



**Institute of
Applied Physics**

Friedrich-Schiller-Universität Jena

Thermal noise in grating reflectors

D. Heinert¹, S. Kroker², D. Friedrich³, S. Hild⁴, E.-B. Kley², S. Leavey⁴, I. W. Martin⁴, R. Nawrodt¹, A. Tünnermann², S. P. Vyatchanin⁵, K. Yamamoto³

¹ IFK, University of Jena, Germany, ² IAP, University of Jena, Germany, ³ ICRR, University of Tokyo, Japan, ⁴ IGR, University of Glasgow, UK, ⁵ Relativity Group, Moscow State University, Russia

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seit 1558

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東京大学
THE UNIVERSITY OF TOKYO



University
of Glasgow



Outline

introduction

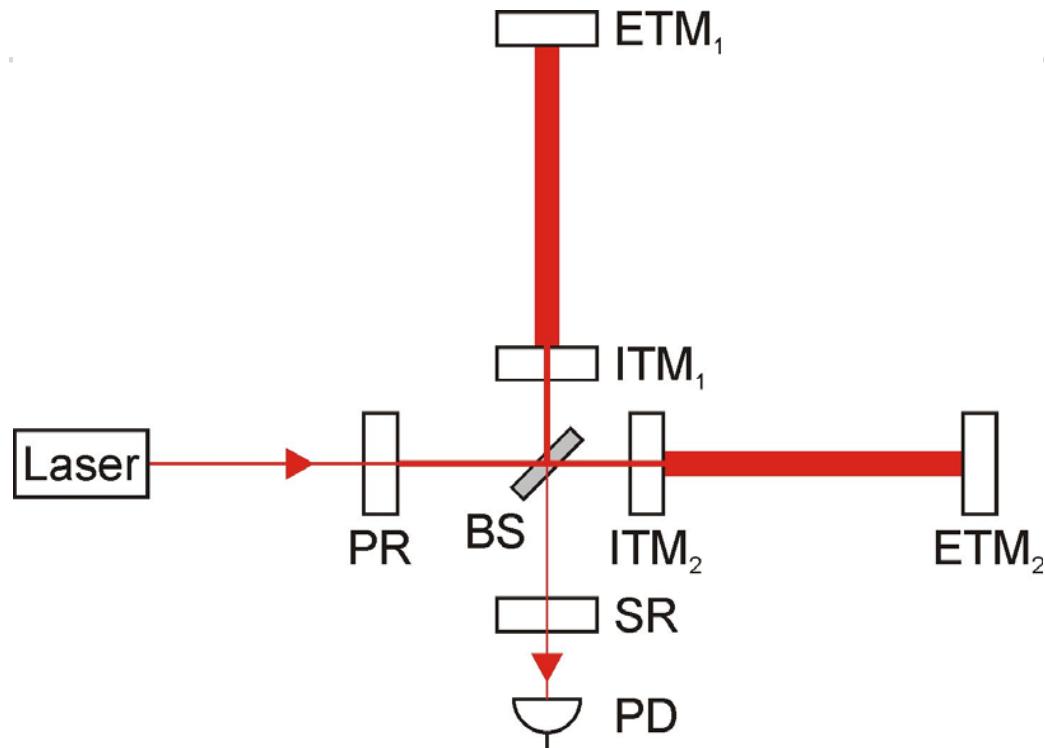
grating reflectors

- functionality
- thermal noise calculation
- application to a GWD of the 3rd generation

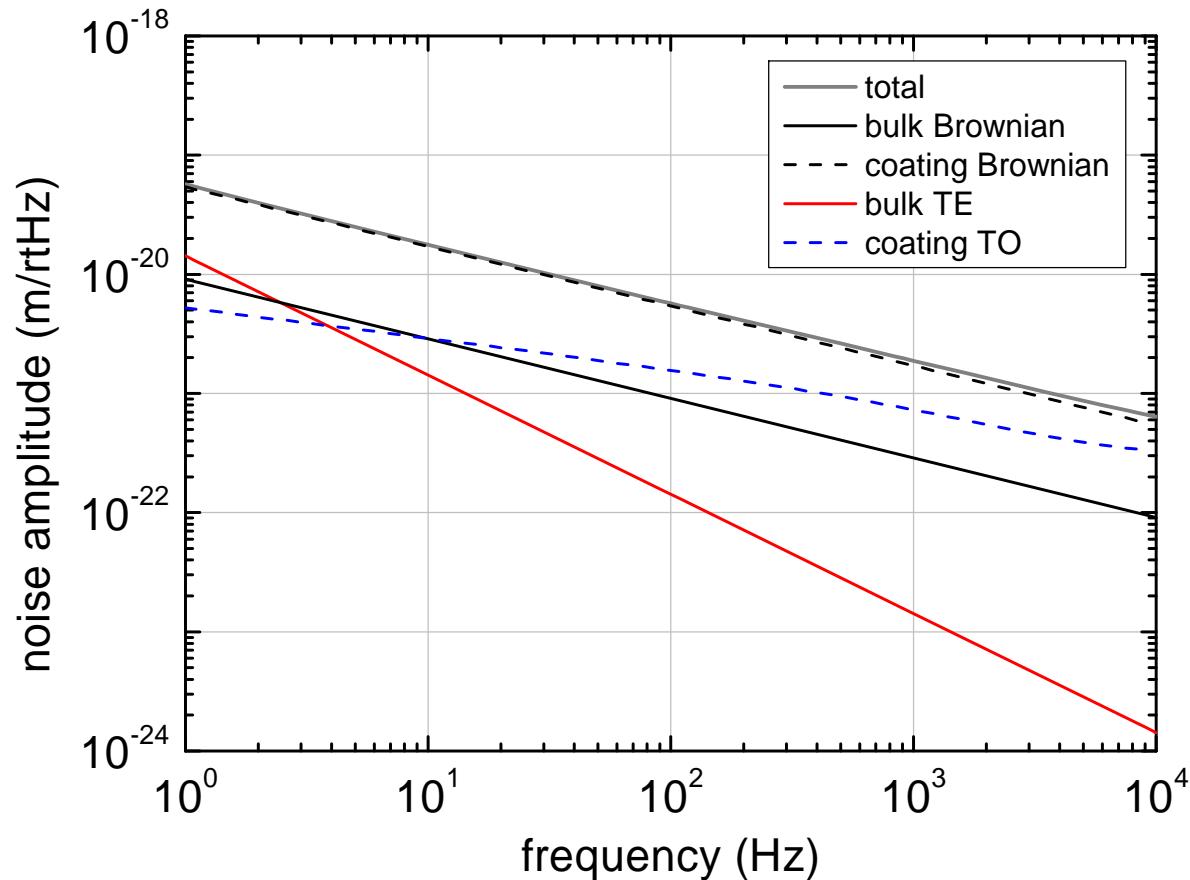
conclusion

Introduction

Detector scheme for 2nd generation detectors



Noise budget of ALIGO

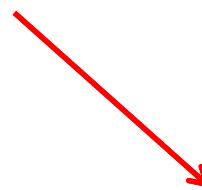
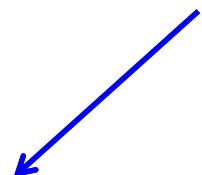


