

# Short summary on the study of the ET Cryogenic Plant



*Steffen Grohmann*



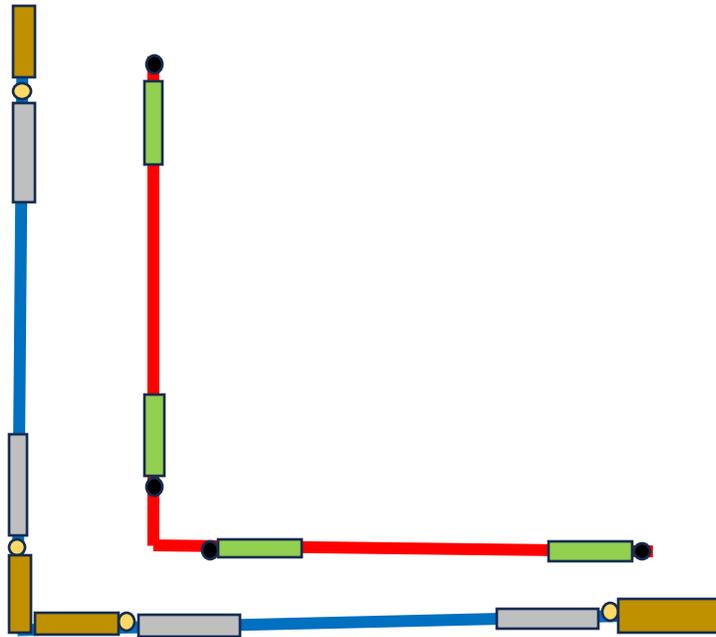
*Fulvio Ricci*



# Cryogenics for the L shape configuration

*At the L vertex n. 6 Cryopumps, 2 Cryostats*

*At each end n.3 Cryopumps, 1 Cryostat*



n. 4 ○ Cold test mass

n. 4 ● Hot test mass

n. 4 □ Cryopump of the Hot Interferometer

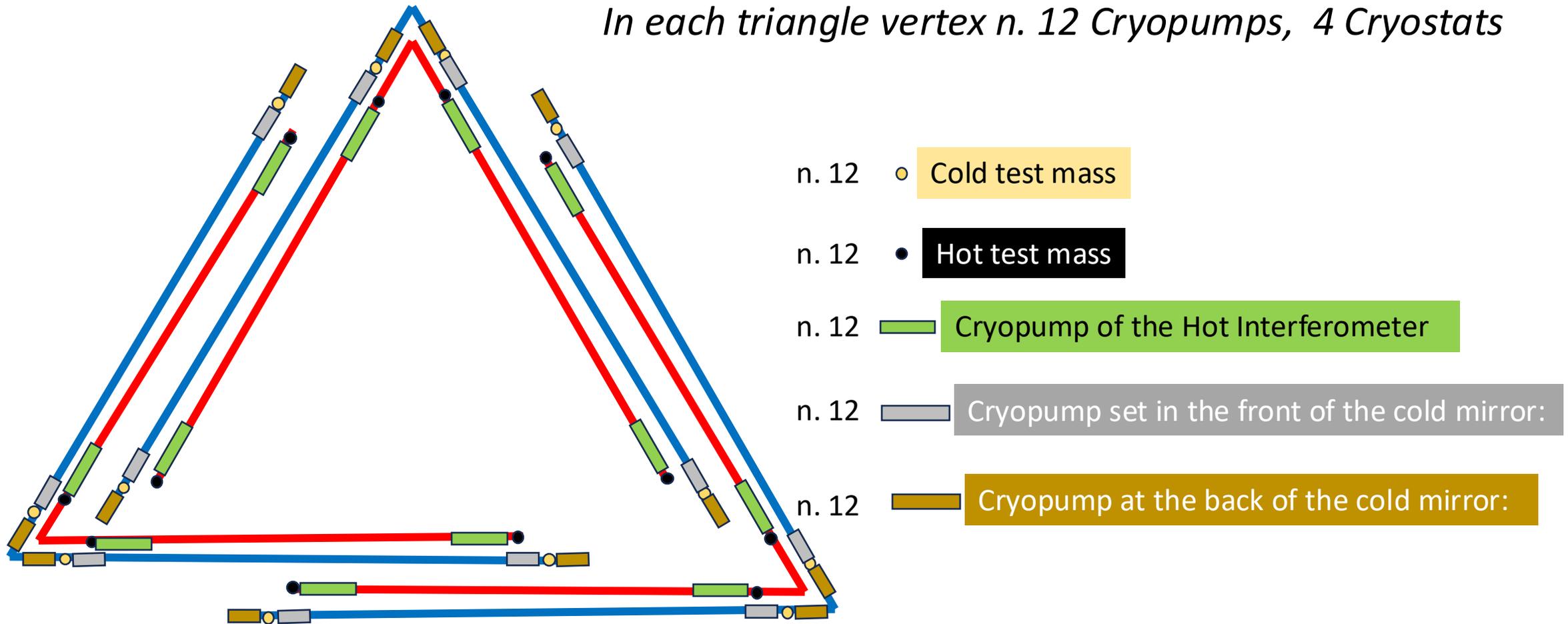
n. 4 □ Cryopump set in the front of the cold mirror:

n. 4 □ Cryopump at the back of the cold mirror:

***Disclaimer: the inclusion in the project of addition cryopumps (shorter) is under study !!***

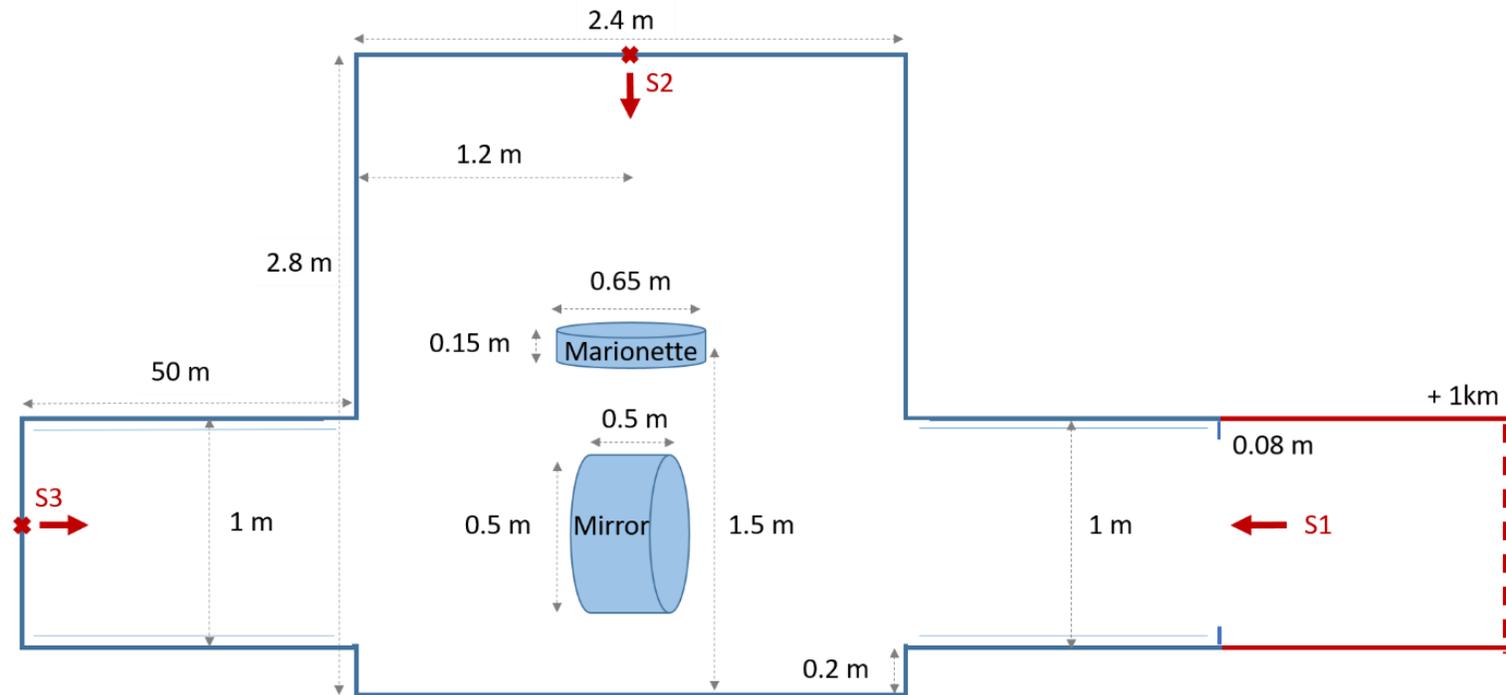
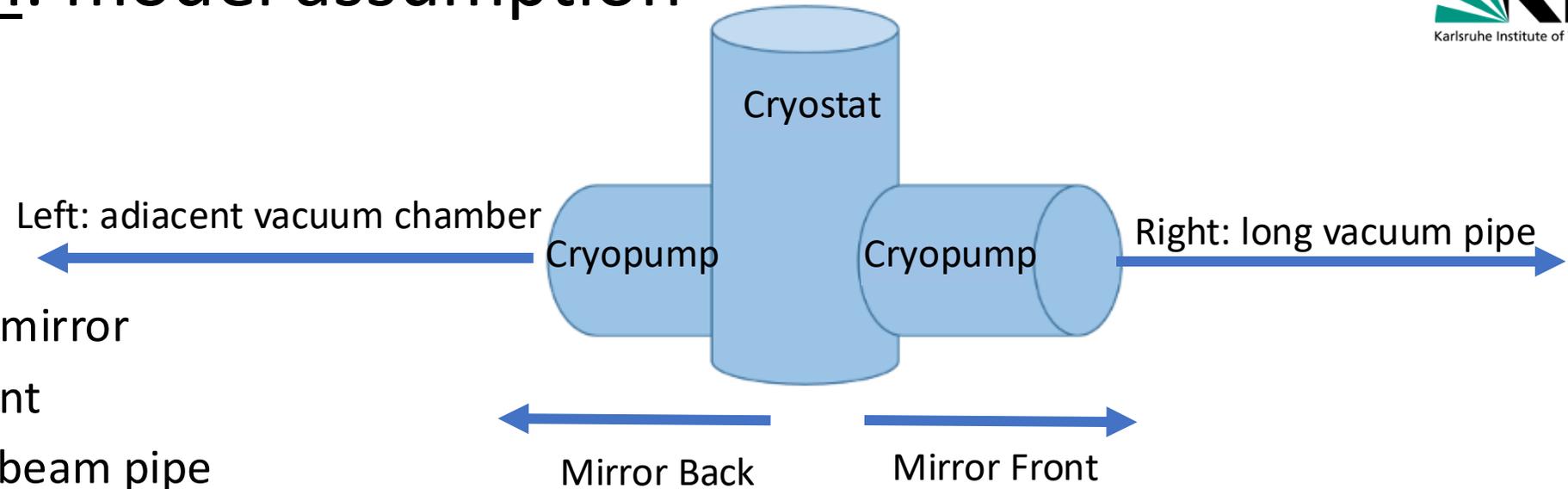
# Cryogenics for the triangular configuration

*In each triangle vertex n. 12 Cryopumps, 4 Cryostats*



***Disclaimer: the inclusion in the project of addition cryopumps (shorter) is under study !!***

# ET- LF vacuum: model assumption



- Cryostat with 10-20 K mirror
- Suspension not relevant
- S1: source by 1000 m beam pipe outgassing (right)
- S2: upper tower source (with developed pre-concept for semi-closure drastically reduced to  $2 \cdot 10^{-9} \text{ Pa} \cdot \text{m}^3/\text{s}$  for  $\text{H}_2$  and  $\text{H}_2\text{O}$  each)
- S3: adjacent tower source ( $10^{-7}$  and  $10^{-6} \text{ Pa} \cdot \text{m}^3/\text{s}$  for  $\text{H}_2$  and  $\text{H}_2\text{O}$ )
- First finding: beam pipe vacuum strongly decoupled

