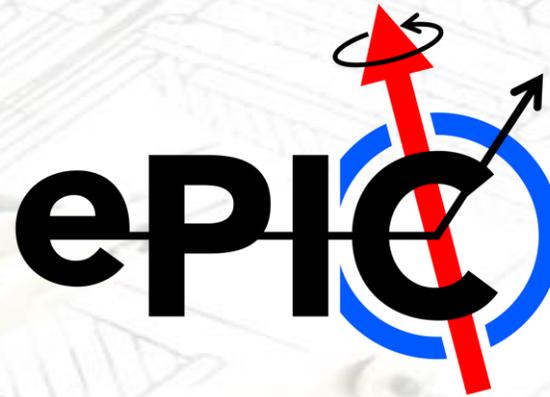




Istituto Nazionale di Fisica Nucleare
SEZIONE DI FERRARA



Università
degli Studi
di Ferrara



dRICH

Mechanical Design Status

Overview

dRICH Mechanical Design

- Main requirements: position, clearance and envelope
- Components: vessel, detector box, aerogel
- Integration

PCB Cooling

- Main requirements

Prototype

- Design

Target R&D and Generic R&D

- Spectrometer Chamber
- High Pressure Chamber

Mechanical Design Team

INFN FERRARA: mechanical design

- Alessandro Saputi
- Michele Melchiorri

INFN Torino: thermal simulations and cooling

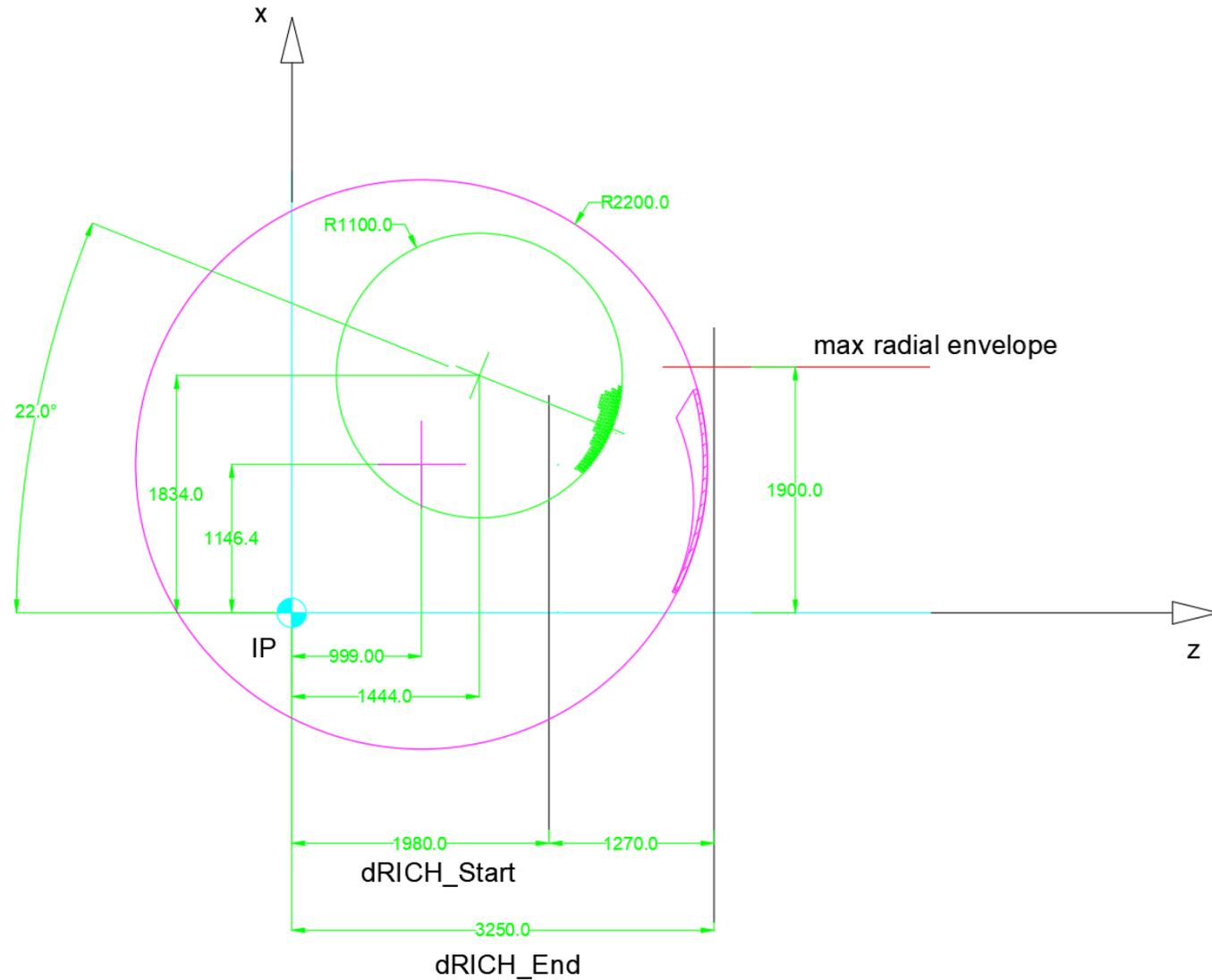
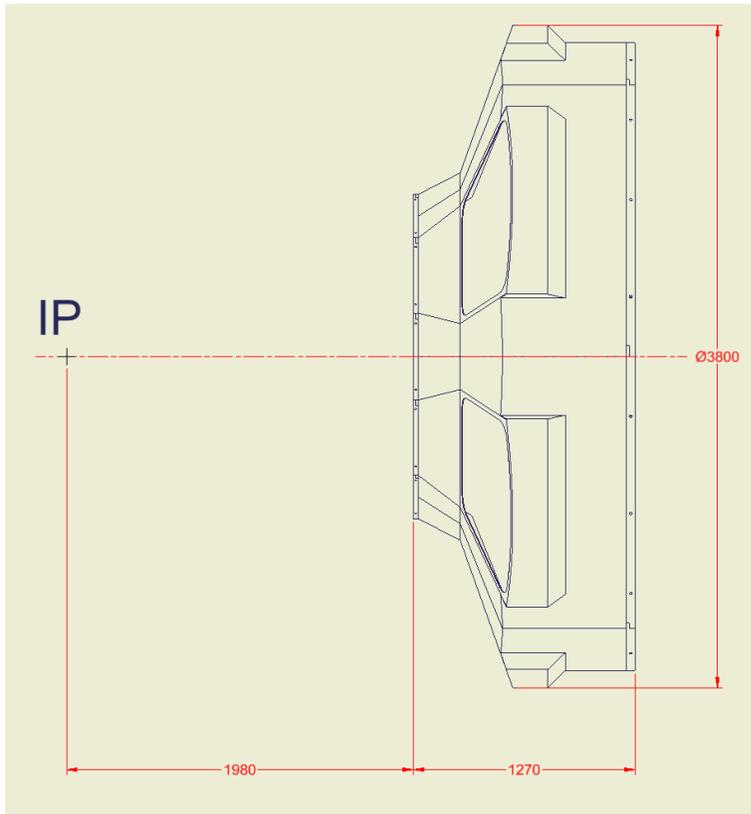
- Carlo Mingioni
- Marco Nenni

JLAB: mirrors design

- Alex Eslinger

dRICH: main requirements

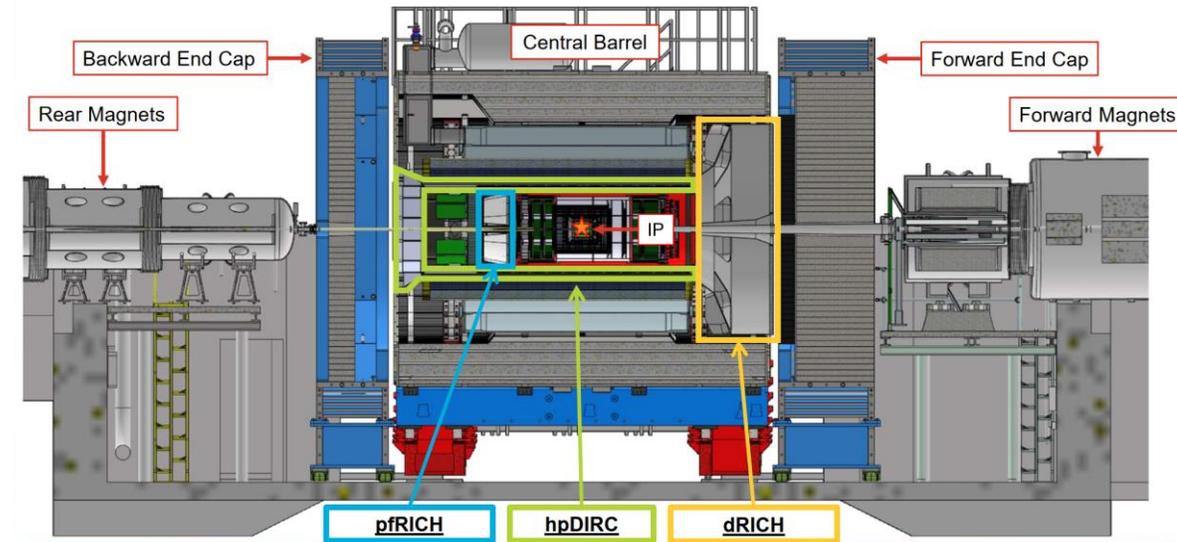
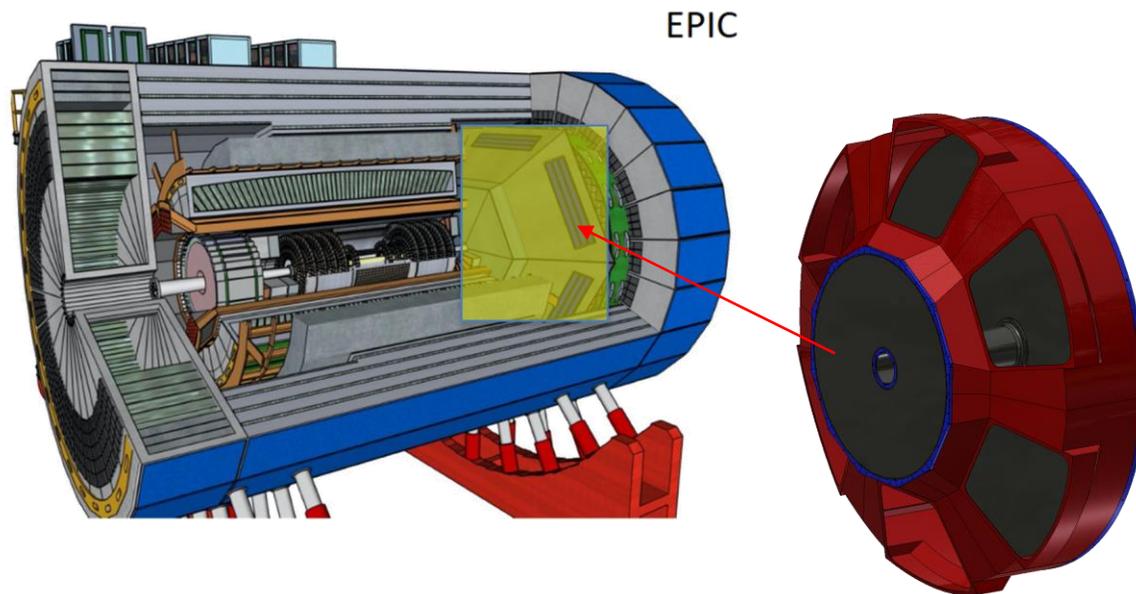
- **Envelope overall size:** $\text{Ø}3800 \text{ mm} \times 1270 \text{ mm}$
- **Operating pressure:** Up to 3 - 10 mbar
- **Operating temperature:** 22 °C
- **Gas mixture:** C_2F_6 - Nitrogen



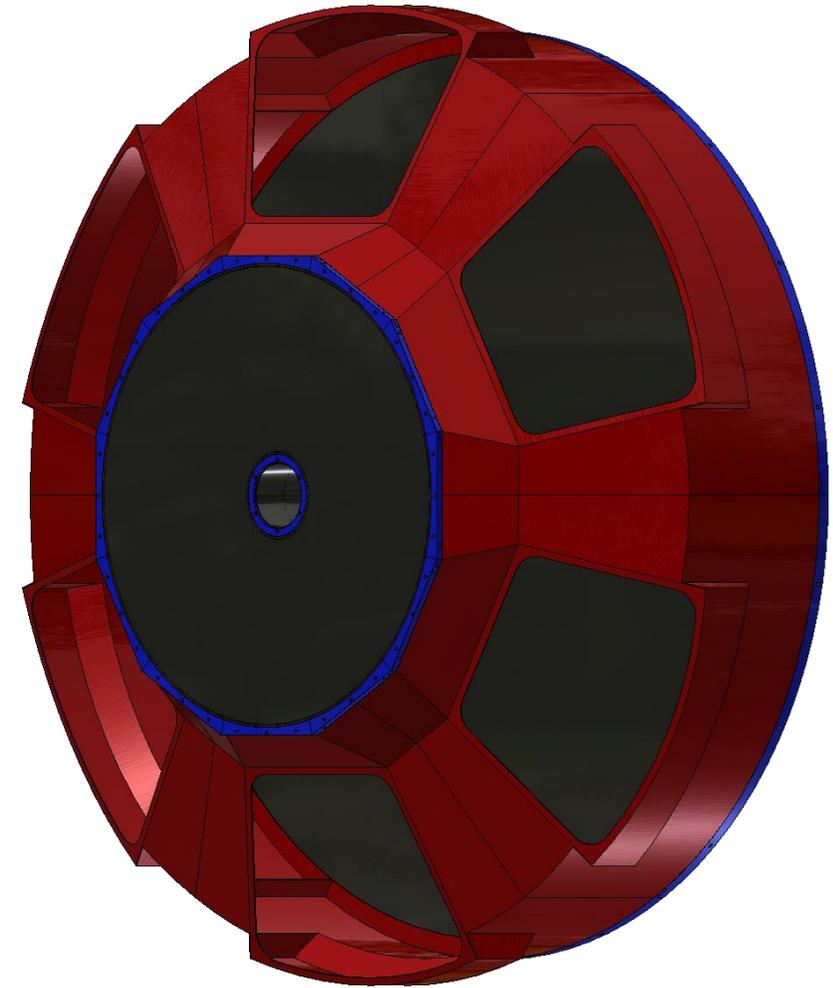
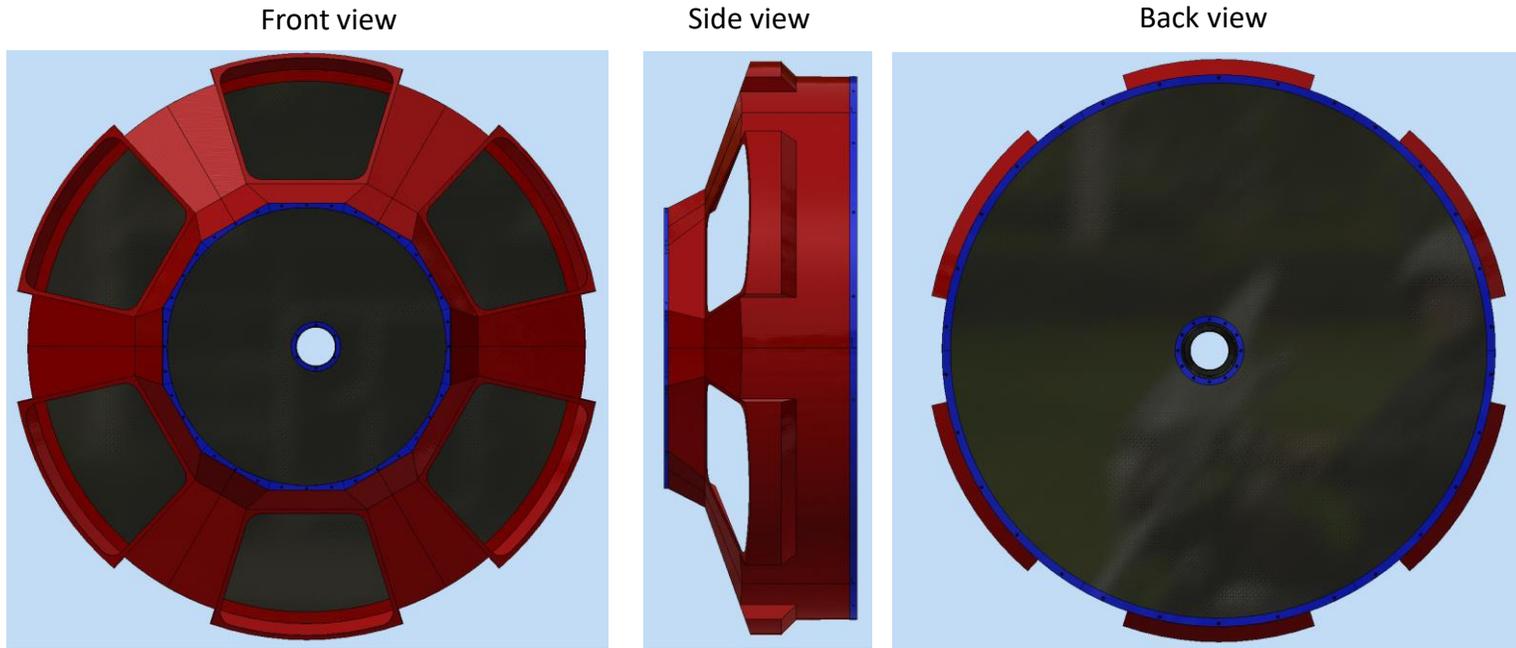
dRICH: main requirements

The major functions of the dRICH mechanical structure (gas enclosure) are to provide containment for the dRICH gas radiator and to act as a stable frame for the optical components (the mirrors and aerogel):

- It must be light-tight.
- It must ensure the stability of the structure under the influence of the magnetic field.
- The enclosure must withstand a differential pressure of 3-10 mbar without compromising the mirror alignment.
- The minimum amount of material must be placed within the ePIC experiment acceptance limits.