Brownian coating noise represents the most critical contribution

Brownian coating thermal noise of optical coating

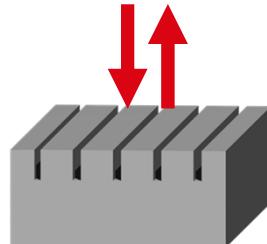
$$S_z(f) \propto \frac{k_B T}{f} \frac{d}{r_0^2} \phi$$

T... temperature
d.... coating thickness
f... frequency
 r_0 ... beam radius
 ϕ ... mechanical loss

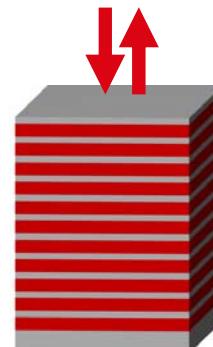


Grating Concepts

IAP Jena



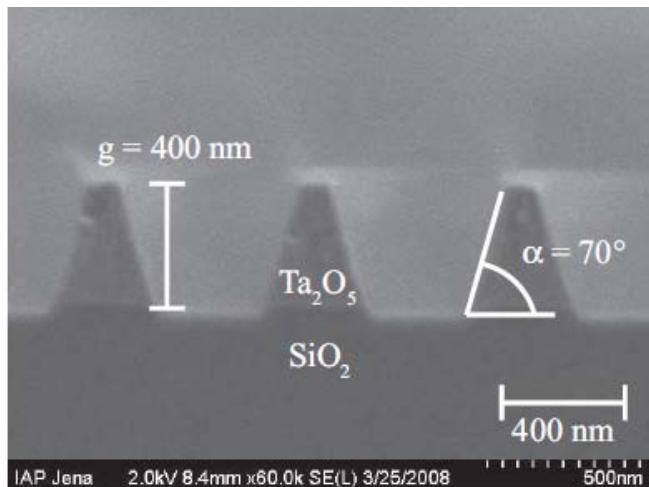
Crystalline Coatings



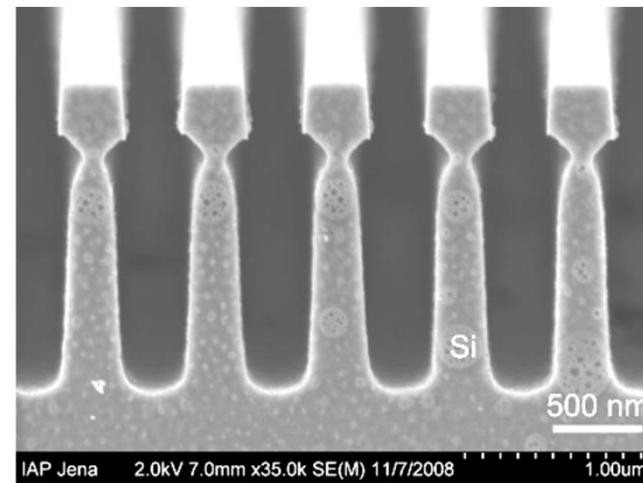
See talks by
G. Cole and A. Lin!

Grating reflector topologies

non-monolithic 1D $\lambda=1064$ nm

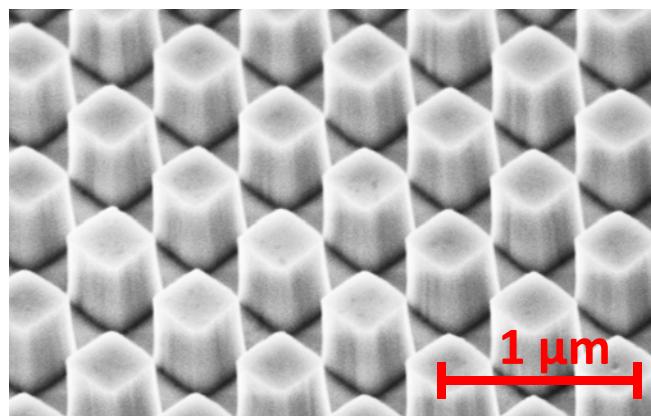


monolithic 1D $\lambda=1550$ nm

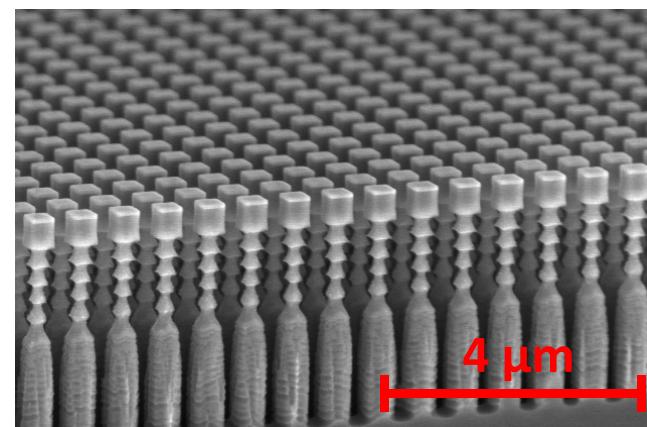


Brückner et al., Opt. Express (2008).
Brückner et al., Phys. Rev. Lett. (2010).

non-monolithic 2D $\lambda=1550$ nm



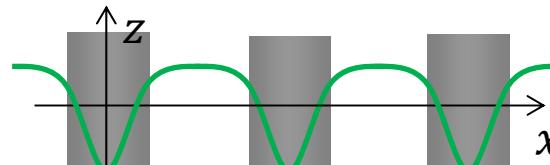
monolithic 2D $\lambda=1550$ nm



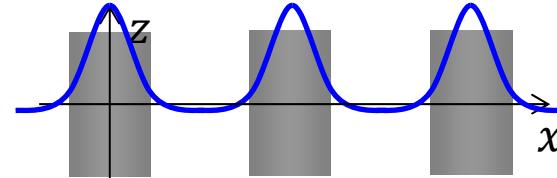
Kroker et al., Appl. Phys. Lett. (2013)

