

Metrology measurements and alignment in MUonE

Riccardo Nunzio Pilato
MuonE-Pisa meeting

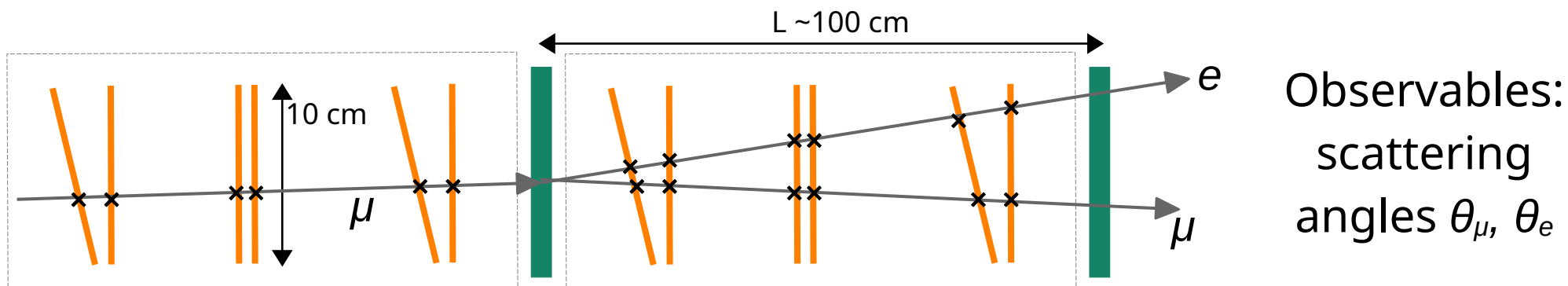
16 March 2026

Outline

- Why does MUonE need a precise alignment?
- Detector alignment workflow
- Detector description
- Metrology measurements in 2023 data reconstruction
- Metrology measurements to improve the MUonE simulation

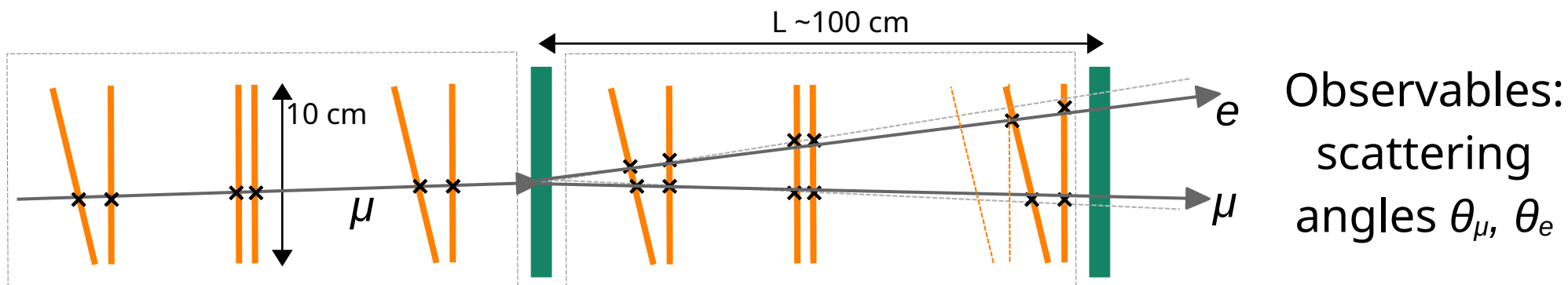
The need of precise alignment tools in MUonE

MUonE: measurement of $\mu e \rightarrow \mu e$ interactions
at 10ppm systematic accuracy



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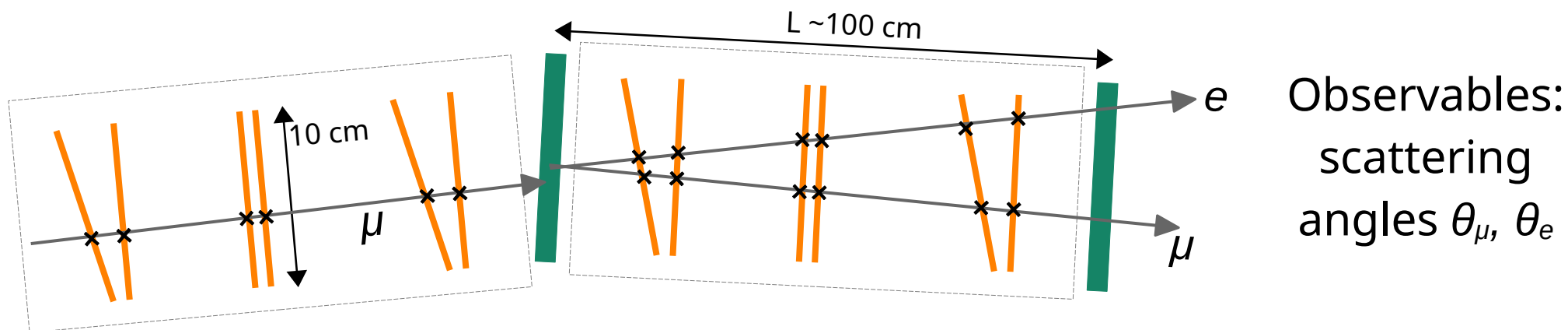


If the sensors z-position is wrong by $\sim 10 \mu\text{m}$:
10ppm systematic error on θ

$$\theta \sim \frac{x}{L} \quad \rightarrow \quad \frac{\Delta\theta}{\theta} \sim \frac{\Delta L}{L}$$

The need of precise alignment tools in MUonE

MUonE: measurement of $\mu e \rightarrow \mu e$ interactions
at 10ppm systematic accuracy



If the relative position/orientation
between two stations is wrong:
bad vertex reconstruction

(systematic uncertainties to be evaluated)

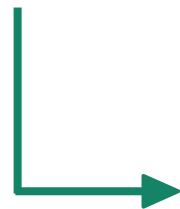
**Precise alignment
tools must be
developed**

MUonE alignment workflow

0. Use the stepper motors to align each station to the beam (and align each station relative to the others)
1. Laser survey: determine the position of the stations in the experimental hall. $O(100 \mu\text{m})$ precision
2. 3D scanner photogrammetry: determine position and orientation of 2S modules and targets (precision better than $100 \mu\text{m}$?)
3. Software alignment (iterative local χ^2 minimization): use events with one single muon passing through the detector to refine the metrology measurements

MUonE alignment workflow

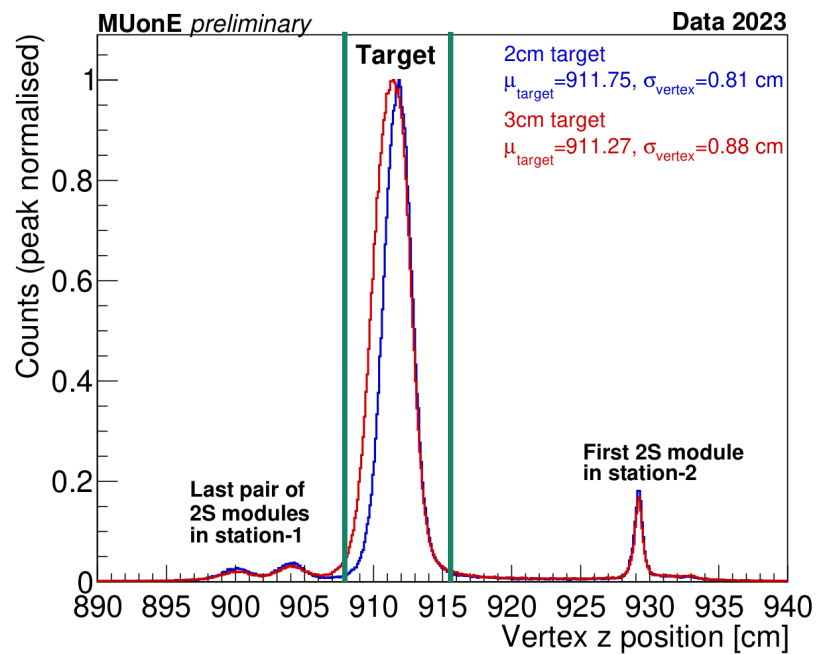
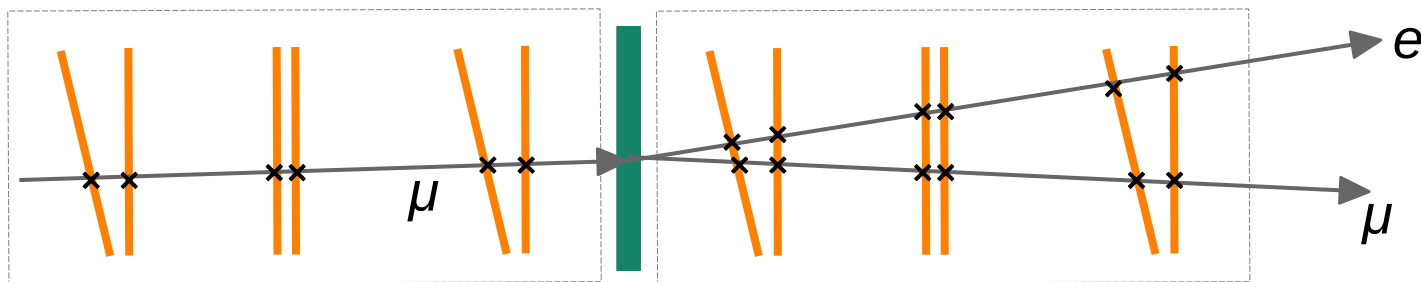
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**starting point of the software alignment.
Metrology results must be expressed
in the track reconstruction formalism**

