

Strain Gage measurements

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Strain Gage: Intro

Strain gage measure the strain

- $\epsilon_i = \Delta L_i / L_i$
- $\Delta R_i / R_i = K \epsilon_i$
- $K \sim 2$ is the gage factor
- $L_i \sim 7\text{mm}$ is the strain-gage length

$$\left(\frac{\Delta R}{R_0} \right)_{T/O} = \left[\beta_G + F_G \left(\frac{1 + K_t}{1 - \nu_0 K_t} \right) (\alpha_S - \alpha_G) \right] \Delta T \quad (1)$$

where, in consistent units:

$\left(\frac{\Delta R}{R_0} \right)_{T/O}$ = unit change in resistance from the initial reference resistance, R_0 , caused by change in temperature resulting in thermal output.

β_G = temperature coefficient of resistance of the grid conductor.

F_G = gage factor of the strain gage.†

K_t = transverse sensitivity of the strain gage.

ν_0 = Poisson's ratio (0.285) of the standard test material used in calibrating the gage for its gage factor.

TABLE 1—NOMINAL THERMAL EXPANSION COEFFICIENTS OF ENGINEERING MATERIALS

MATERIAL DESCRIPTION	EXPANSION COEFFICIENTS**		RECOMMENDED S-T-C NUMBER
	Per °F	[Per °C]	
ALUMINA, fired	3.0	[5.4]	03
ALUMINUM Alloy, 2024-T4*, 7075-T6	12.9	[23.2]	13*
BERYLLIUM, pure	6.4	[11.5]	06
BERYLLIUM COPPER, Cu 75, Be 25	9.3	[16.7]	09
BRASS, Cartridge, Cu 70, Zn 30	11.1	[20.0]	13
BRONZE, Phosphor, Cu 90, Sn 10	10.2	[18.4]	09
CAST IRON, gray	6.0	[10.8]	06
COPPER, pure	9.2	[16.5]	09
GLASS, Soda, Lime, Silica	5.1	[9.2]	05
INCONEL, Ni-Cr-Fe alloy	7.0	[12.6]	06
INCONEL X, Ni-Cr-Fe alloy	6.7	[12.1]	06
INVAR, Fe-Ni alloy	0.8	[1.4]	00
MAGNESIUM Alloy*, AZ-31B	14.5	[26.1]	15*
MOLYBDENUM*, pure	2.7	[4.9]	03*
MONEL, Ni-Cu alloy	7.5	[13.5]	06
NICKEL-A, Cu-Zn-Ni alloy	6.6	[11.9]	06
QUARTZ, fused	0.3	[0.5]	00
STEEL Alloy, 4340	6.3	[11.3]	06
STEEL, Carbon, 1008, 1018*	6.7	[12.1]	06*
STEEL, Stainless, Age Hardenable (17-4PH)	6.0	[10.8]	06
STEEL, Stainless, Age Hardenable (17-7PH)	5.7	[10.3]	06
STEEL, Stainless, Age Hardenable (PH15-7Mo)	5.0	[9.0]	05
STEEL, Stainless, Austenitic (304*)	9.6	[17.3]	09*
STEEL, Stainless, Austenitic (310)	8.0	[14.4]	09
STEEL, Stainless, Austenitic (316)	8.9	[16.0]	09
STEEL, Stainless, Ferritic (410)	5.5	[9.9]	05
TIN, pure	13.0	[23.4]	13
TITANIUM, pure	4.8	[8.6]	05
TITANIUM Alloy, 6AL-4V*	4.9	[8.8]	05*
TITANIUM SILICATE*, polycrystalline	0.0	[0.0]	00*
TUNGSTEN, pure	2.4	[4.3]	03
ZIRCONIUM, pure	3.1	[5.6]	03

* Indicates type of material used in determining thermal output

Strain Gage: Methodology

In our samples thermal output vs T given for Steel 1018

$$\epsilon_{T/O} = \left(\frac{\beta_G}{F_G} - \alpha_G \right) \Delta T + \alpha_s \Delta T \quad \epsilon = \Delta L / L$$

For Another material X:

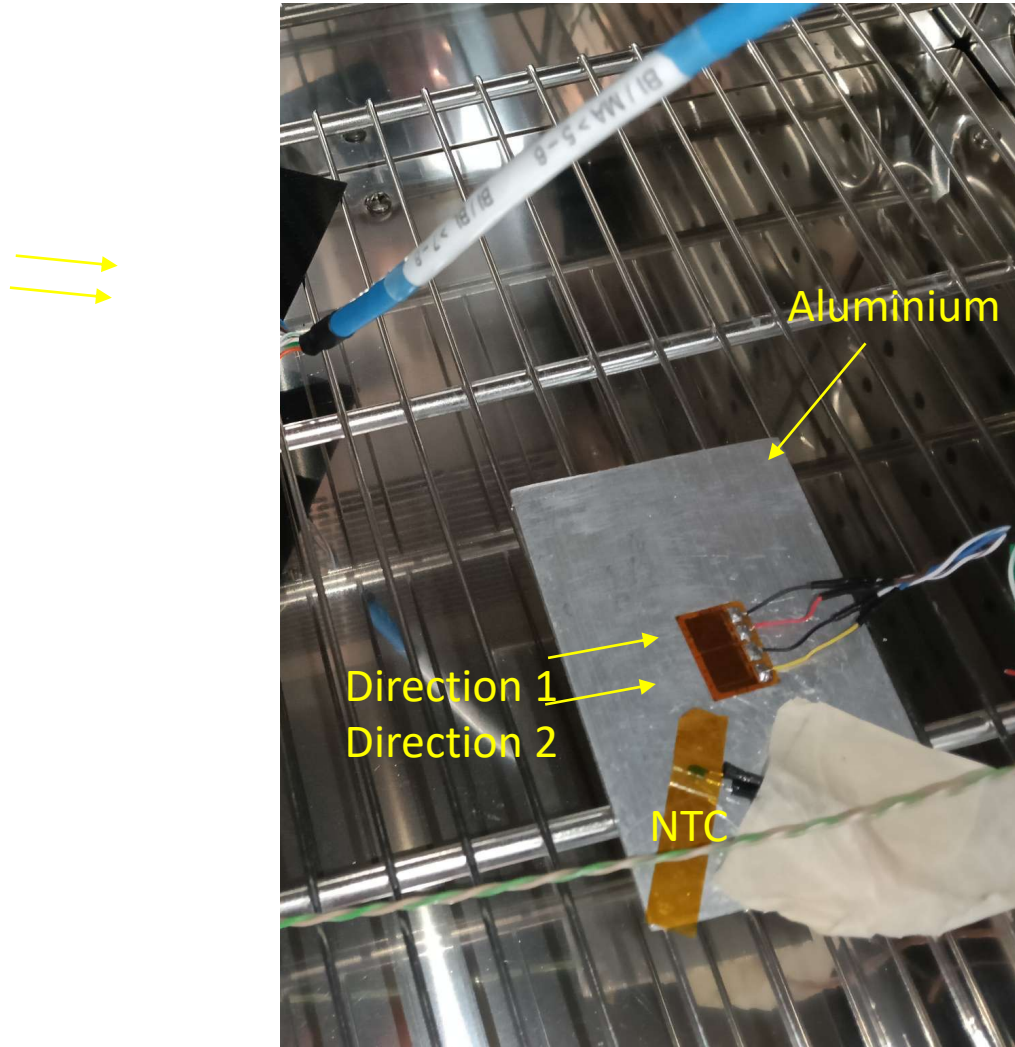
$$\epsilon_X = \left(\frac{\beta_G}{F_G} - \alpha_G \right) \Delta T + \alpha_X \Delta T$$

- $\epsilon_X - \epsilon_{T/O} = (\alpha_X - \alpha_{\text{steel}}) \Delta T$
 - The subtraction removes the thermal response of the strain gage and leaves just the part that depends on the substrate
- Measure ϵ_X as a function of T
- Fit $\epsilon_X - \epsilon_{T/O}$ vs T

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* Indicates type of material used in determining thermal output