Two mode Fabry-Perot resonator

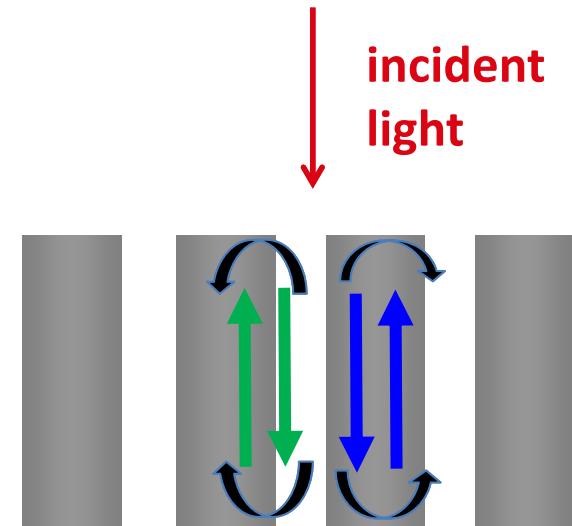
Grating = periodic array of slab waveguides



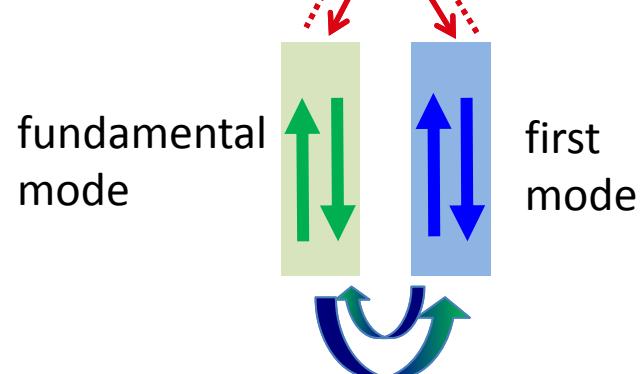
n_{eff} high



n_{eff} low



incident light reflected light

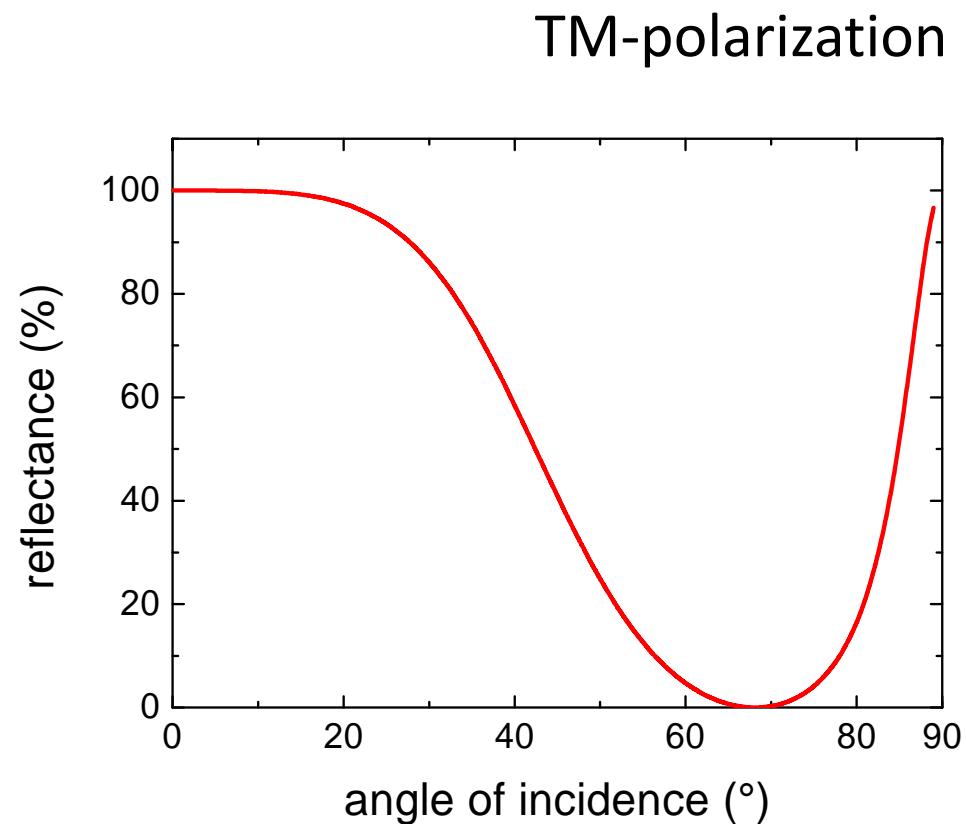
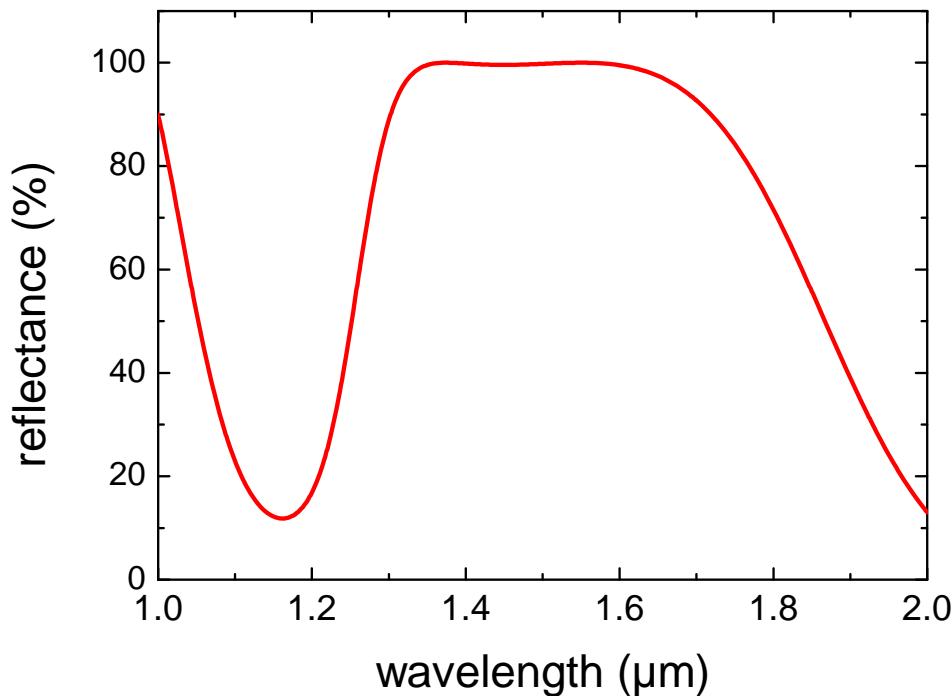