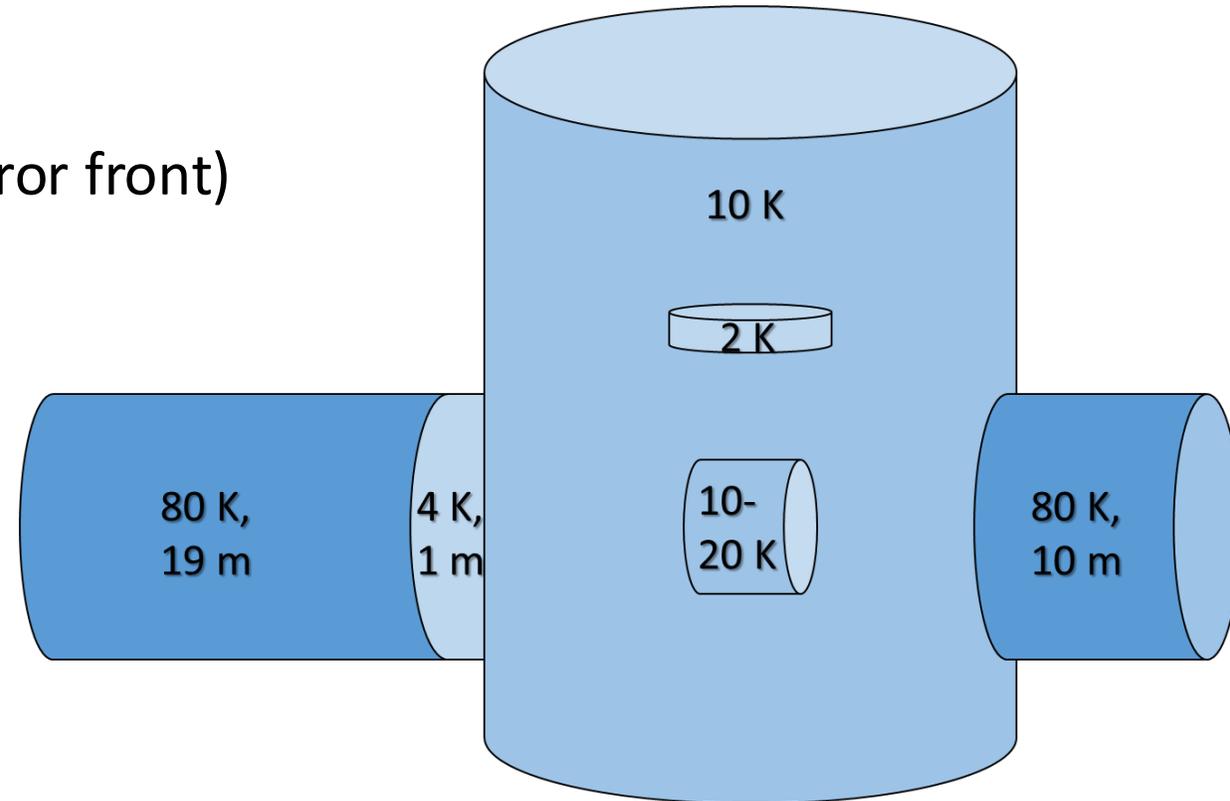
# Montecarlo results for LF vacuum

- All gas sources managed for hydrogen and water (non-sticky and sticky ones)
- Cryopumps:  
 $H_2O$ : 20 m left ( Mirror back) + 10 m right (Mirror front)  
 $H_2$ : 1 m left ( Mirror back)

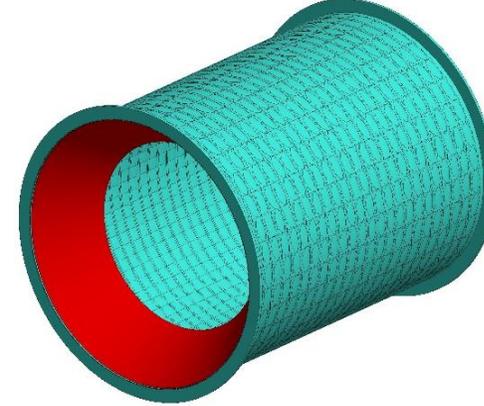
## ■ Pressure requirements fulfilled:

$H_2$ :  $3 \cdot 10^{-11}$  Pa,  $H_2O$ :  $1 \cdot 10^{-12}$  Pa

Water ice build-up ~2 years for 1 ML

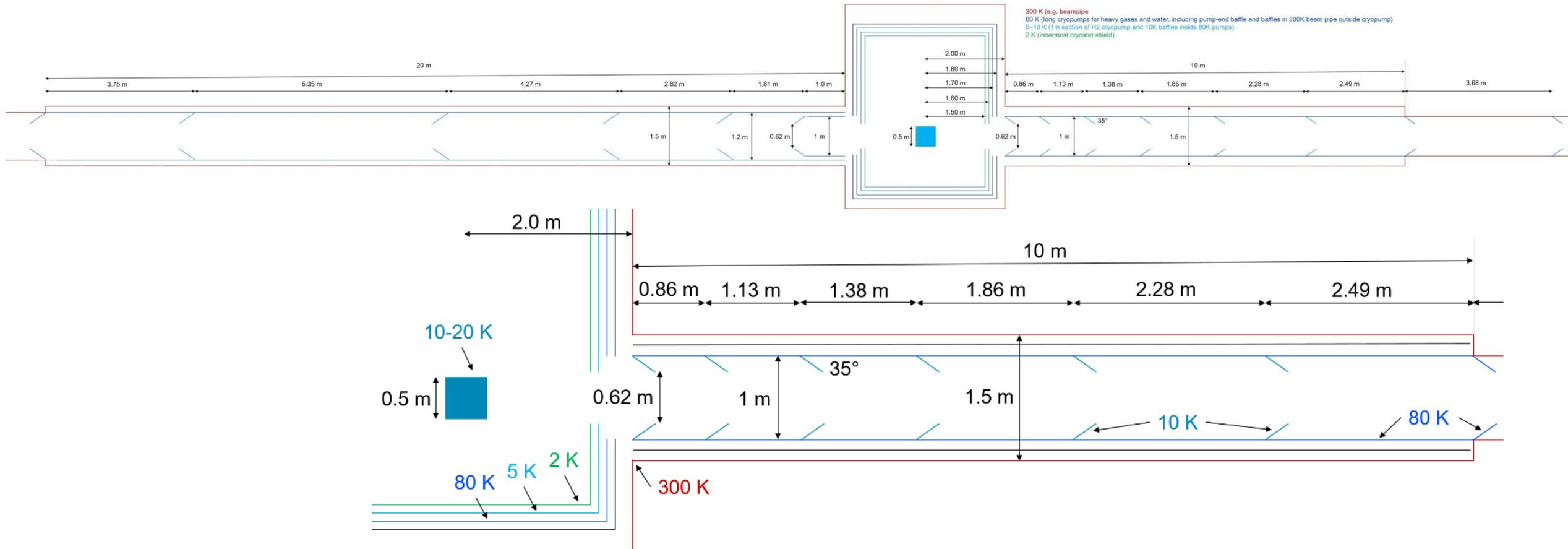


# Heat load simulation



Concept:  
Tubular  
cryopump  
segment with  
baffle

Cryopumps with baffles to avoid 80 K radiation onto 10 K mirror



# ET-LF: role of the 10 K baffles

Credits S. Hanke

**Disclaimer: Losses, thermal conductivity by supports and other details are not yet considered**

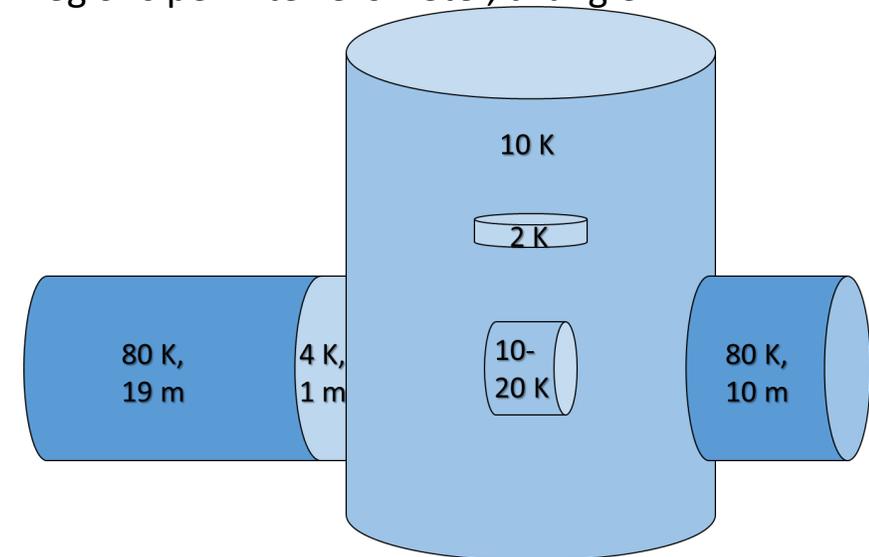
Mirror with 1% emissivity (99% reflectivity)	80 K system	3.7 K system	10 K system	Mirror (10 K)	Cryostat (2 K)
System with 10 K baffles in cryopumps	7.1 kW*	1.65 W	43 W	1.3 mW	263 mW
No baffles in cryopumps (80 K in simulation)	7.2 kW*	2.41 W	-	3.4 mW	892 mW
Total value for ET-LF with baffles**	~52 kW	20 W	516 W	-	3.2 W

Impact of 10 K baffles on mirror load: reduction by factor 2.6

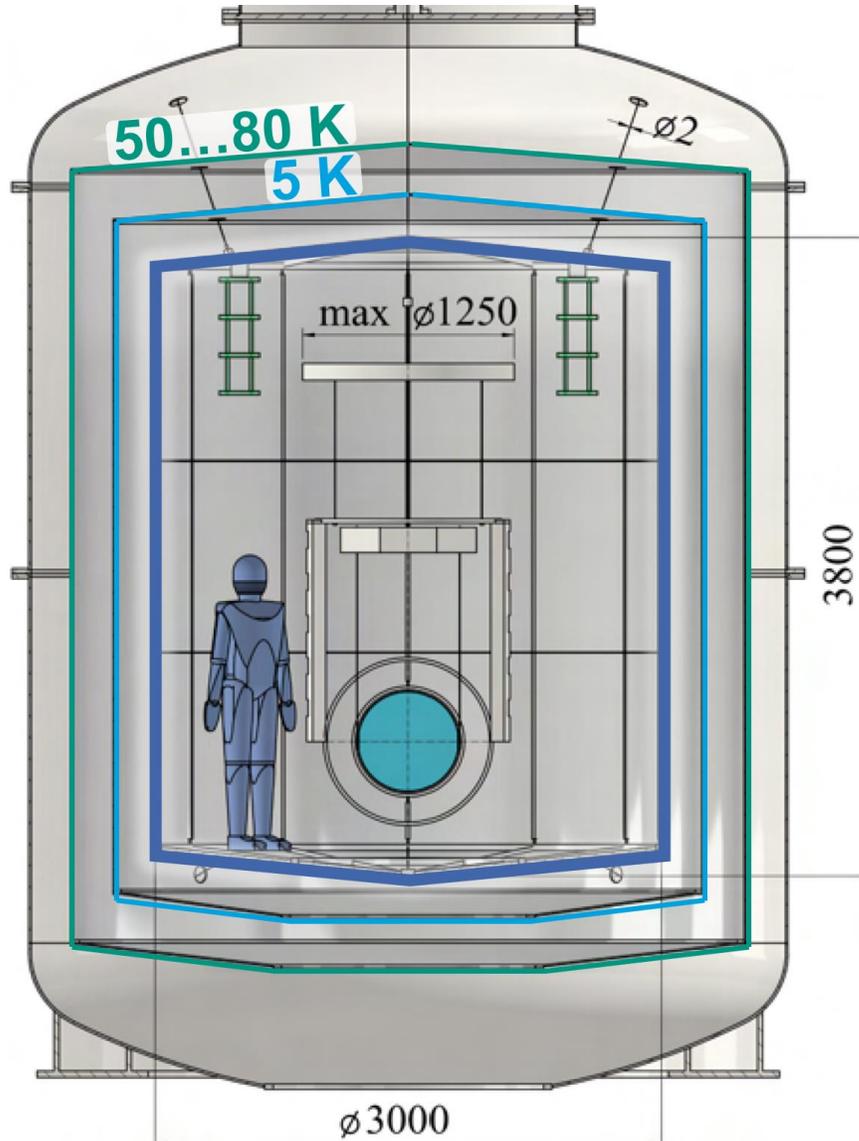
\*more real values reduced to ~60% via passive shielding between cryopump and beam pipe (theoretical 50% reduction by one passive shield layer, plus margin)

\*\*For the entire ET instrument **factor 12** this value of the LF region simulated here (4 LF regions per interferometer, triangle configuration means 3 interferometer)

Thermal load on:	ε of mirror	ε of mirror	ε of mirror	ε of mirror
	0.01	0.1	0.3	0.5
Mirror	1.3 mW	13 mW	37 mW	59 mW
Cryostat	262 mW	253 mW	232 mW	213 mW
3.7 K	1.65 W	1.65 W	1.65 W	1.65 W
10 K	43 W	43 W	43 W	43 W
80 K	7.1 kW	7.1 kW	7.1 kW	7.1 kW



# The cryostat



## Key features of the cryostat

- Bottom access
- Several layers of thermal shielding
- Vacuum separation between the upper warm tower and the cold cryostat
- External dimensions  $\phi \approx 4.5 \text{ m}$   $h \approx 6.4 \text{ m}$