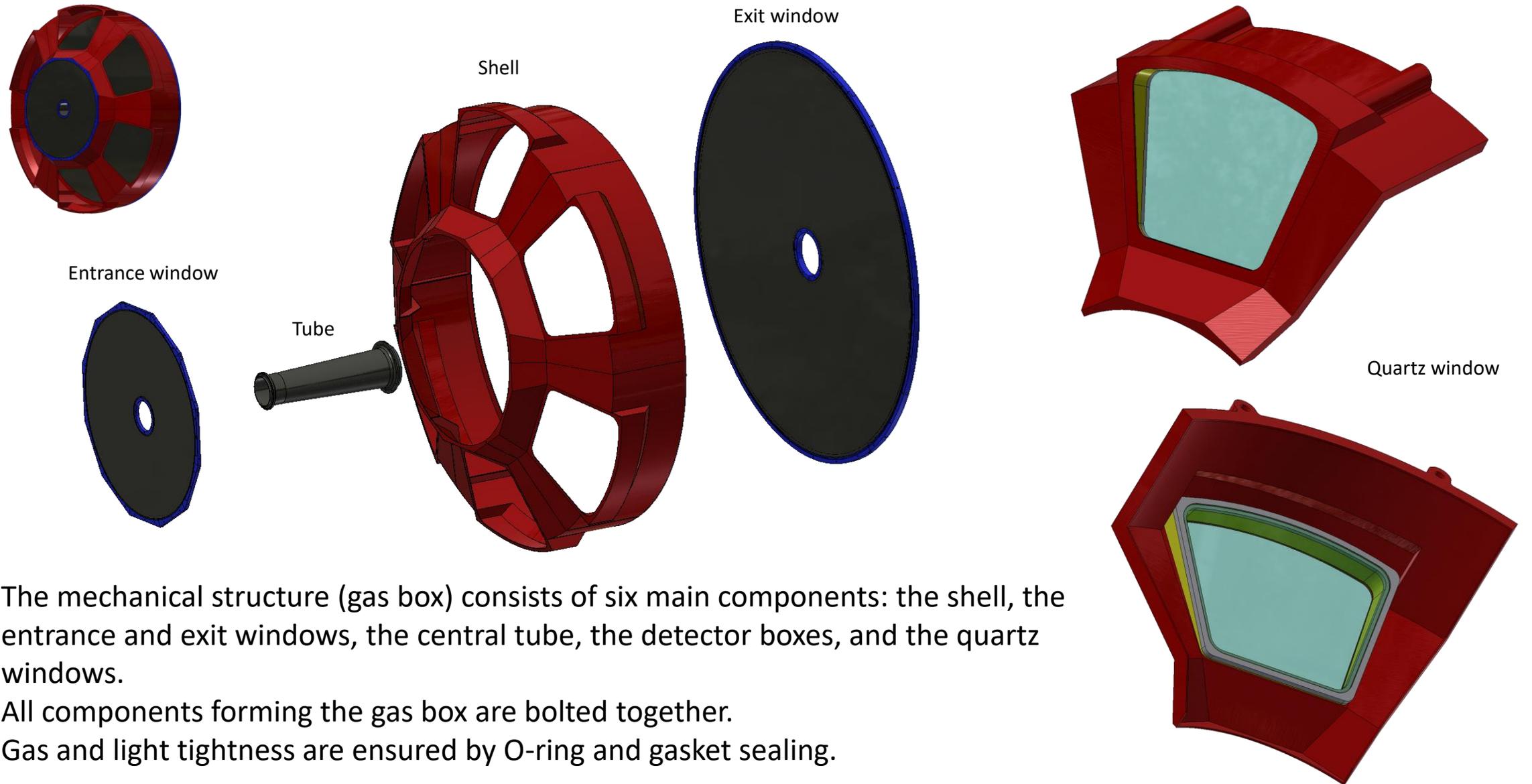


dRICH Gas Box: mechanical preliminary design



The gas box is essentially a cylindrical box made of carbon fibers, that hosts mirrors and aerogel tiles.

dRICH Gas Box: mechanical structure

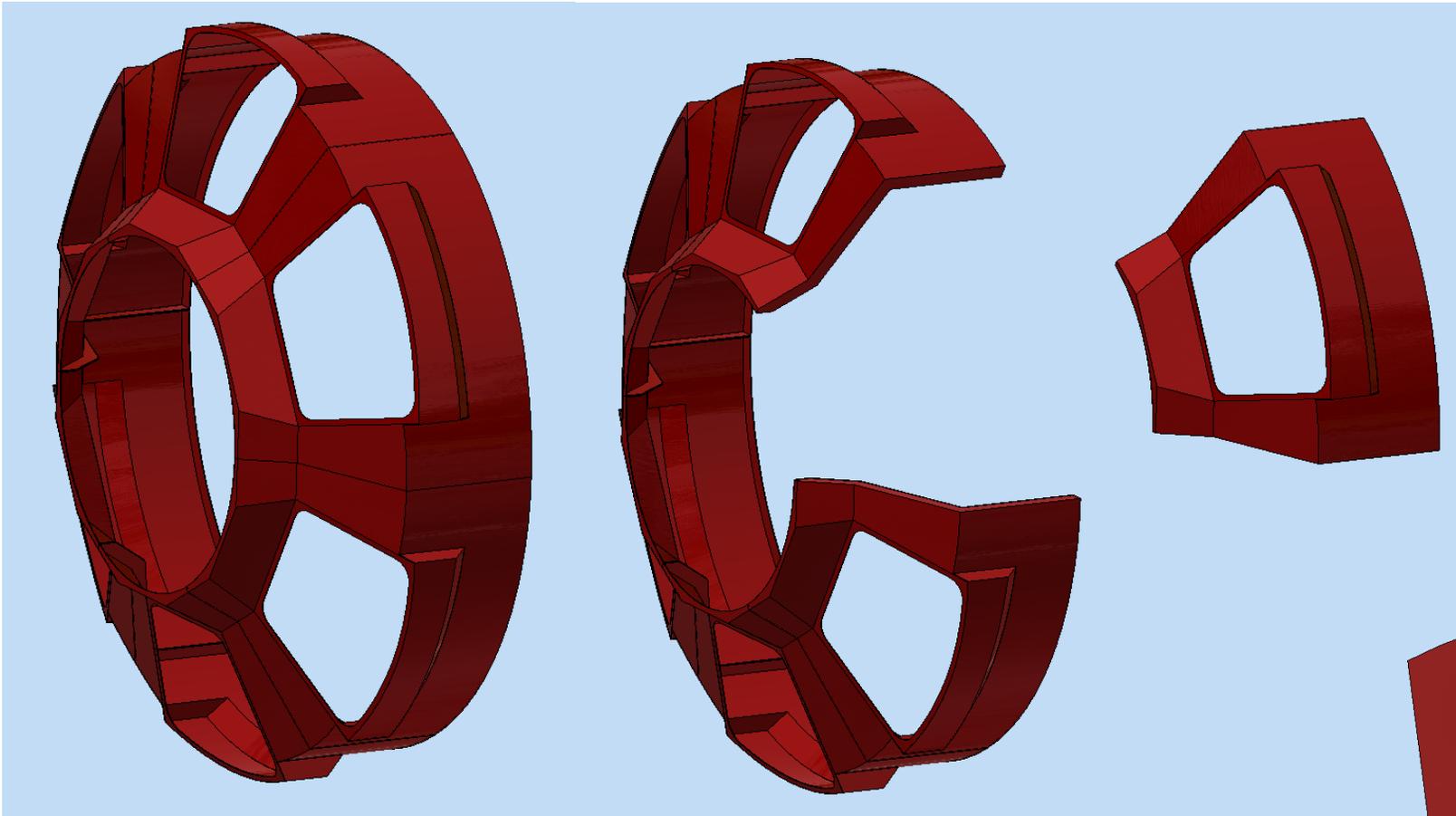


The mechanical structure (gas box) consists of six main components: the shell, the entrance and exit windows, the central tube, the detector boxes, and the quartz windows.

All components forming the gas box are bolted together.

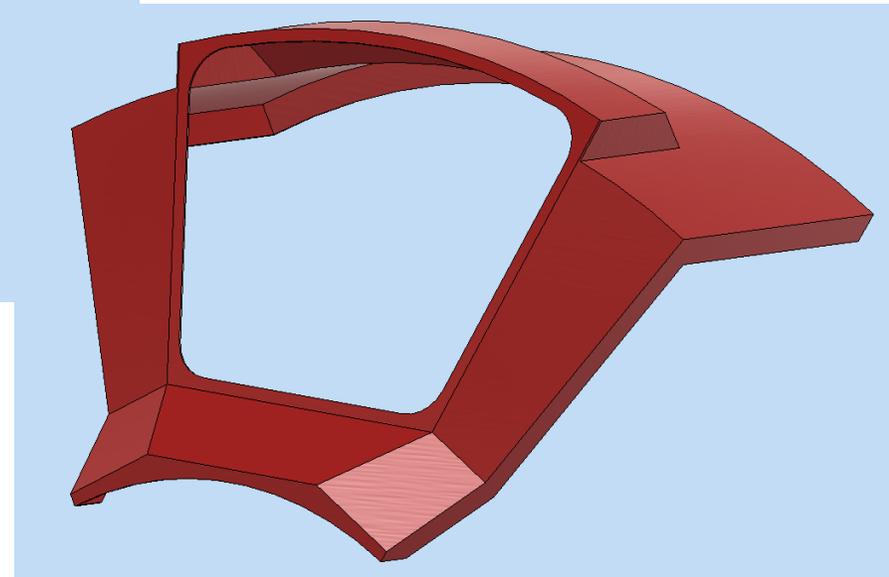
Gas and light tightness are ensured by O-ring and gasket sealing.

dRICH: shell

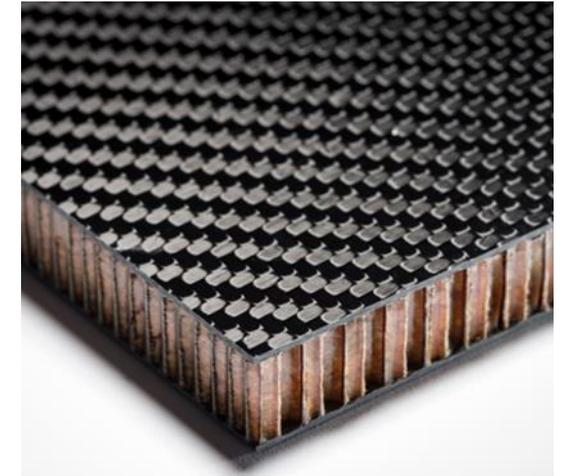
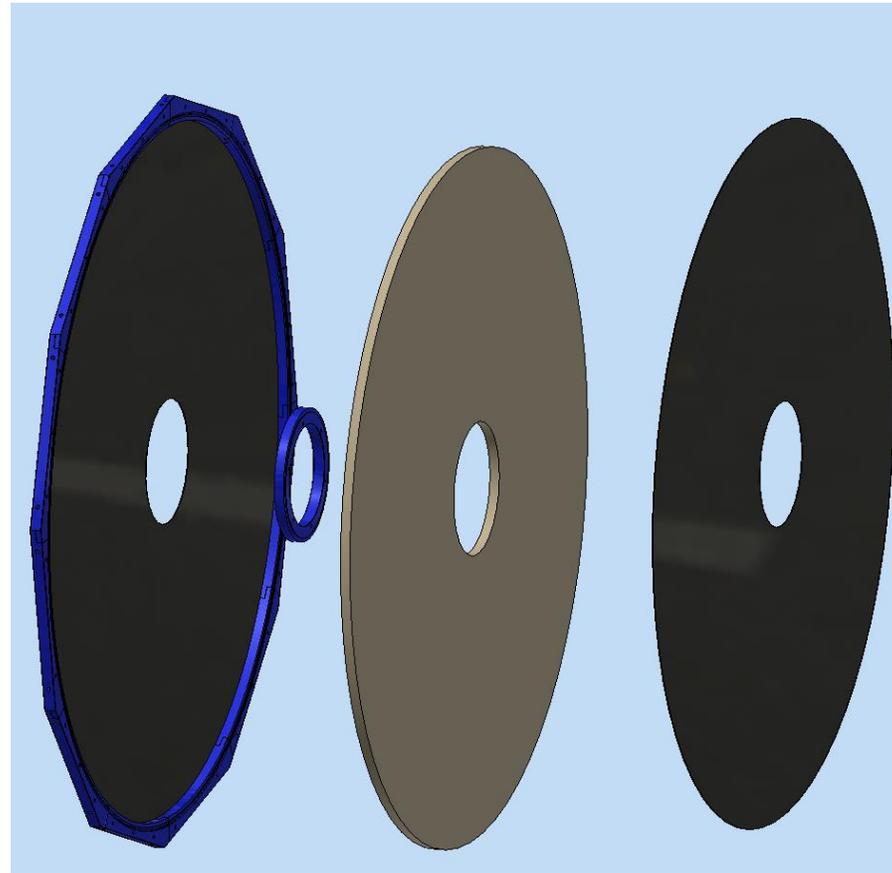


The shell will be made of an 10 mm thick carbon fibre epoxy composite. Each laminate will consist of six layers of balanced weave fabric, with fibres oriented at $0^\circ/90^\circ$ in one layer and $\pm 45^\circ$ in the adjacent layer.

The shell is composed of six parts that are bolted and glued together to ensure structural integrity and the gas/light tightness.



dRICH: entrance windows

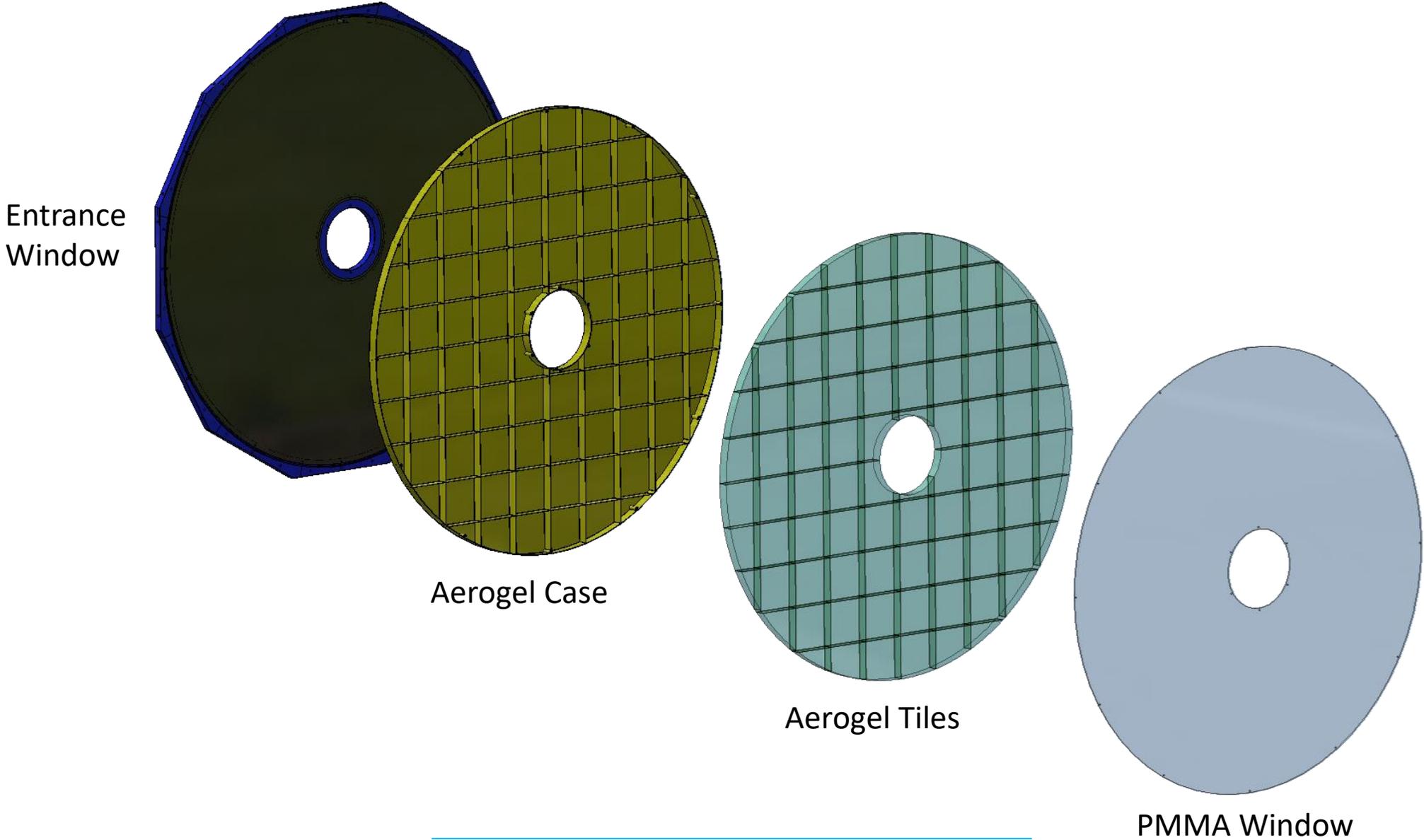


The Entrance Window will be a sandwich panel consisting of two carbon fiber-reinforced epoxy skins, each 2.28 mm thick, separated by a 25 mm thick Nomex honeycomb core. Each skin is composed of six layers of balanced weave laminate, with fibers oriented at $0^{\circ}/90^{\circ}$ in one layer and overlapped with $\pm 45^{\circ}$ in the adjacent layer.

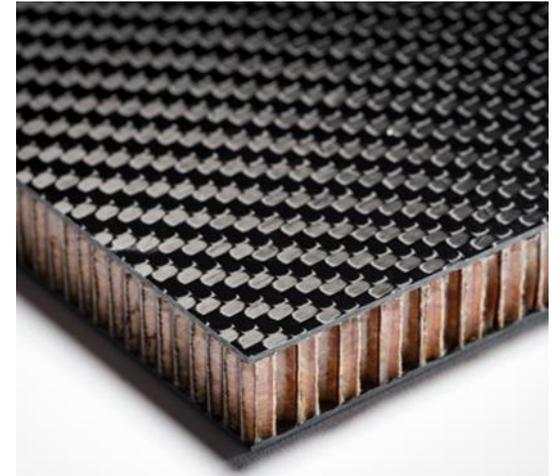
The external sides are enclosed by two solid frames made of carbon fiber (CF) or aluminum.

dRICH: aerogel support structure

nil volentibus arduum



dRICH: exit windows



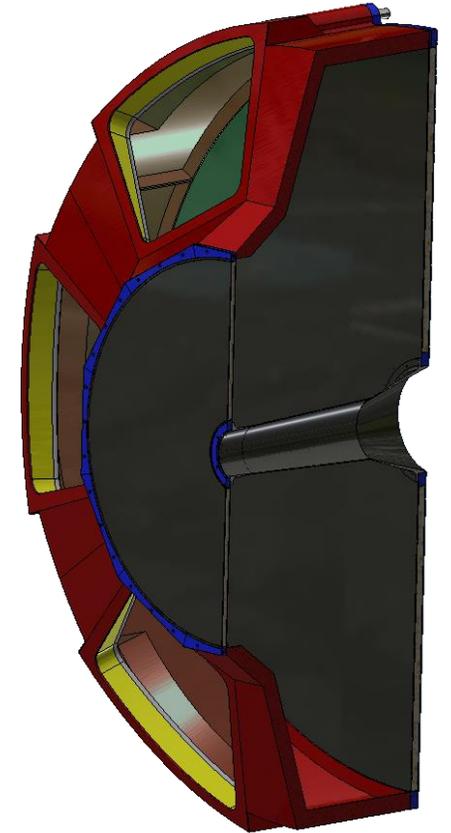
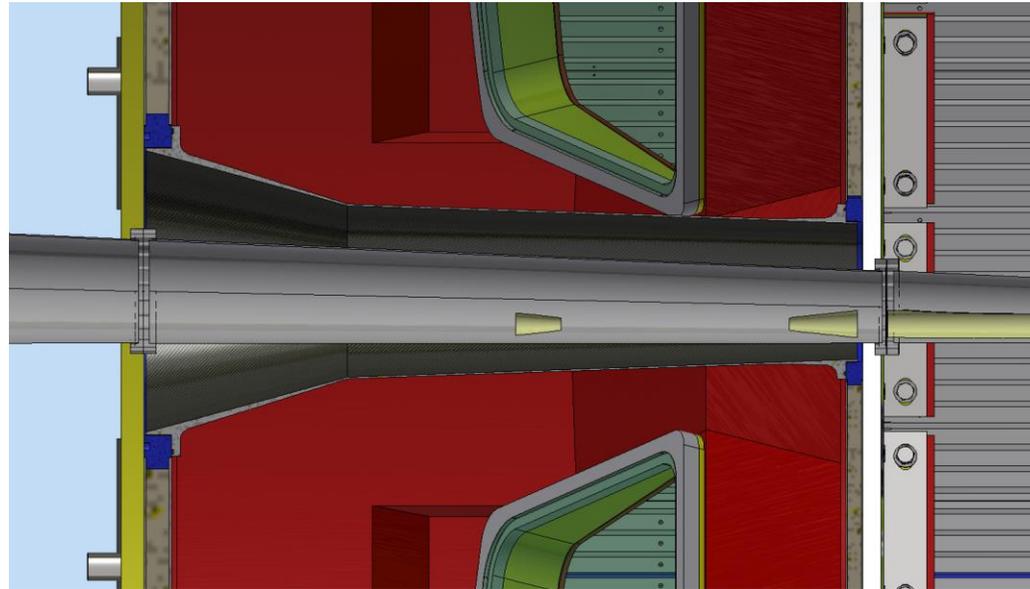
The Exit Window will be a sandwich panel consisting of two carbon fiber-reinforced epoxy skins, each 4.56 mm thick, separated by a 40 mm thick Nomex honeycomb core. Each skin is composed of six layers of balanced weave laminate, with fibers oriented at $0^{\circ}/90^{\circ}$ in one layer and overlapped with $\pm 45^{\circ}$ in the adjacent layer.