One mechanism for R=100%:

- cavities in antiresonance
- destructive interference at bottom
- intercoupling of modes

Optical properties of grating reflectors

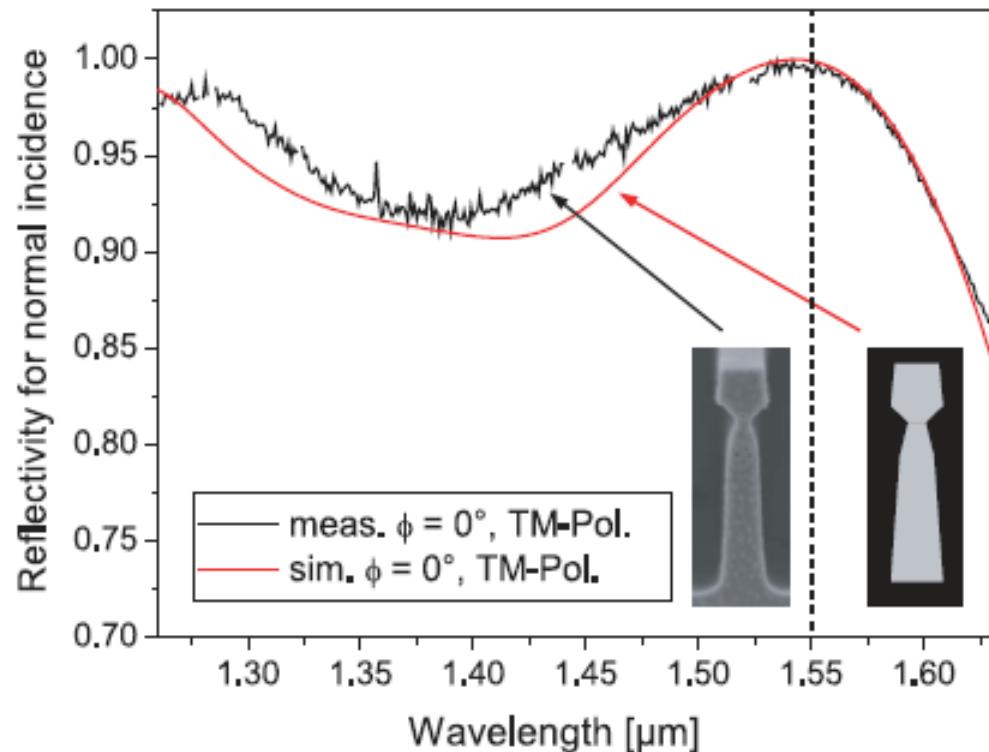
Free standing silicon reflector - broadband behavior due to high index contrast



