

## *Digital twins for intelligent production of submarine optical fibers*

### **Author:**

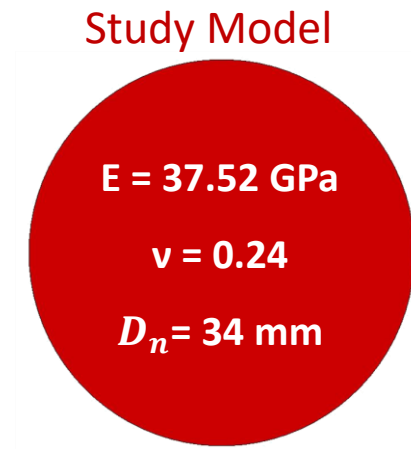
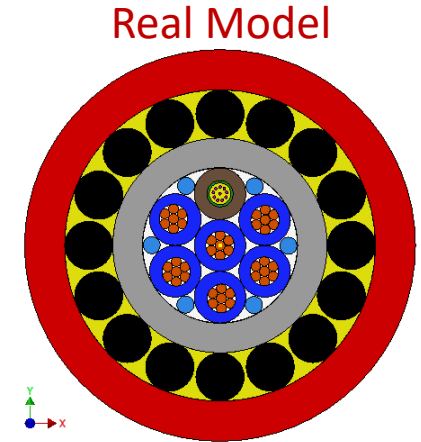
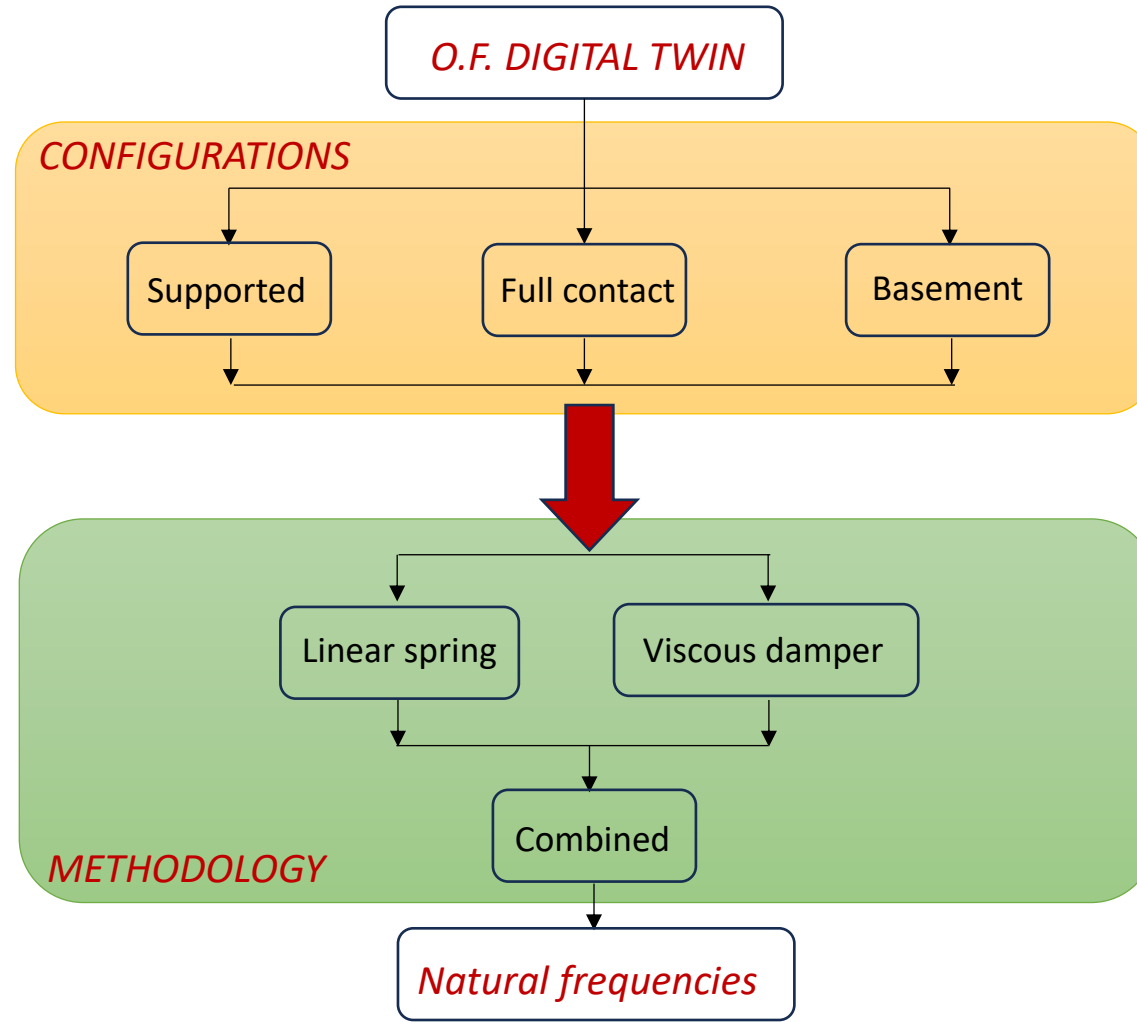
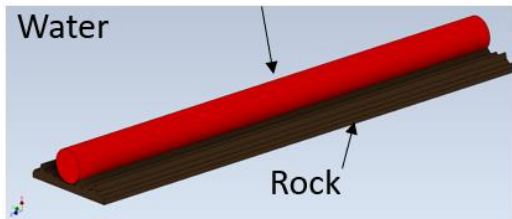
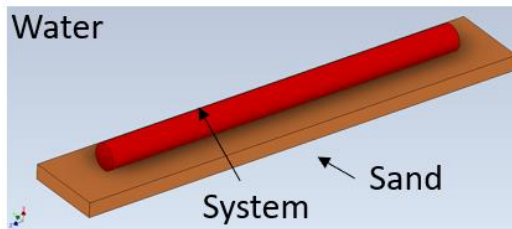
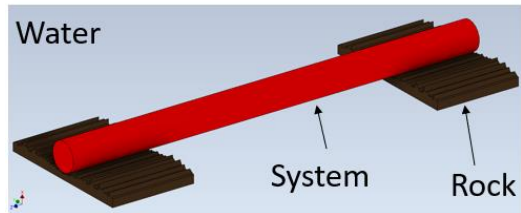
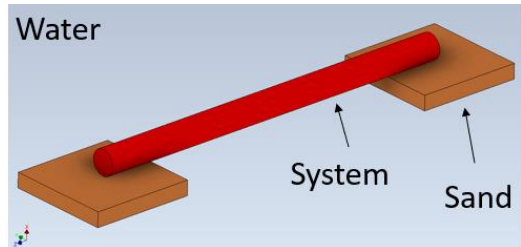
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## Study methodology



