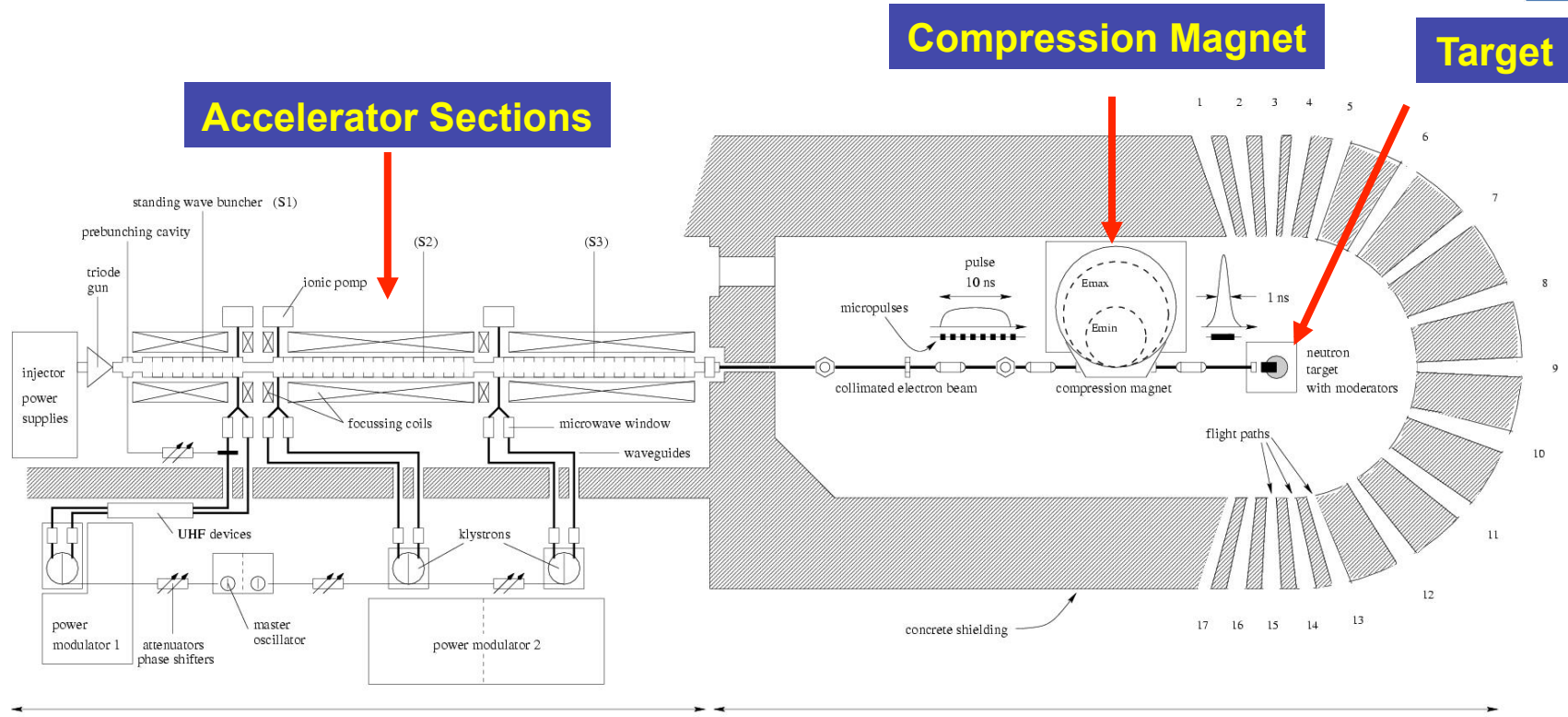


# TOF - Facility GELINA



- Pulsed white neutron source  
( $10 \text{ meV} < E_n < 20 \text{ MeV}$ )
- Neutron energy : time-of-flight (TOF)
- Multi-user facility: 12 flight paths  
( $10 \text{ m} - 400 \text{ m}$ )
- Measurement stations with special equipment to perform:
  - Total cross section measurements
  - Partial cross section measurements

# Accelerator

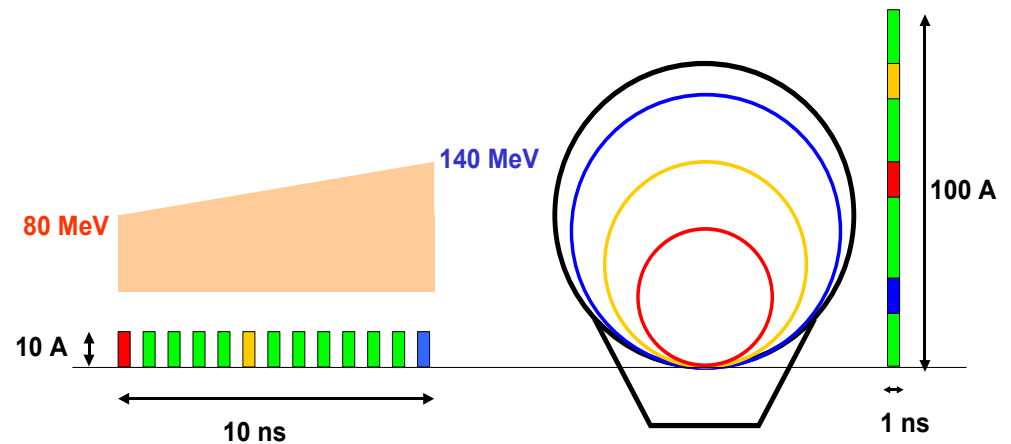
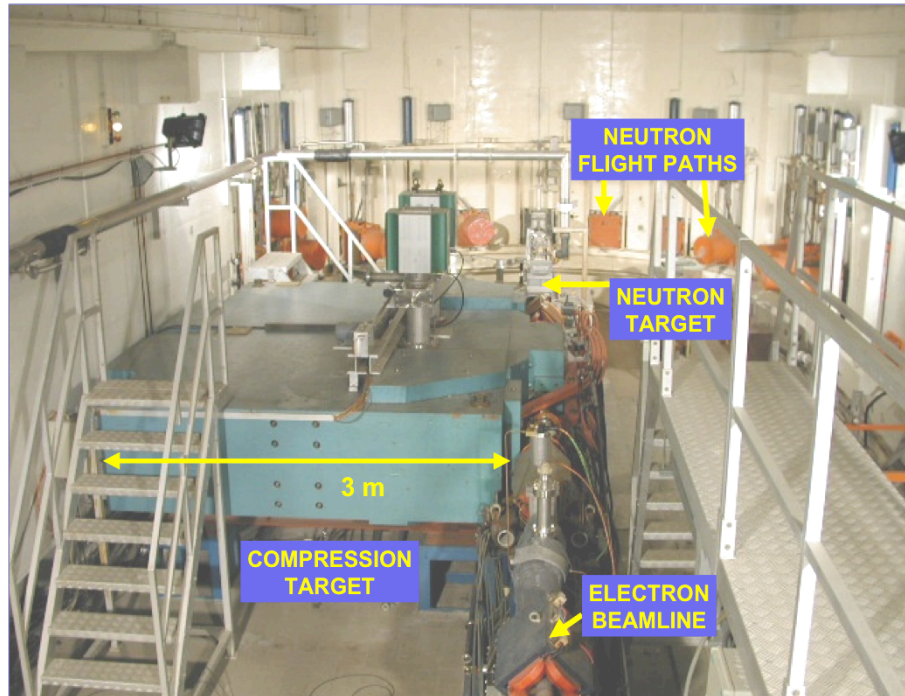


## Normal Operating Parameters

Average Current : 75  $\mu$ A  
 Average Electron Energy : 100 MeV  
 Mean Power : 7.5 kW

Frequency : 800 Hz  
 Pulse Width : 1 ns  
 Neutron Flux :  $3.4 \times 10^{13}$  n/s