TM-polarization

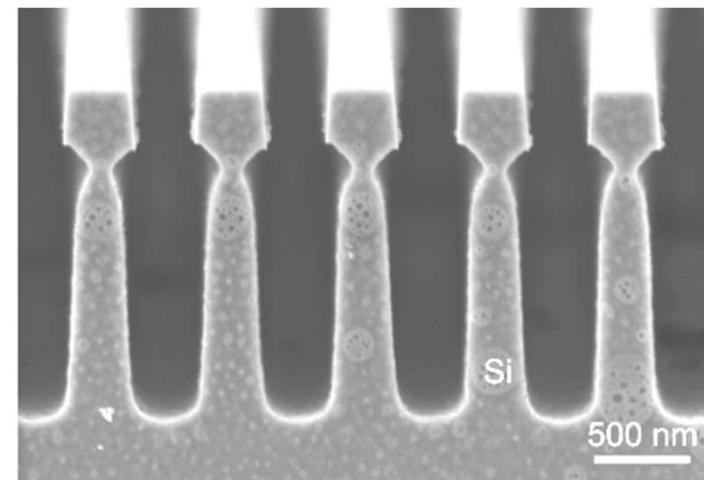
Monolithic silicon reflectors

For scalability

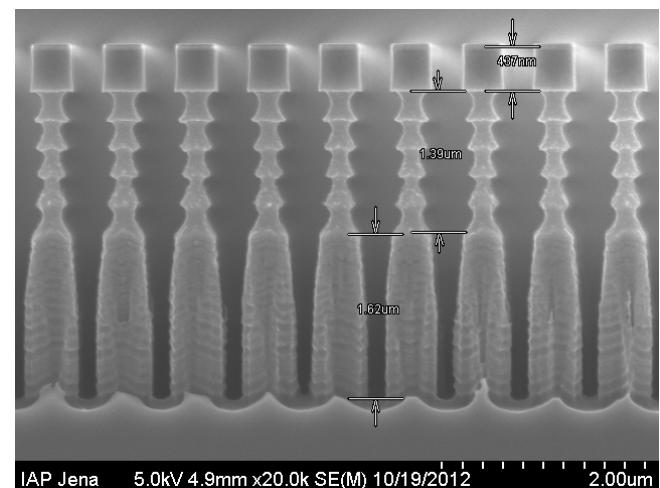
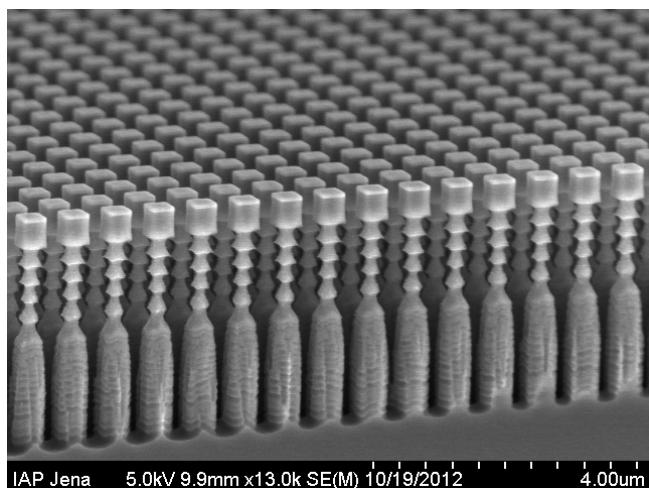
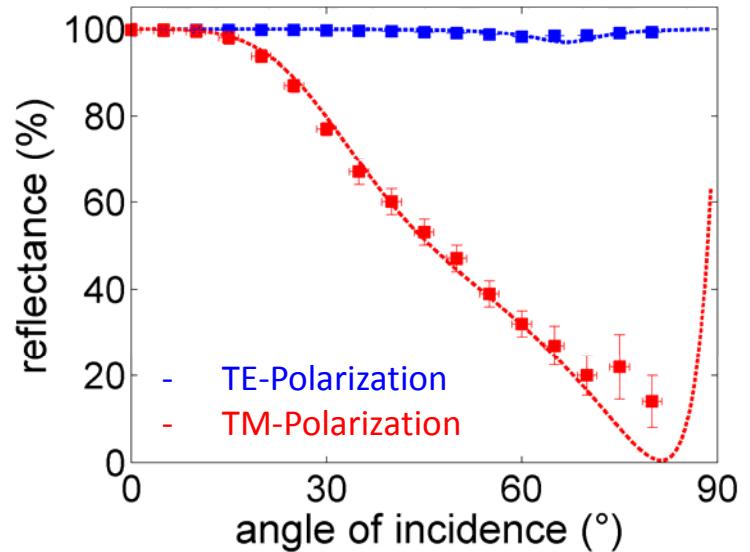
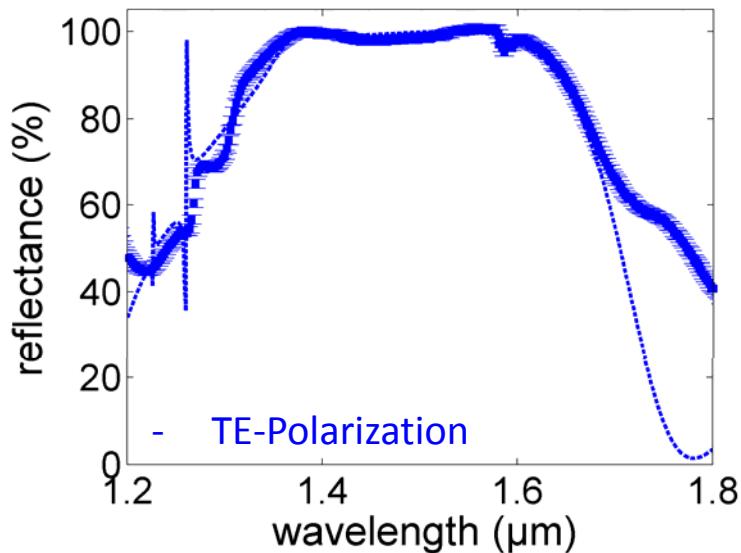


$$R(1550 \text{ nm}) = (99.80 \pm 0.01)\%$$

same optical function as free ridges:
 only one mode in lower grating
 (~ effective medium)



Monolithic Silicon Reflectors with 2D periodicity



Thermal noise of grating reflectors

Brownian coating thermal noise of coated test mass:

$$S_z(f) \propto \frac{k_B T}{f} \frac{d}{r_0^2} \phi \quad \longrightarrow \text{lossy amorphous materials critical}$$

non-monolithic grating reflector:

$$d_{grating} \sim 0.1 \times d_{coatingstack}$$

$$S_{grating} \sim 0.1 \times S_{coatingstack}$$

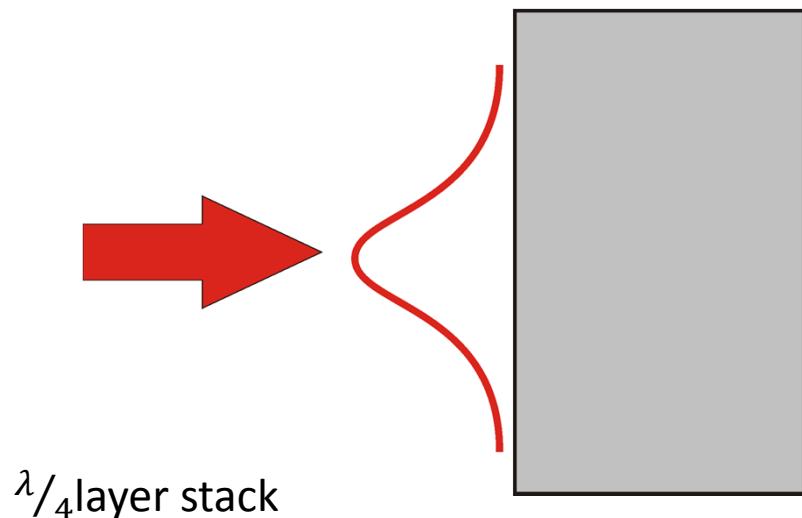
monolithic grating reflector:

$$d \rightarrow 0:$$

$$S_{grating} \rightarrow 0$$

Thermal noise of coated test mass

Fluctuation-Dissipation theorem



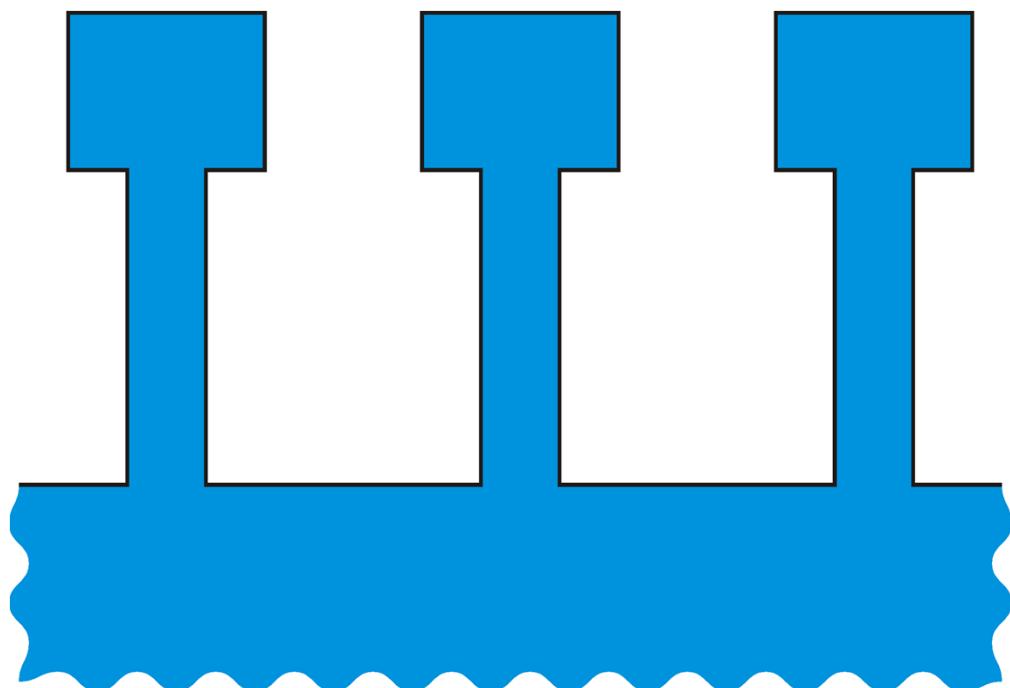
$$1. \quad p(r) = \frac{F_0}{\pi r_0^2} \exp\left(-\frac{r^2}{r_0^2}\right)$$