The external sides are enclosed by two solid frames made of carbon fiber (CF) or aluminum.

dRICH: central tube



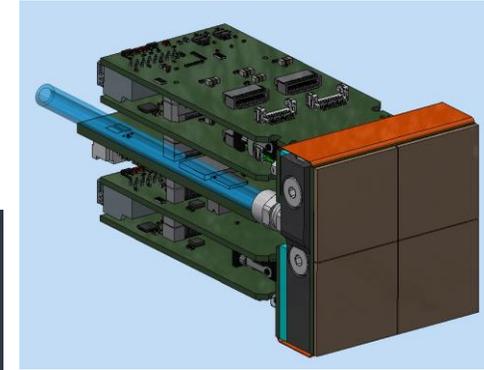
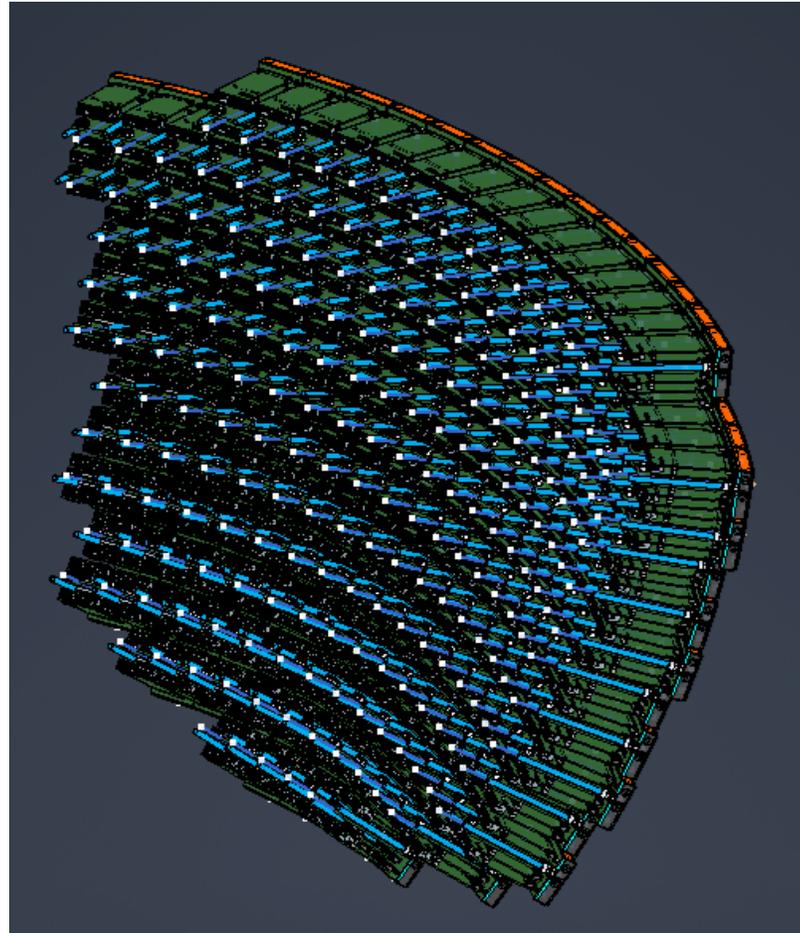
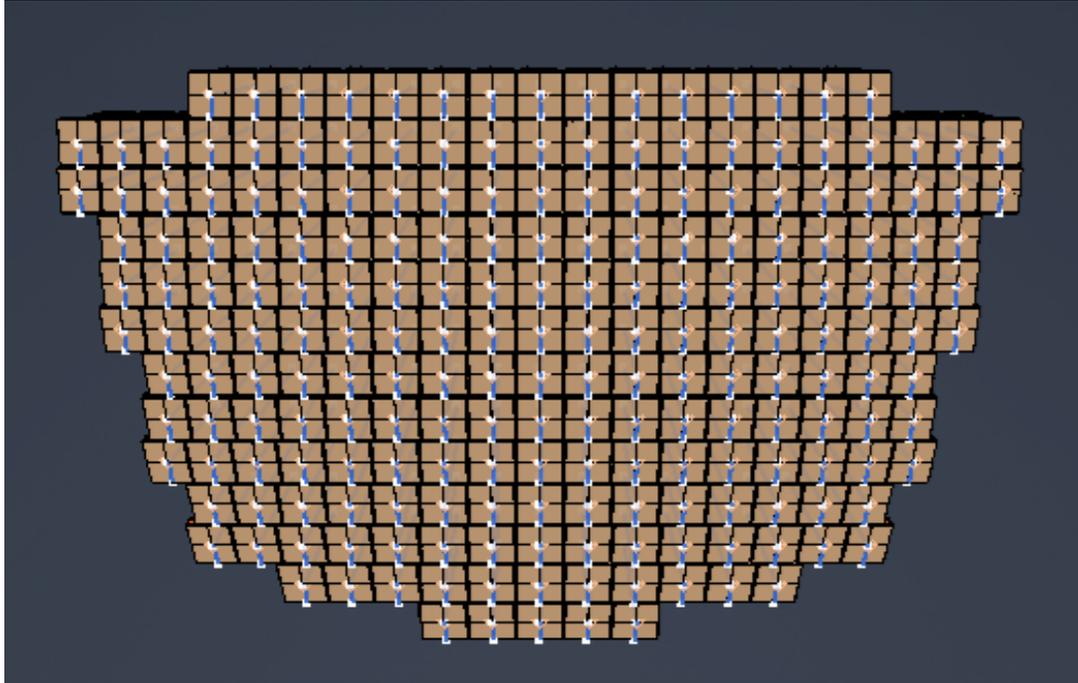
Central tube



Both the entrance and exit windows are connected by the central tube. The central tube will be made of a 5 mm thick carbon fiber epoxy composite and will have an inside diameter of 242 mm at the entrance window, tapering to 500 mm at the exit window. This design ensures a radial separation between the vacuum chamber and the central tube.

dRICH: PDU - detector

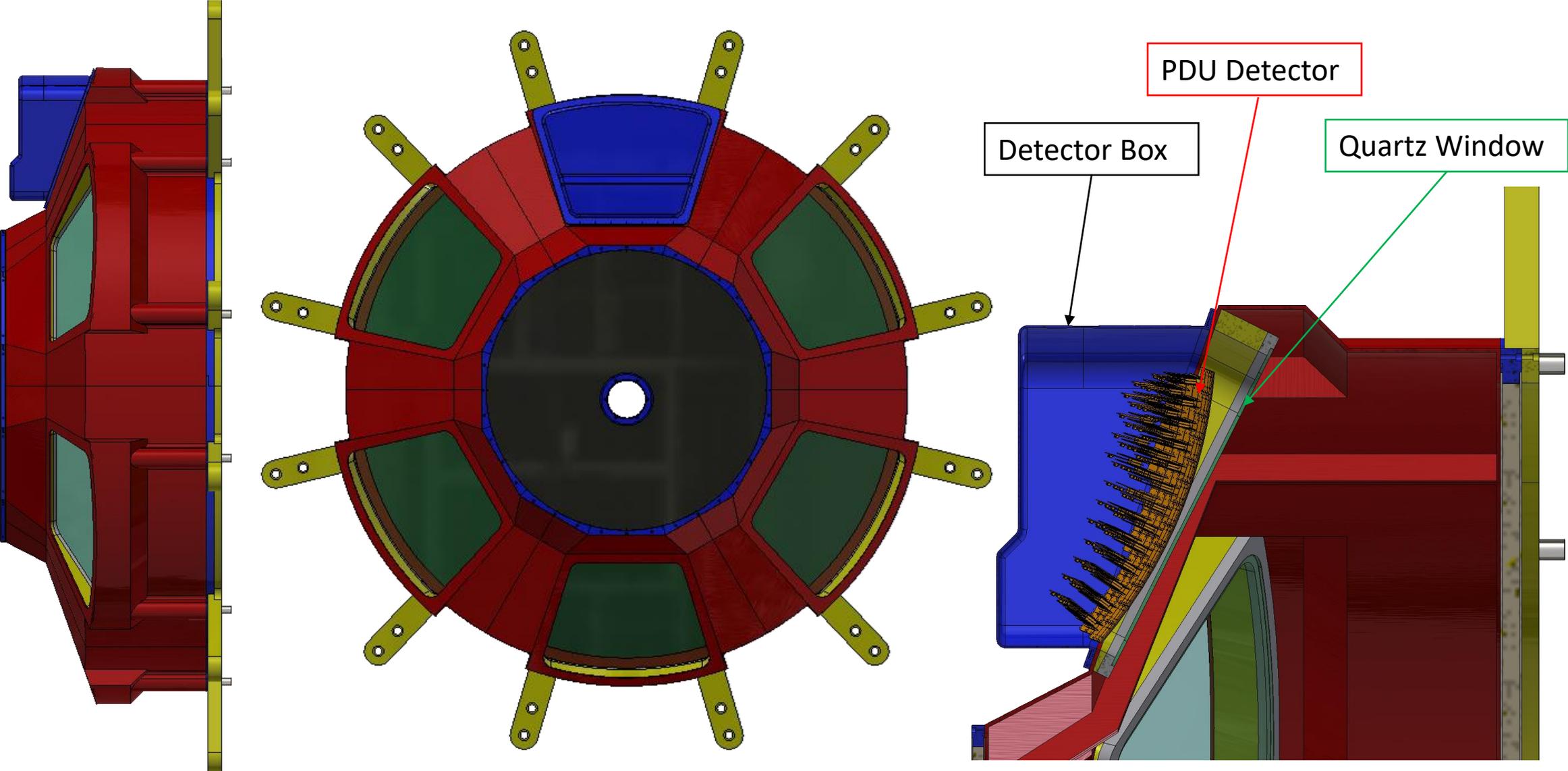
The detector is composed of 211 PDUs arranged on a sphere with a radius of 1100 mm



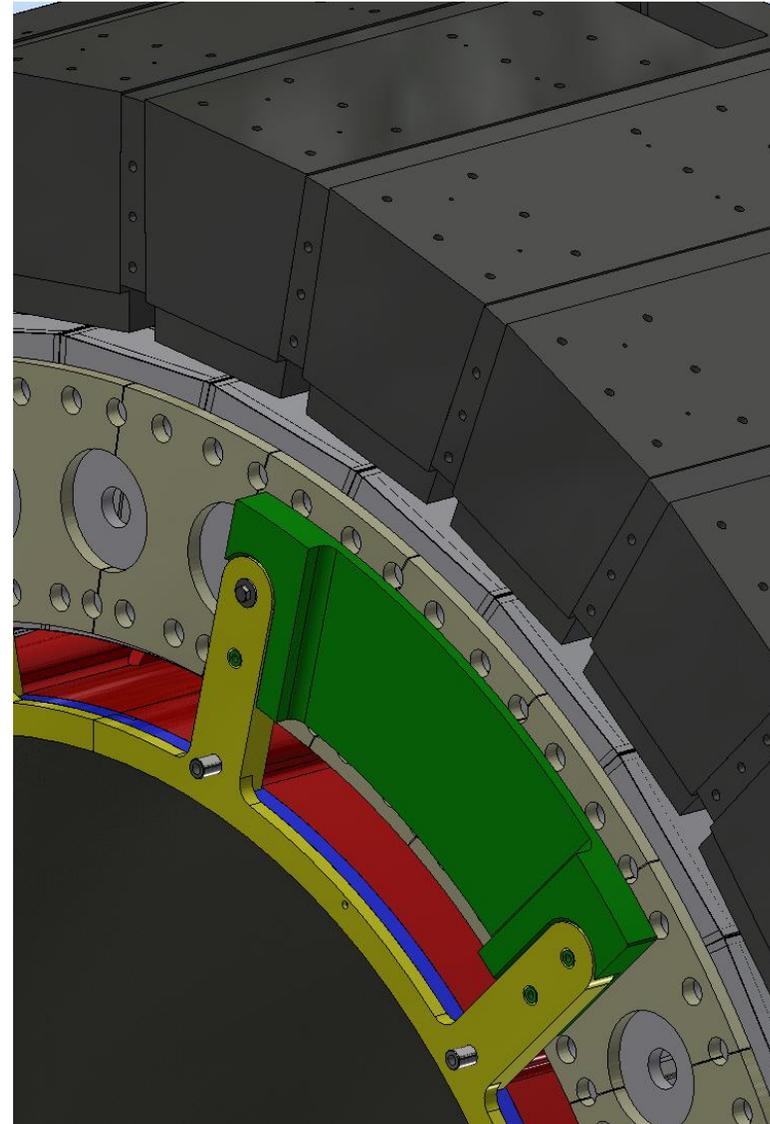
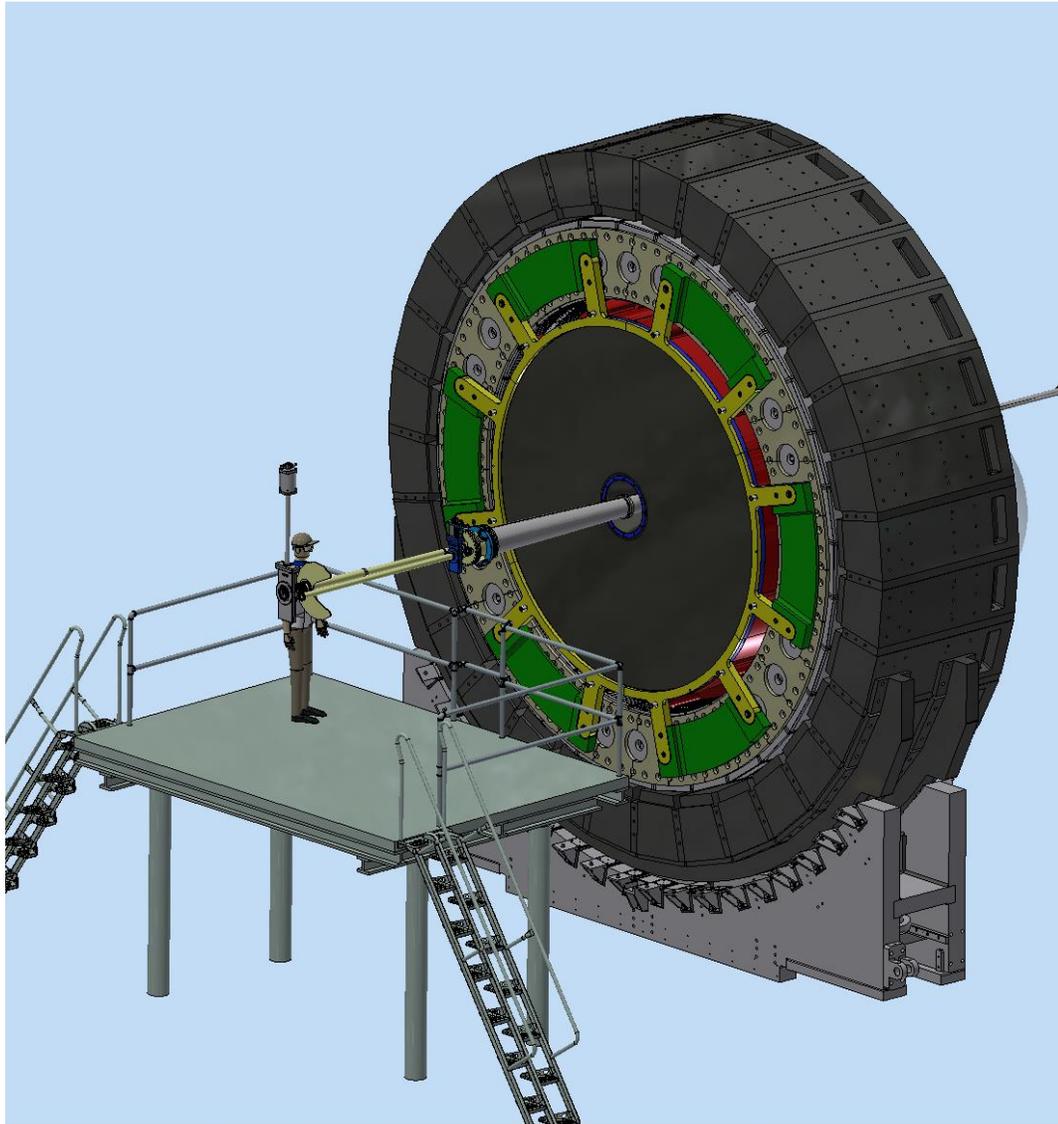
PDU designed by R. Preghenella