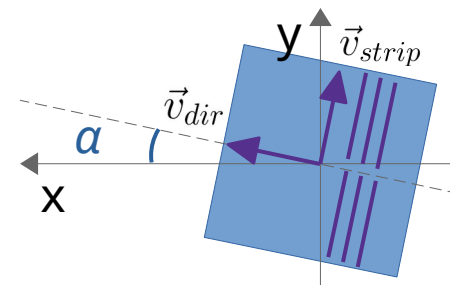
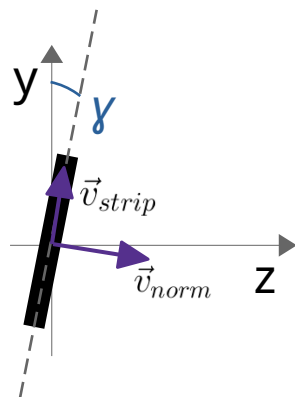
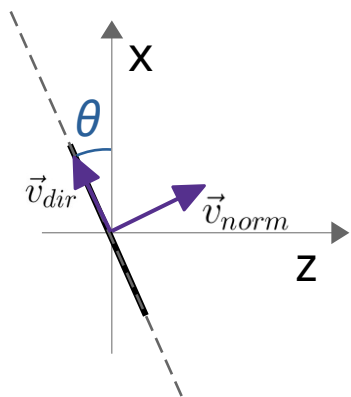
Detector description

- Target (x, y, z) position. Needed for the event selection: select interactions that actually occurred in the target



Detector description

- 2S modules (x, y, z) position and orientation
(3 angular parameters α , θ , γ). Needed for track reconstruction



- \mathbf{v}_{strip} = strips direction
- \mathbf{v}_{dir} = direction measured by the module (orthogonal to \mathbf{v}_{strip})
- \mathbf{v}_{norm} = vector orthogonal to the module surface

$$\alpha = \arctan \left(-\frac{v_{strip,X}}{v_{strip,Y}} \right)$$

$$\gamma = \arcsin (v_{strip,Z})$$

$$\theta = \arctan \left(-\frac{v_{dir,Z}}{v_{norm,Z}} \right)$$

Full calculations
in backup

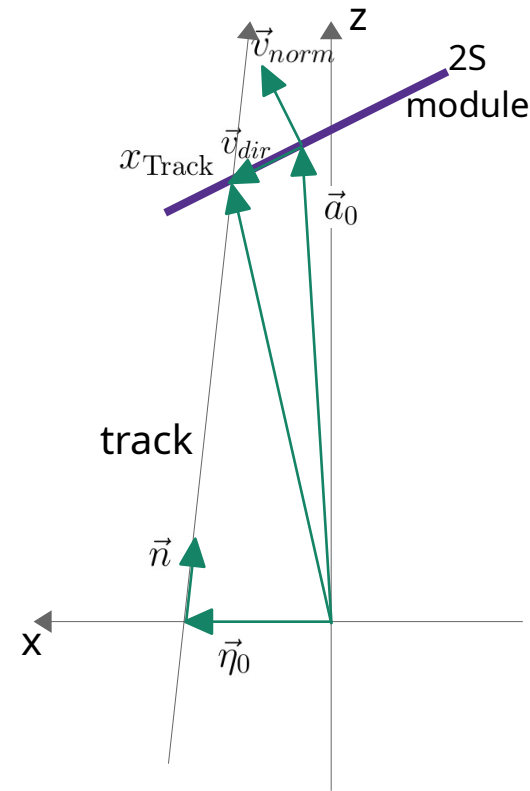
Detector description in the track reconstruction

$$\chi_{\text{Track}}^2 = \sum_{i=0}^{N_{\text{Modules}}} \left(\frac{x_{\text{Track},i}(\vec{p}) - x_{\text{Stub},i}}{\sigma_{\text{Stub}}} \right)^2 \quad \vec{p} = (x_{\text{Slope}}, x_0, y_{\text{Slope}}, y_0)$$

x_{Stub} : stub position on the 2S module

x_{Track} : track position along the measurement direction of the 2S module

$$x_{\text{Track},i}(\vec{p}) = (\vec{\eta}_0 + \vec{n}t_i^* - \vec{a}_{0,i}) \cdot \vec{v}_{dir,i}$$



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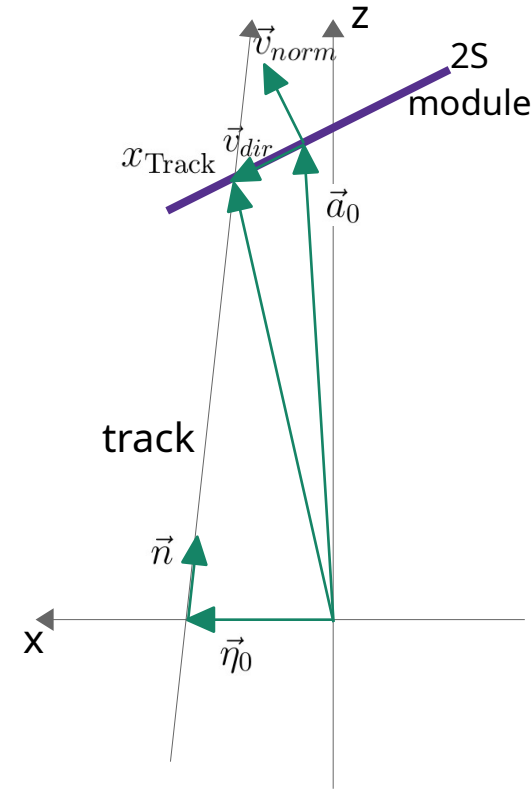
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 Fit parameters

$$\vec{\eta}_0 = \begin{pmatrix} x_0 \\ y_0 \\ 0 \end{pmatrix} \quad \vec{n} = \begin{pmatrix} x_{\text{Slope}} \\ y_{\text{Slope}} \\ 1 \end{pmatrix}$$



Detector description in the track reconstruction

$$\chi_{\text{Track}}^2 = \sum_{i=0}^{N_{\text{Modules}}} \left(\frac{x_{\text{Track},i}(\vec{p}) - x_{\text{Stub},i}}{\sigma_{\text{Stub}}} \right)^2 \quad \vec{p} = (x_{\text{Slope}}, x_0, y_{\text{Slope}}, y_0)$$