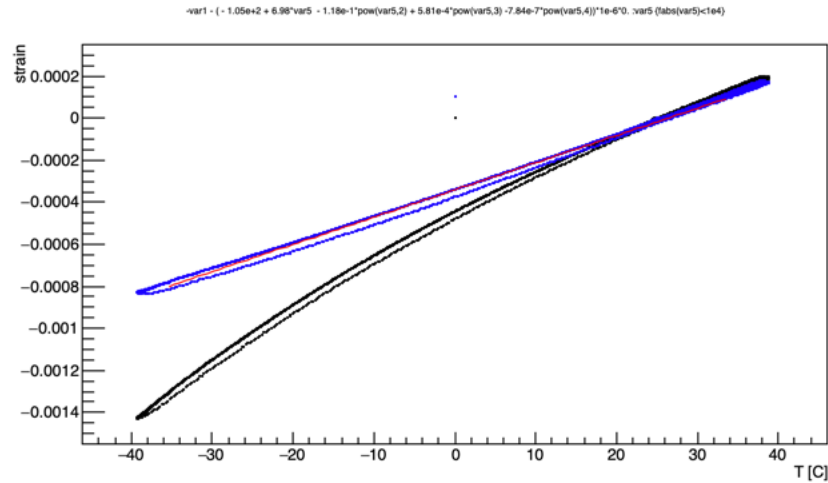
Experimental setup with Aluminium



The setup is inside a climate chamber

Blue points and Fit: : after thermal correction

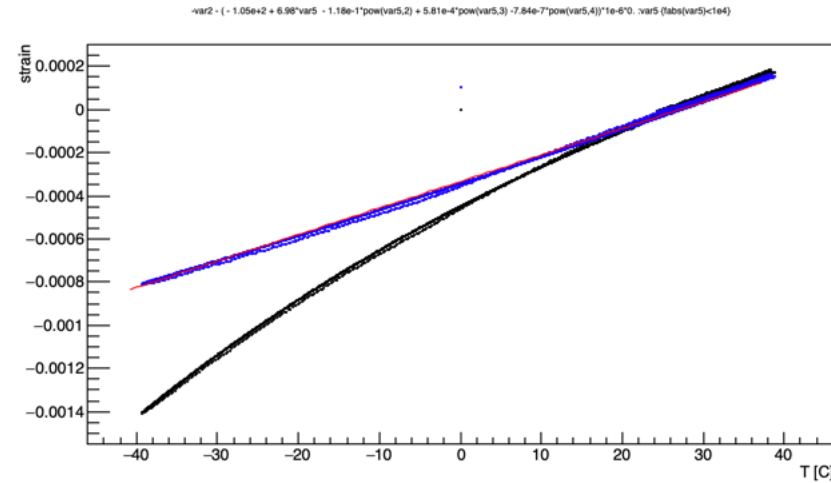
Strain-gage 1 Al



slope_measured $\sim 13.0 \text{ e-6 / C}$

$\alpha_{Al} = \text{slope_measured} + \alpha_{steel} \sim 25.1 \text{ e-6 / C}$

Strain-gage 2 Al

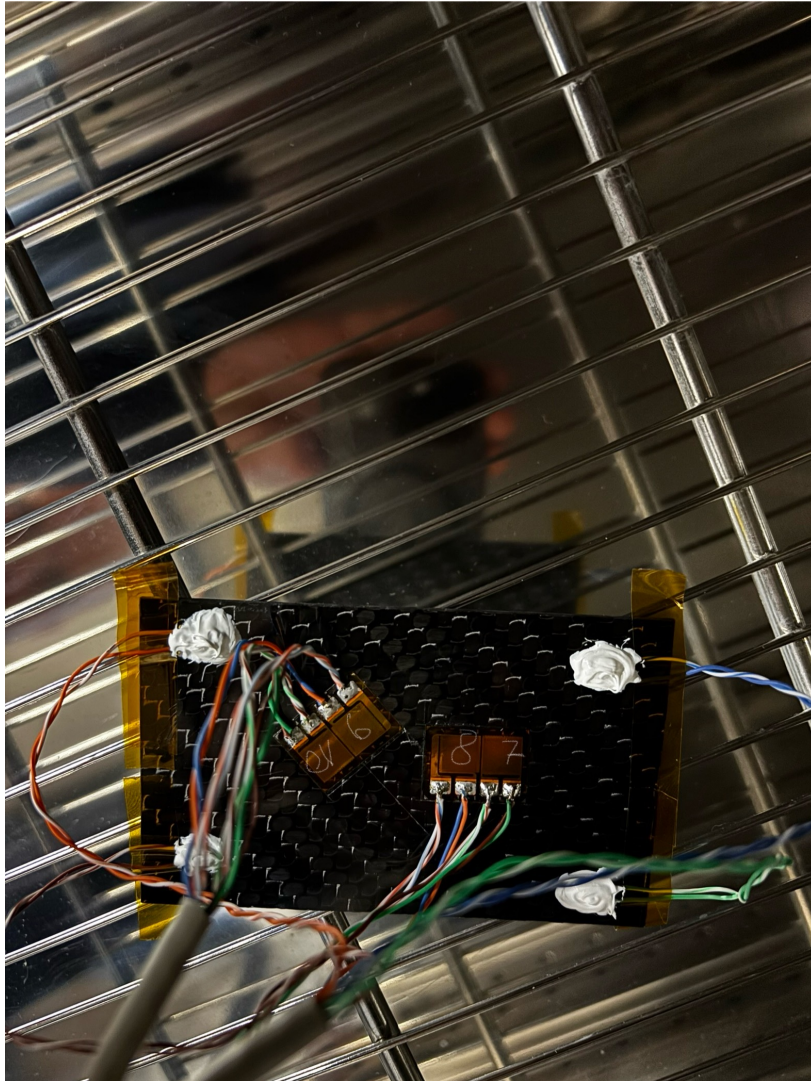


slope_measured $\sim 12.3 \text{ e-6 / C}$

$\alpha_{Al} = \text{slope_measured} + \alpha_{steel} \sim 24.5 \text{ e-6 / C}$

For both sensors decent agreement with expected CTE of Aluminium

Experimental setup with CF foil



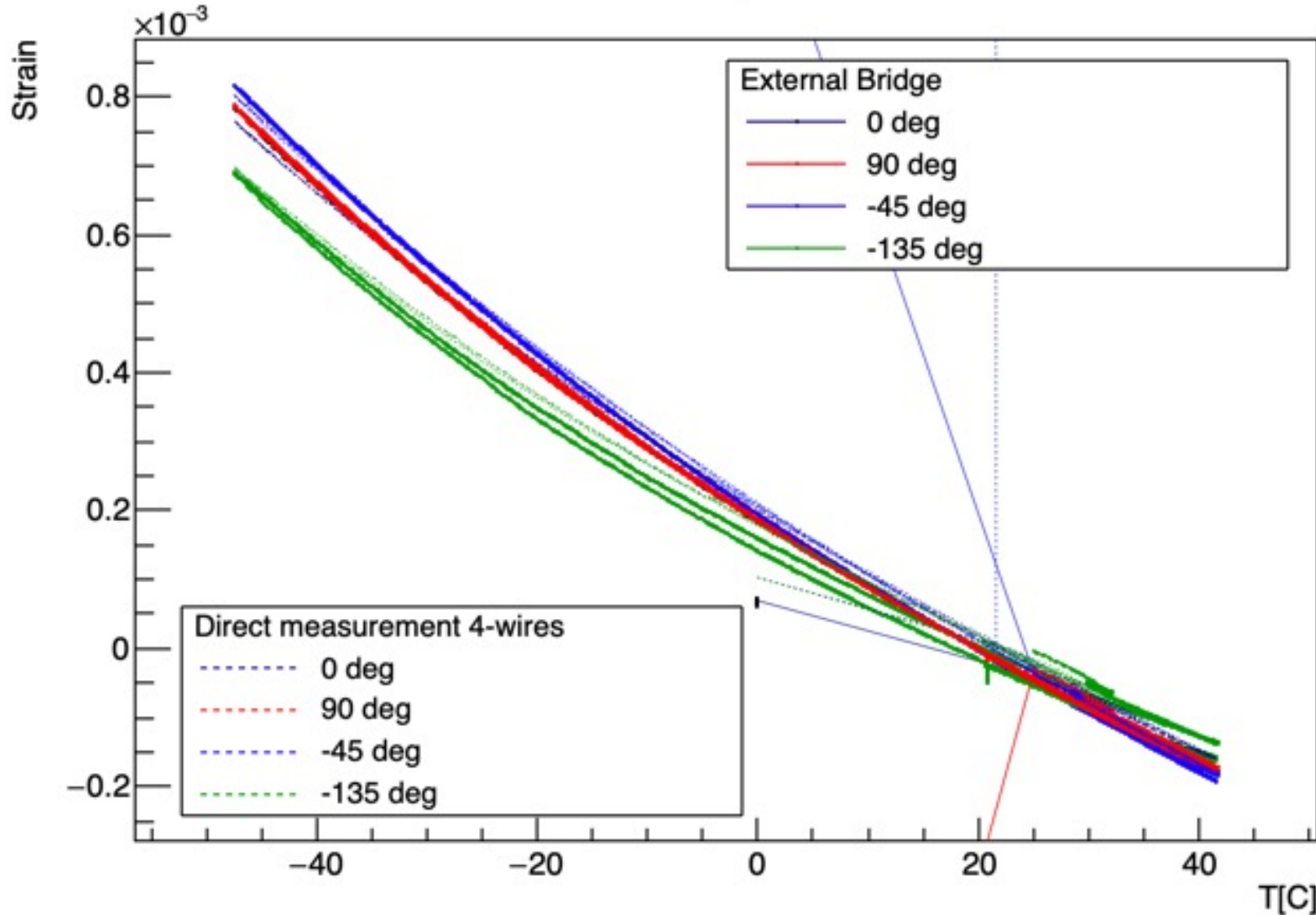
Properties for Carbon/Epoxy Composite Sheet

Property	Units	Value
Coefficient of thermal expansion - Longitudinal	$\times 10^{-6} \text{ K}^{-1}$	2.1
Coefficient of thermal expansion - Transverse	$\times 10^{-6} \text{ K}^{-1}$	2.1
Compressive Strength - Longitudinal	MPa	570
Compressive Strength - Transverse	MPa	570
Density	g cm^{-3}	1.6
Shear modulus - in-plane	GPa	5
Shear strength - in-plane	MPa	90
Ultimate Compressive Strain - Longitudinal	%	0.8
Ultimate Compressive Strain - Transverse	%	0.8
Ultimate Shear Strain - in-plane	%	1.8
Ultimate Tensile Strain - Longitudinal	%	0.85
Ultimate Tensile Strain - Transverse	%	0.85
Volume fraction of fibres	%	50
Young's Modulus - Longitudinal	GPa	70
Young's Modulus - Transverse	GPa	70

We perform a strain measurement in two ways:

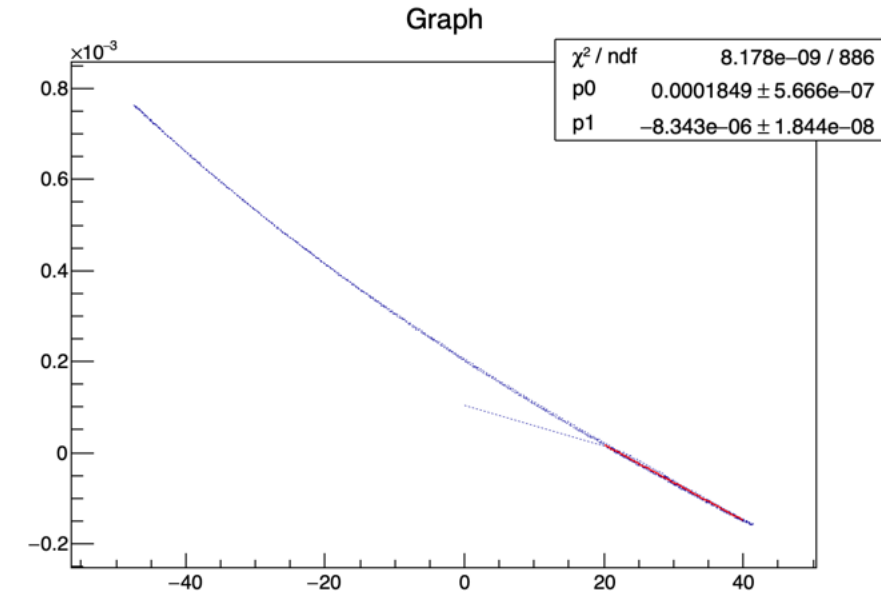
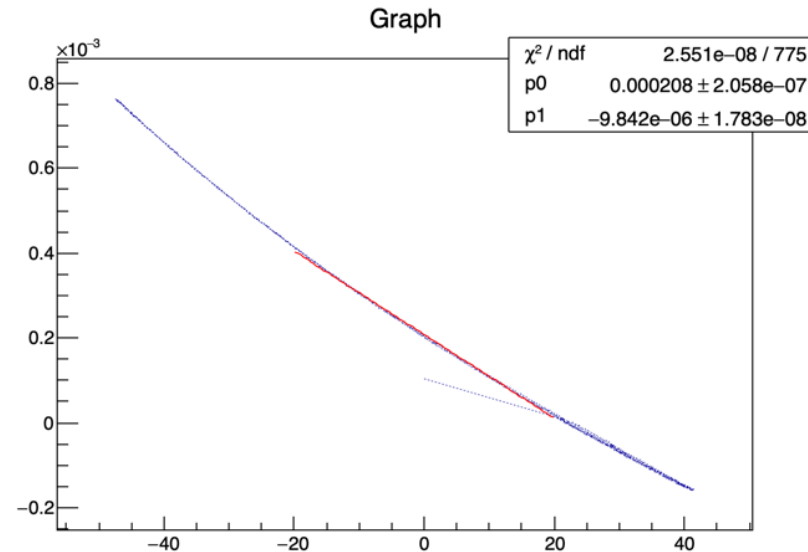
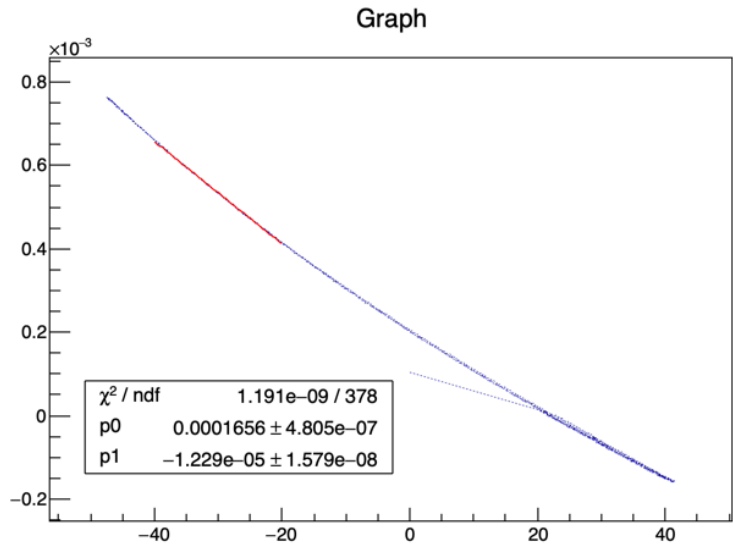
- External wheatstone bridge + Voltage measurement from Keysight DAQM901A module Data Acquisition System
- Direct 4 wire measurement of strain (resistance) from Keysight DAQM901A module Data Acquisition System

Graph



- in each direction, for the two types of measurement, we have same trend of strain vs T
- for 0 and 90 degrees same trend of "strain vs T " and, therefore, same CTE, as expected from RS specs
- the trend of "strain vs T " of -45C and -135 C are a bit different. No specs available for these directions