dRICH: detector box

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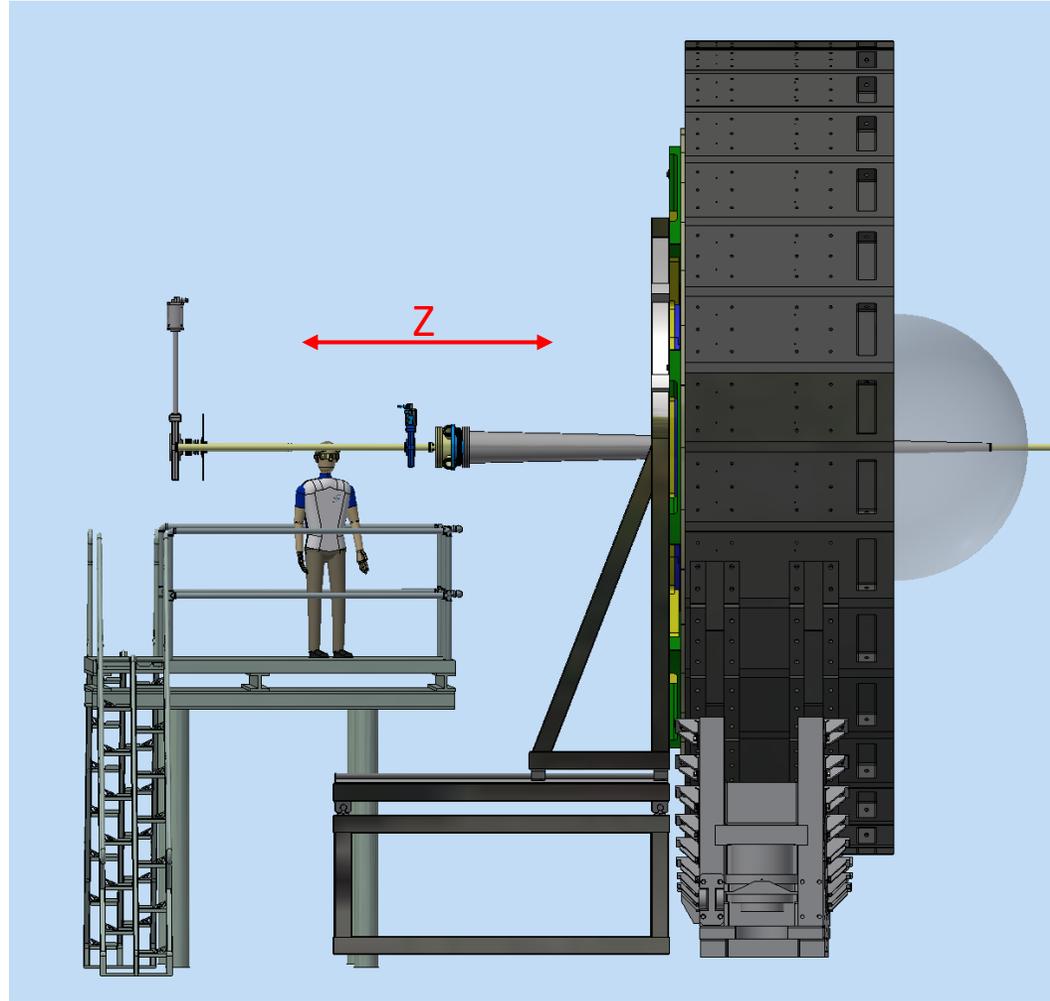
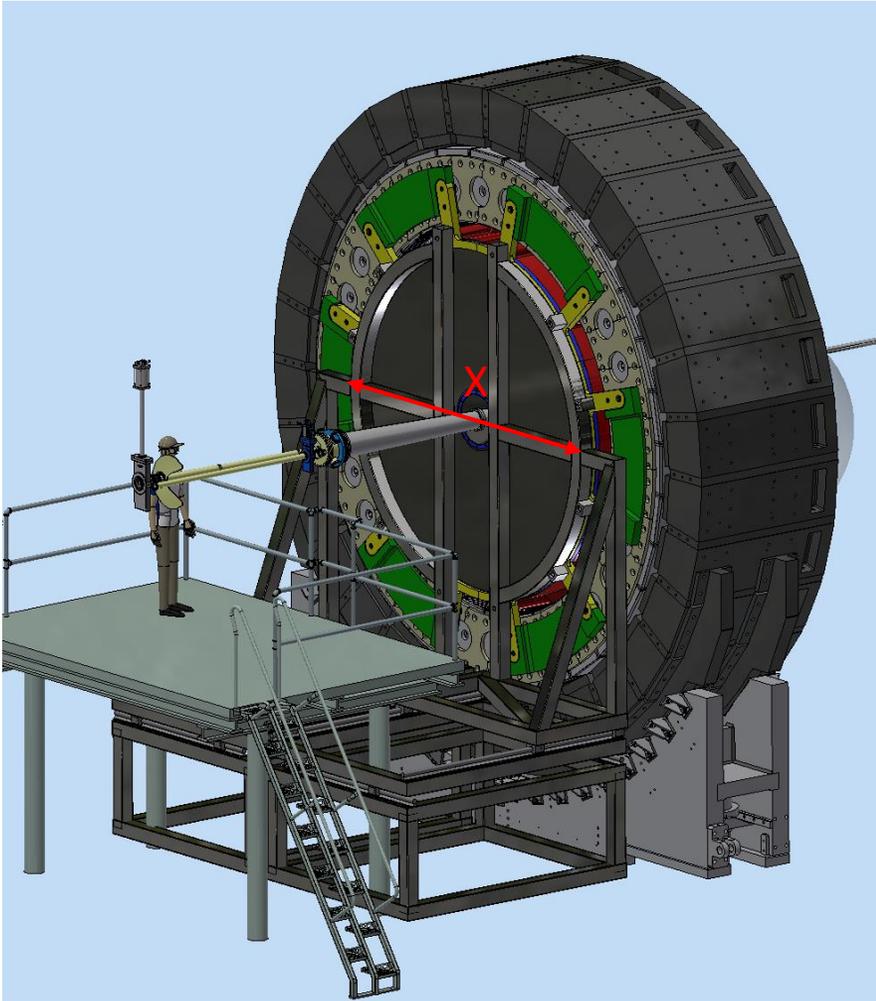


dRICH: integration with ePIC apparatus



- dRICH (yellow arms) are bolted to the green plates.
- Green plates are bolted to the calorimeter structure.

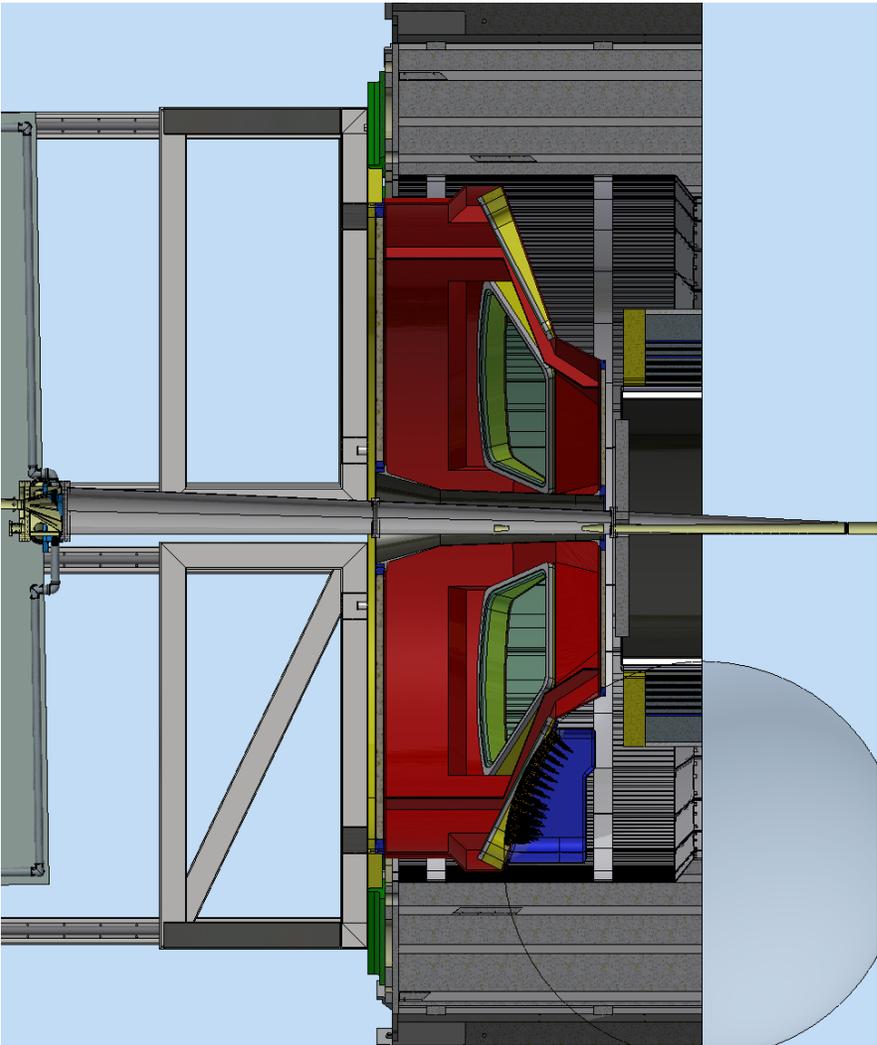
dRICH: extractio/insertion tool



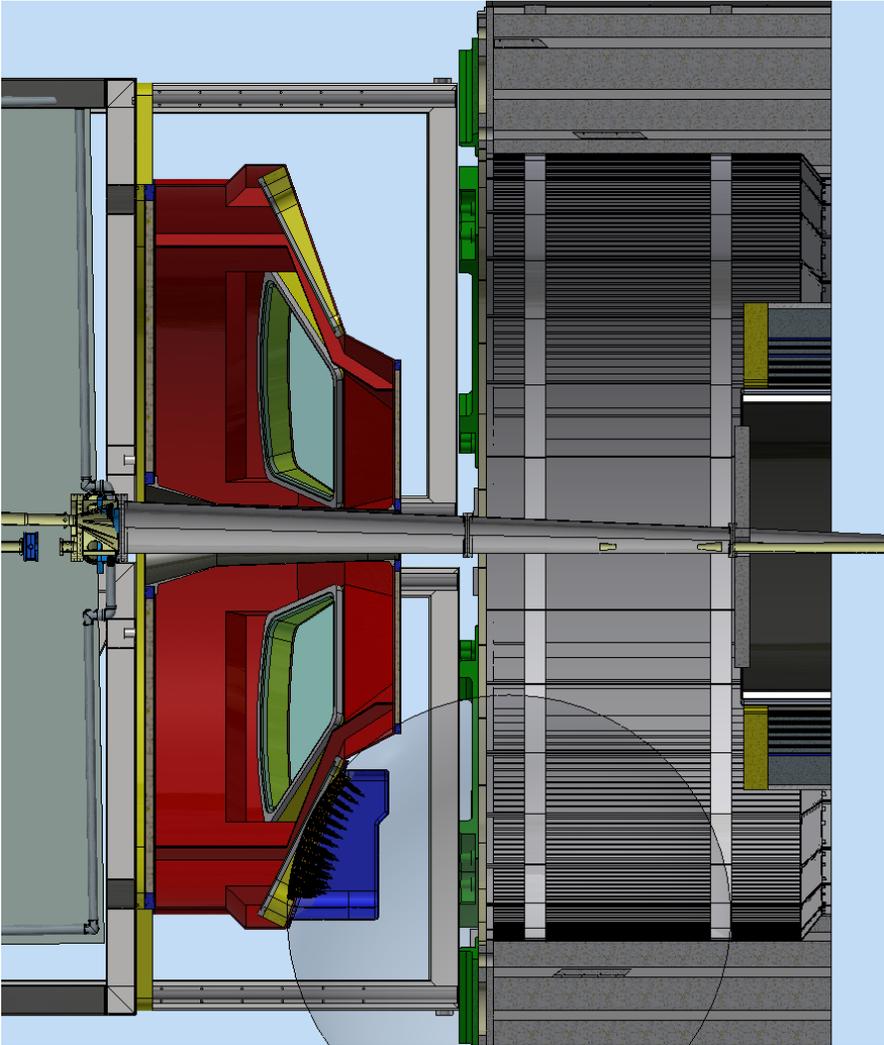
The extraction/insertion tool allows for moving the dRICH in and out, as well as shifting it in both the Z and X directions.

dRICH: closed and open position

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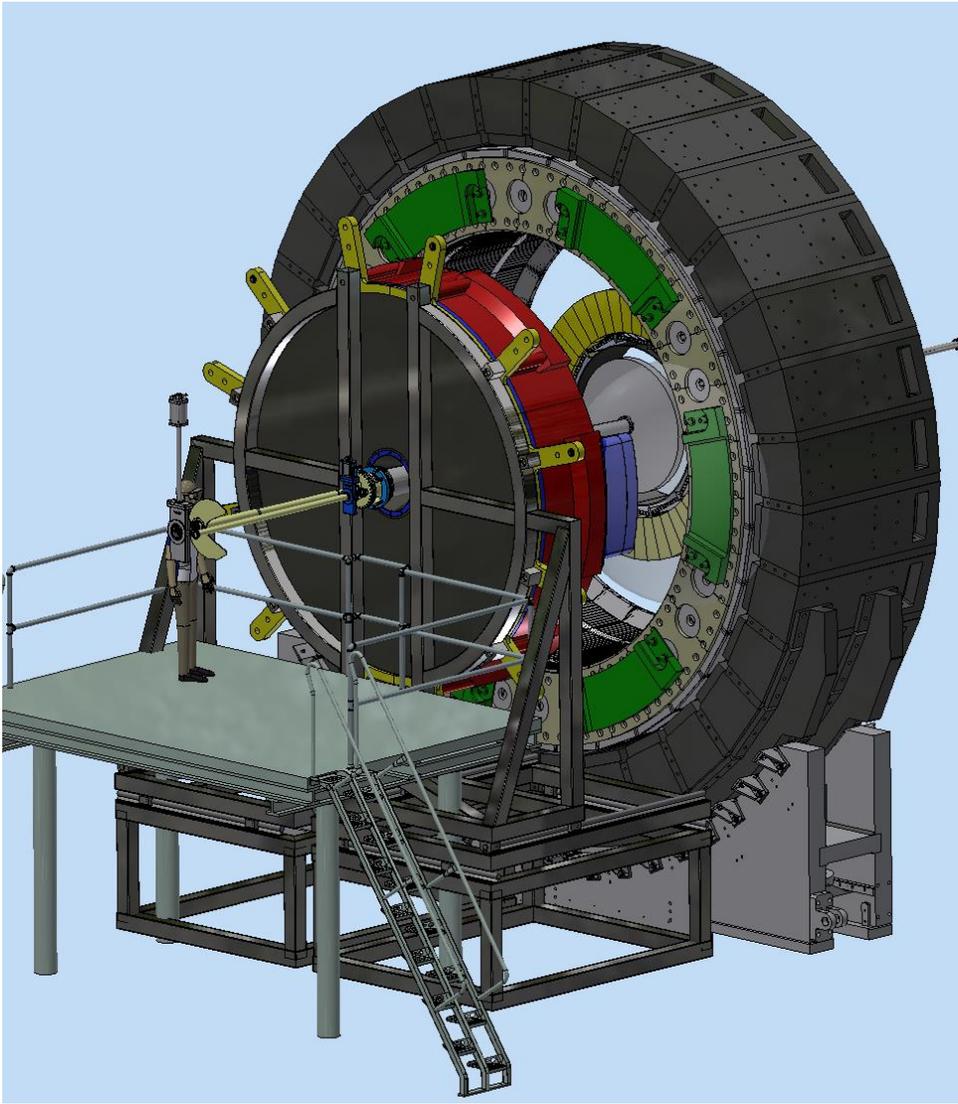
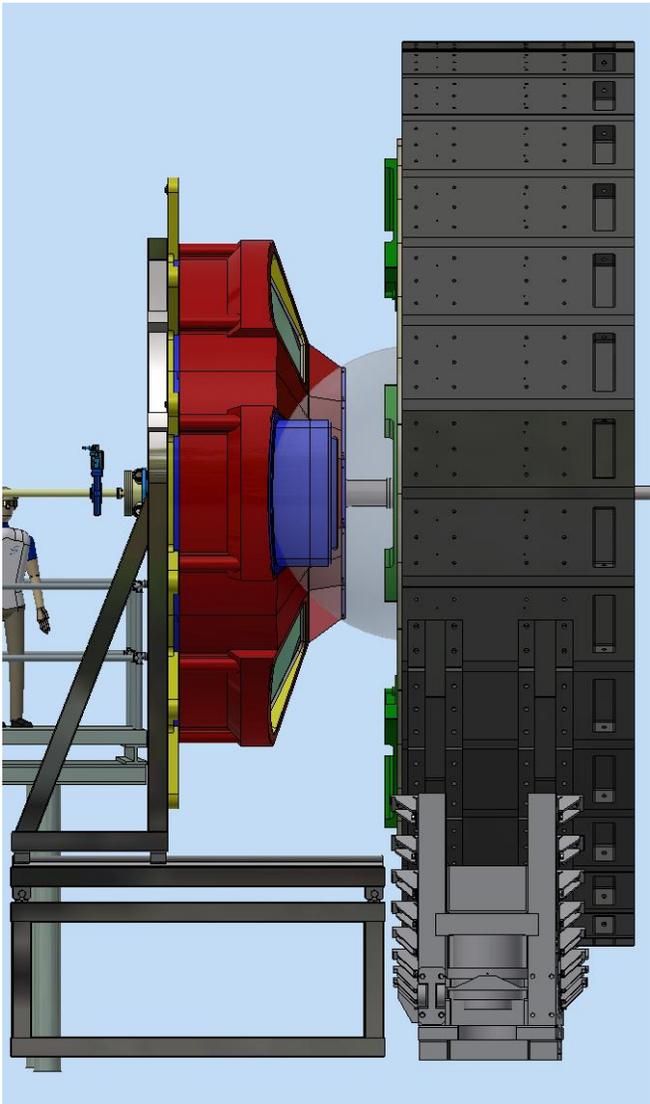
Closed position



Open position: no conflict with beam pipe

dRICH: open position

nil volentibus arduum



AEROGEL LAYOUT STUDIES

dRICH: aerogel layout

Aerogel Density $\approx 0.15 \text{ g/cm}^3$.

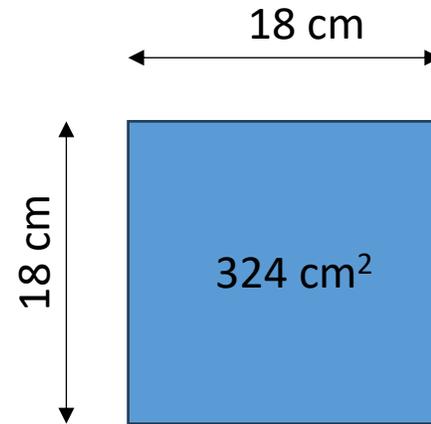
Tile size = 180 mm x 180 mm - 20 mm thick

Requirements:

Aerogel Total Thickness 40 mm

Minimize dead space between the aerogel tiles

Light-tight material on the edges of the aerogel tiles



AEROGEL – Layout_A: nesting_A

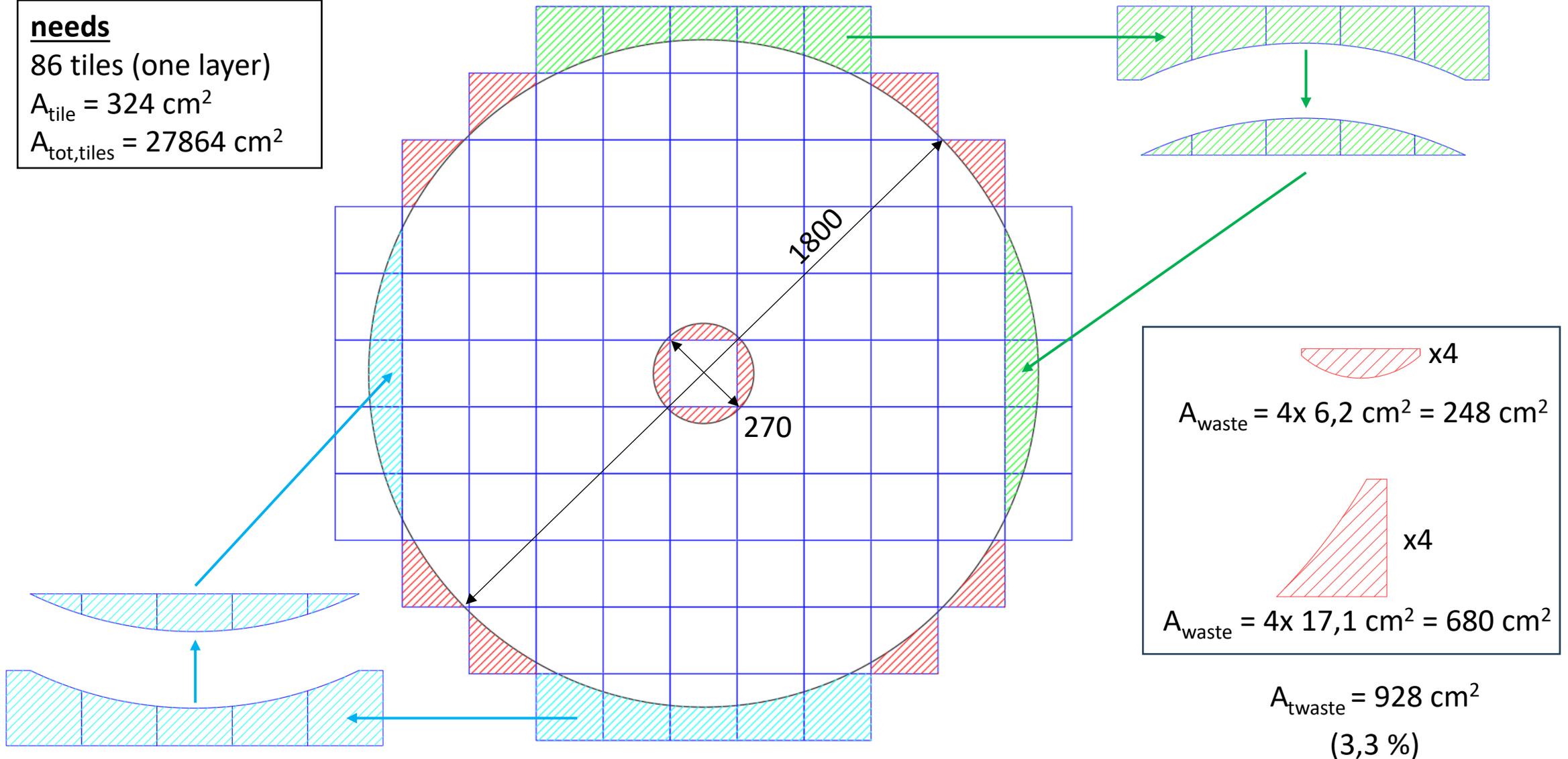
nil volentibus arduum

needs

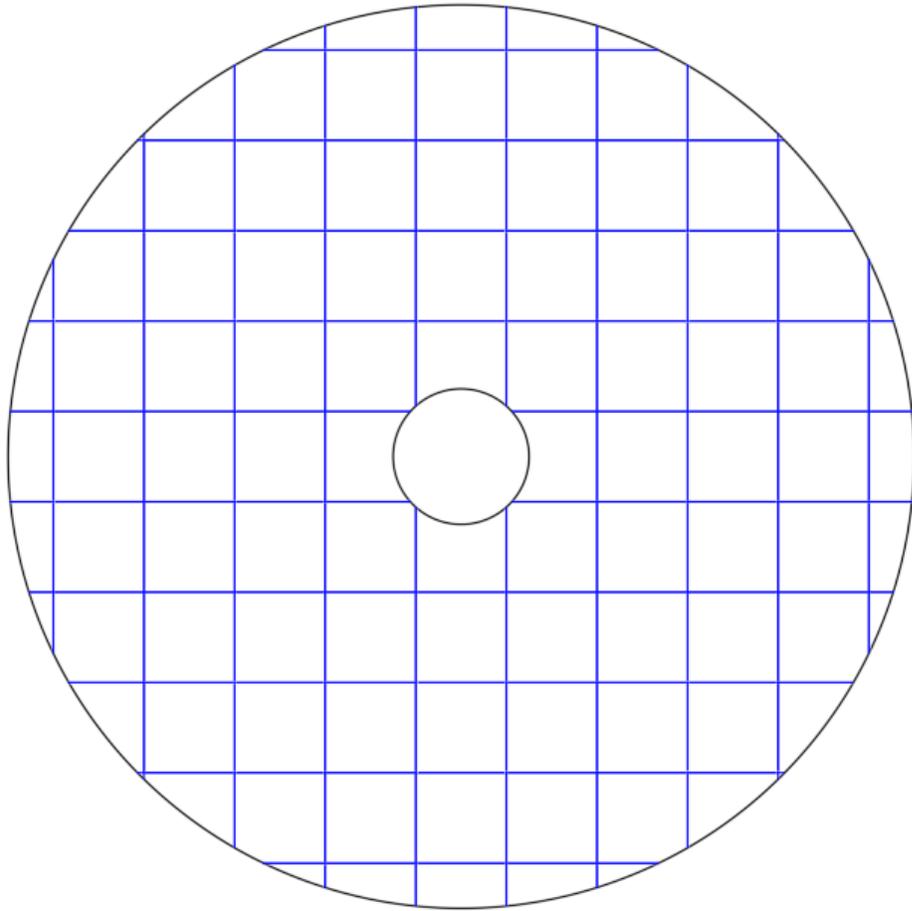
86 tiles (one layer)

$$A_{\text{tile}} = 324 \text{ cm}^2$$

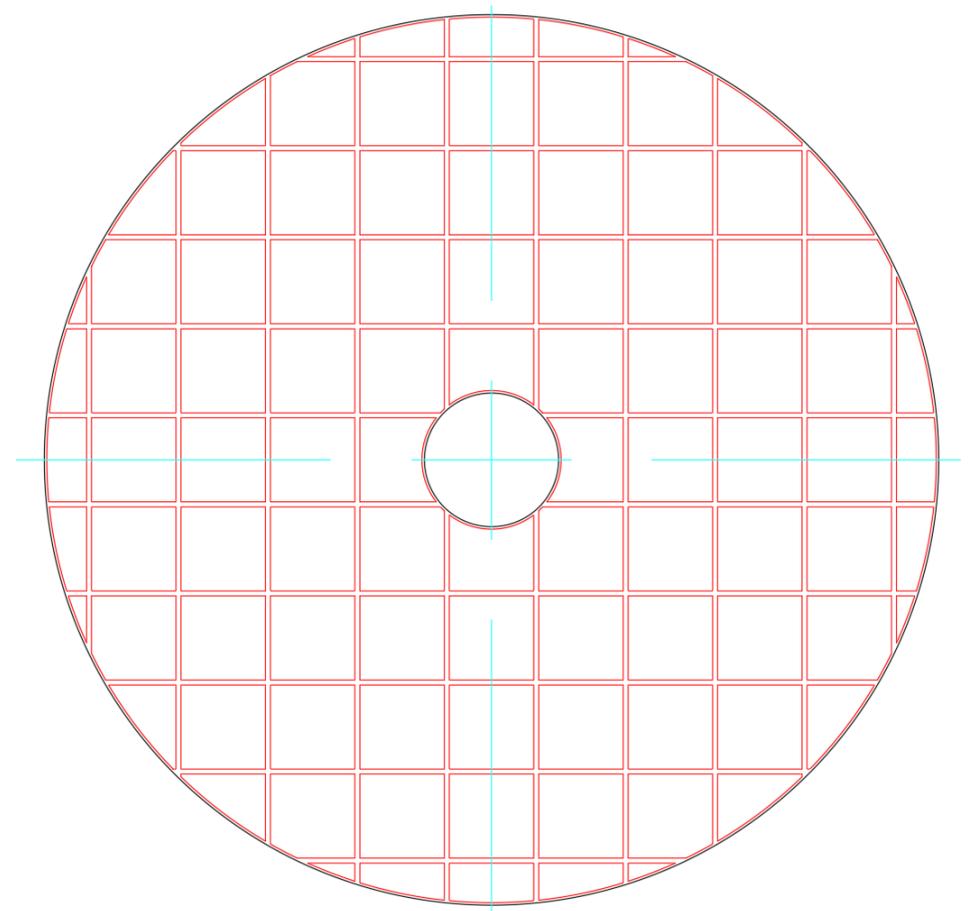
$$A_{\text{tot,tiles}} = 27864 \text{ cm}^2$$



AEROGEL – Layout_A: Active Area and Dead Space



Nominal Active Area (A_n) = 24874 cm²



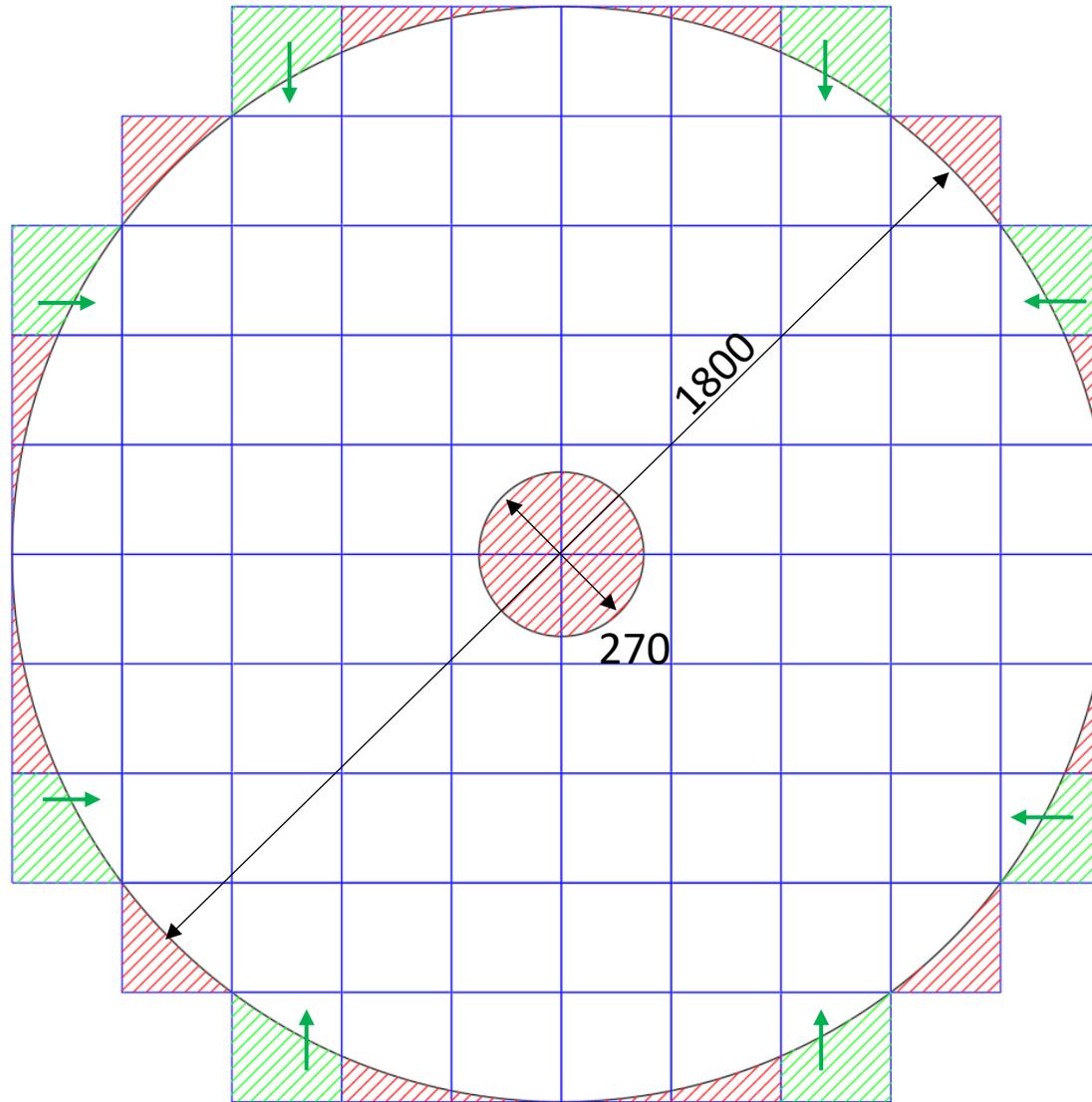
Active Area (A_a) = 21883,5 cm²

Dead Active Area (A_{da}) = $A_n - A_a = 2990,5$ mm²
(12%)

AEROGEL – Layout_B: nesting_B

nil volentibus arduum

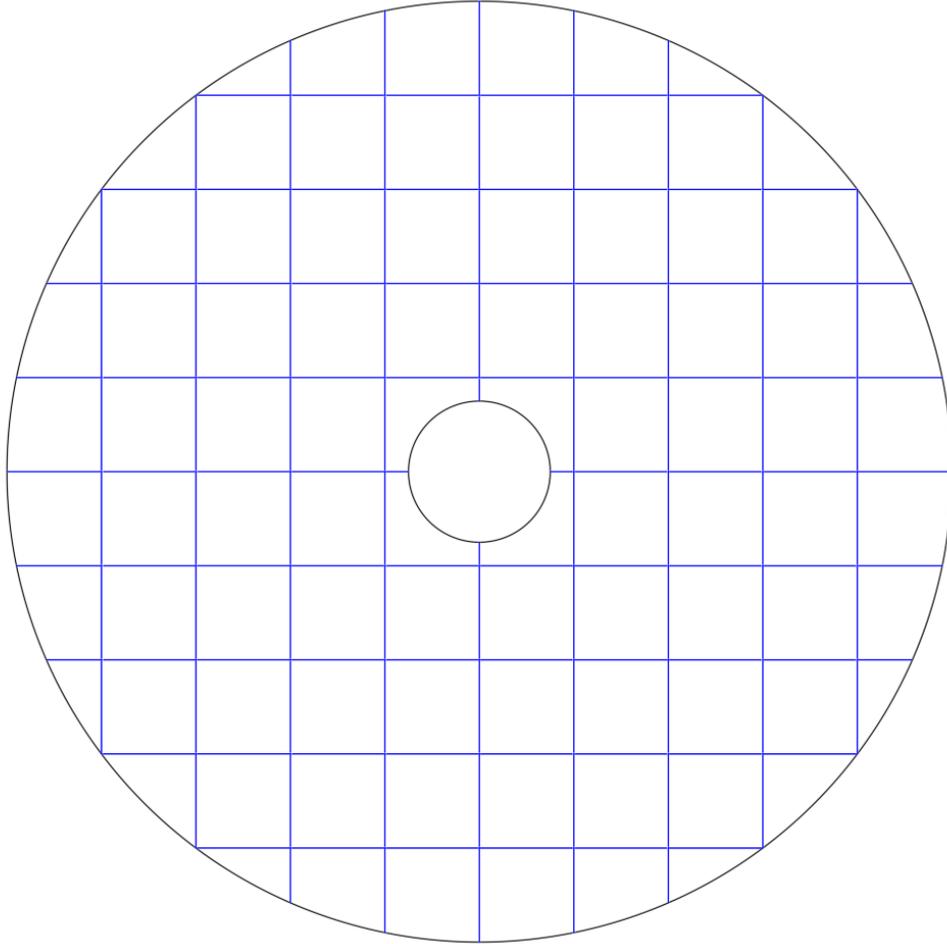
84 tiles (one layer)
 $A_{\text{tile}} = 324 \text{ cm}^2$
 $A_{\text{tot,tiles}} = 27216 \text{ cm}^2$



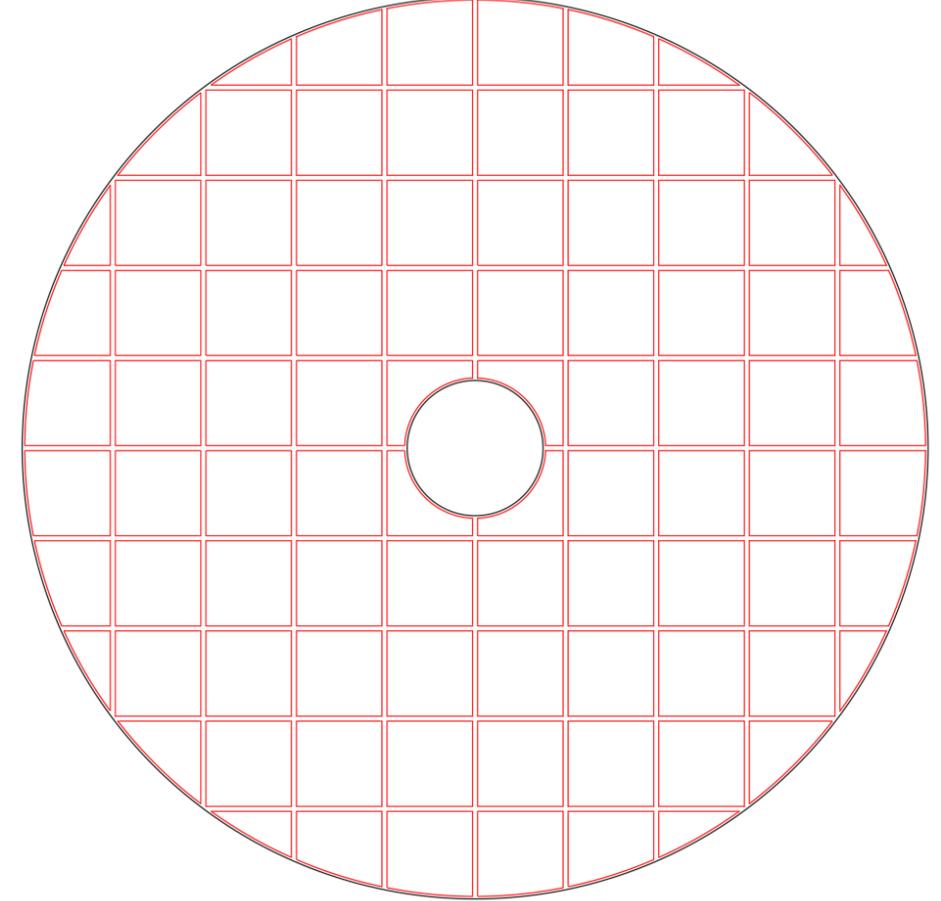
$A_{\text{waste}} = 1868 \text{ cm}^2$
(6,8 %)

AEROGEL – Layout_B: Active Area and Dead Space

nil volentibus arduum



Nominal Active Area (A_n) = 24874 cm²



Active Area (A_a) = 21368 cm²
Dead Active Area (A_{da}) = $A_n - A_a = 3506$ cm²
(14%)