# Compression magnet



$$B\rho = \frac{p}{q}; E \cong pc; q = e$$

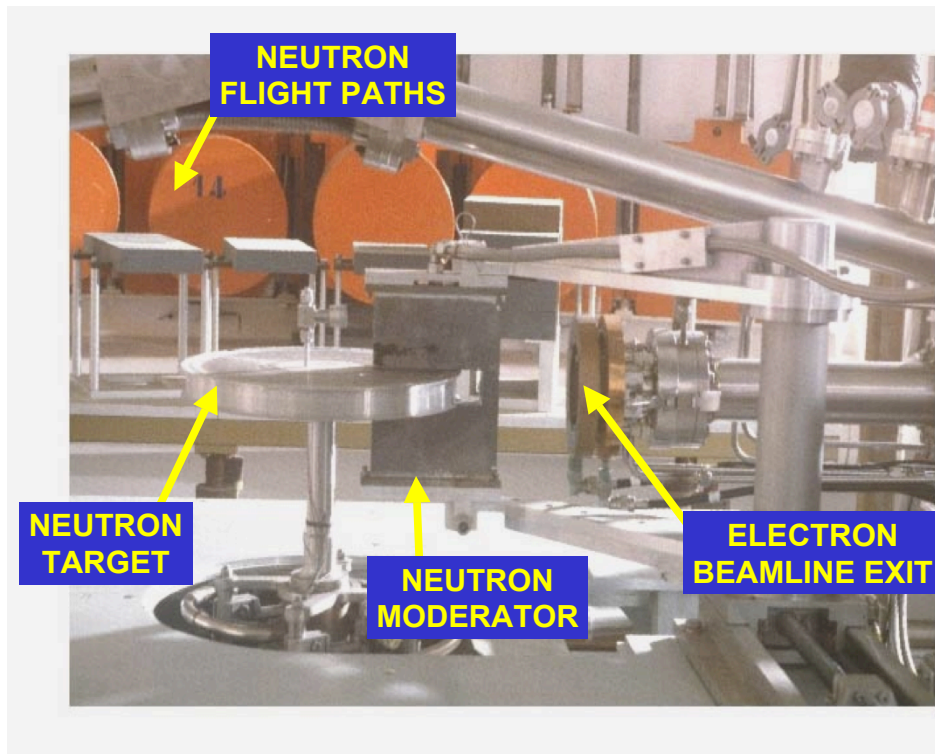
$$\Rightarrow \rho = \frac{1}{B} \frac{E}{qc}$$

$$\Rightarrow B = \frac{2\pi}{qc^2} \frac{\Delta E}{\Delta\tau}$$

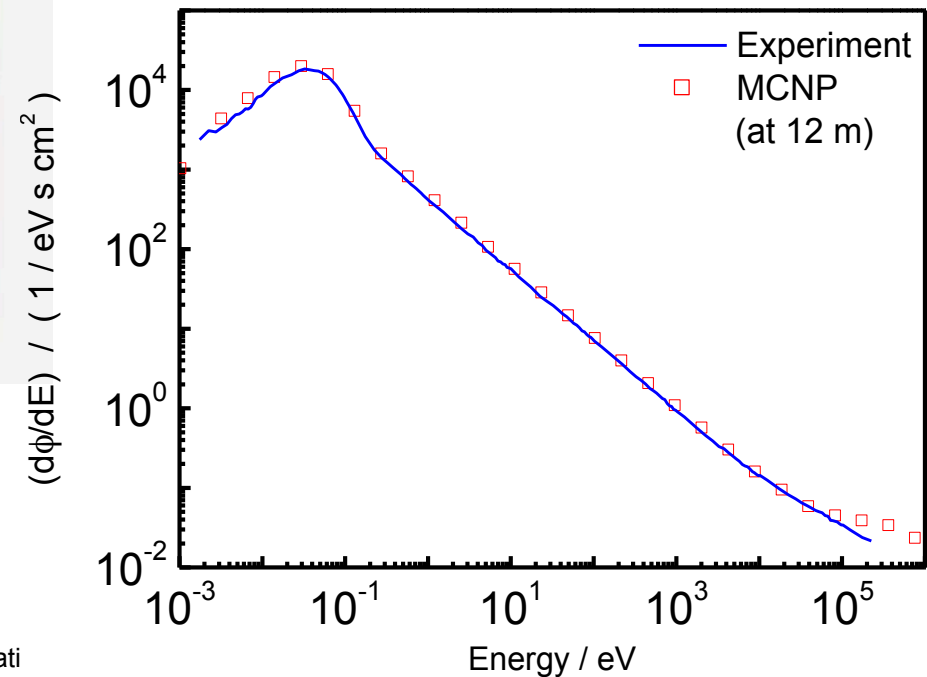
$$\begin{aligned} \Delta E &= 60 \text{ MeV} \\ \Delta\tau &= 10 \text{ ns} \end{aligned}$$

→ compressed pulse length ~ 1 ns

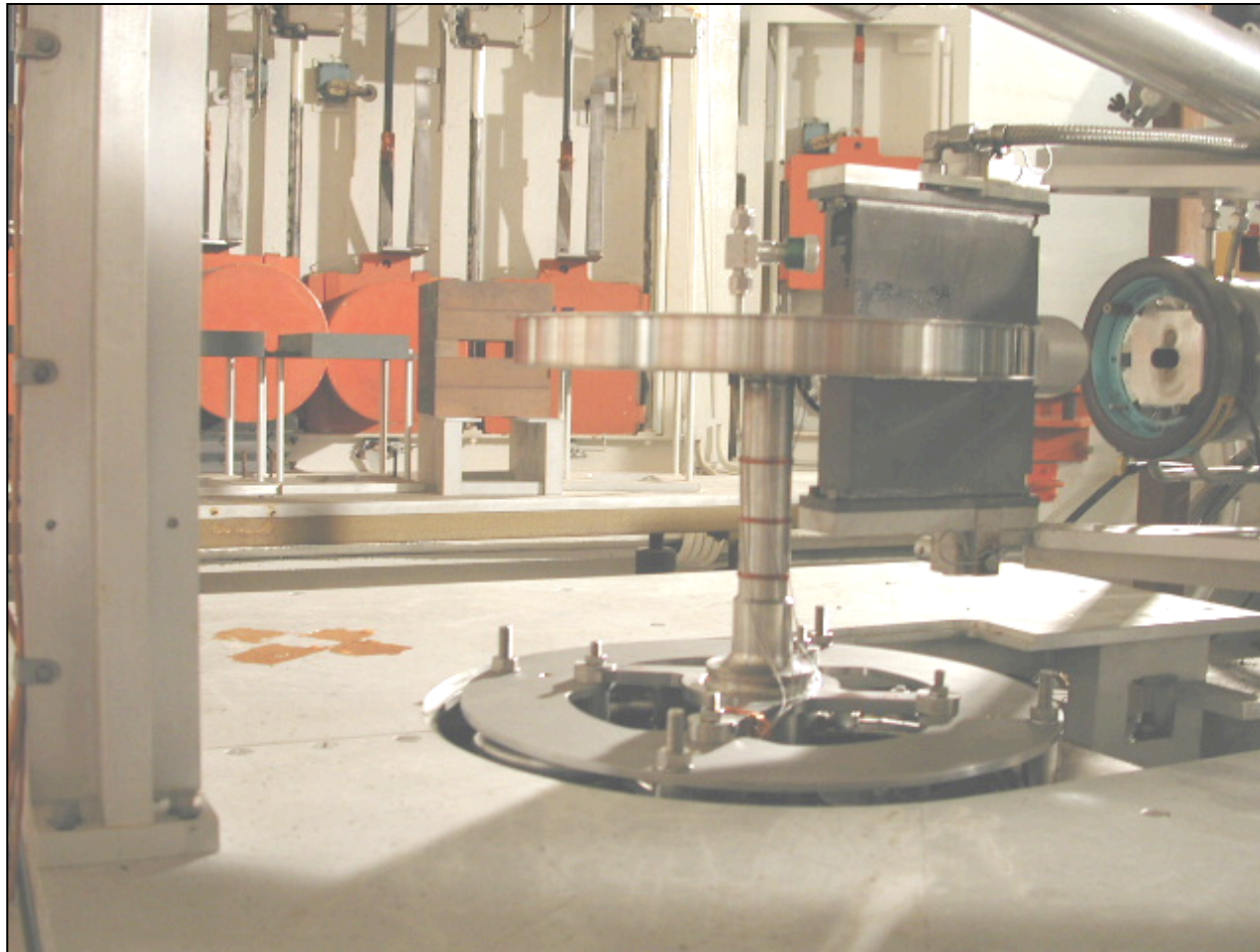
# Neutron production



- $e^-$  accelerated to  $E_{e^-, \max} \approx 140 \text{ MeV}$
- Bremsstrahlung in U-target
- $(\gamma, n)$ ,  $(\gamma, f)$  in U-target
- Low energy neutrons by moderation (water moderator in Be-canning)