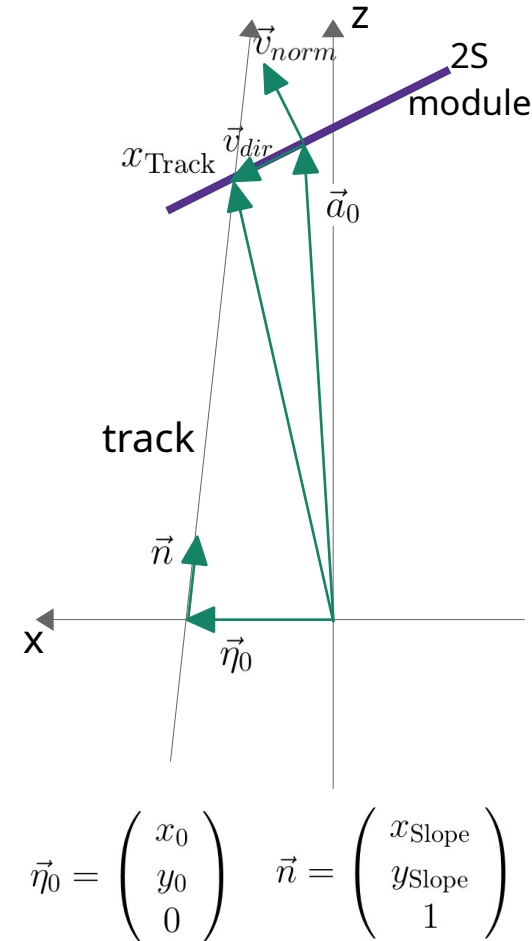
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↑
↑
 2S module
 position and orientation

$$\vec{a}_{0,i} = \begin{pmatrix} x_{\text{module}} \\ y_{\text{module}} \\ z_{\text{module}} \end{pmatrix} \quad \vec{v}_{\text{Dir},i}(\alpha, \theta, \gamma) \quad \vec{v}_{\text{Norm},i}(\alpha, \theta, \gamma)$$



Detector description in the track reconstruction

$$\chi_{\text{Track}}^2 = \sum_{i=0}^{N_{\text{Modules}}} \left(\frac{x_{\text{Track},i}(\vec{p}) - x_{\text{Stub},i}}{\sigma_{\text{Stub}}} \right)^2 \quad \vec{p} = (x_{\text{Slope}}, x_0, y_{\text{Slope}}, y_0)$$

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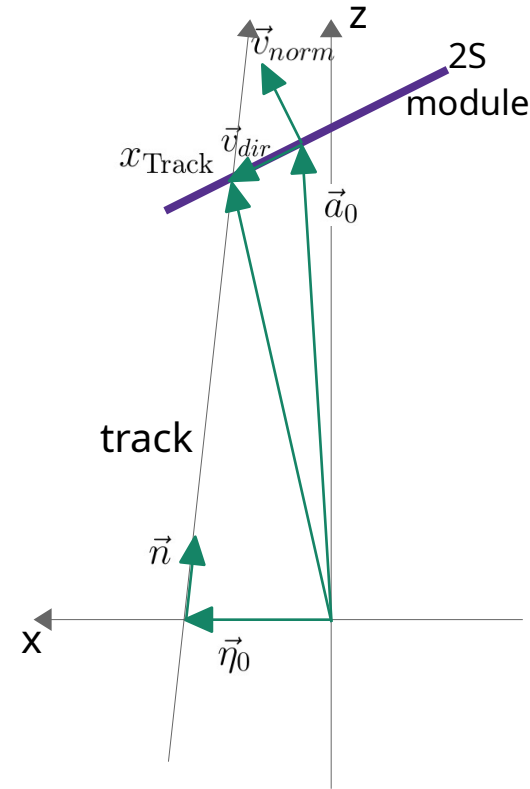
x_{Track} : track position along the measurement direction of the 2S module

$$x_{\text{Track},i}(\vec{p}) = (\vec{\eta}_0 + \vec{n}t_i^* - \vec{a}_{0,i}) \cdot \vec{v}_{\text{dir},i}$$

$$t_i^* = \frac{(\vec{a}_{0,i} - \vec{\eta}_0) \cdot \vec{v}_{\text{norm},i}}{\vec{n} \cdot \vec{v}_{\text{norm},i}}$$

Parameter t to evaluate the track position on the 2S module.

Depends both on the fit parameters and the 2S module position and orientation



$$\vec{\eta}_0 = \begin{pmatrix} x_0 \\ y_0 \\ 0 \end{pmatrix} \quad \vec{n} = \begin{pmatrix} x_{\text{Slope}} \\ y_{\text{Slope}} \\ 1 \end{pmatrix}$$

$$\vec{a}_{0,i} = \begin{pmatrix} x_{\text{module}} \\ y_{\text{module}} \\ z_{\text{module}} \end{pmatrix} \quad \vec{v}_{\text{Dir},i}(\alpha, \theta, \gamma) \quad \vec{v}_{\text{Norm},i}(\alpha, \theta, \gamma)$$

Metrology measurements in 2023

The first attempt

[Carlo's slides - 5th MUonE collab meeting](#)

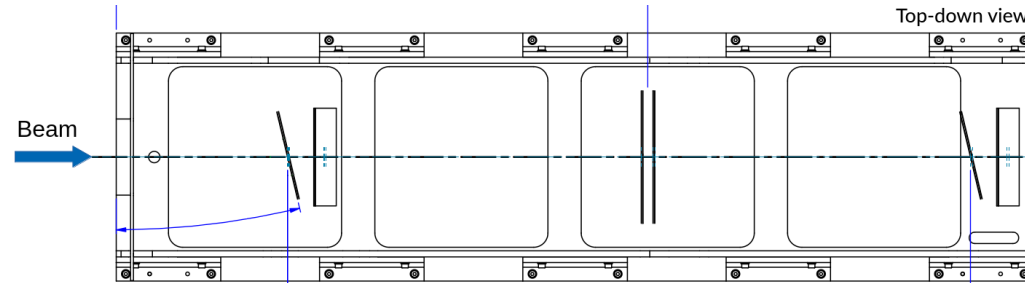


After various meetings with metrology group at CERN, we developed a five-step procedure:

- 1) **Laser survey** on the beamline (main Invar structure of the whole station, 2S installed)
- 2) **Metrology** on each whole station (2S installed), using the device **Leitz PMM-C**:
measuring uncertainty: $\pm(0.3\mu\text{m} + L/1000)$
- 3) **Metrology** on the singles module un-installed from the station, using the device **ZEISS O-Inspect**:
measuring uncertainty: $2.2\mu\text{m} + L/150\text{mm}$
- 4) Find the rototranslation that brings the spheres (fiducial markers) on the frames holding the modules of measurements 2) and 3) to coincide
- 5) Find the rototranslation that brings the spheres on the main structure of measurements 1) and 2) to coincide
- 6) **Translate the results into numbers that can be used in FairMUonE for track reconstruction and simulation**

Metrology measurements in 2023

2S modules position



A) Metrology: position of the sensor facing outwards

X modules



Y modules



U modules

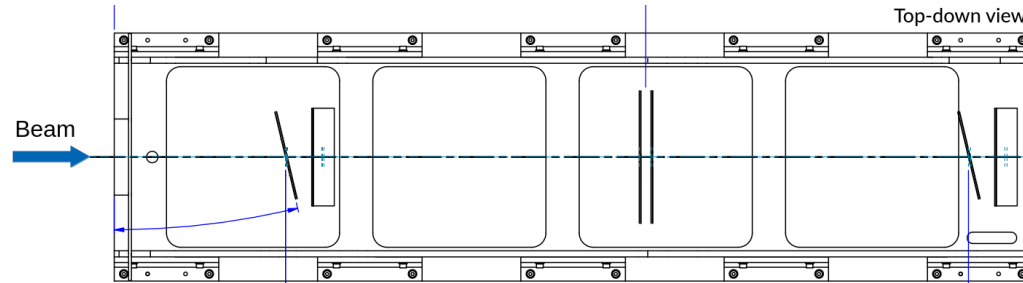


V modules



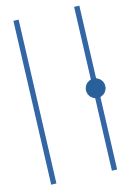
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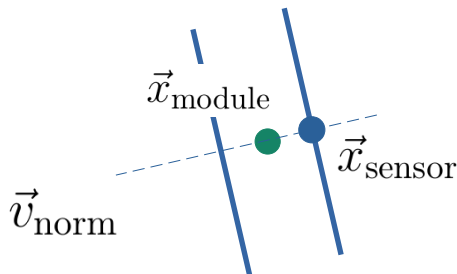
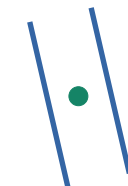
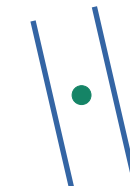
U modules