$$2. \quad \langle P_{diss} \rangle$$

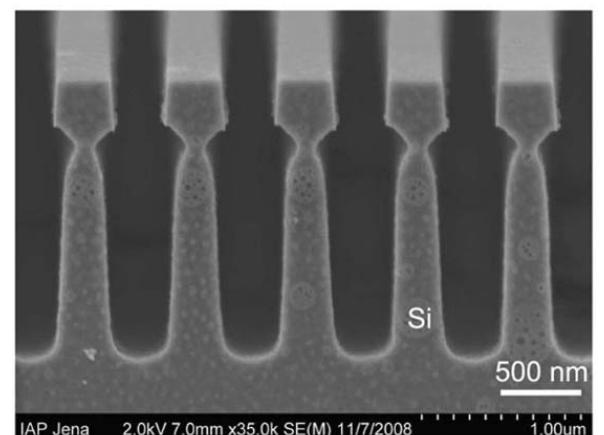
$$3. \quad S_z(\omega) = \frac{8k_B T}{\omega^2} \frac{\langle P_{diss} \rangle}{F_0^2}$$

- Brownian coating noise: $S_z(\omega) \propto \frac{4k_B T}{\pi\omega} \frac{d}{r_0^2} \frac{(1+\sigma)(1-2\sigma)}{E} \phi$

Chosen reflector geometry



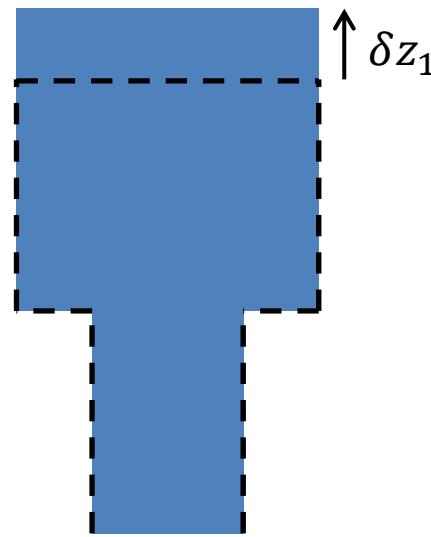
design wavelength	1550 nm
period	688 nm
ridge height	350 nm
ridge width	388 nm
support height	800 nm
support width	200 nm



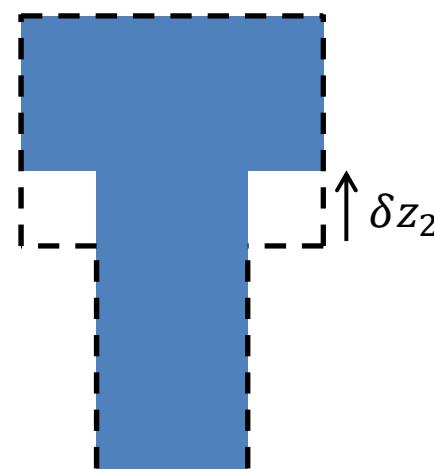
reflectivity 99.8%

[F. Brückner et al., 2010, PRL 104, 163903]

How do thermal structure fluctuations couple into the phase of the reflected light?



$$\delta\varphi = K_{Br,1} \delta z_1$$



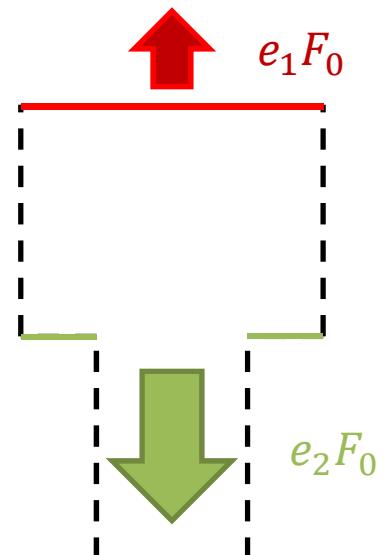
$$\delta\varphi = K_{Br,2} \delta z_2$$

- weighting factors by **Rigorous Coupled Wave Analysis (RCWA)**

$$e = \frac{4\pi}{\lambda} K_{Br}$$

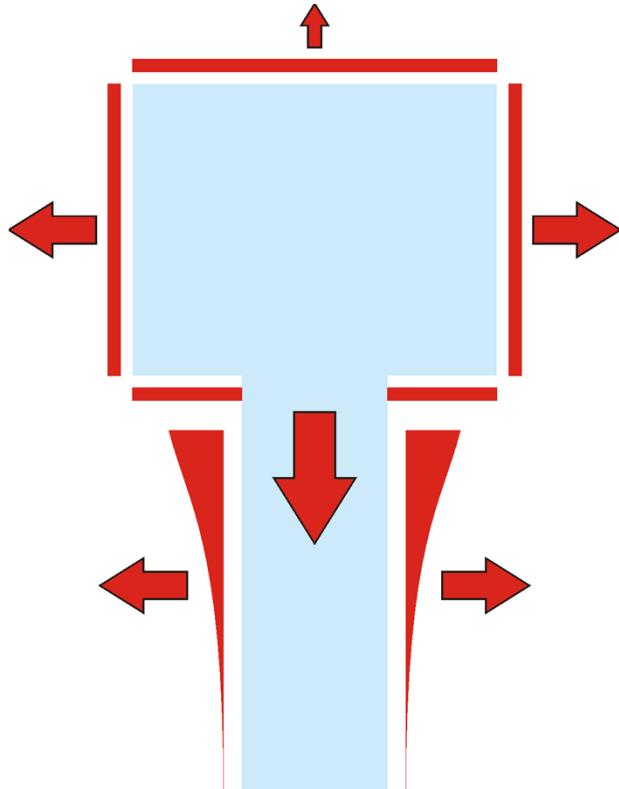
here: $e_1 = 0.02$ and $e_2 = 1.02$

- check of all kinds of surface fluctuations



Virtual load scheme

application of virtual loads



1. calculation of mechanical energy E
2. dissipated power $\langle P_{diss} \rangle = \omega \phi E$
3. Brownian noise power of the grating