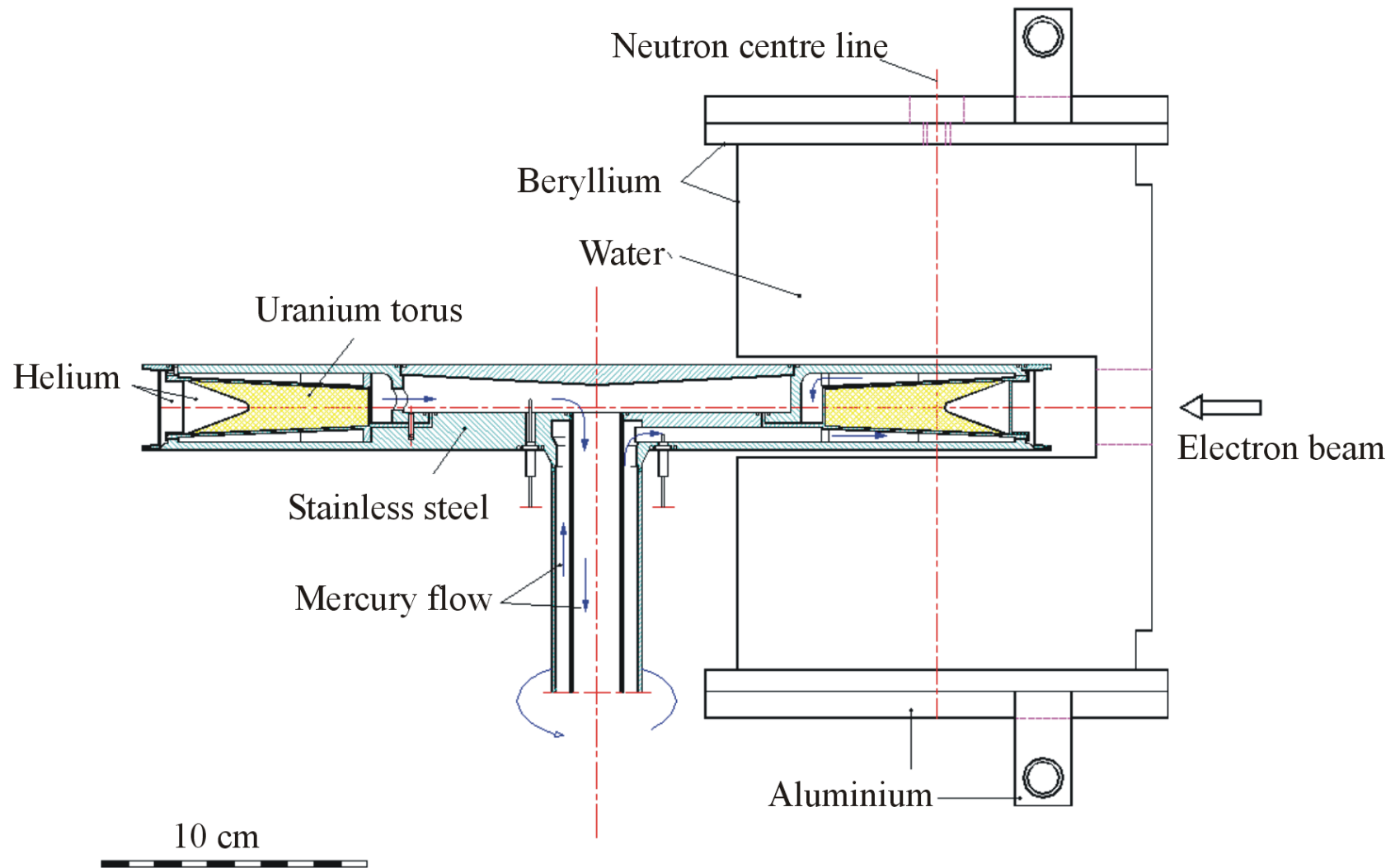


# Neutron target

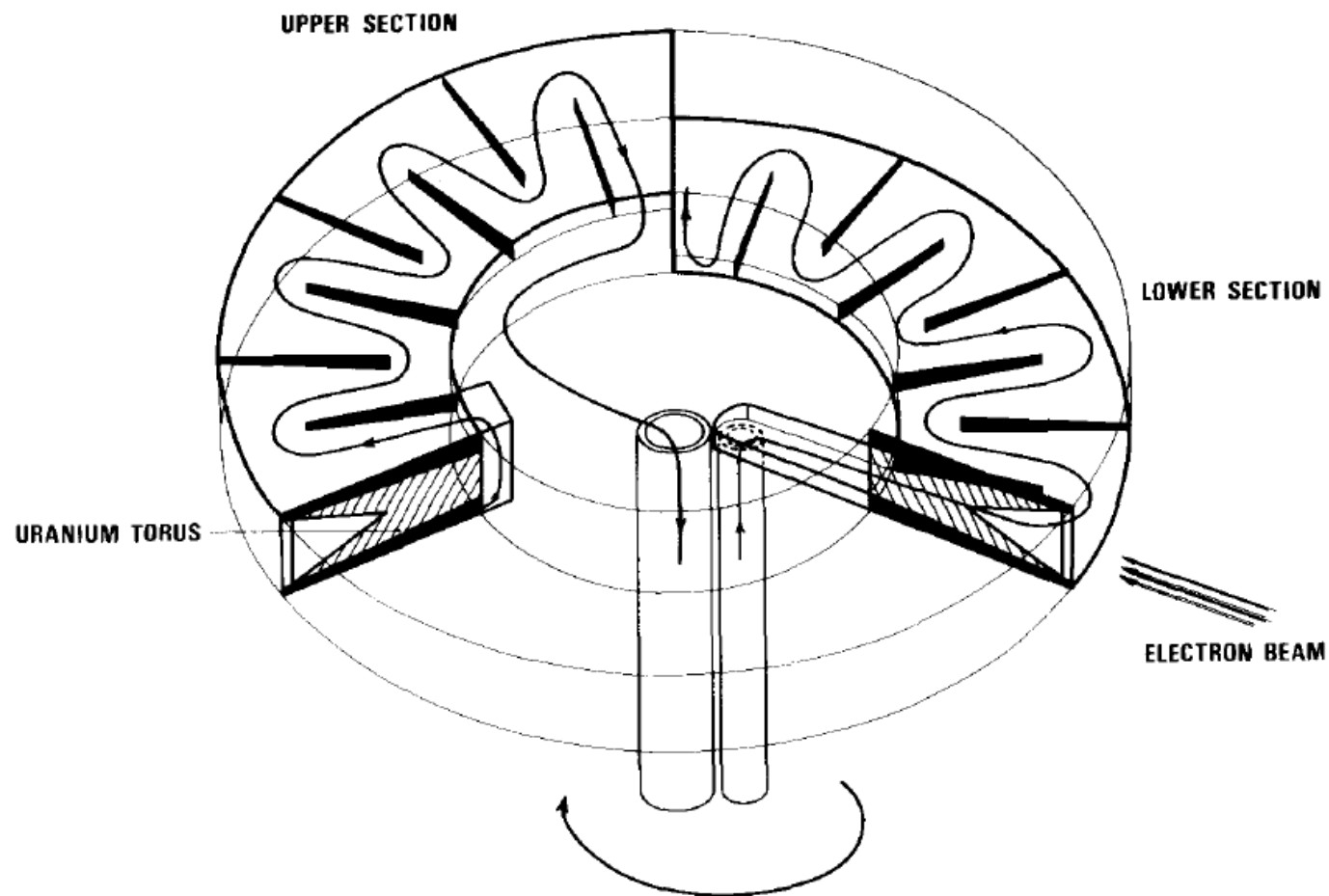


- **Depleted uranium**
  - high (e, $\gamma$ ) yield
  - high ( $\gamma$ ,n) yield
- **10-wt% Mo**
- **Up to 10 kW**
- **Mercury cooled**
  - low moderation
- **Rotating**
  - 10 kW/cm<sup>3</sup>
- **Canned in SS**
- **Remote handling**