V modules



B) FairMUonE: the module position is averaged between the two sensors positions



$$\vec{x}_{\text{module}} = \vec{x}_{\text{sensor}} \pm \vec{v}_{\text{norm}} \cdot \Delta s$$

$$\Delta s = \frac{\text{sensors spacing} + 320 \mu\text{m}}{2}$$

Metrology measurements in 2023

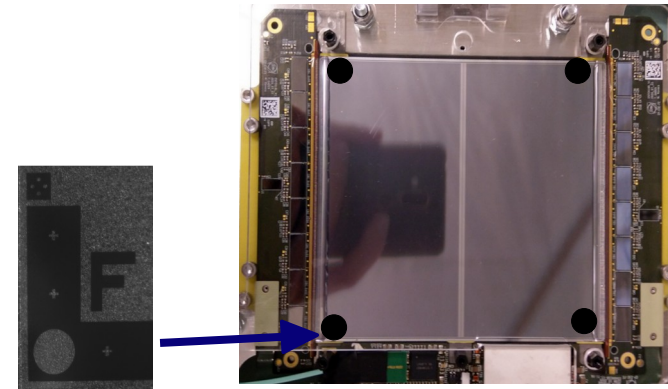
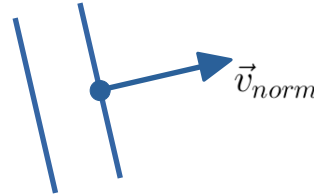
2S modules orientation

Metrology measured:

A) \mathbf{v}_{norm}

B) reference markers on the modules

To be computed: \mathbf{v}_{dir} and \mathbf{v}_{strip}



Metrology measurements in 2023

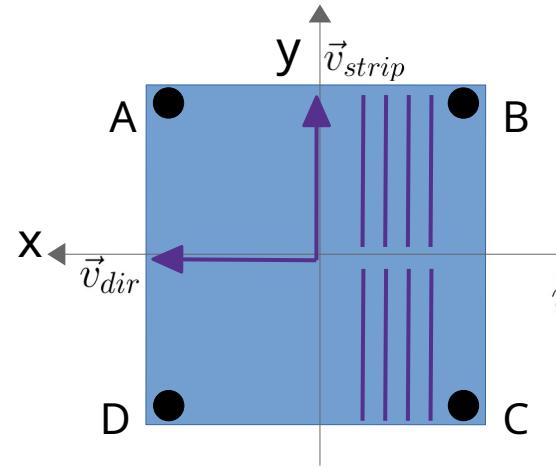
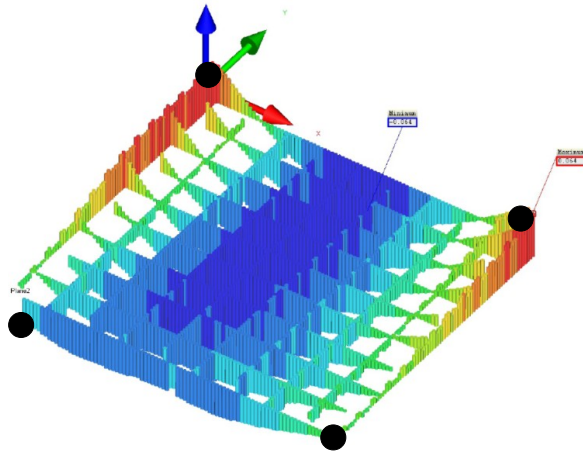
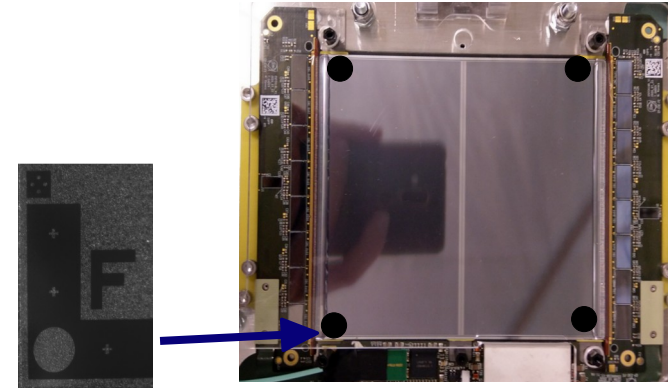
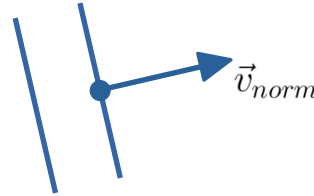
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A) \mathbf{v}_{norm}

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$$\vec{v}_{dir} = \vec{A} - \vec{B} = \vec{D} - \vec{C}$$

$$\vec{v}_{strip} = \vec{A} - \vec{D} = \vec{B} - \vec{C}$$

1) The sensors are not flat

(~100 μm deformation): project the four markers on the average plane

2) Compute \mathbf{v}_{dir} and \mathbf{v}_{strip}

(take the average of the two possibilities)

Outcome: modules position and orientation can be used as starting point of the software alignment

Estimated precision on these parameters:

$$\begin{array}{lll} \Delta x = 200 \mu\text{m} & \Delta y = 200 \mu\text{m} & \Delta z = 100 \mu\text{m} \\ \Delta \alpha = 1.8 \text{ mrad} & \Delta \theta = 1.0 \text{ mrad} & \Delta \gamma = 1.0 \text{ mrad} \end{array}$$

More details
in backup

Station 0. $z_{origin} = 8002.908 \text{ mm}$

ModuleID	$x_{offset} \text{ [mm]}$	$y_{offset} \text{ [mm]}$	$z_{module} \text{ [mm]}$	$\theta_{offset} \text{ [mrad]}$	$\gamma_{offset} \text{ [mrad]}$	$\alpha_{offset} \text{ [mrad]}$
0 (X)	1.405	0.094	166.420	4.564	-4.403	0.800
1 (Y)	-0.407	0.970	204.743	1.146	-0.020	1.019
2 (U)	-1.138	0.231	537.205	2.353	-2.034	4.009
3 (V)	-0.696	0.680	551.588	-2.150	-2.023	-5.730
4 (X)	1.092	0.094	885.526	-0.706	-0.003	1.009
5 (Y)	0.001	0.244	923.722	-0.972	0.983	2.108

Station 1. $z_{origin} = 9014.997 \text{ mm}$

ModuleID	$x_{offset} \text{ [mm]}$	$y_{offset} \text{ [mm]}$	$z_{module} \text{ [mm]}$	$\theta_{offset} \text{ [mrad]}$	$\gamma_{offset} \text{ [mrad]}$	$\alpha_{offset} \text{ [mrad]}$
6 (X)	0.217	-2.102	166.418	-0.075	11.171	-2.536
7 (Y)	-1.152	-1.314	204.608	2.402	0.315	-0.278
8 (U)	-0.851	-0.229	536.988	4.271	1.387	0.762
9 (V)	-0.863	-0.003	551.402	1.285	-4.247	4.689
10 (X)	1.379	0.589	885.290	-1.564	-5.855	-3.935
11 (Y)	0.030	1.739	923.382	3.896	0.114	-4.178

Software alignment procedure

- 1) Select events with 1 stub/module
- 2) Track reconstruction using all modules
- 3) Find the alignment corrections on each module separately:
numerical minimisation of the local χ^2
Start from the metrology and repeat iteratively until convergence

$$\chi_{\text{align, module-}j}^2 = \sum_{i=0}^{N_{\text{tracks}}} \left(\frac{x_{\text{Track}}^{ij}(\vec{p}_j) - x_{\text{Hit}}^{ij}}{\sigma_{\text{Hit}}^j} \right)^2$$

\mathbf{p} = alignment parameters

- XY modules: 4 parameters aligned:
 $x, y_{\text{offset}}, \alpha_{\text{offset}}, \theta_{\text{offset}}$
- UV modules: 3 parameters aligned:
 $x, y_{\text{offset}}, \alpha_{\text{offset}}$

Final precision (studied by simulation): $\Delta x, y_{\text{offset}} \sim 5 \mu\text{m}$ $\Delta \alpha, \theta_{\text{offset}} \sim 2 \text{ mrad}$

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 $x, y_{\text{offset}}, \alpha_{\text{offset}}, \theta_{\text{offset}}$
- UV modules: 3 parameters aligned:
 $x, y_{\text{offset}}, \alpha_{\text{offset}}$