$$S_z(\omega) = \frac{8k_B T}{\omega^2} \frac{\langle P_{diss} \rangle}{F_0^2}$$

Temperature fluctuations – thermo-optic noise

Significant fluctuations on a scale larger than the thermal pathlength

$$r_{th} = \sqrt{\kappa / \rho C \omega}$$

κ ... thermal conductivity
 ρ ... mass density
 C ... heat capacity

Values for silicon ($\omega = 2\pi \times 100$ Hz)

T [K]	κ [W/m/K]	C [J/kg/K]	r_{th} [mm]
300	148	713	0.37
10	2110	0.276	72

$r_{th} \gg$ grating dimensions (ridge/period)

→ homogeneous temperature distribution along a grating ridge

Temperature fluctuations

Scheme of Braginsky et al. adapted

- Temperature fluctuations in a thin layer on top of a half space substrate

$$S_T(\omega) = \frac{\sqrt{2}k_B T^2}{\pi r_0^2 \sqrt{\rho C \kappa \omega}}$$

Effect of a homogeneous temperature change via RCWA

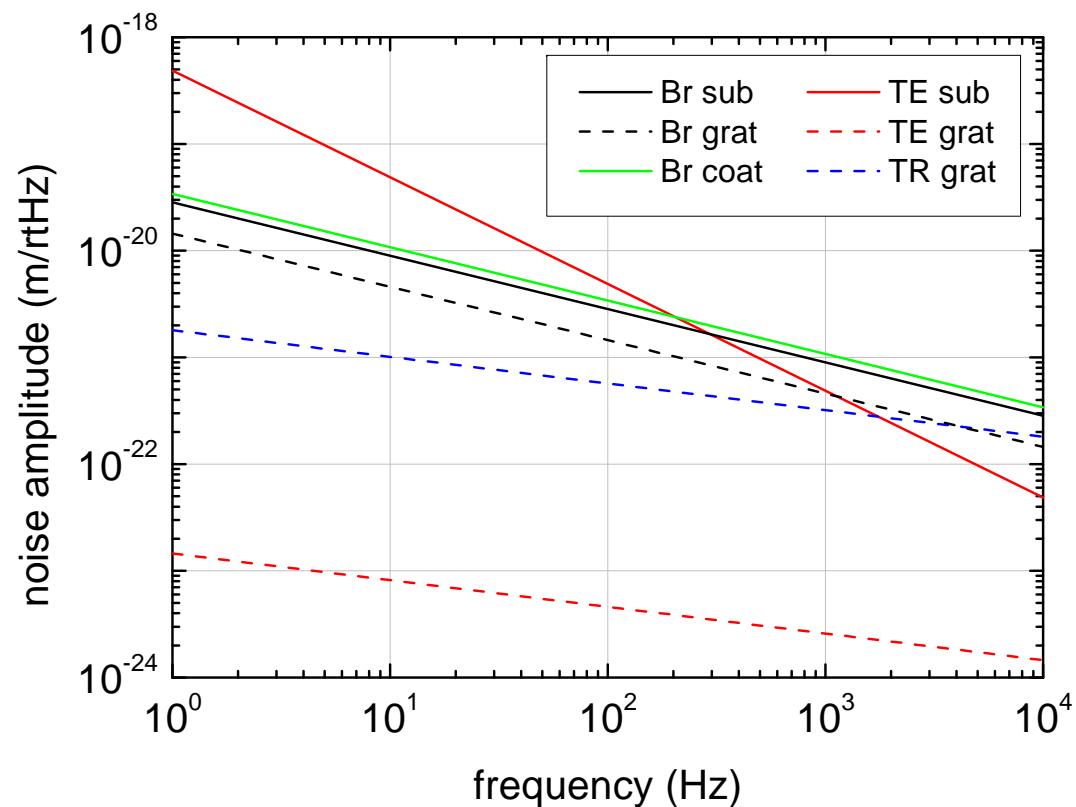
- Phase of reflected light $\Delta\varphi = K_{TR}\beta\Delta T + K_{TE}\alpha\Delta T$
- Effective displacement noise

$$S_{z,TR}(\omega) = \left(\frac{\lambda_0}{4\pi} K_{TR} \beta \right)^2 S_T(\omega)$$

$$S_{z,TE}(\omega) = \left(\frac{\lambda_0}{4\pi} K_{TE} \alpha \right)^2 S_T(\omega)$$