# Neutron target



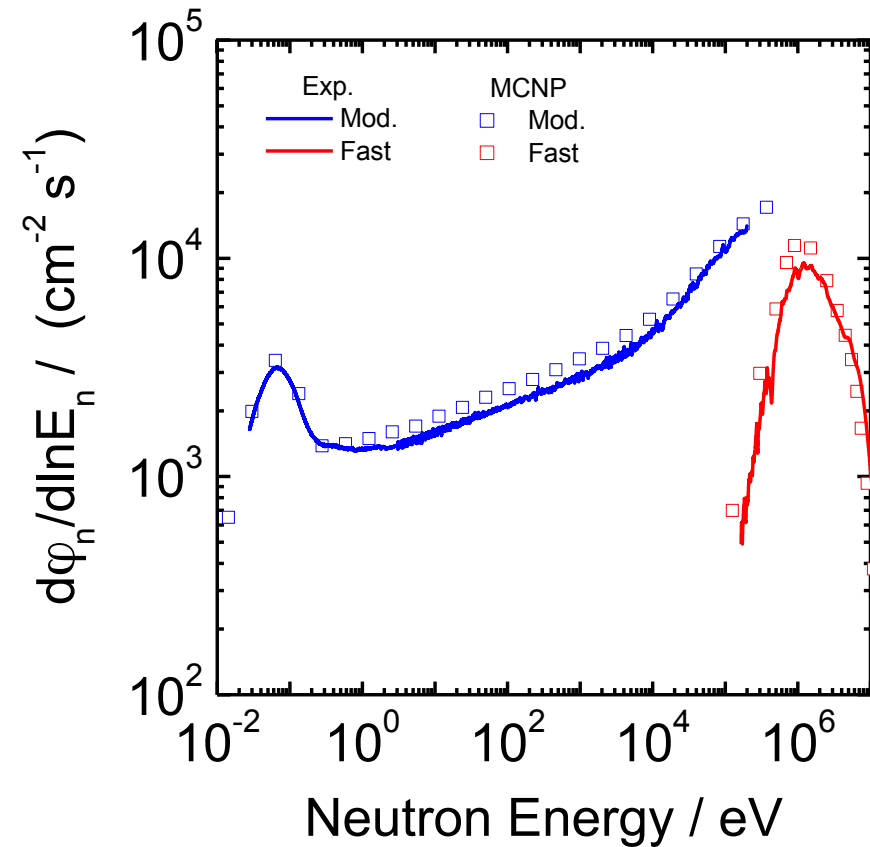
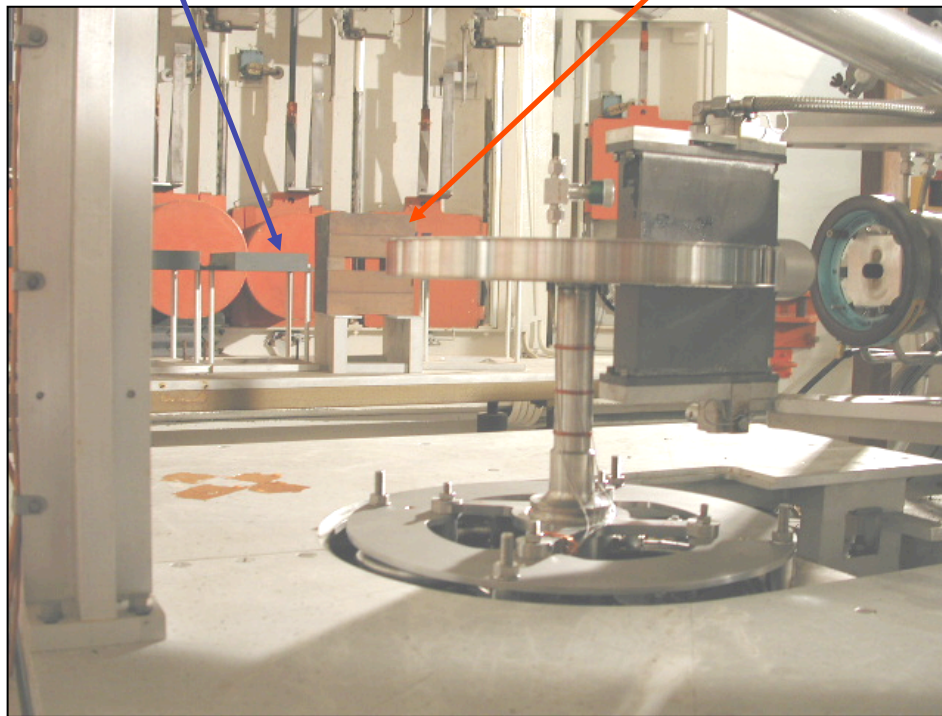
# Neutron target