**NB: some alignment parameters
are not minimised in this procedure.**

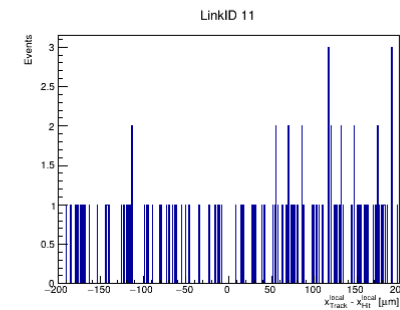
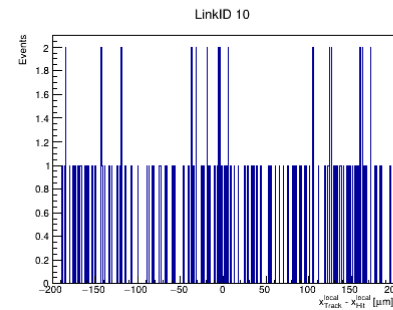
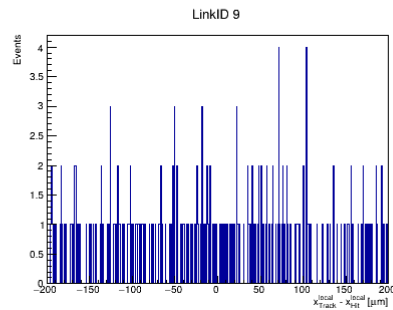
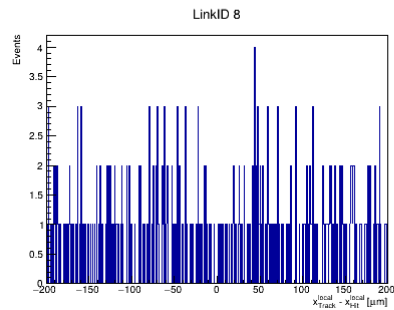
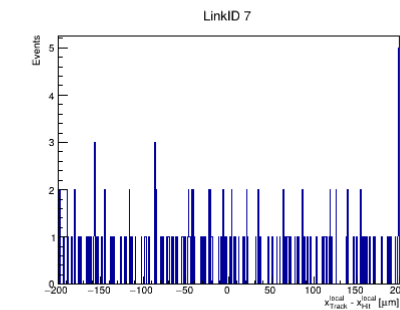
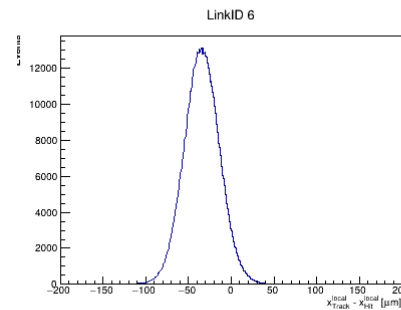
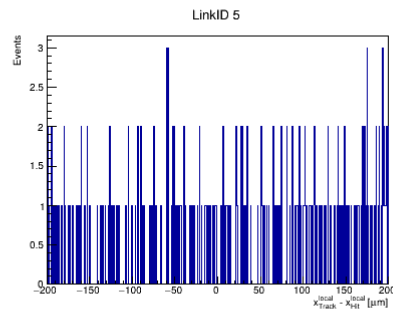
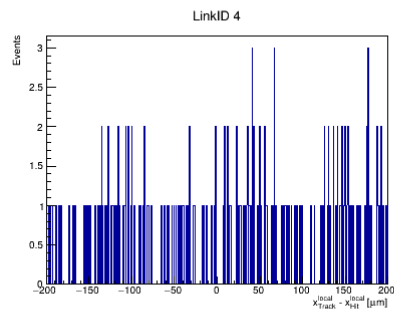
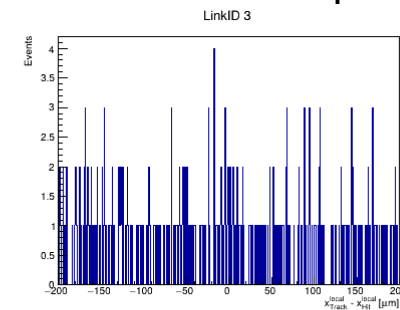
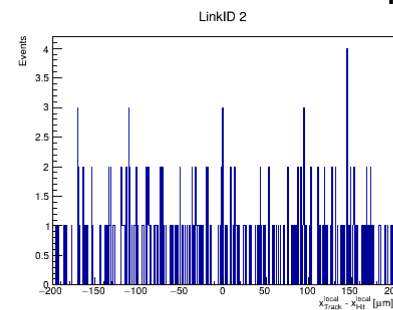
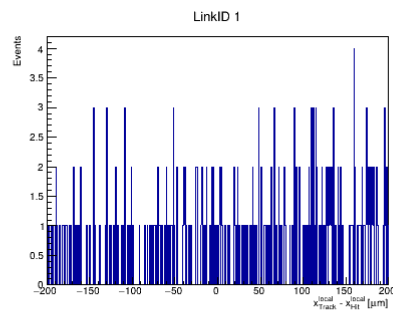
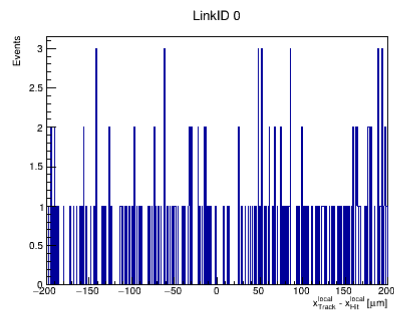
Their value is fixed to the metrology outcome (y, θ_{UV}, z)

Residuals before the alignment

ideal detector description (CAD)

Residuals $x_{\text{track}} - x_{\text{Stub}}$ for
all the modules

No clear peaks within $\pm 200 \mu\text{m}$, except for
module 6 \rightarrow poor detector description

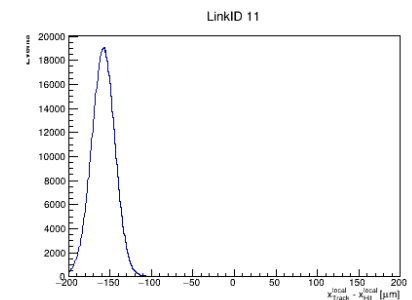
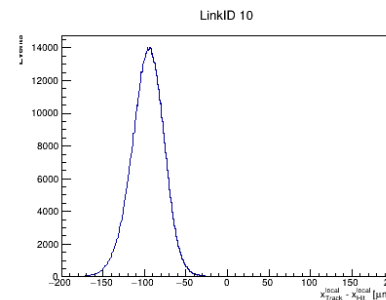
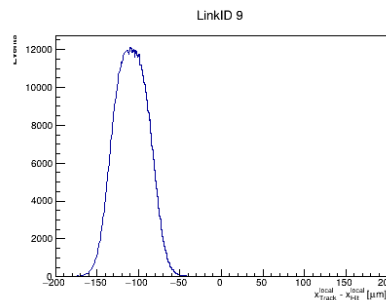
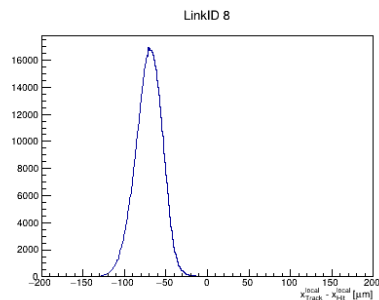
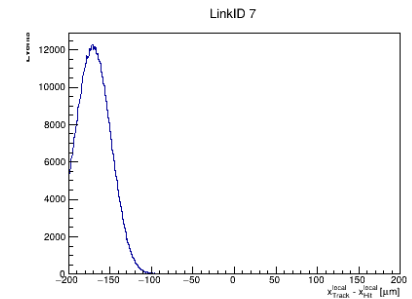
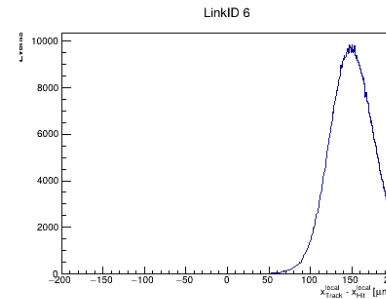
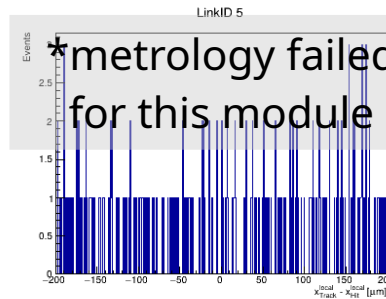
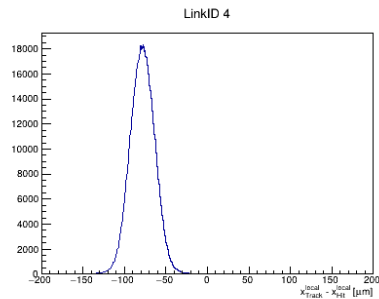
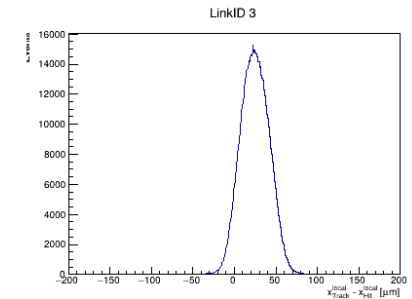
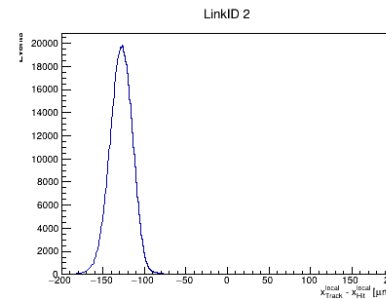
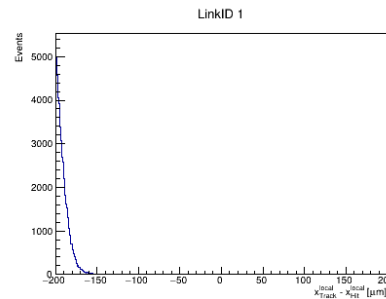
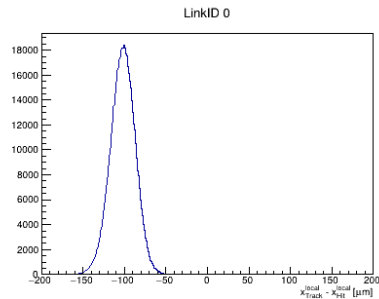