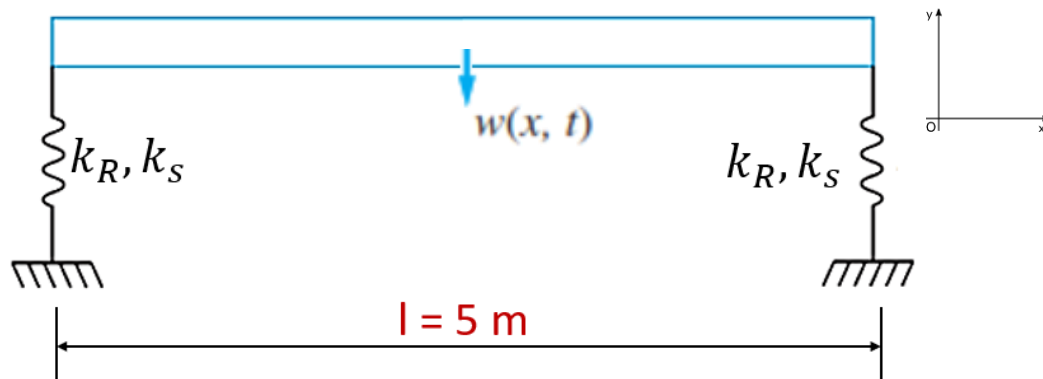
## Study Model: Supported

$$\frac{\partial^2 \omega}{\partial t^2} + \frac{\partial^4 \omega}{\partial x^4} = \frac{f_m L^3}{EI} f(x, t) \quad \Rightarrow \quad \omega(x, t) = X(x) \cdot T(t) \quad \xrightarrow{f=0 \text{ (Free vibration)}} \quad \frac{1}{T(t)} + \frac{d^2 T}{dt^2} = -\frac{1}{X(x)} \frac{d^4 X}{dx^4}$$

$$T(t) = A \cos \sqrt{\lambda} t + B \sin \sqrt{\lambda} t$$

$$X(x) = C_1 \cos \lambda^{\frac{1}{4}} x + C_2 \sin \lambda^{\frac{1}{4}} x + C_3 \cosh \lambda^{\frac{1}{4}} x + C_4 \sinh \lambda^{\frac{1}{4}} x$$