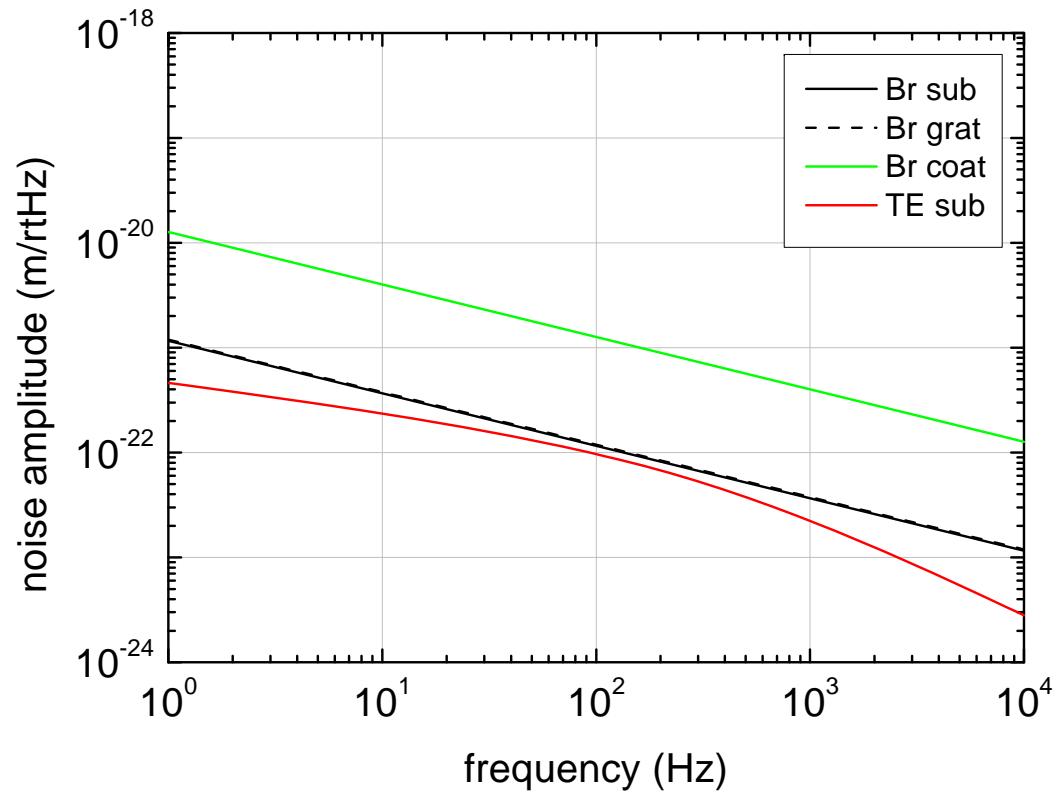
Application to ET-LF

silicon substrate (diam. 50 cm x 46 cm, beam radius 9 cm) at 300 K



Application to ET-LF

silicon substrate (diam. 50 cm x 46 cm, beam radius 9 cm) at 10 K

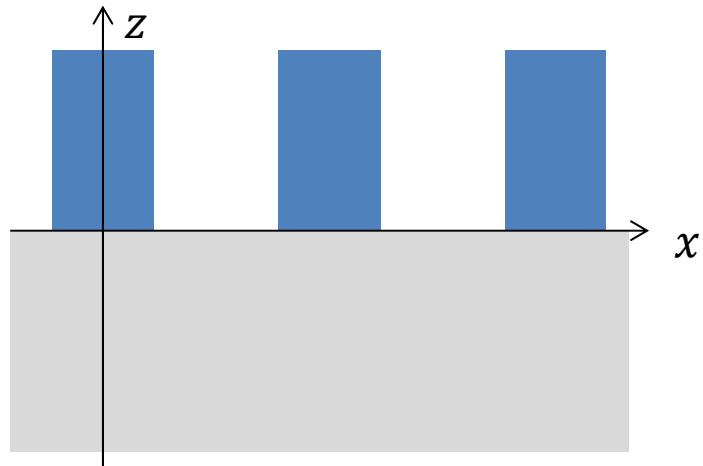


- possible decrease in noise amplitude by a factor of 10

Alternative grating design

Lamellar tantalum grating on fused silica substrate

- Allows for a direct use in aLIGO (at 1064 nm and 300 K)

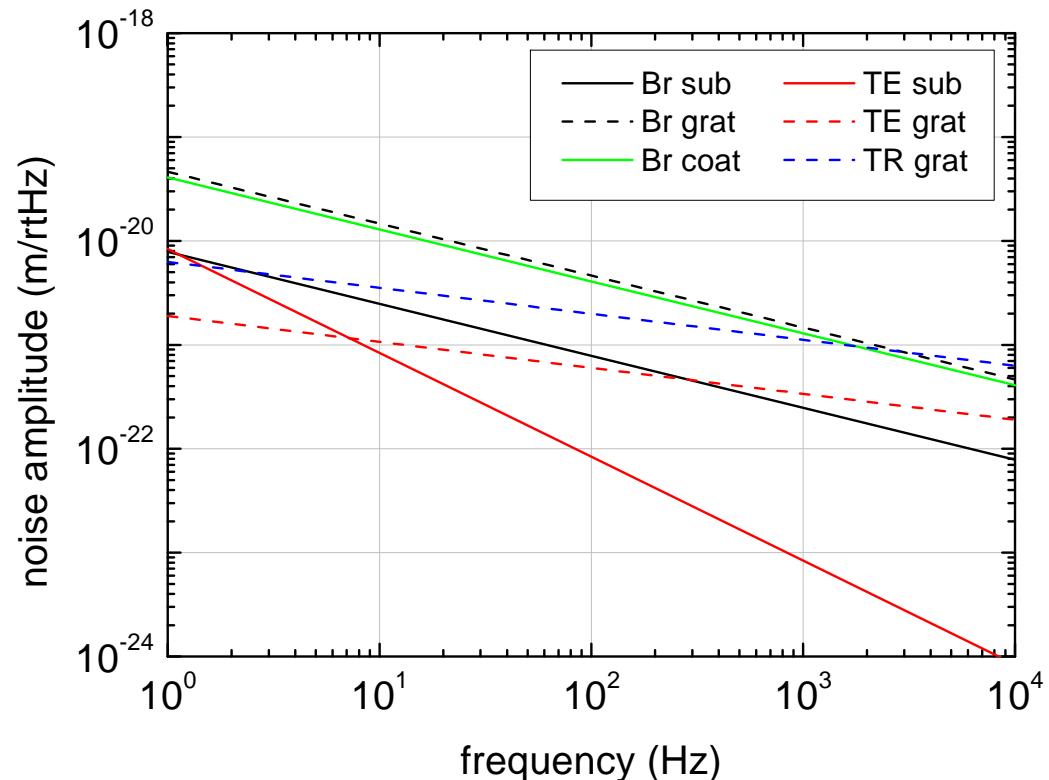


design wavelength	1064 nm
period	680 nm
ridgeheight	570 nm
ridgewidth	354 nm
$n_{tantalum}$	2.1
$n_{substrate}$	1.45

Repeated estimate of Brownian, TR and TE noise

Thermal noise of tantalum grating

Noise curves for tantalum grating



It is not just all about scaling layer thicknesses!

$$S_z(f) \propto \frac{k_B T}{f} \frac{d}{r_0^2} \phi$$

Coating thickness decreased by one order of magnitude – no benefit in Brownian TN for investigated configuration

Conclusion

Brownian coating noise is the dominating thermal noise process in current and future GWD's

grating reflectors circumvent lossy coating materials

a thermal noise reduction by a factor of 10 is predicted for the use of a monolithic silicon grating (demand cryogenics and 1550 nm)

Investigated tantalum grating configuration on fused silica compatible with existing detectors but promise no noise benefit

Acknowledgement:

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