Residuals before the alignment

detector description from metrology measurements

Residuals $x_{\text{track}} - x_{\text{Stub}}$ for all the modules

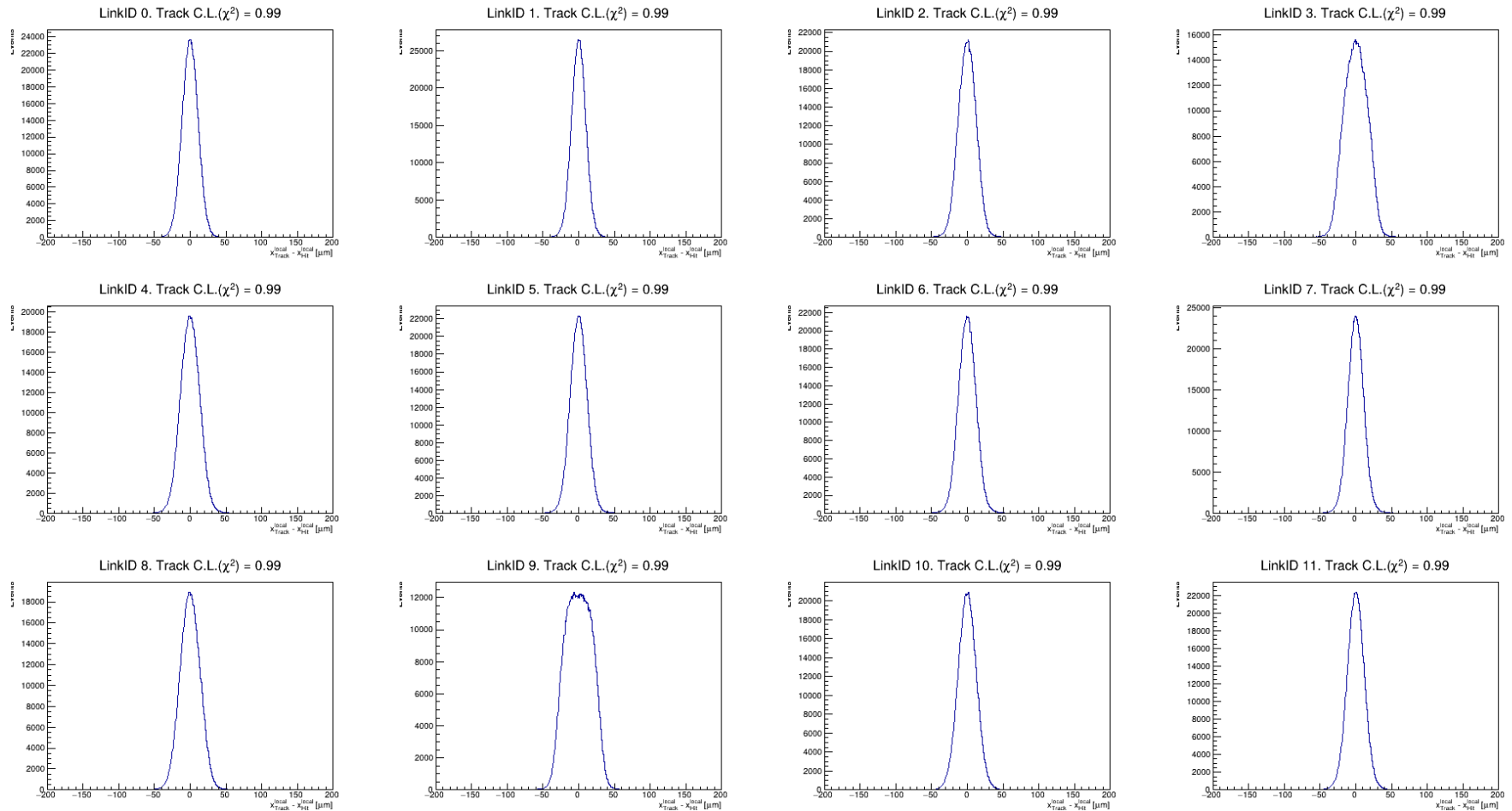
All residuals are centered within $\sim 200 \mu\text{m}$



Residuals after the alignment

Residuals $x_{\text{track}} - x_{\text{Stub}}$ for
all the modules

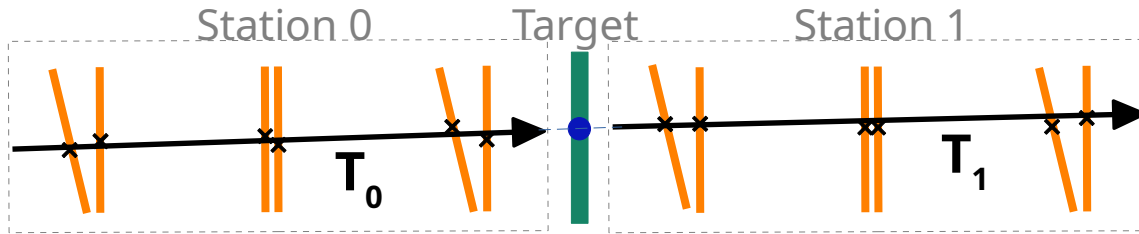
All residuals are well centered within $0.1 \mu\text{m}$
Using the result of metrology measurements allows faster
convergence towards parameters closer to the real value



Metrology measurements in the MUonE simulation

- MUonE: precise data/MonteCarlo comparison
- To be achieved, a precise simulation of the detector geometry is required
- The metrology measurements are used to simulate a realistic detector geometry, which is then aligned following the same procedure as the real data
- This has a huge impact in reproducing the angular resolution of the real detector