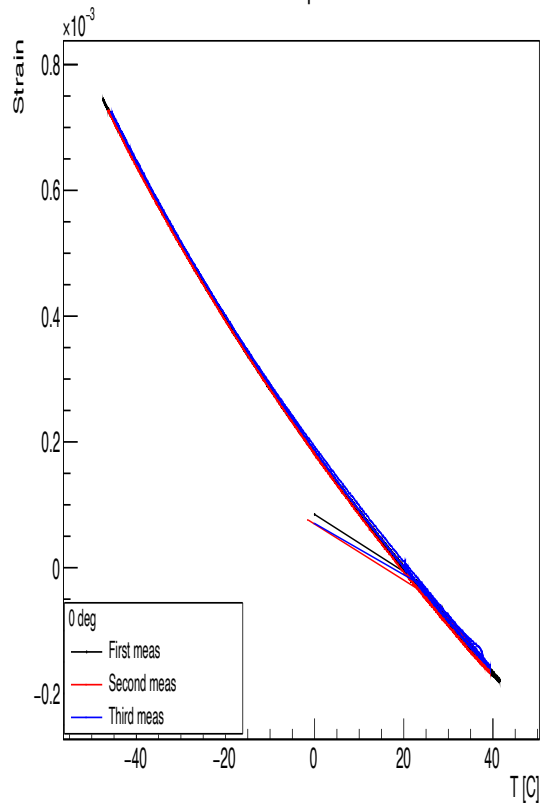
Fit and CTE extraction



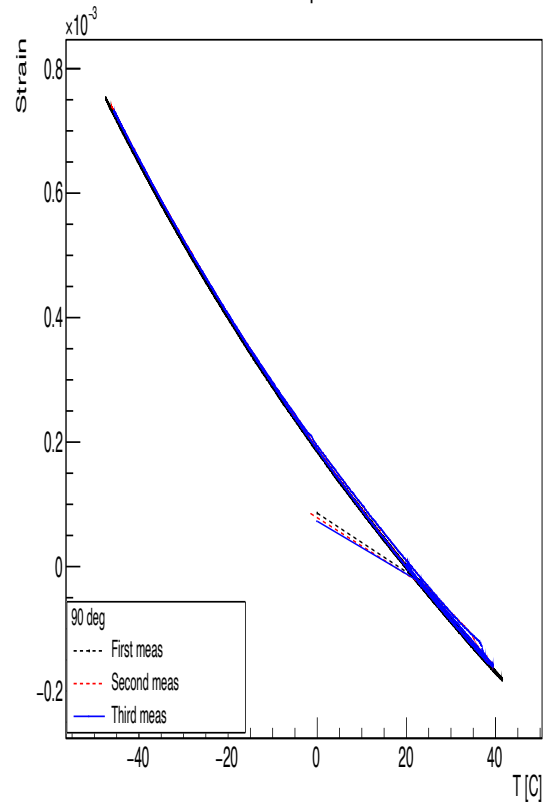
- The linear fit of in the [-20, + 20]C region for 0 deg gives CTE $\sim (-9.8 + 12.1)$ ppm/C = 2.3 ppm/C, in decent agreement with RS specs of 2.1 ppm/C
- In the region [+20, +40]C the fitted CTE is $\sim (-8.3 + 12.1)$ ppm/C = 3.8 pp/C
- In the region [- 40, - 20]C the fitted CTE is $\sim (-12.2 + 12.1)$ ppm/C $\sim$ -0.1 ppm/C
- 12.1 ppm/C is the CTE of steel 2018 used for thermal compensation