# Neutron spectra

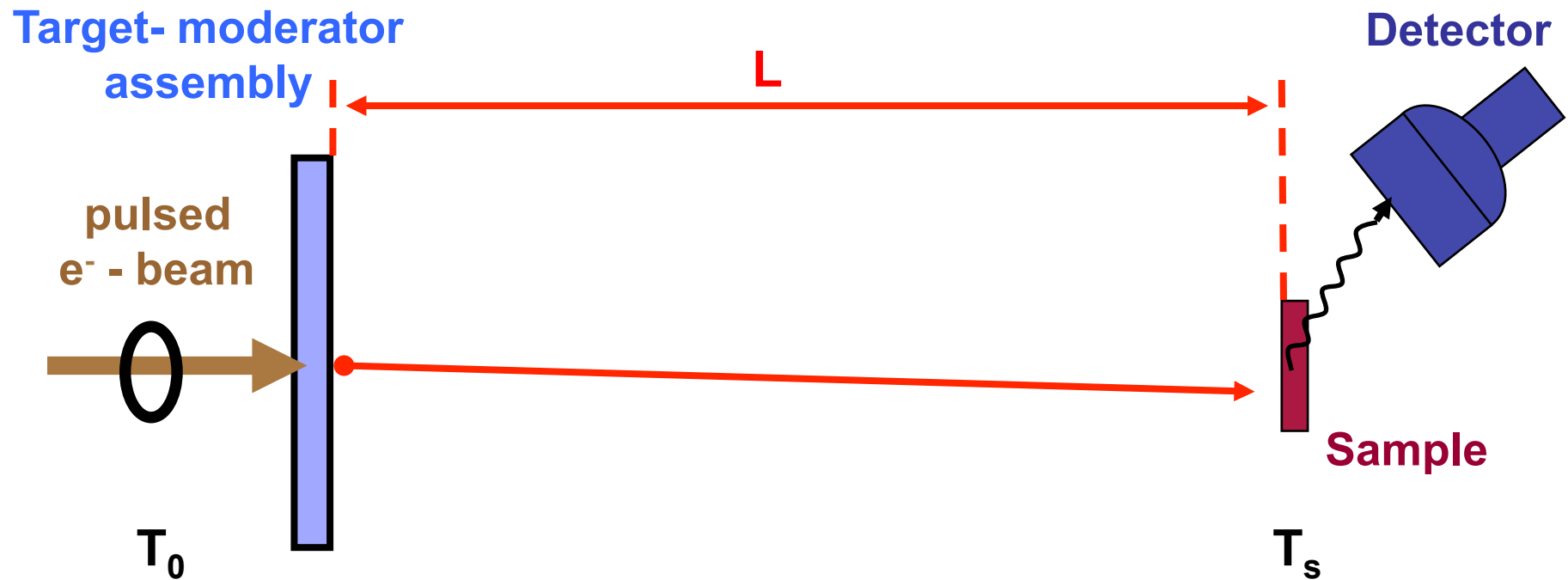
SHIELDING for MODERATED SPECTRUM

SHIELDING for FAST SPECTRUM





# Time – of – flight (TOF) technique

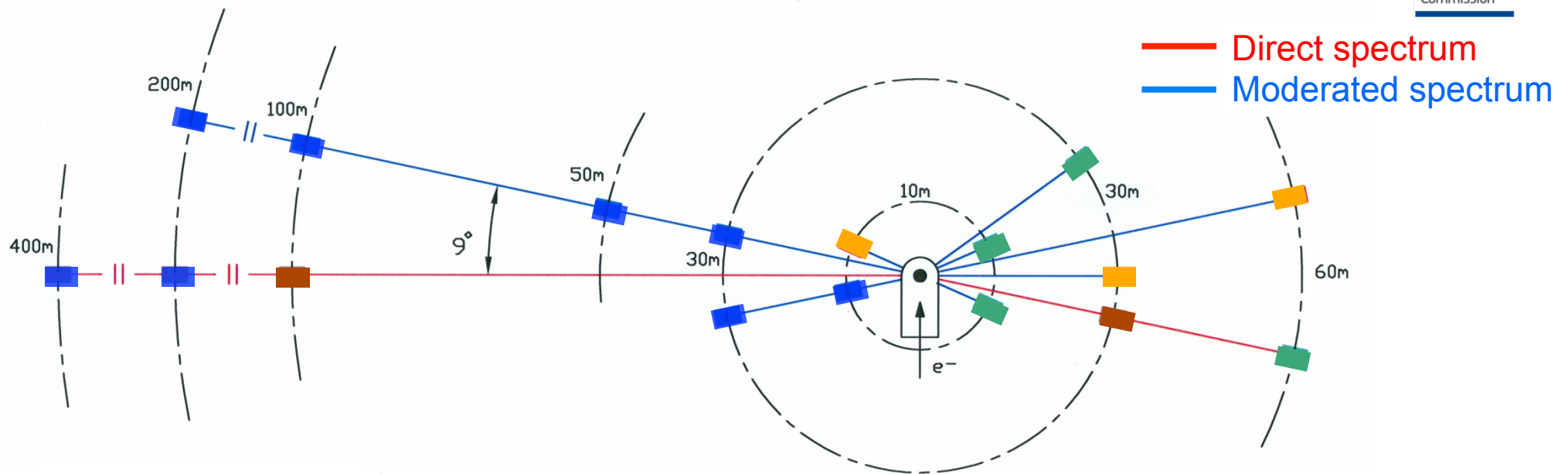






$$t_m = (T_s - T_0) + t_0$$

$$v = \frac{L}{t_m}$$

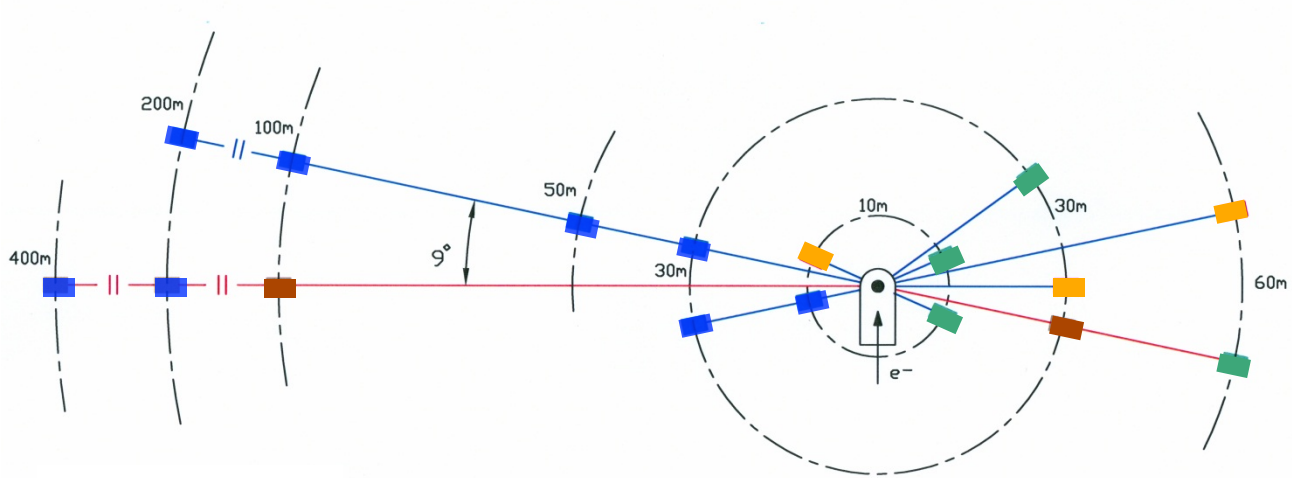
$$E = mc^2 \left( \frac{1}{\sqrt{1 - (v/c)^2}} - 1 \right)$$

# Measurement stations



	(n, $\gamma$ )	NIM A, 577, 626 (2007)
	(n,tot)	NP A 773, 173 (2006)
	(n,f) and (n,cp)	NSE 156, 211 (2007)
	(n,n' $\gamma$ )	NP A 786, 1 (2007)

# TOF - measurements



- (n,γ)** NIM A, 577, 626 (2007)
- (n,tot)** NP A 773, 173 (2006)
- (n,f) and (n,cp)** NSE 156, 211 (2007)
- (n,n'γ)** NP A 786, 1 (2007)

## ▪ Velocity from TOF

$$v = \frac{L}{t_m}$$

## ▪ Neutron flux



$$\varphi(L) \propto \frac{1}{L^2}$$

## ▪ Resolution



$$\frac{\Delta E}{E} \cong 2 \frac{\Delta v}{v} = 2 \sqrt{\frac{\Delta t_m^2}{t_m^2} + \frac{\Delta L^2}{L^2}}$$

# Response of TOF-spectrometer

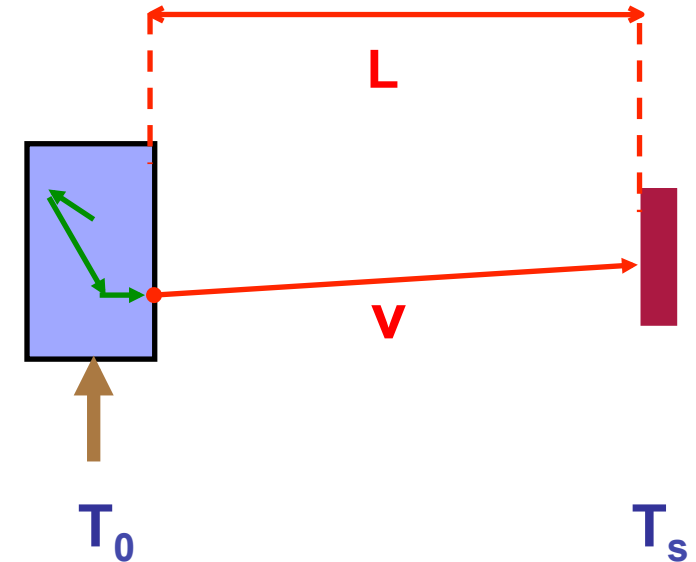


$$v = \frac{L}{t} \quad \Rightarrow \quad E = m c^2 (\gamma - 1)$$

$$\frac{\Delta v}{v} = \sqrt{\frac{\Delta t^2}{t^2} + \frac{\Delta L^2}{L^2}} \quad \Rightarrow \quad \frac{\Delta E}{E} = (\gamma + 1) \gamma \frac{\Delta v}{v}$$