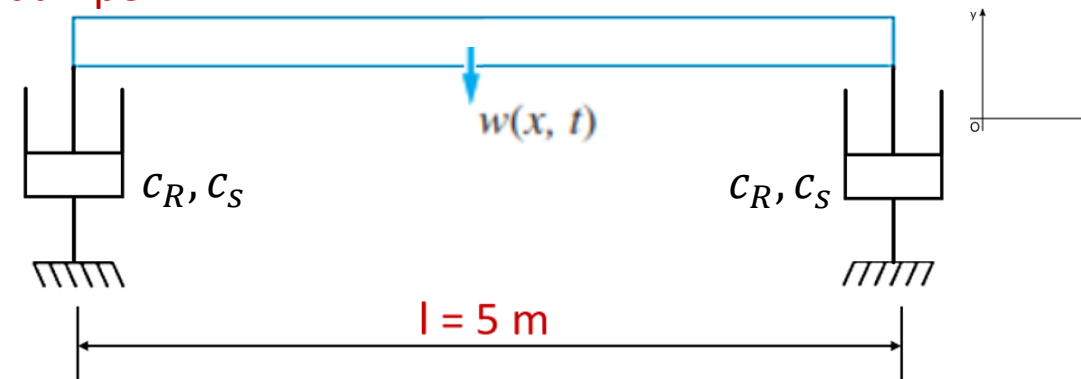
Linear spring:



Boundary Condition

$$\begin{aligned} x = 0 &\rightarrow \frac{\partial^2 \omega}{\partial x^2} = 0 & \text{and} & \quad \frac{\partial^3 \omega}{\partial x^3} = -\beta \omega \\ x = 5 &\rightarrow \frac{\partial^2 \omega}{\partial x^2} = 0 & \text{and} & \quad \frac{\partial^3 \omega}{\partial x^3} = \beta \omega \end{aligned} \quad \beta = \frac{kL^3}{EI}$$

Viscous damper:

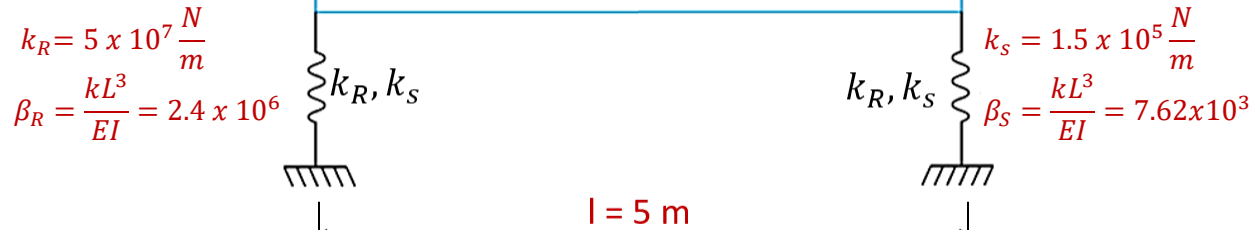


Boundary Condition

$$\begin{aligned} x = 0 &\rightarrow \frac{\partial^2 \omega}{\partial x^2} = 0 & \text{and} & \quad \frac{\partial^3 \omega}{\partial x^3} = -\beta \frac{\partial \omega}{\partial t} \\ x = 5 &\rightarrow \frac{\partial^2 \omega}{\partial x^2} = 0 & \text{and} & \quad \frac{\partial^3 \omega}{\partial x^3} = \beta \frac{\partial \omega}{\partial t} \end{aligned} \quad \beta = \frac{cL}{\sqrt{\rho E I A}}$$

## Study Model: Supported

Linear spring:



$$\begin{bmatrix}
 -\sqrt{L} & 0 & \sqrt{L} & 0 \\
 B & -L^{3/4} & -B & L^{3/4} \\
 -\sqrt{L} \cos(\sigma_1) & -\sqrt{L} \sin(\sigma_1) & \sqrt{L} \cosh(\sigma_1) & \sqrt{L} \sinh(\sigma_1) \\
 L^{3/4} \sin(\sigma_1) - B \cos(\sigma_1) & -B \sin(\sigma_1) - L^{3/4} \cos(\sigma_1) & L^{3/4} \sinh(\sigma_1) - B \cosh(\sigma_1) & -B \sinh(\sigma_1) - L^{3/4} \cosh(\sigma_1)
 \end{bmatrix}$$

where  $\sigma_1 = 5 L^{1/4}$

[A]: Coefficient Matrix

Natural frequencies

$$\det[A] = 0 \rightarrow 2 L^{5/2} - 2 L^{5/2} \cosh(\sigma_1)^2 + 2 B L^{7/4} \cos(\sigma_1) \sinh(\sigma_1) - 2 B L^{7/4} \cosh(\sigma_1) \sin(\sigma_1) = 0$$