Innermost shield  $h=3.8 \text{ m}$ ,  $\phi = 3.0 \text{ m}$  @ 2K

Payload 1250 mm height

Mirror 550 mm diameter

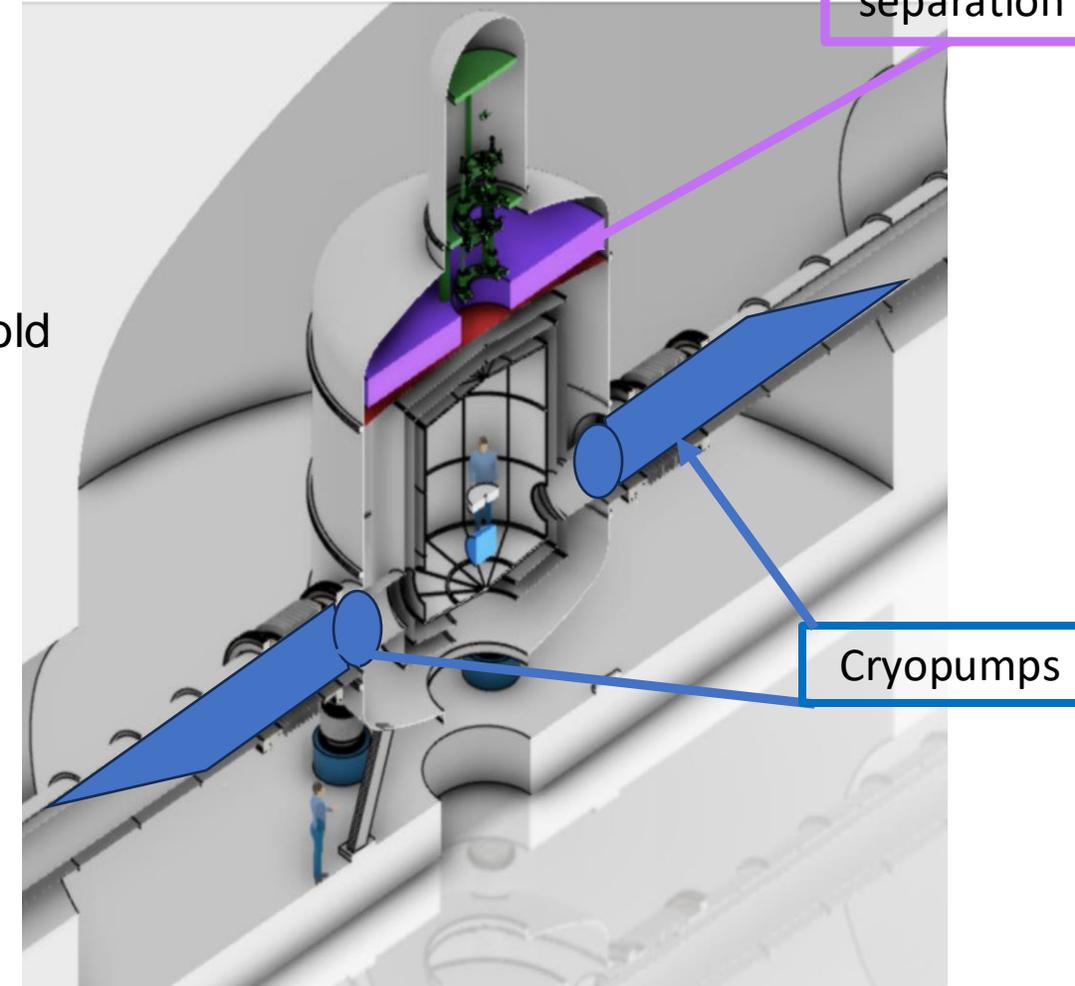
Cooling the shields

2 K → He II

5 K → He<sup>4</sup>

50 - 80 K → Helium Gas exchange

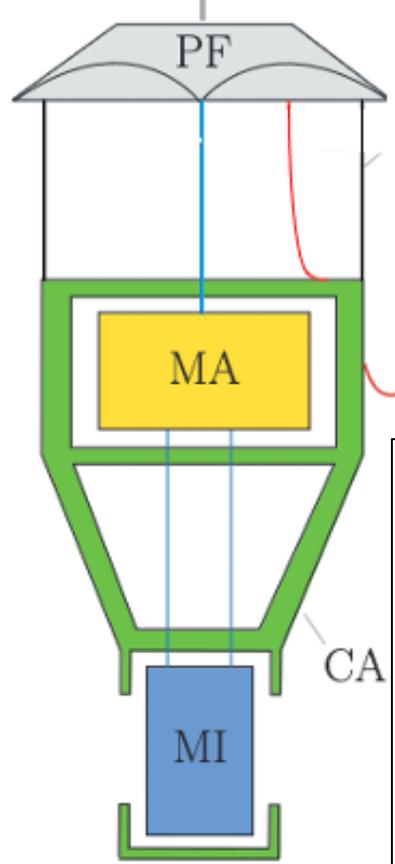
+ Extra shields to insure superinsulation