Reproducibility

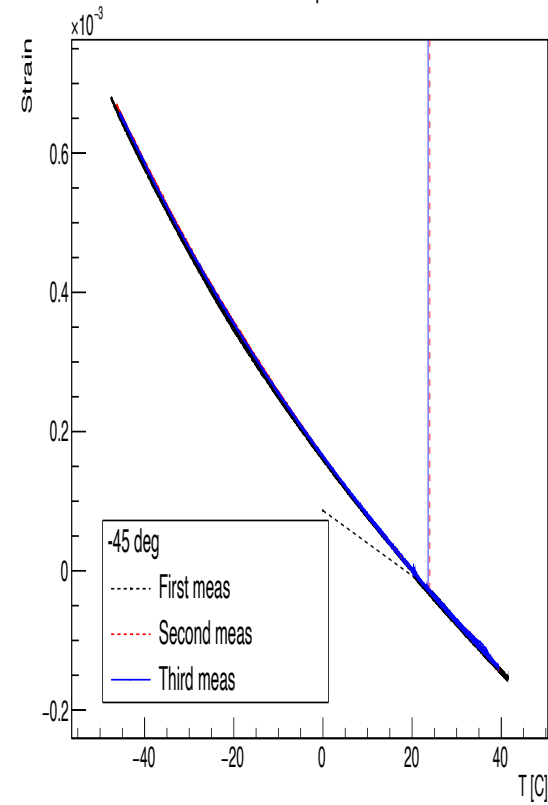
Graph



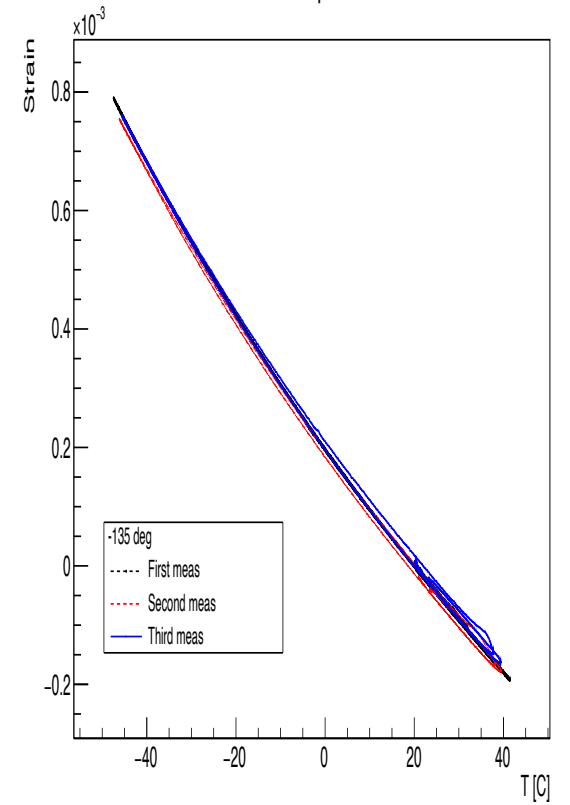
Graph



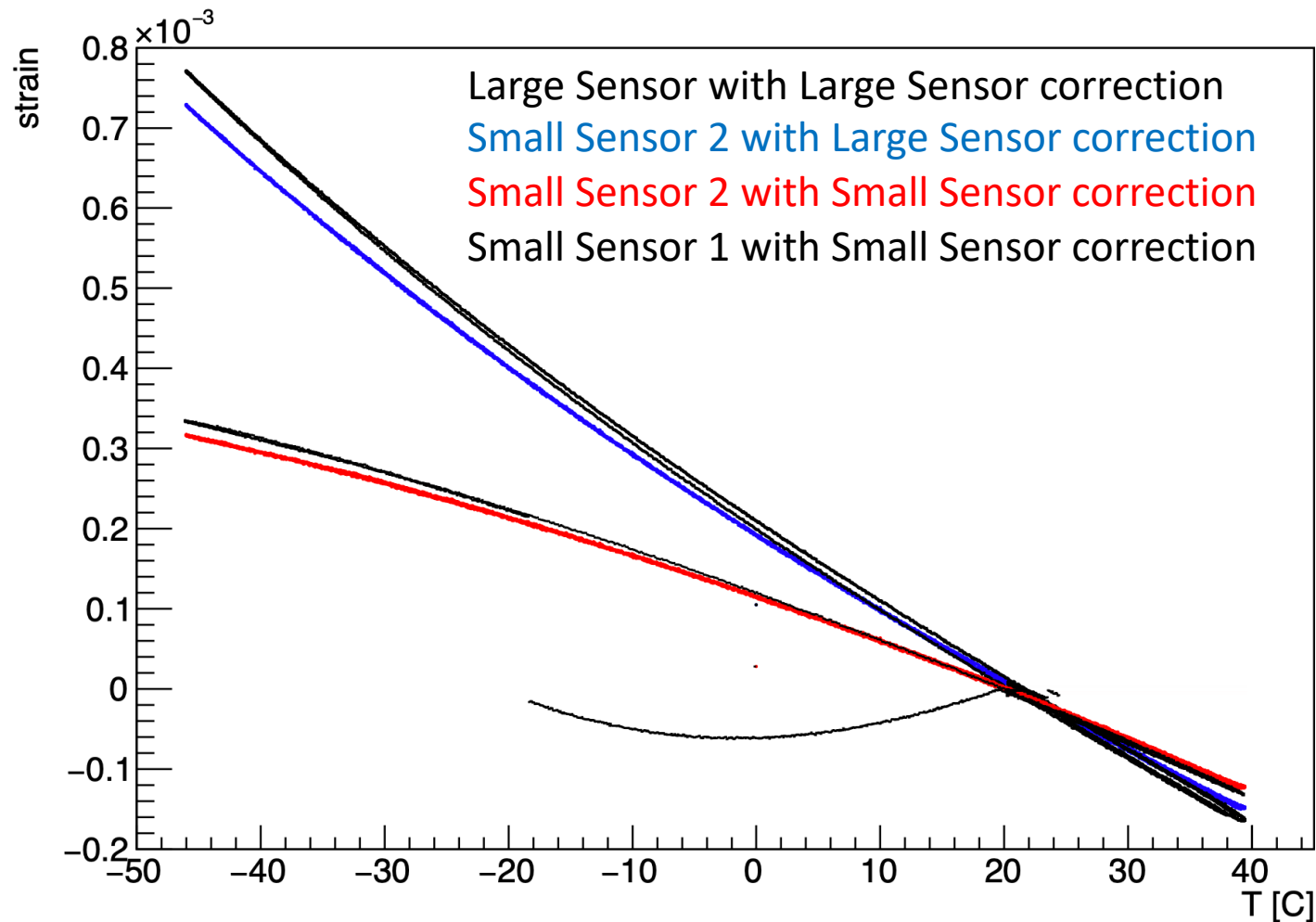
Graph



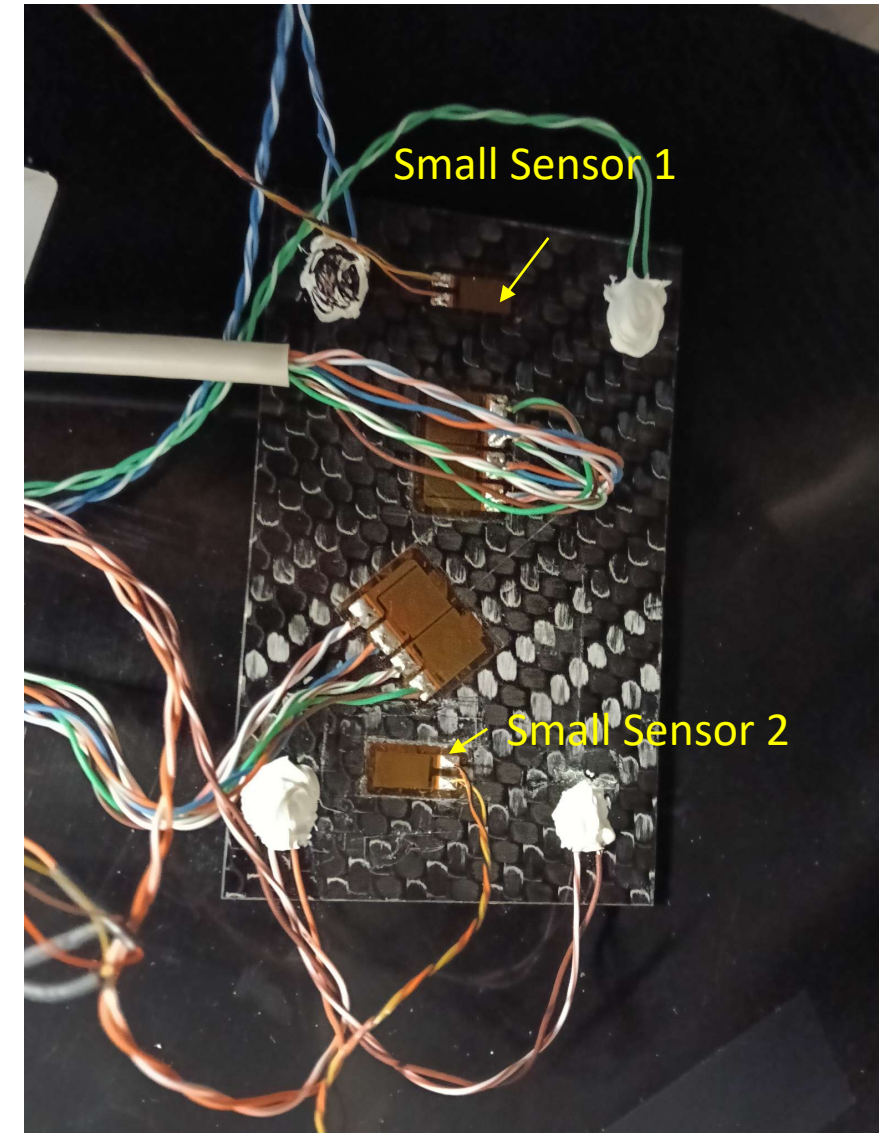
Graph



Small Mono-directional sensors



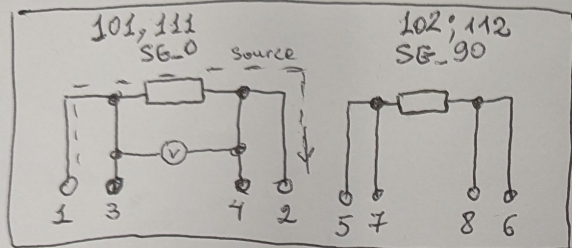
To be understood



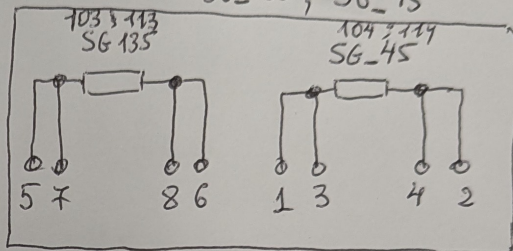
Backup

$\frac{28.14}{(28.14+1)}$