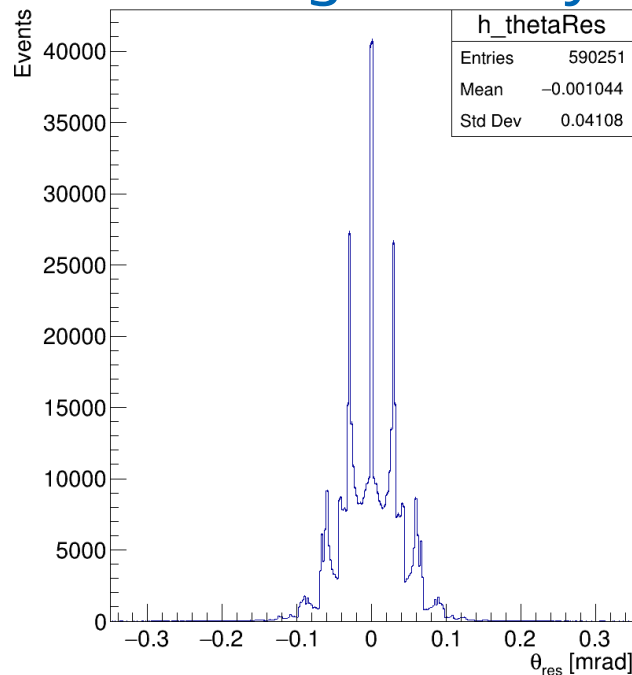
Angular resolution



Define the angular resolution as

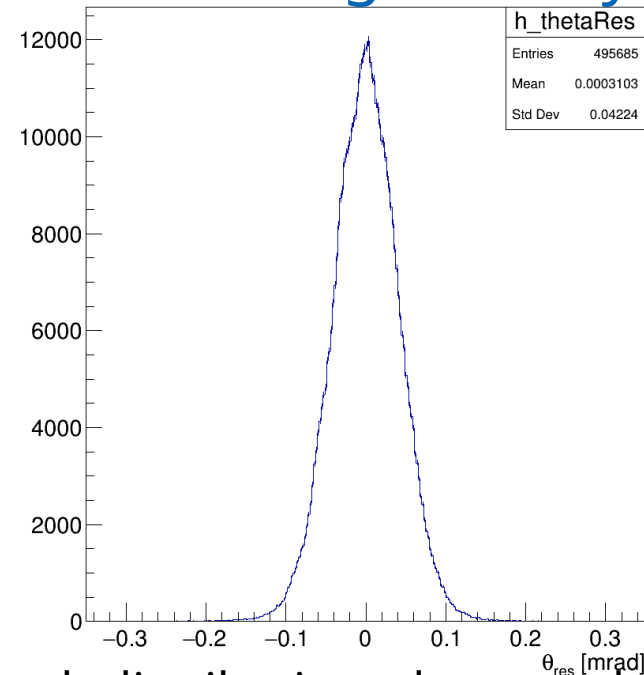
$$\theta_{res} = \theta_0 - \theta_1$$

Ideal geometry



These peaks are due to the binary strip readout of the 2S modules, which are visible in a perfectly aligned apparatus

Realistic geometry



Smooth distribution, closer to the data (the actual angular resolution value depends on the simulation of 2S modules electronics)₂₆

Metrology measurements in the MUonE simulation

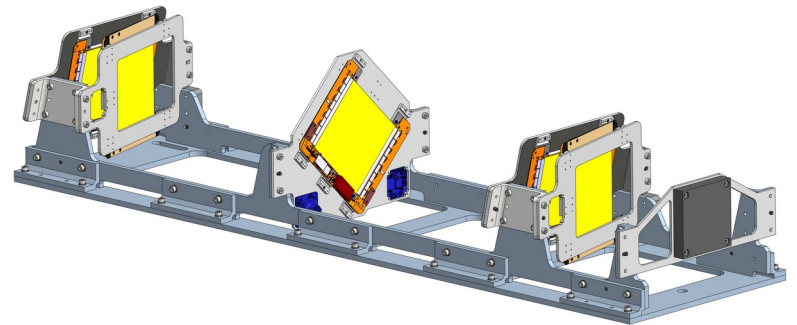
Possible improvement

Current simulation



Only target and 2S modules are simulated.
The mechanical structure is missing
(i.e. objects are floating in air)

Improved simulation



Include the invar structure from the 3D
scan → simulate muon interaction with the
mechanical structure

Conclusions

- Metrology measurements are crucial for MUonE
- **Analysis of real data:**
metrology is used as starting point of the software alignment.
Current sw alignment precision: $\Delta x, y_{\text{offset}} \sim 5 \mu\text{m}$ $\Delta \alpha, \theta_{\text{offset}} \sim 2 \text{ mrad}$
Hopefully this can improve in 2025 given the new metrology procedure (3D scan).
- **MUonE simulation:**
metrology is used to simulate a detector which has realistic misalignments
Possible improvement in 2025: include the invar 3D scan in the simulation (and possibly also the target 3D scan)

Backup

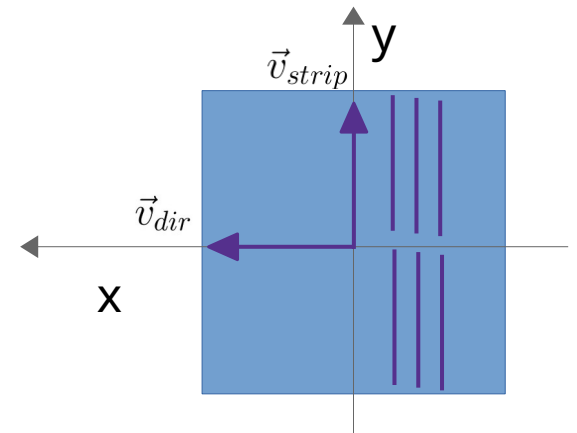
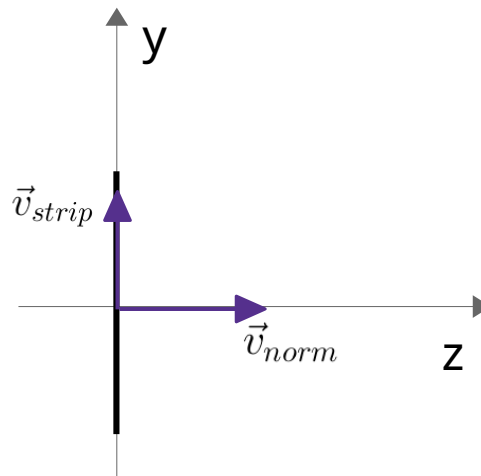
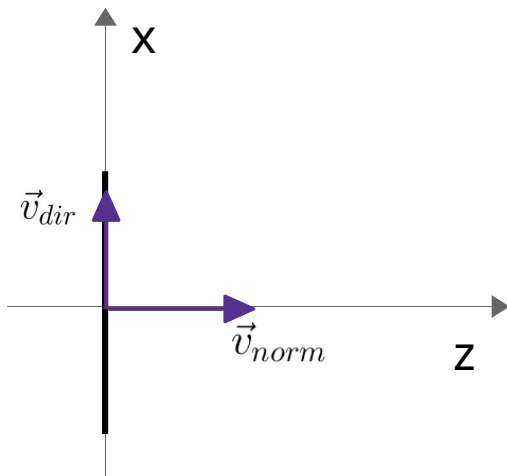
2S modules orientation – calculations

Start with an X module perpendicular to the beam axis

$$\vec{v}_{dir} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$\vec{v}_{strip} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$\vec{v}_{norm} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$



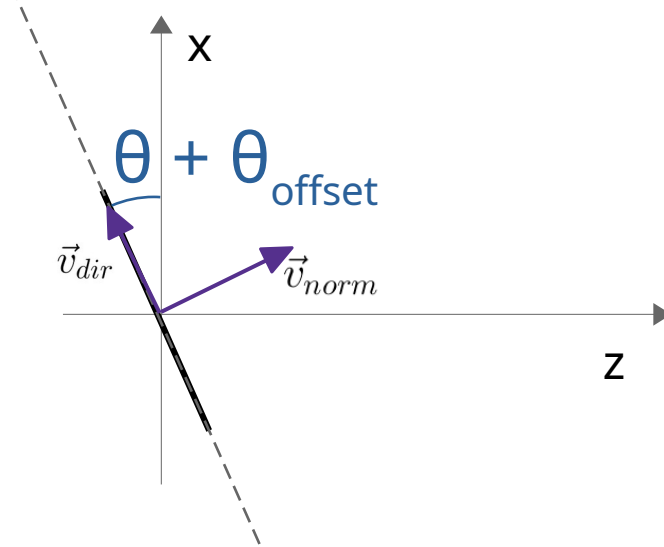
2S modules orientation – calculations

1) Apply the tilt

$$\vec{v}_{dir} = R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$\vec{v}_{strip} = R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$\vec{v}_{norm} = R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$