AEROGEL – Layout_C: nesting_C

nil volentibus arduum

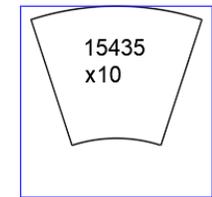
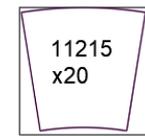
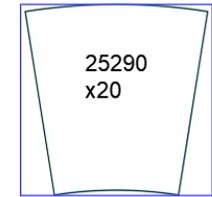
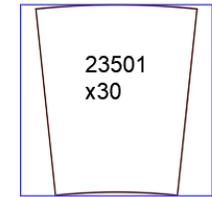
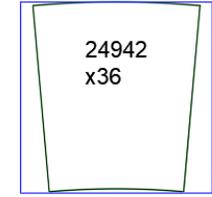
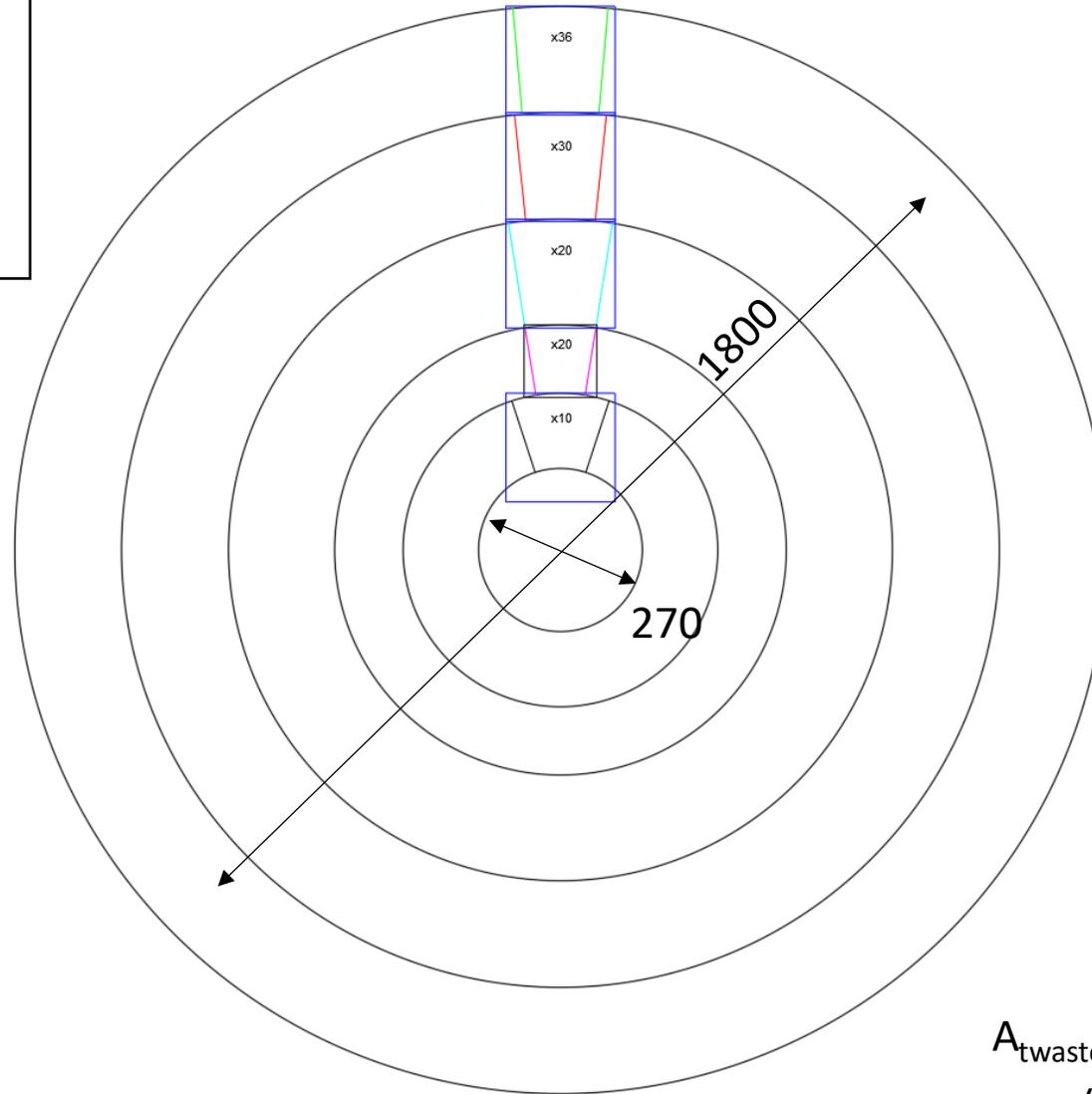
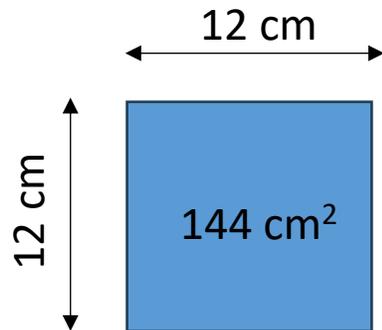
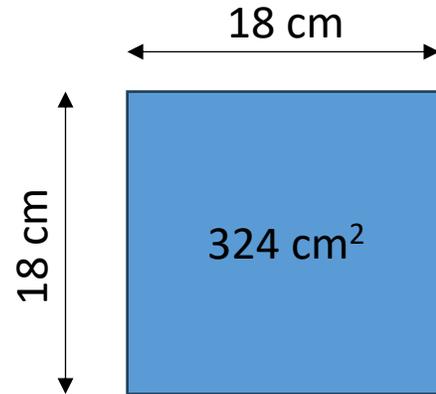
needs

116 tiles (one layer)

$$A_{\text{tile}} = 18\text{cm} \times 18\text{cm} = 324 \text{ cm}^2$$

$$A_{\text{tile}} = 12\text{cm} \times 12\text{cm} = 144 \text{ cm}^2$$

$$A_{\text{tot,tiles}} = 33984 \text{ cm}^2$$

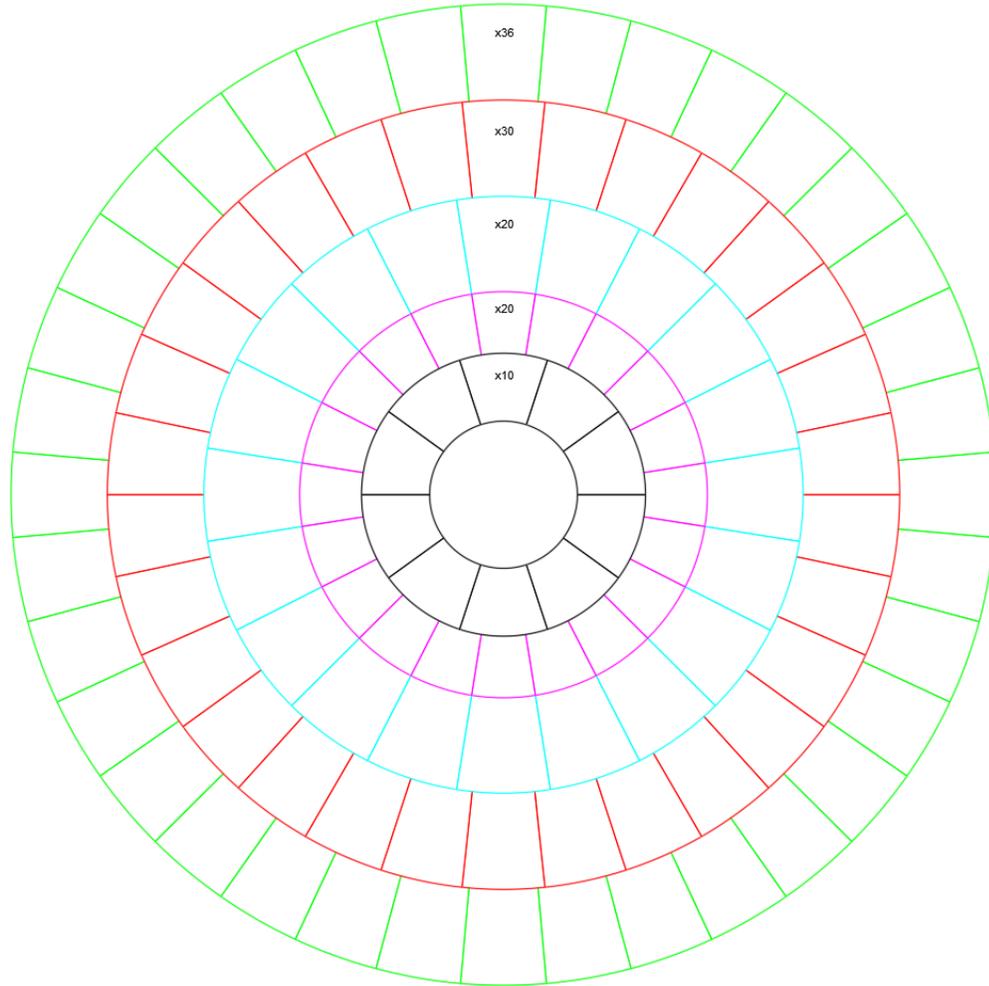


$$A_{\text{twaste}} = 9112 \text{ cm}^2$$

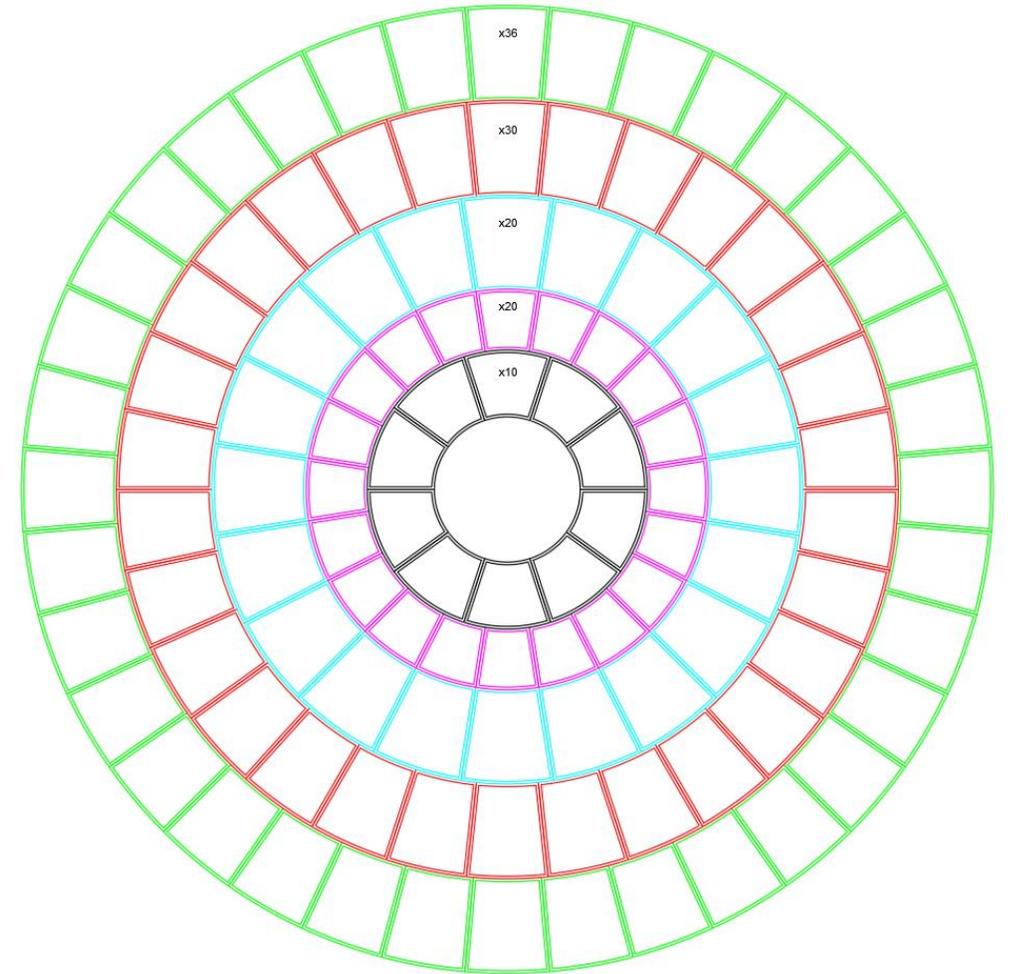
(26,8 %)

AEROGEL – Layout_C: Active Area and Dead Space

nil volentibus arduum



Nominal Active Area (A_n) = 24874 cm²



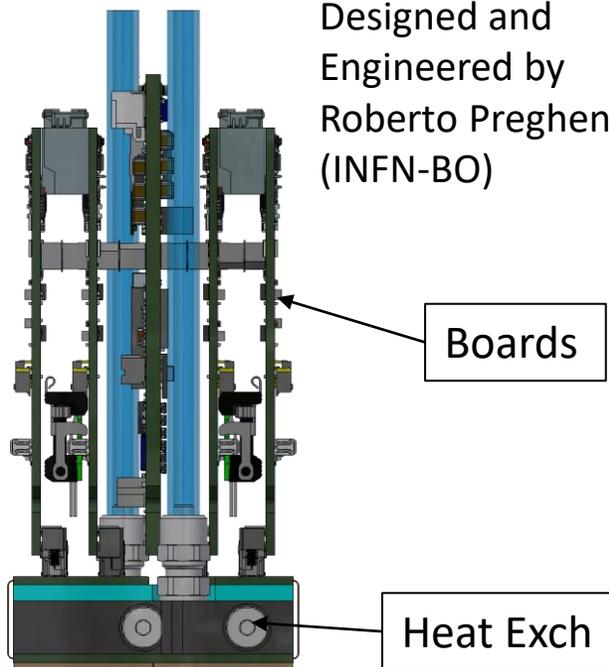
Active Area (A_a) = 21605 cm²
Dead Active Area (A_{da}) = $A_n - A_a = 3269$ cm²
(13,1%)

PCB COOLING STUDIES

PDU and boards: cooling and thermal power

Designed and
Engineered by
Roberto Preghenella
(INFN-BO)

dRICH PDU = 1200
Detector Box PDU = 211
dRICH Detector Boxes = 6



SiPM

$P_{\text{PDU}} = 5 \text{ W}$ (cooling power to be supplied to each PDU unit)

$T_{\text{SiPM}} = -40^\circ\text{C}$ (SiPM temperature)

$P_{\text{DT}} = 211 \times 5 \text{ W} = 1055 \text{ W}$ (cooling power to be supplied to each detector box)

$P_{\text{dRICH}} = 6 \times 1055 \text{ W} = 6330 \text{ W}$ (cooling power to be supplied to dRICH)

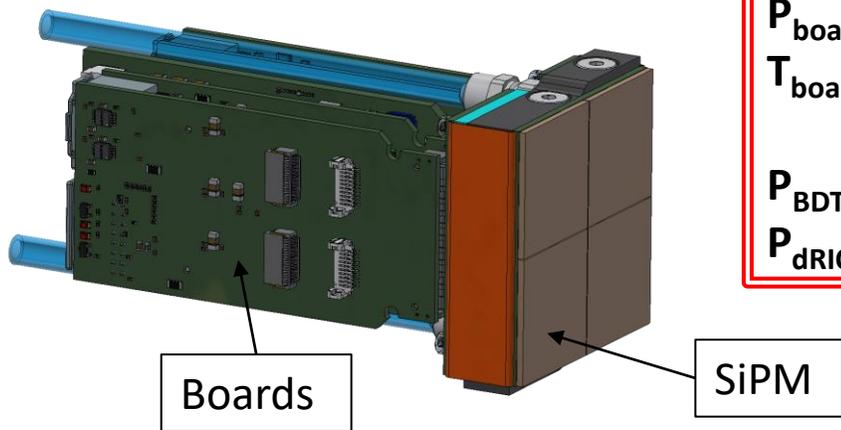
Electronic Boards

$P_{\text{boards}} = 11 \text{ W}$ (thermal power generated by each PDU unit)

$T_{\text{boards}} = 30^\circ\text{C}$ (maximum admissible boards temperature)

$P_{\text{BDT}} = 211 \times 11 \text{ W} = 2321 \text{ W}$ (thermal power generated by each detector box)

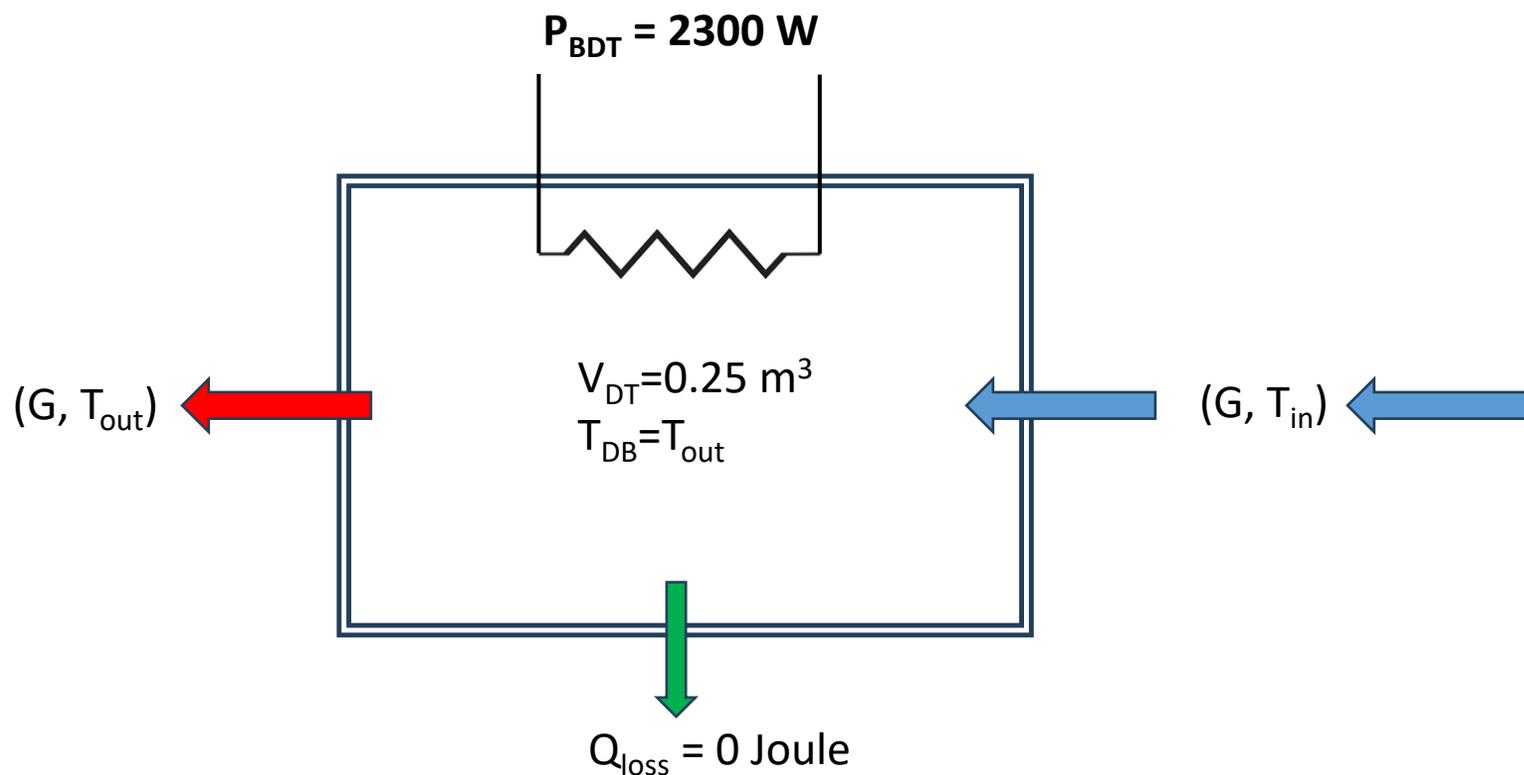
$P_{\text{dRICH}} = 6 \times 2321 \text{ W} = 13926 \text{ W}$ (thermal power generated by dRICH)



Detector Box: board's air cooling

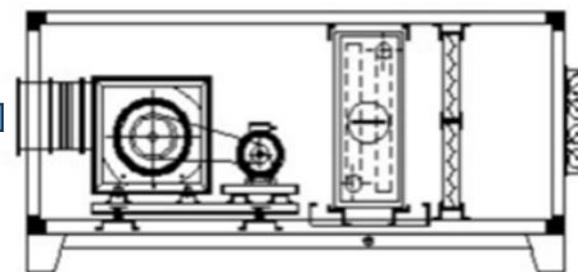
Hypothesis:

- Detector box perfectly insulated
- Thermal interaction with the SiPM cooling system not considered



Disadvantages:

- Risk of condensation
- High noise
- High vibrations
- Big size of ducts

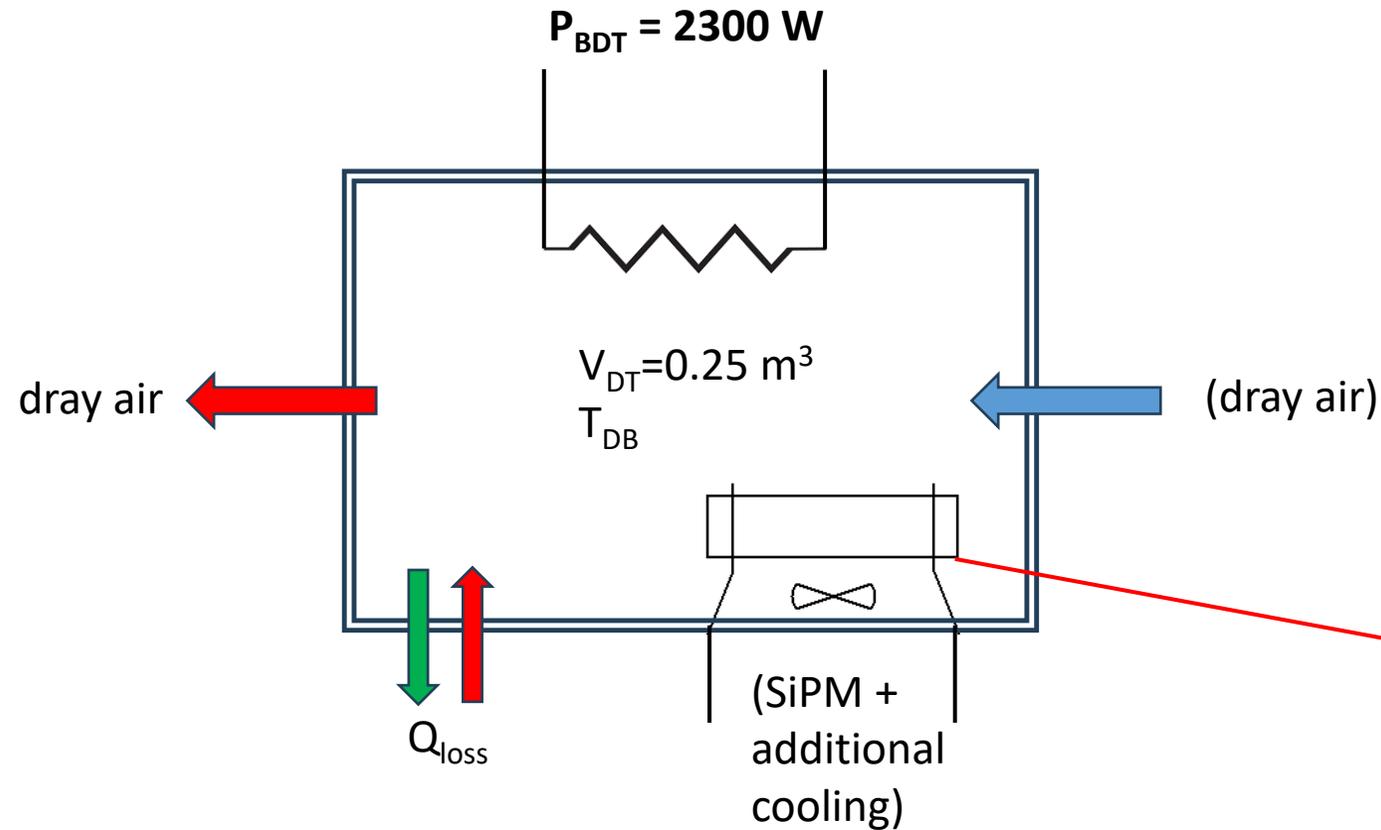


- External air intake
- Bag filter
- Cold coil
- Fan

Detector Box: FEE cooling

Hypothesis:

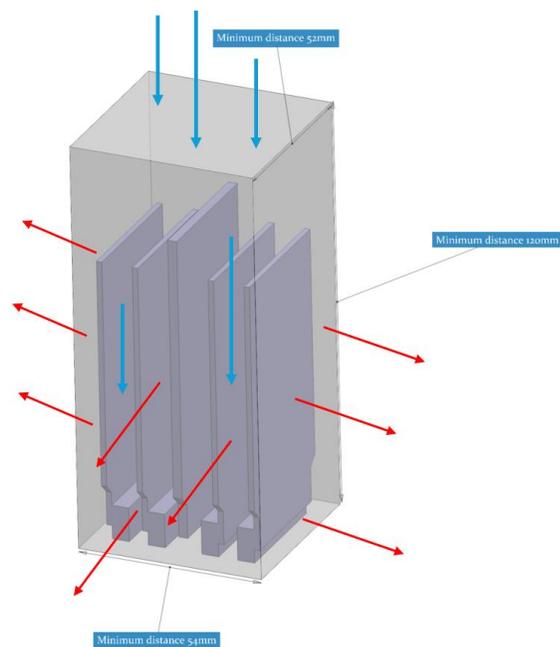
- Detector box no perfectly insulated
- Thermal interaction with the SiPM cooling system considered



Inlet/Outlet pipe diameter: 15/20 mm

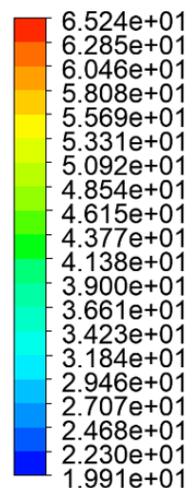


Singola PDU, aria dall'alto



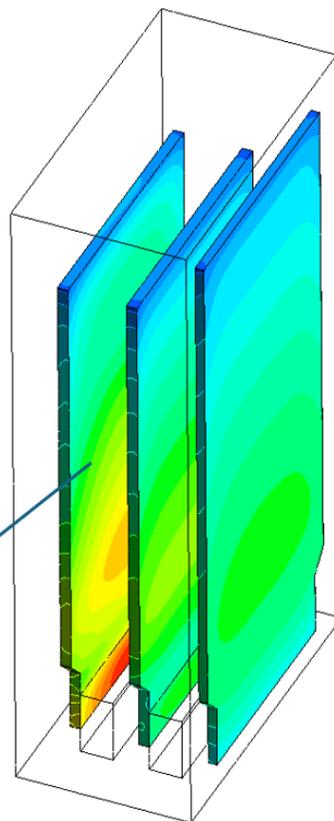
Condizioni su
sezione inlet: $v = 1 \text{ m/s}$, $T = 20^\circ \text{ C}$.

Temperature
Contour T alette

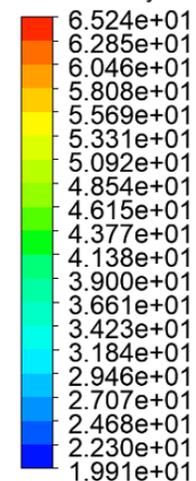


[C]

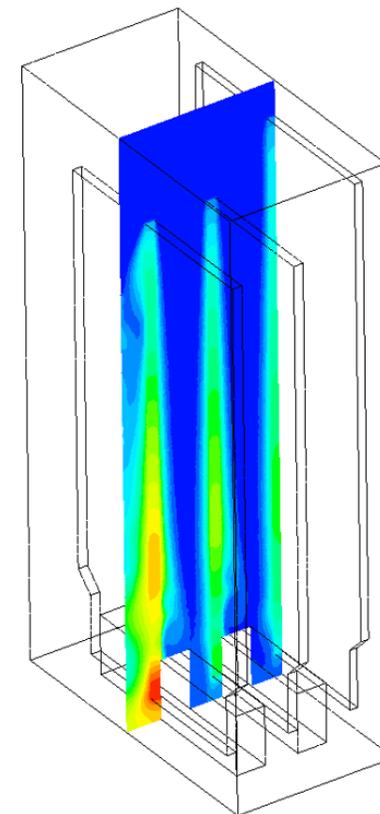
Conseguenza di ciò è che la
scheda più esterna raggiunge
alte temperature.



Temperature
Contour T zy

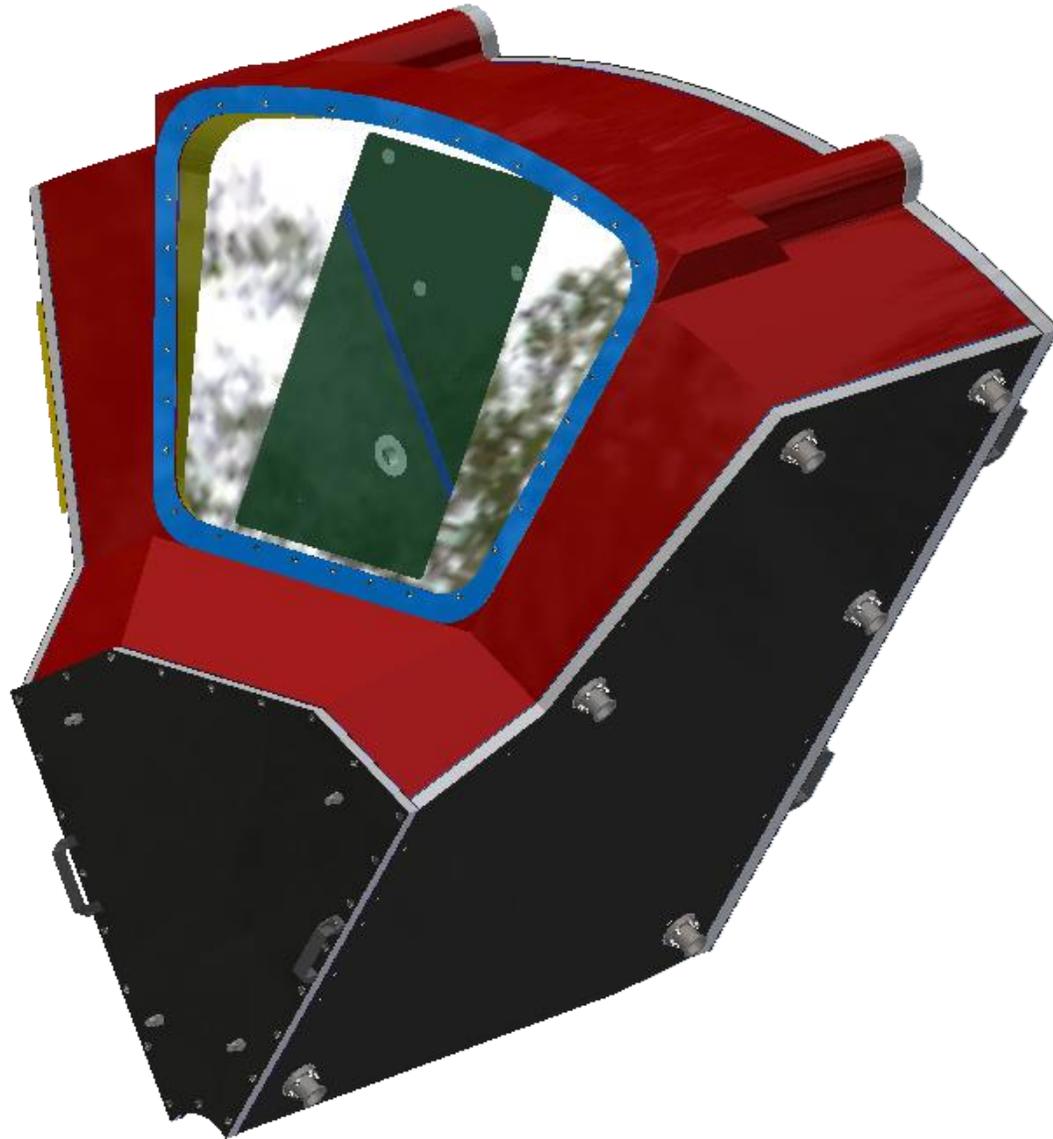


[C]



PROTOTYPE and R&D projects

dRICH: prototype



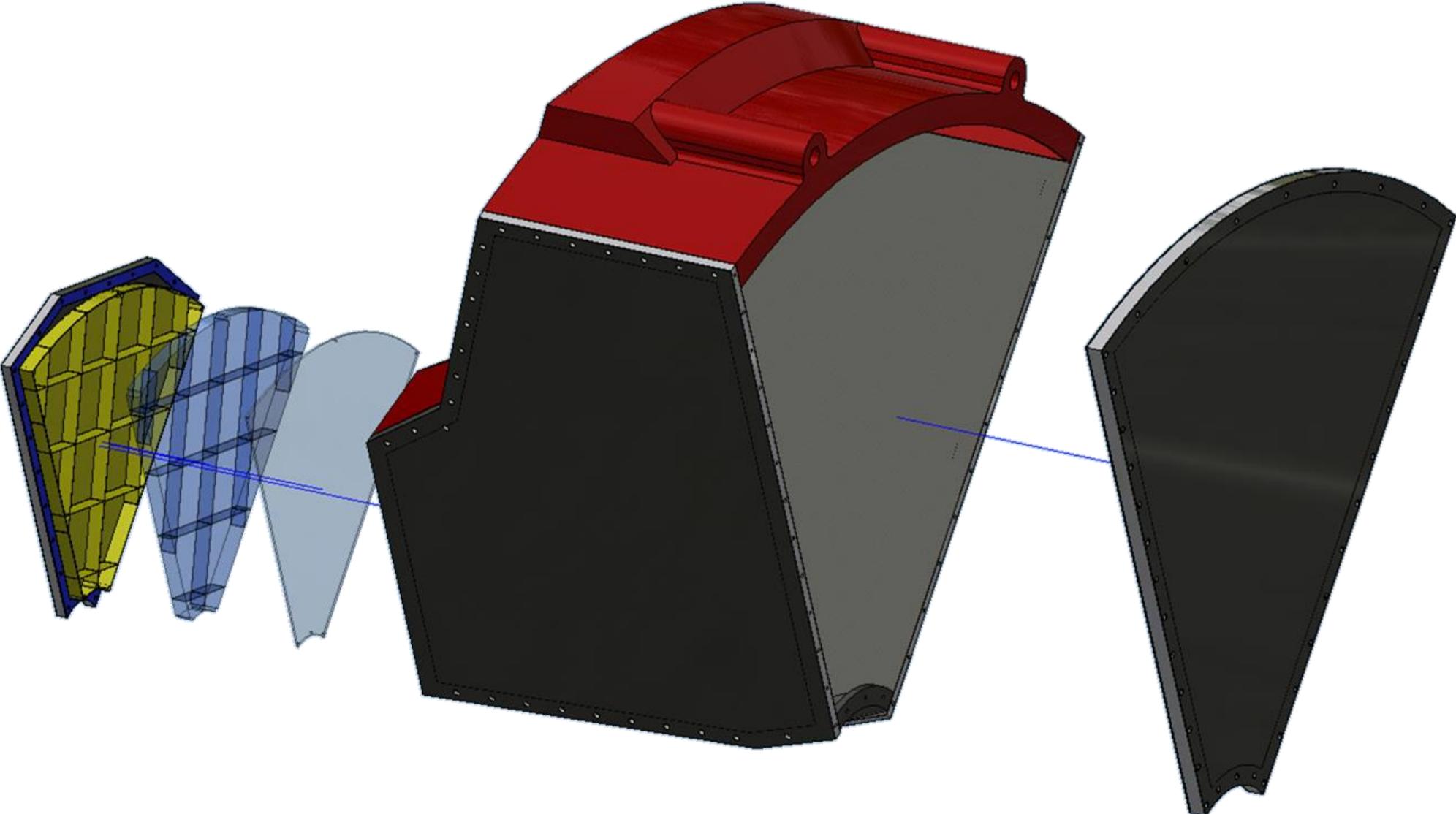
Full-scale (1:1) prototype representing one-sixth of the complete dRICH detector.

Status:

- The drawings are ready.
- The tender has been completed.
- Construction should start before the end of June 2025.