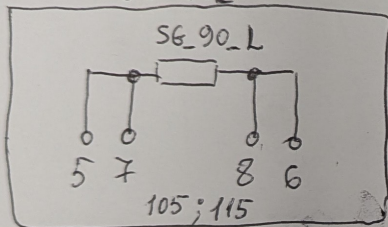
SG_0; SG_90



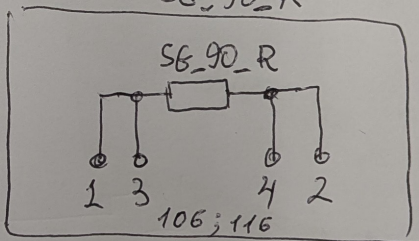
SG_135; SG_45



SG_90_L



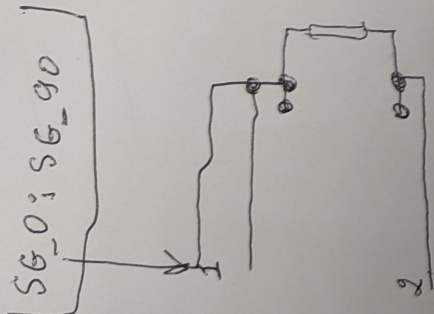
SG_90_R



NTCS

107, 108, (10K) calibrated

109, 110, (10K) no calibrated.



Metrics
 Voltage
 Current
 Temperature
 IGBT1 Status
 IGBT2 Status
 IGBT3 Status
 IGBT4 Status

4040
 2nd 1
 rel 2
 rel 3
 rel 4
 rel 5