# Mirror @10/20 K: thermal links, path of vibrations and additional dissipation

## ET-LF Payload

To the superattenuator

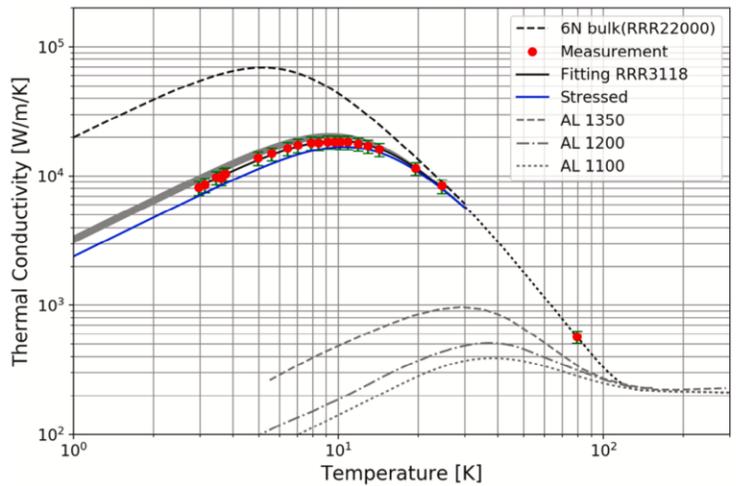


TLs end thermally connected to the innermost shield of the cryostat

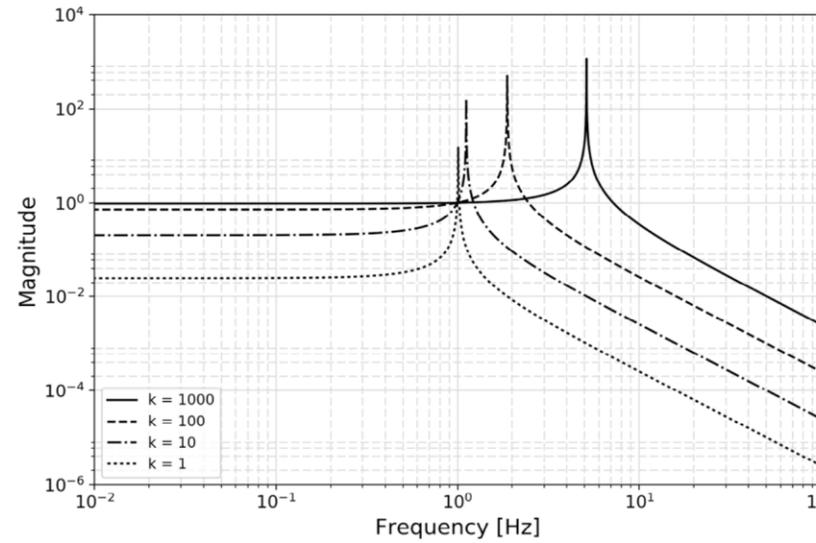
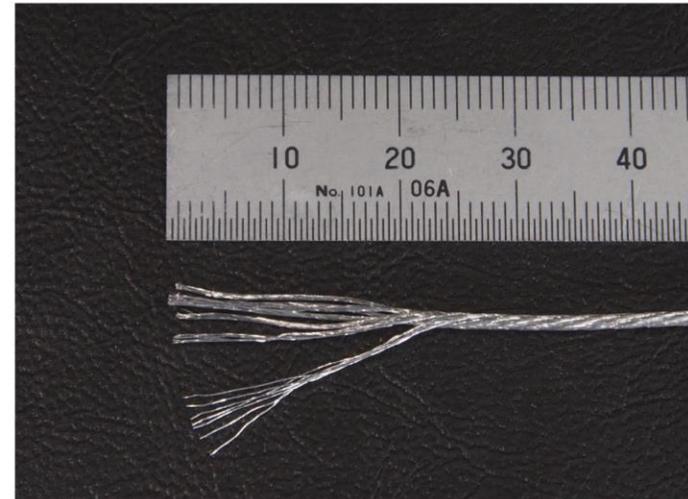
- PF → Platform
- MA → Marionette
- TL → Thermal links
- CA → Cage
- MI → Mirror

Tomohiro Yamada Et al.  
[Cryogenics](#) Volume 116, June 2021, 103280

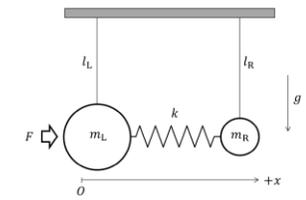
## KAGRA study: stress changes the thermal conductivity



KAGRA:  
 TL anchored to vibration dampers set inside the innermost shield of the cryostat



TLs with smaller spring constant  $k$  to reduce overall vibration transfer.



# Cryogenic Infrastructures

Baseline solution:

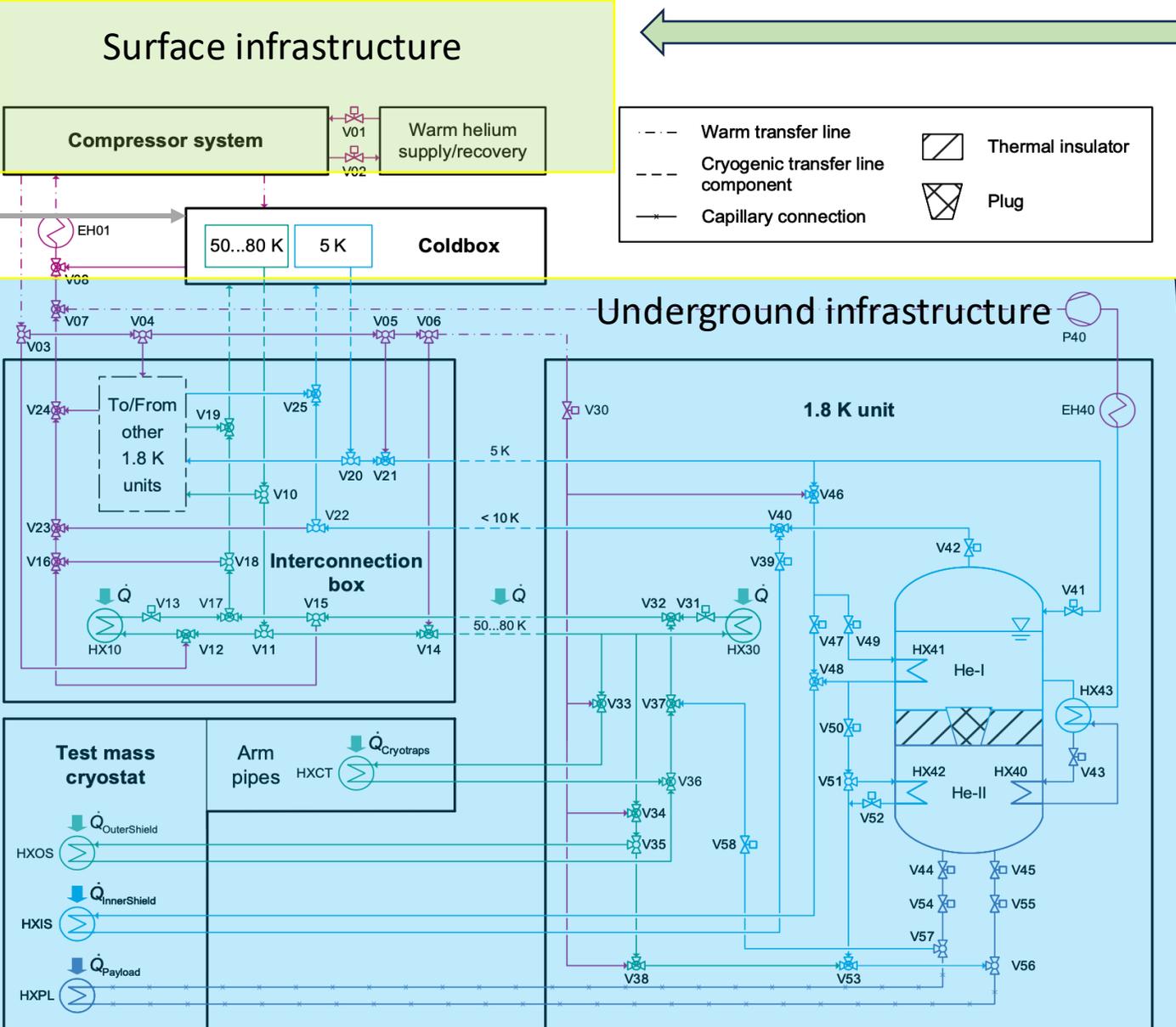
--Just 1 cryo-facility for each vertex based on the use of He fluid