$$\tilde{\alpha} = \alpha + \alpha_{offset}$$

$$\tilde{\gamma} = \gamma + \gamma_{offset}$$

$$\tilde{\theta} = \theta + \theta_{offset}$$

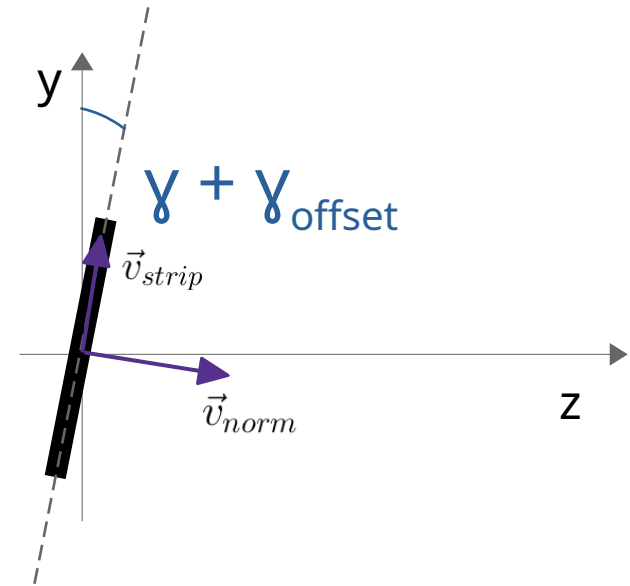
2S modules orientation – calculations

2) Apply the γ rotation

$$\vec{v}_{dir} = R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$\vec{v}_{strip} = R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$\vec{v}_{norm} = R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$



$$\tilde{\alpha} = \alpha + \alpha_{offset}$$

$$\tilde{\gamma} = \gamma + \gamma_{offset}$$

$$\tilde{\theta} = \theta + \theta_{offset}$$

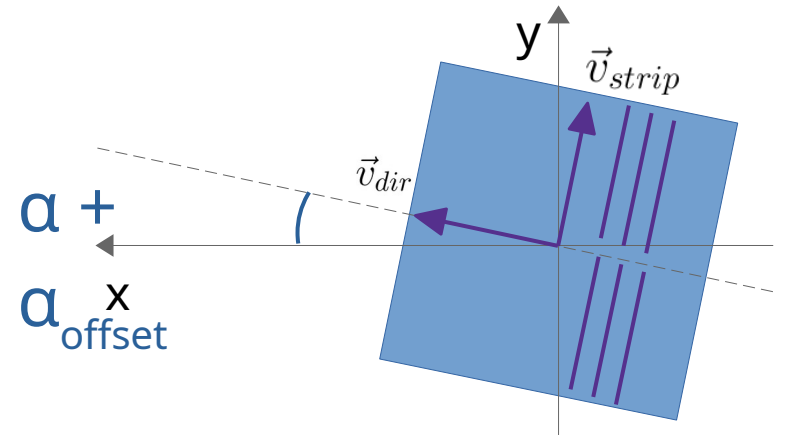
2S modules orientation – calculations

3) Rotate to adjust the strip orientation

$$\vec{v}_{dir} = R_Z(\tilde{\alpha}) \cdot R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$\vec{v}_{strip} = R_Z(\tilde{\alpha}) \cdot R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$\vec{v}_{norm} = R_Z(\tilde{\alpha}) \cdot R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$



$$\tilde{\alpha} = \alpha + \alpha_{offset}$$

$$\tilde{\gamma} = \gamma + \gamma_{offset}$$

$$\tilde{\theta} = \theta + \theta_{offset}$$

2S modules orientation – calculations

$$\vec{v}_{dir} = R_Z(\tilde{\alpha}) \cdot R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \cos \tilde{\alpha} \cos \tilde{\theta} - \sin \tilde{\alpha} \sin \tilde{\gamma} \sin \tilde{\theta} \\ \sin \tilde{\alpha} \cos \tilde{\theta} + \cos \tilde{\alpha} \sin \tilde{\gamma} \sin \tilde{\theta} \\ -\cos \tilde{\gamma} \sin \tilde{\theta} \end{pmatrix}$$

$$\vec{v}_{strip} = R_Z(\tilde{\alpha}) \cdot R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \begin{pmatrix} -\sin \tilde{\alpha} \cos \tilde{\gamma} \\ \cos \tilde{\alpha} \cos \tilde{\gamma} \\ \sin \tilde{\gamma} \end{pmatrix}$$

$$\vec{v}_{norm} = R_Z(\tilde{\alpha}) \cdot R_X(\tilde{\gamma}) \cdot R_Y(\tilde{\theta}) \cdot \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} = \begin{pmatrix} \cos \tilde{\alpha} \sin \tilde{\theta} + \sin \tilde{\alpha} \sin \tilde{\gamma} \cos \tilde{\theta} \\ \sin \tilde{\alpha} \sin \tilde{\theta} - \cos \tilde{\alpha} \sin \tilde{\gamma} \cos \tilde{\theta} \\ \cos \tilde{\gamma} \cos \tilde{\theta} \end{pmatrix}$$

$$\tilde{\alpha} = \arctan \left(-\frac{v_{strip,X}}{v_{strip,Y}} \right) \quad \tilde{\gamma} = \arcsin (v_{strip,Z}) \quad \tilde{\theta} = \arctan \left(-\frac{v_{dir,Z}}{v_{norm,Z}} \right)$$

2023 survey – determine the errors on modules position and orientation

a) 2S modules position

Determined from the position of fiducial markers on the frames + optical reference markers on the 2S modules.

3 sets of measurements:

- 1) laser survey on the beamline
- 2) metrology in lab with frames mounted ON the station
- 3) metrology in lab with frames OFF the station

Carlo's note on metrology
Carlo's slides on metrology 5th collab meeting

Found differences

up to 400 μm in the measurements

ON and OFF the station

Conservative estimate:

$\Delta x, y = 200 \mu\text{m}$

$\Delta z = 100 \mu\text{m}$

(see Carlo's presentation)

Station1

X: P41
Y: P42
U,V: B3,B5
U,V: B3,B5
X: P4V1
Y: FNL4
Y: FNL4

Vertical, on the structure

162.462	78.1686	176.305
152.595	114.814	191.014
165.269	111.411	165.071
165.269	111.411	165.071
162.255	77.6505	176.237
152.352	114.976	190.803

Horizontal, off the structure

162.686	78.173	176.482
152.618	114.816	191.006
165.032	111.356	165.008
165.034	111.356	165.005
162.247	77.65	176.264
152.343	114.976	190.775

$\Delta \sim 200 \mu\text{m}$

Station2

X: KIT 1
Y: BRN 10
U,V: KIT N
U,V: KIT N
X: KIT 2
Y: BRN 11

162.171	77.7927	175.902
152.291	114.818	190.621
165.242	111.401	165.19
165.242	111.401	165.19
162.22	77.837	176.31
152.124	115.076	190.677

161.775	77.8191	175.564
152.14	114.917	190.538
165.192	111.309	165.302
165.16	111.334	165.28
162.015	77.8308	176.134
152.214	115.067	190.672

$\Delta \sim 400 \mu\text{m}$

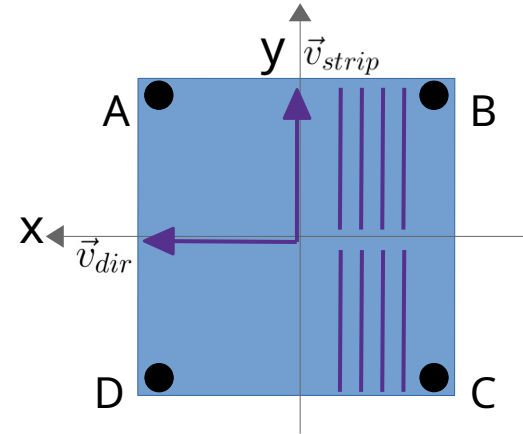
2023 survey – determine the errors on modules position and orientation

b) 2S modules orientation

$$\begin{aligned}\vec{v}_{dir} &= \vec{A} - \vec{B} = \vec{D} - \vec{C} \\ \vec{v}_{strip} &= \vec{A} - \vec{D} = \vec{B} - \vec{C}\end{aligned} \quad \longrightarrow \quad 1) \Delta v = 200 \mu\text{m}$$

(see previous slide)

A, B, C, D: optical markers on the 2S modules



2) These vectors are normalized, then the modules orientation is parameterized using the angles:

$$\tilde{\alpha} = \arctan \left(-\frac{v_{strip,X}}{v_{strip,Y}} \right)$$

$$\tilde{\gamma} = \arcsin (v_{strip,Z})$$

$$\tilde{\theta} = \arctan \left(-\frac{v_{dir,Z}}{v_{norm,Z}} \right)$$

3) Errors on α , θ , γ are then obtained by error propagation

$$\Delta\alpha = 1.8 \text{ mrad}$$

$$\Delta\theta = 1.0 \text{ mrad}$$

$$\Delta\gamma = 1.0 \text{ mrad}$$