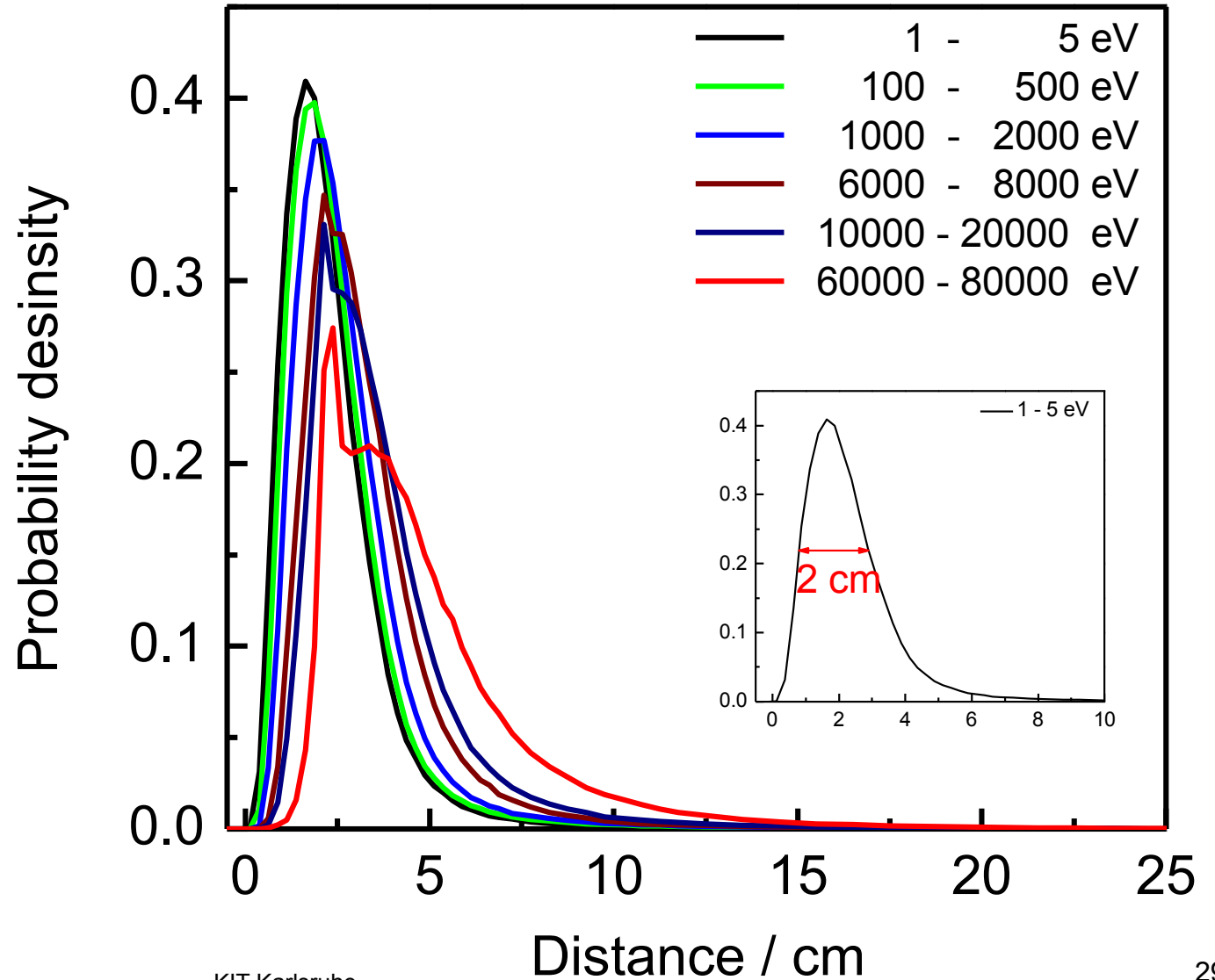
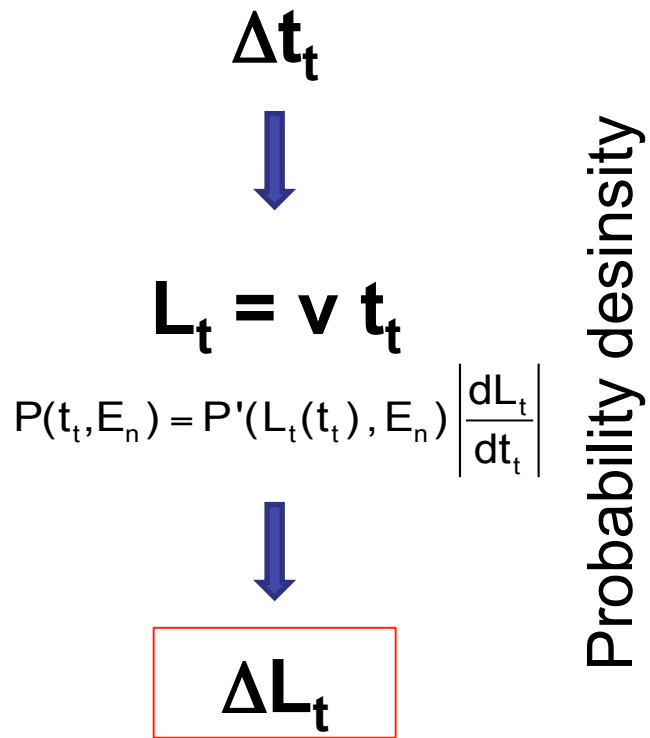
- $\Delta L$  (~ 1 mm)
- $\Delta t$

- Initial burst width  $\Delta T_0$
- Time jitter detector & electronics  $\Delta T_s$
- Neutron transport in target - moderator  $\Delta t_t$
- Neutron transport in detector  $\Delta t_d$