Alternative approach

-- KAGRA solution considered

# Cooling Infrastructure based on Cryogenic fluids

Lennard Busch, Steffen Grohmann - ET-0376A-2

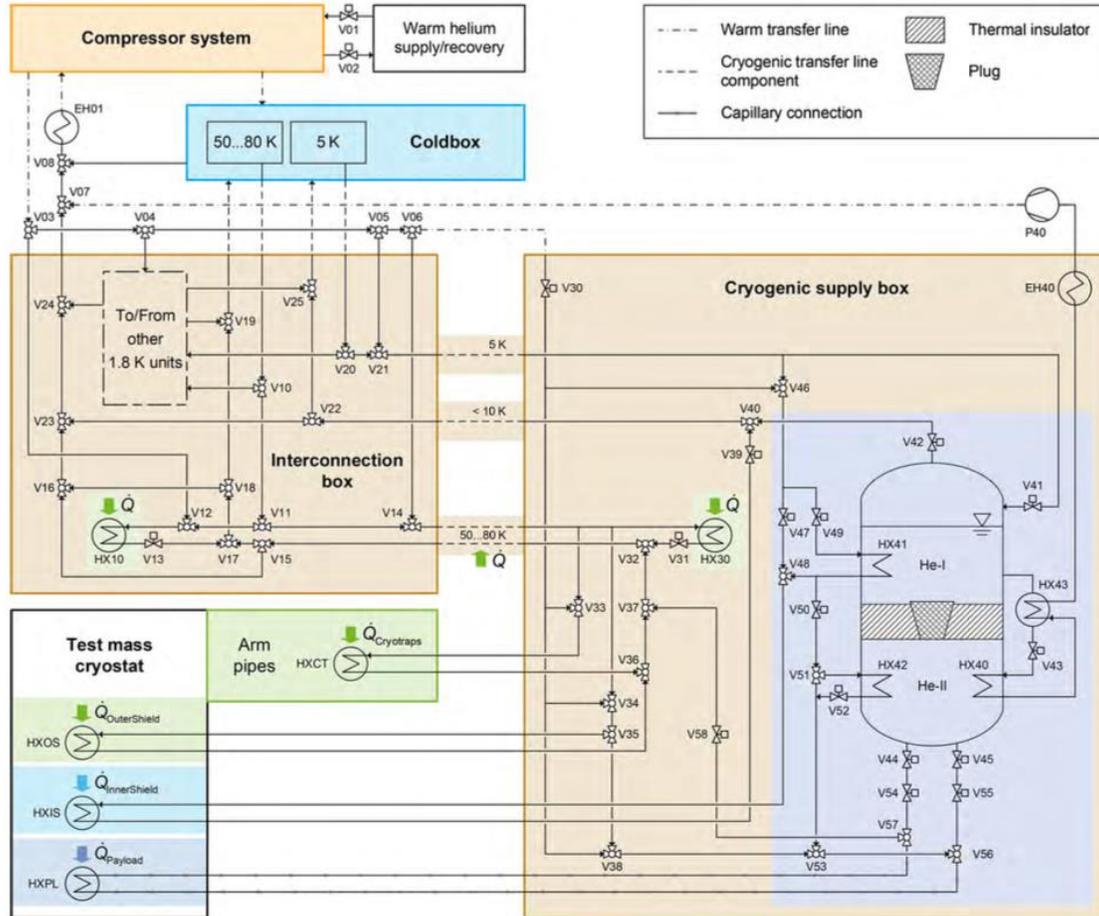


Cold bx in an intermediate cave: a noisy room

Noise generators:  
Level of noise to be evaluated by measuring similar systems installed in HEP laboratories

*IOP Conf. Series: Materials Science and Engineering 1240 (2022) 012095*  
*doi:10.1088/1757-899X/1240/1/012095*

# Cryogenic infrastructure concept [\*\*]



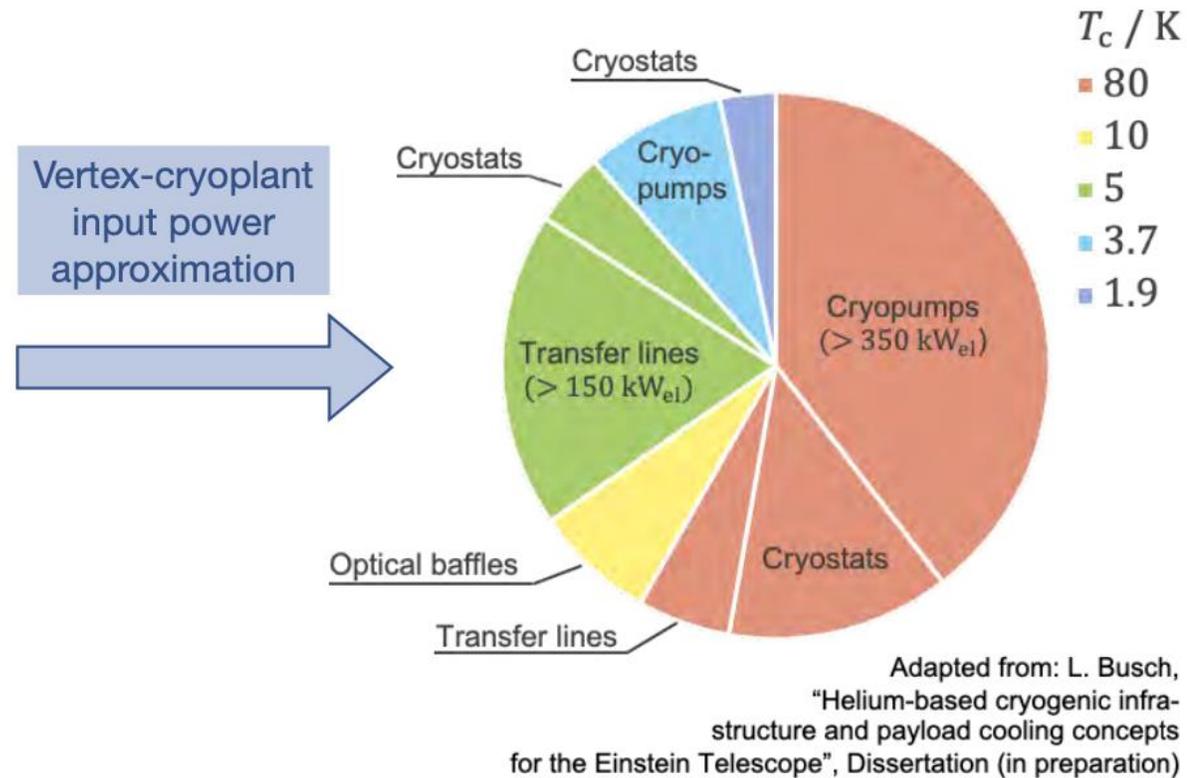
- No underground LN2 (safety)
- One He refrigerator at each vertex
  - (Remote) surface compressors
  - Underground cold box
  - Interconnection box to several cryogenic supply boxes (1 for each tower/cryostat)
  - Up to c. 500 m long transfer lines
  - 1-phase cooling for 80 K cryopumps/outer shields
  - 1-phase cooling for 10 K baffles, 5 K inner shields and 3.7 K cryopumps
  - He-II payload cooling/inner shield