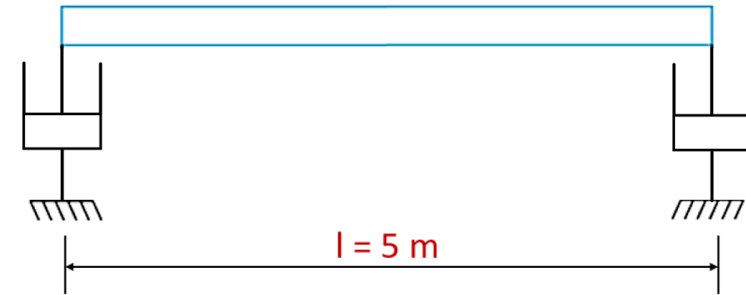
$$\lambda_R = 0.38, 3.99, 17.62, 40.51 \rightarrow \omega = \sqrt{\frac{\lambda EI}{\mu L^4}} \rightarrow \omega_R = 1 - 3.24 - 6.8 - 10.31 \left[ \frac{\text{rad}}{\text{s}} \right]$$

$$\lambda_S = 0.38, 3.71, 17.62, 40.51 \rightarrow \omega = \sqrt{\frac{\lambda EI}{\mu L^4}} \rightarrow \omega_S = 1 - 3.12 \left[ \frac{\text{rad}}{\text{s}} \right]$$

Viscous damper:

$$c_r = 2 \times 10^4 \frac{Ns}{m}$$

$$\beta_R =$$



$$c_s = 10^3 \frac{Ns}{m}$$

$$\beta_S =$$

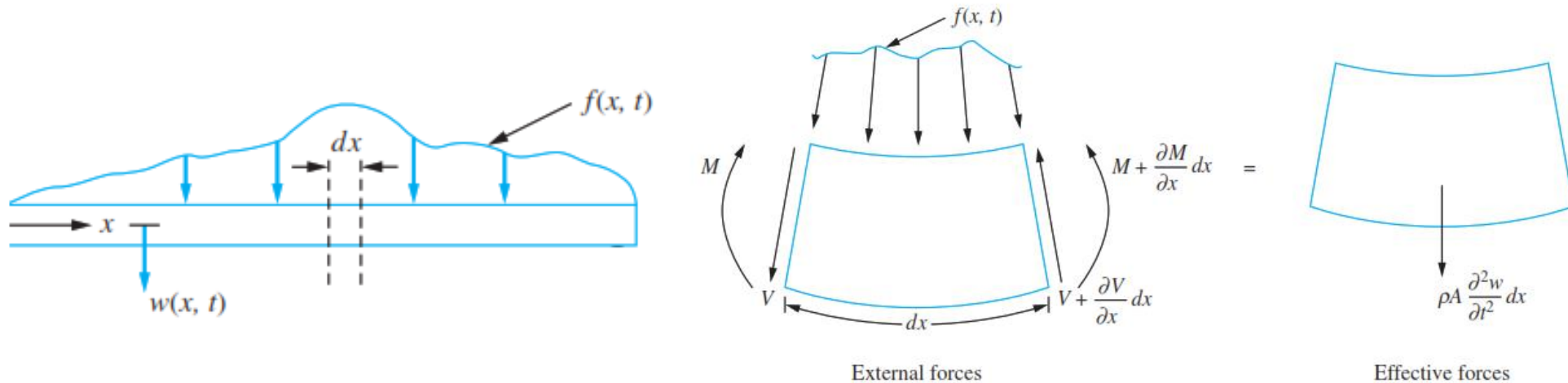
Natural frequencies

$$\beta = \frac{cL}{\sqrt{\rho E I A}} = XXX$$

$$\det[A] = 0 \rightarrow \text{WORK IN PROGRESS}$$

## Future developments

- Finite element analysis to verify the analytical model
- If working, FEM analysis to the other case studies (faster analysis)
- Calculation of the value of  $f(x, t)$  in the different study configurations



*Thank you for your  
attention*