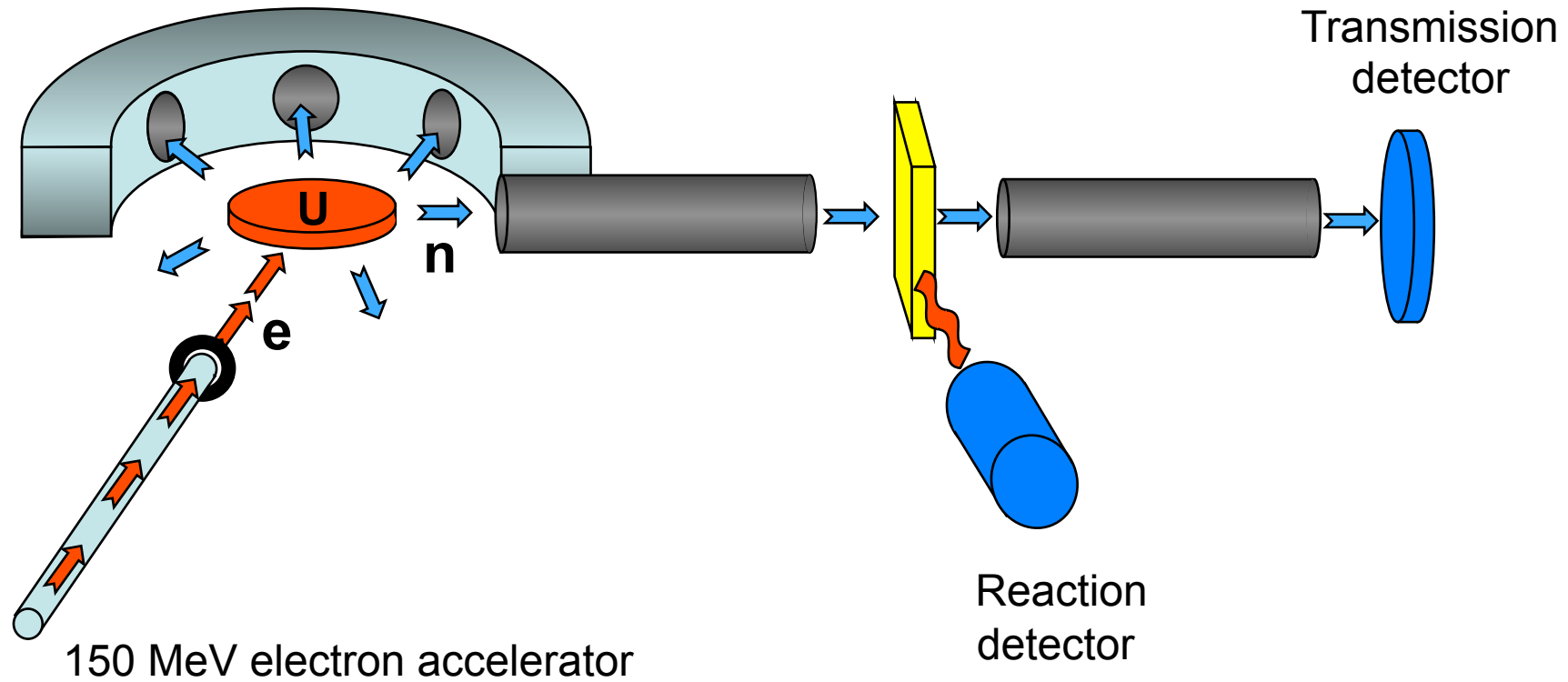
$$t = t_m - (t_t + t_d)$$

# Neutron transport in the target



- IRMM
- GELINA
- **Neutron cross section measurements at GELINA**

# Types of TOF - experiments



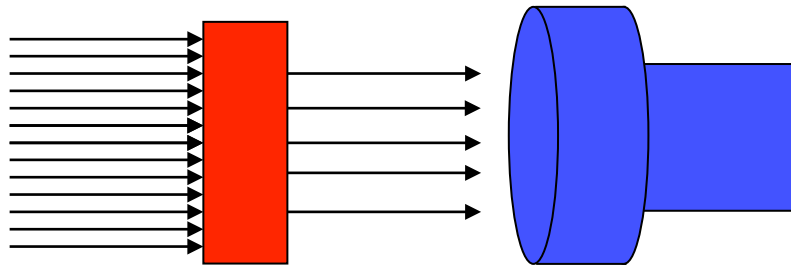
# Cross section measurements



## Transmission

$$T_{\text{exp}} = \frac{C_{\text{in}}}{C_{\text{out}}}$$

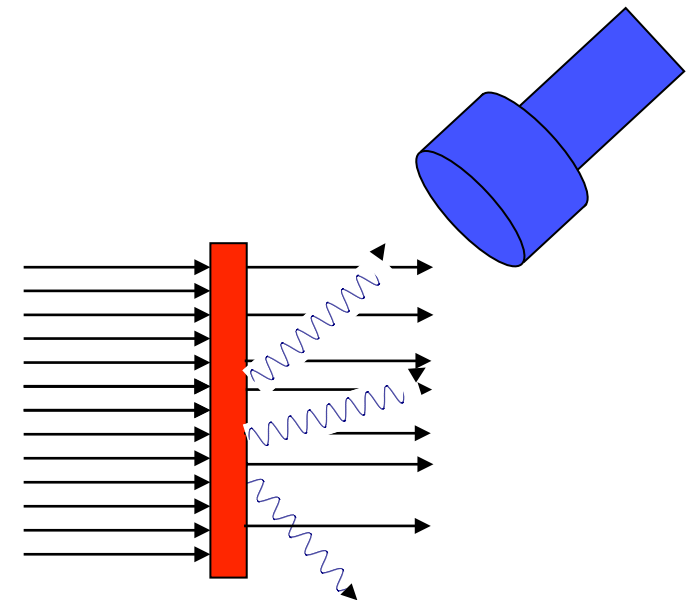
$$T \cong e^{-n \sigma_{\text{tot}}}$$



## Reaction: (n,r)

$$C_r \approx \varepsilon_r \Omega P_r Y_r A_r \varphi$$

$Y_r$  reaction yield  
fraction of neutron beam creating (n,r)  
related to  $\sigma_r$



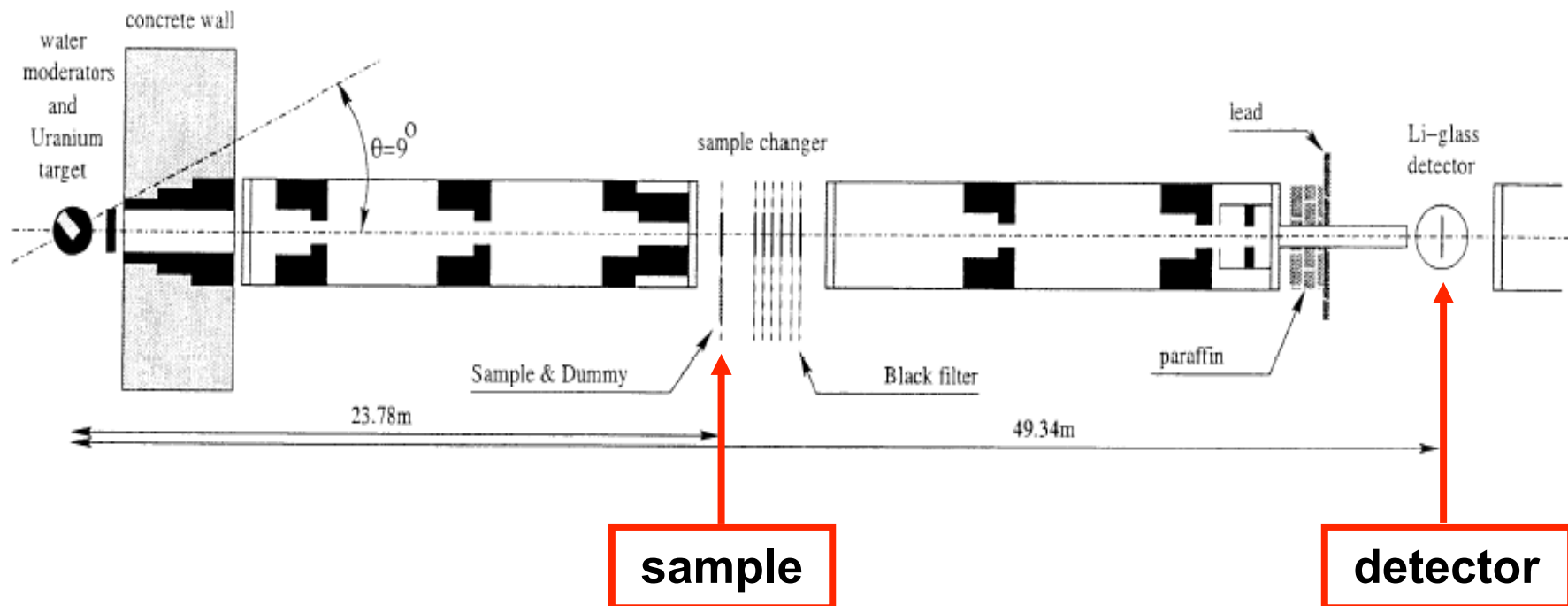


# Transmission : principle

$$T = \frac{C_{in}}{C_{out}} \propto e^{-n \sigma_{tot}}$$

- (1) All detected neutrons passed through the sample
- (2) Neutrons scattered in the target do not reach detector
- (3) Sample perpendicular to parallel neutron beam

- ⇒ Good transmission geometry (collimation)
- ⇒ Homogeneous target (no spatial distribution of  $n$ )



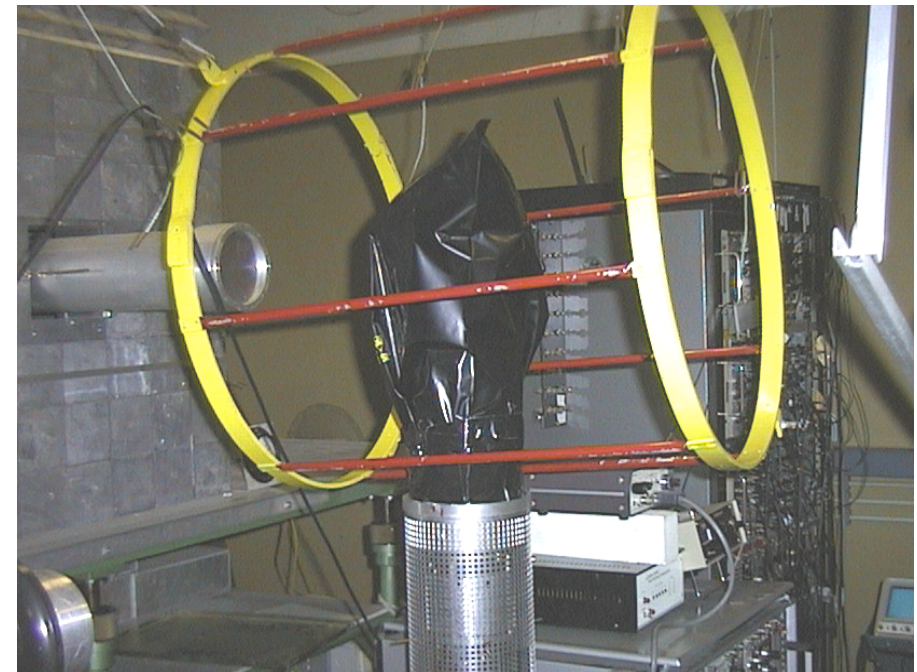
# Transmission: experimental set-up (50 m)