# Summary for the civil infrastructure design

- Compressor hall on surface not far from the service pit of the each vertex: a mean size technical building (100/200 m<sup>2</sup> [??] equipped with a crane )
- Noisy room to host the old box ( and other noisy devices even not related to cryogenics decoupled to the main cavern (50/100 m<sup>2</sup> , 6 m height)
- Interconnection box near the cryostat
- Transfer lines between noisy room and interconnection box up to 500 m

# He plant: rough evaluation of the electric power request

*In the case of the **ET vertex in the triangular configuration***



Total: ~ 1 - 1.2 MW

Credits :  
L. Busch, S. Grohmann

*In the case of the **L configuration** these numbers must be divided*

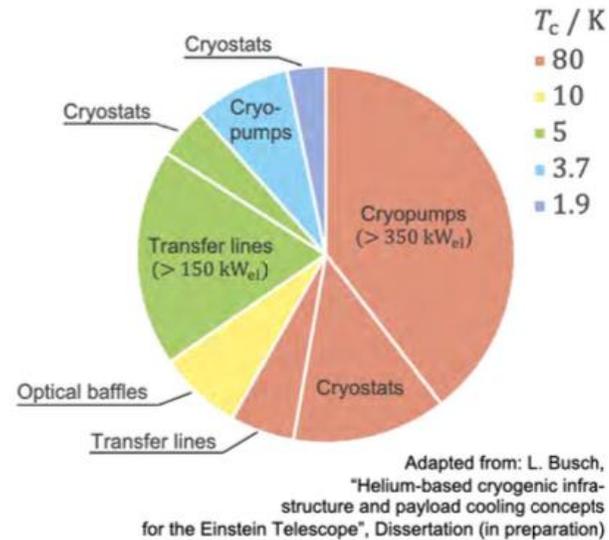
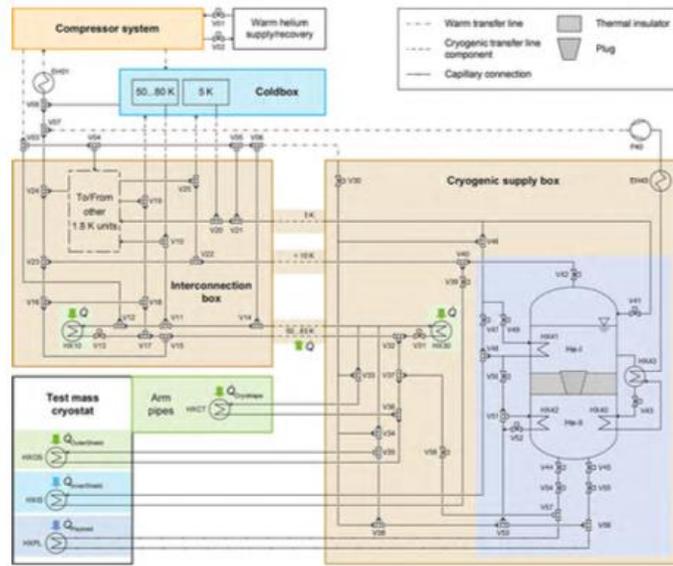
– by a factor 2 at the L vertex

– by a factor 4 at the interferometer end

Total: ~ 500 – 600 kW

Total: ~ 250 – 300 kW

# Cryogenic Infrastructure planning



Additional cryopump evaluation in progress !!

- **CERN contract** to be discussed/initiated by **Project Office**
- Needed to coordinate industry design studies
  - **Technical expertise, manpower** → **Reliable cost estimates**
- No resources in ISB Division IV !



# KAGRA cooling strategy: PT Cryocoolers

## *Pulse Tube nominal performances - CRYOMECH*

PT407 - 0.7 W@4.2 K -- 25 W @55K

+ compr. CPA 2870 → 7 kW

PT410 - 1.0 W@ 4.2 K -- 40 W @ 45 K

+ compr. CPA 289 C → 7.9 kW

PT420 – 2W@ 4.2k – 55 W @45 K

+ compr. CPA1114 – 11.4 kW

PT425 – 2.7W@4.2 K – 55W@45 K

+ compr. CPA1114 → 12kW

PT450 -- 5 W @ 4.2K – 65 W@ 45 K

+ compr. CPA3027 → 25 kW

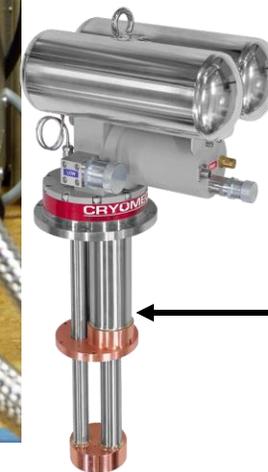
$COP_r \sim 10^{-4} @ 4 K \rightarrow \sim 3 \times 10^{-3} @ 50K$

(  $COP_r$  - Coefficient Of Performance<sub>refrigeration</sub> )



Compressor  
to be located  
in a noisy  
room

High pressure  
lines of He gas:  
maximum length  
100 m



Cold head  
attached  
to the  
element to  
be cooled  
(cryostat  
or  
cryopump)

# Civil Engineering Impact of the KAGRA cooling strategy

- ❖ A cryoplant based on PTs asks for more than a factor 10 of electric power
  - $COP_r$  coefficient  $\rightarrow \sim 1 \times 10^{-4}$  @ 4K , lower than a LHe plant
  - Example of  $COP_r$  of He plants: LR70 system of Linde Kryotechnik AG*
  - $T < 4.4$  K       $COP_r \sim 1.7 \times 10^{-3}$  ( without  $LN_2$  precooling )*
  - $T < 4.4$  K       $COP_r \sim 2.5 \times 10^{-3}$  ( with  $LN_2$  precooling )*
  - Running cost of the electric power significantly higher*
- ❖ Noisy room at 100 m distance of the main cavern
- ❖ High flow of refrigeration water to be provided in the noisy room
- ❖ Electric power to run the cryo facility to be provided underground: *higher fire hazard ?*