Sample & Background Filters  
at 25 m



Neutron detector  
at 50 m



## Detector stations at GELINA

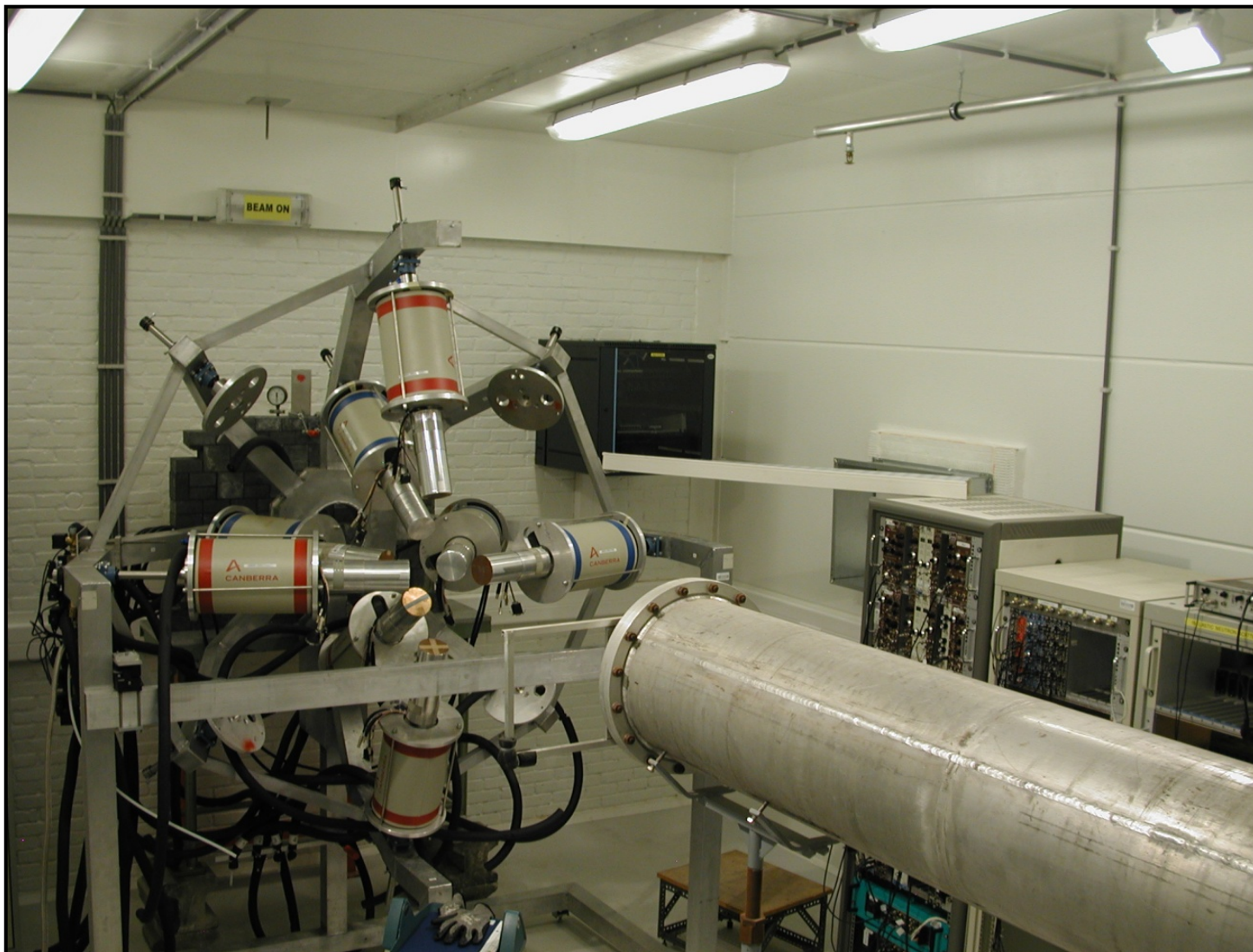
Moderated : at 30 m, 50 m, (100 m, 200 m)  
Fast : at 400 m

## Detectors

Low energy :  ${}^6\text{Li}(n,t)\alpha$  Li-glass  
High energy :  $\text{H}(n,n)\text{H}$  Plastic scintillator

Kopecky and Brusegan, Nucl. Phys. A 773 (2006) 173  
Borella et al., Phys. Rev. C 76 (2007) 014605

# (n,n') reaction: experimental setup (200m)



# Measurement setups

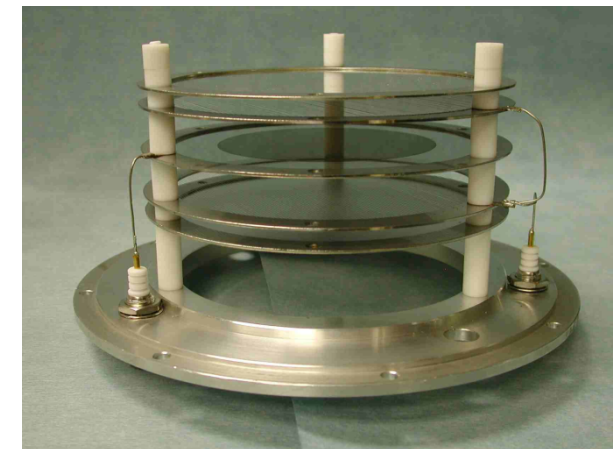
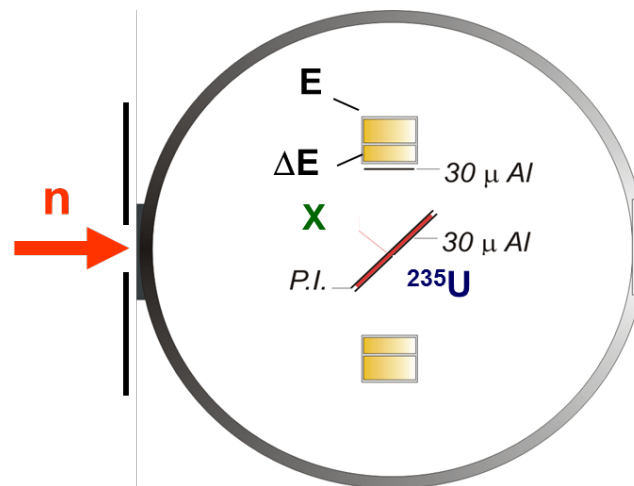


## Transmission

- Li-glass detectors
- Plastic scintillators
- NE213 scintillators
- Cryostat and over for Doppler measurements

## Reaction

- Frisch-gridded ionisation chambers, SBD for (n,f), (n, $\alpha$ ), (n,p)
- HPGe detectors: (n,n'), (n, $\gamma$ )
- C<sub>6</sub>D<sub>6</sub> scintillators: (n, $\gamma$ )



- **Safety assessment of existing reactor systems**
  - dependence of nuclear reactor parameters on nuclear data under different (extreme) operating conditions
  - extension and optimization of the fuel cycle
- **Future reactor systems (GEN IV – ADS)**
  - e.g. support to licensing of MYRRHA
  - LLFP and MA
- **Cross section standards**
  - $^{10}\text{B}(n,\alpha)$
- **Non destructive material analysis**
  - NRCA and NRTA
  - e.g. post Fukushima safeguards support

# Thanks for your attention



VdG

GELINA