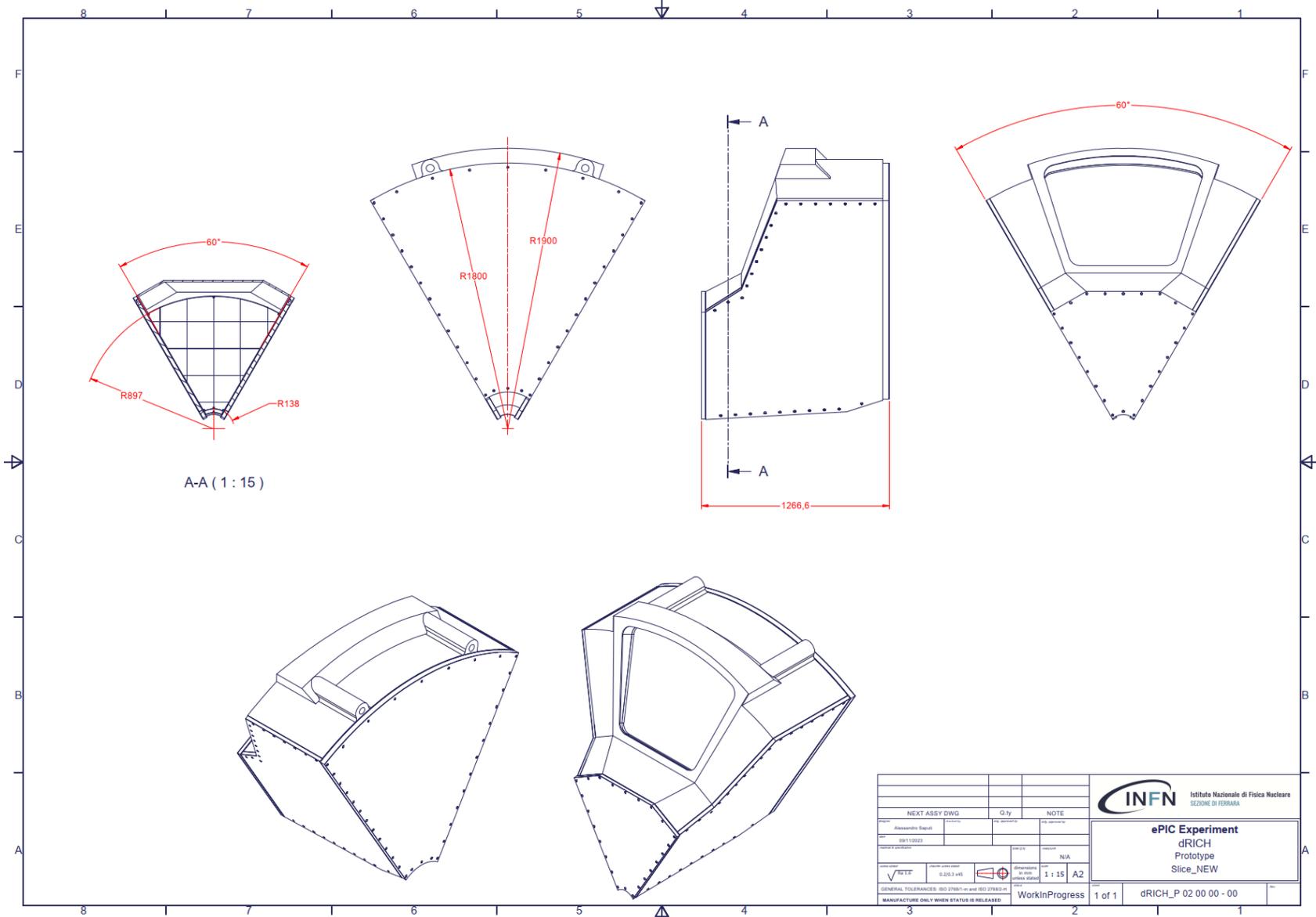
dRICH: prototype

nil volentibus arduum



dRICH: prototype

nil volentibus arduum



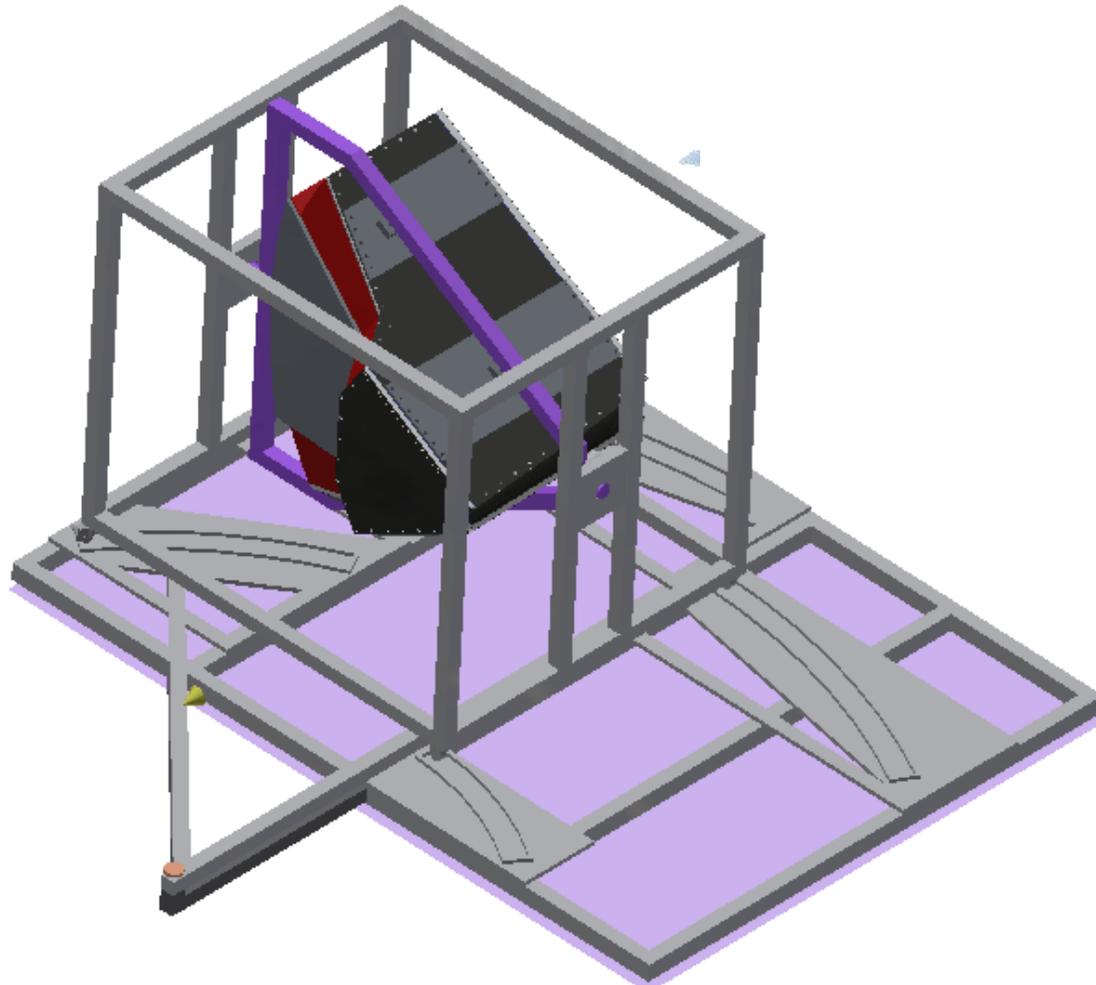
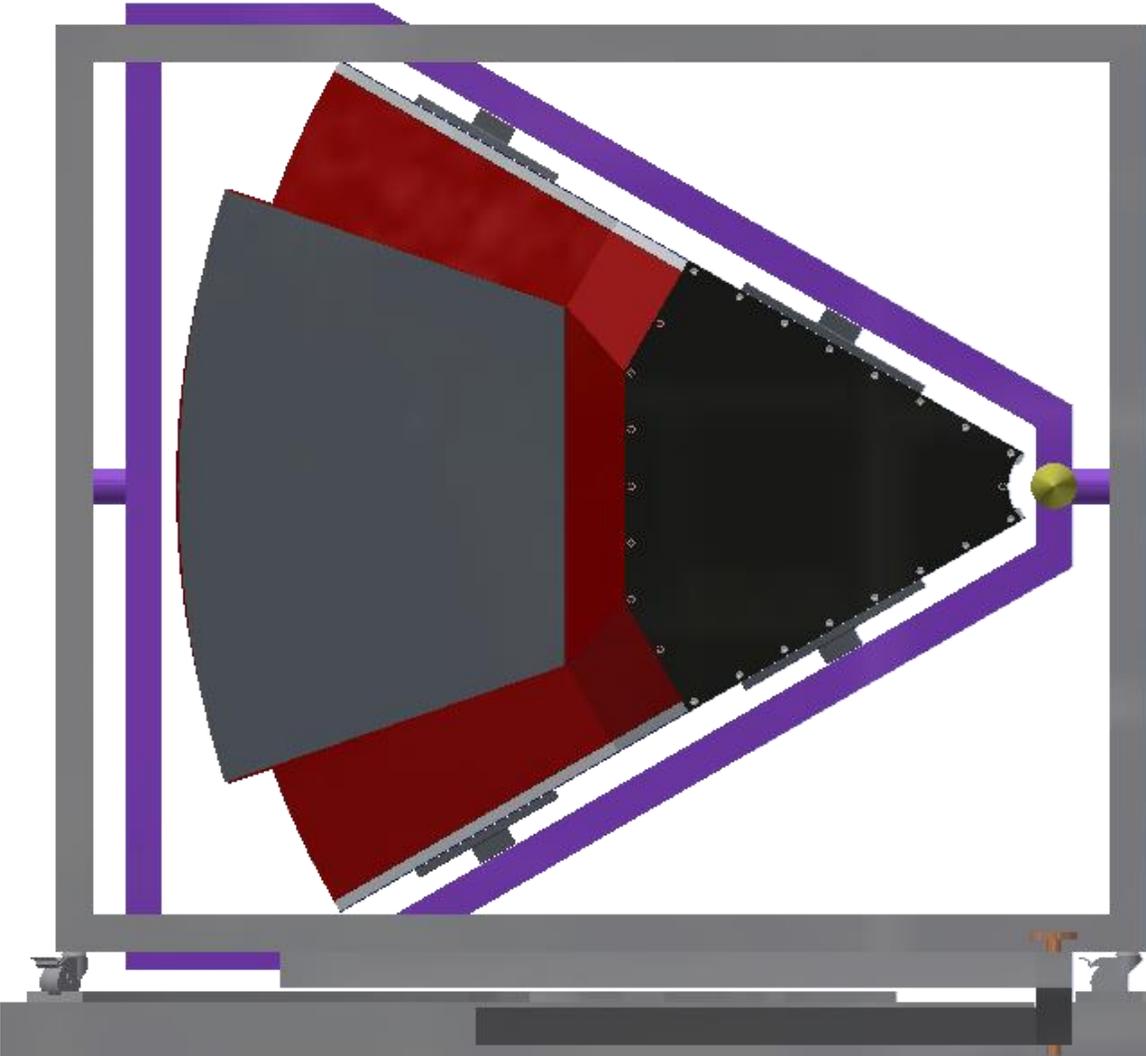
NEXT ASSY DWG		Q ty	NOTE
Alessandro Saputi			
02/11/2023			
02/11/2023			
VERIFIED	0.2/0.3 x45	1:15	A2
GENERAL TOLERANCES: ISO 2768-Ts and ISO 2768-Ms		WorkInProgress	1 of 1
MANUFACTURE ONLY WHEN STATUS IS RELEASED			dRICH_P_02 00 00 - 00



ePIC Experiment
dRICH
Prototype
Slice_NEW

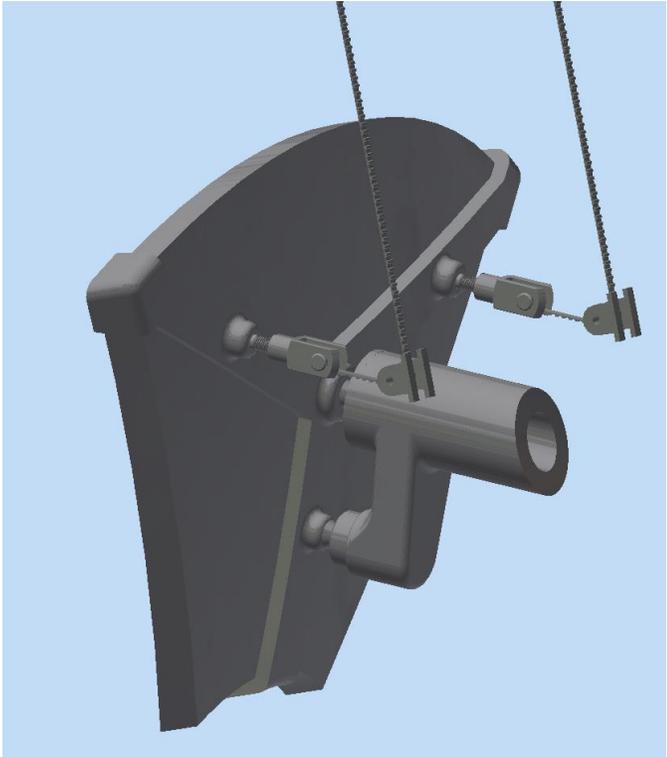
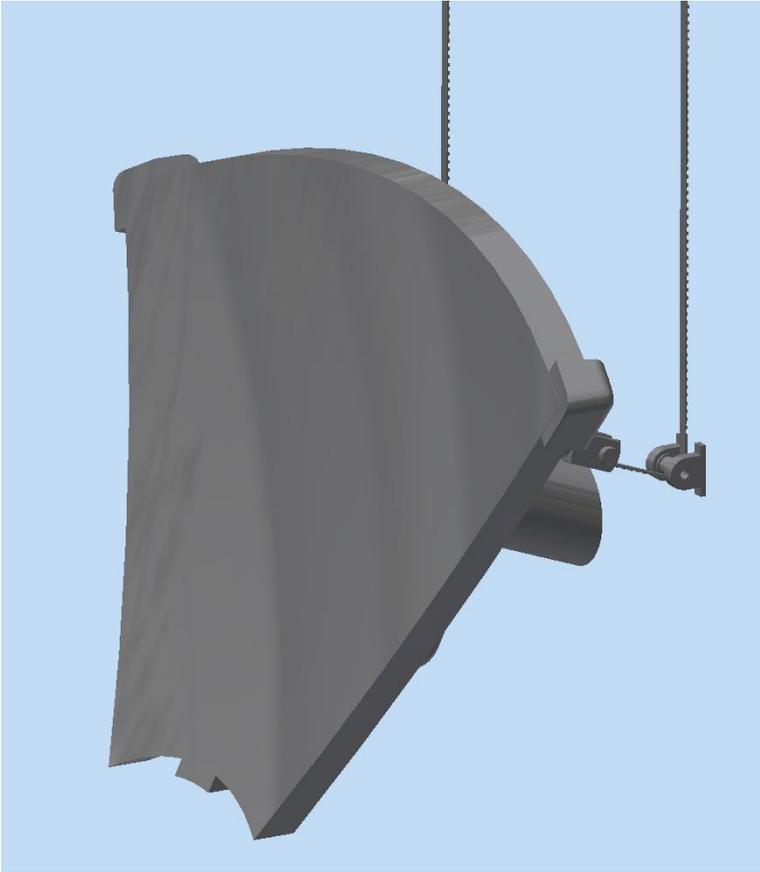
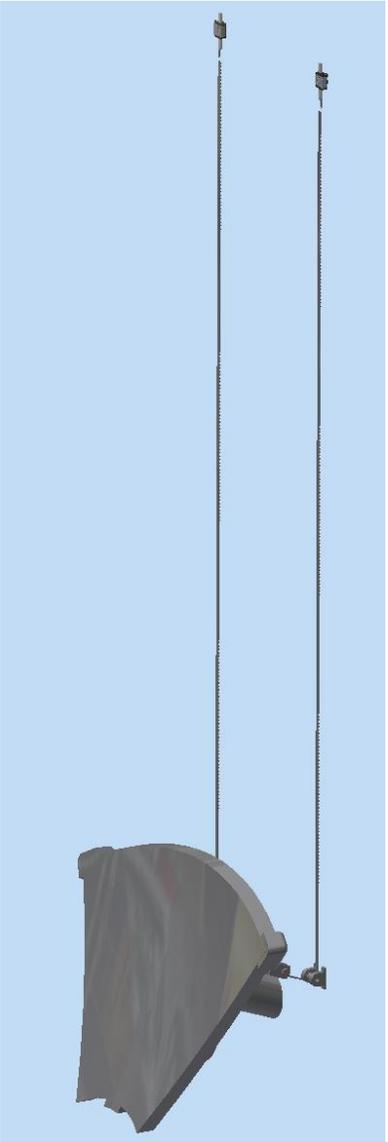
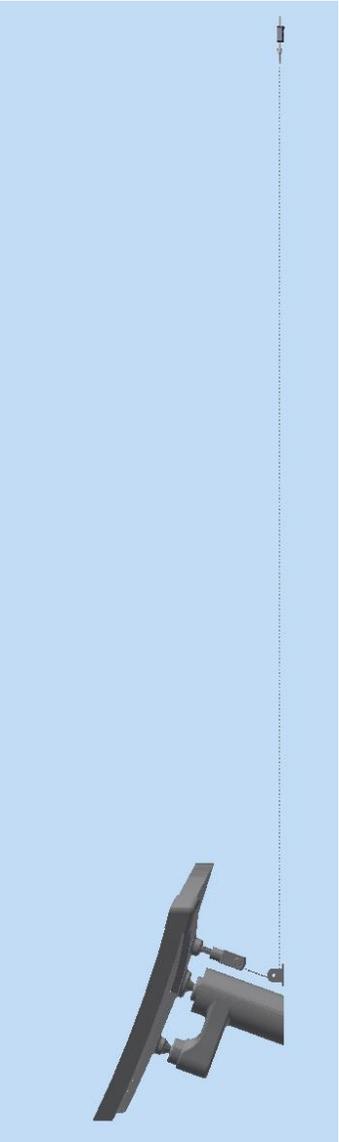
dRICH: test beam setup

nil volentibus arduum



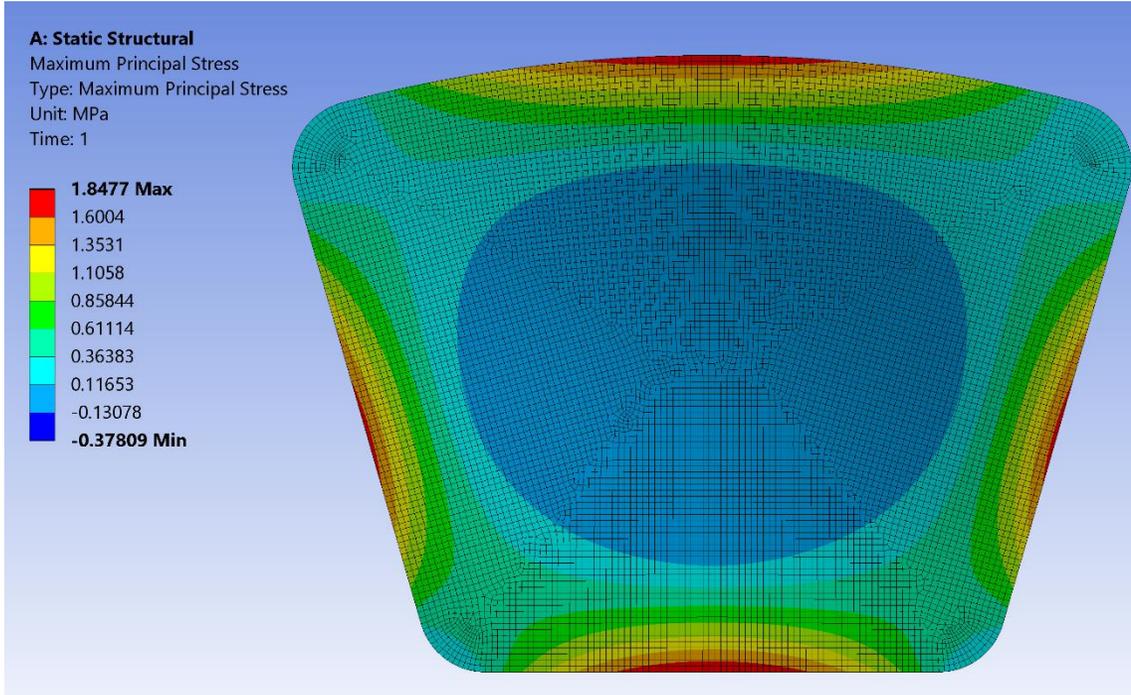
dRICH: mirror for prototype

nil volentibus arduum



Quartz Window: FEA

Maximum Principal Stress (S1)

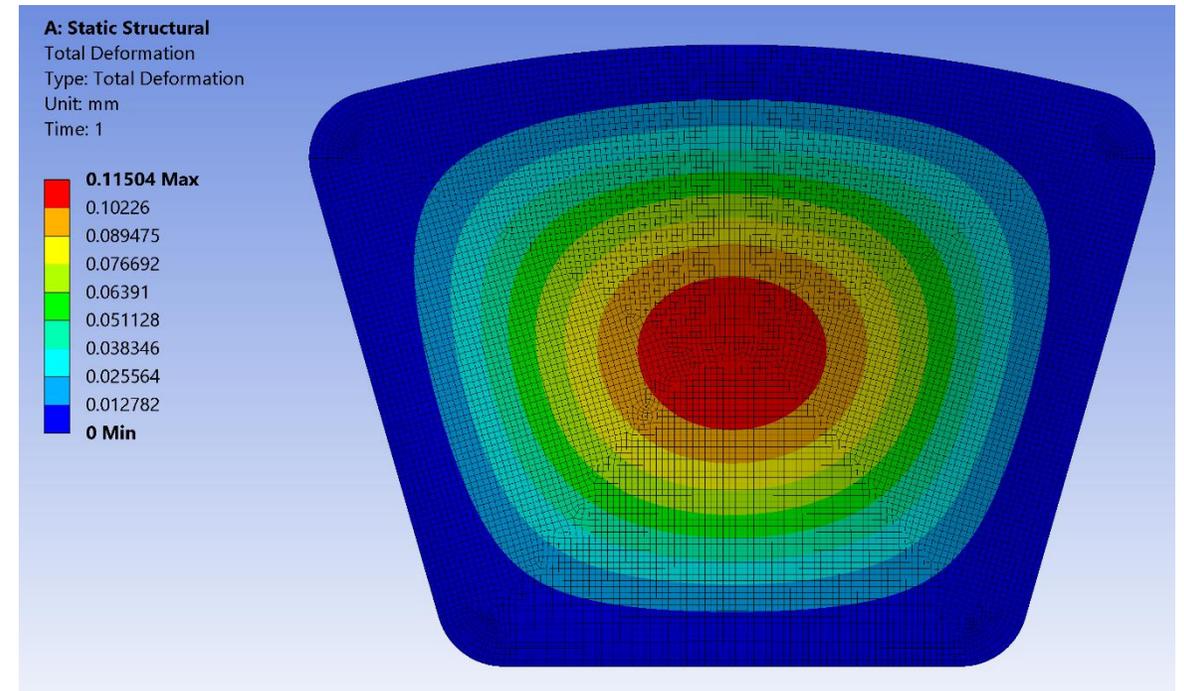


- Thickness: $t_1=8$ mm;
- Uniformly distributed (absolute) pressure over the entire surface: 0,0005 MPa (5 mbar)
- Constrains: Fixed along the edge surface

- Maximum Principal Stress $S1=1,9$ MPa;
- Maximum Deformation along Z Axis = -0,11 mm
- Minimum Calculated Safety Factor $SF_c = 15$

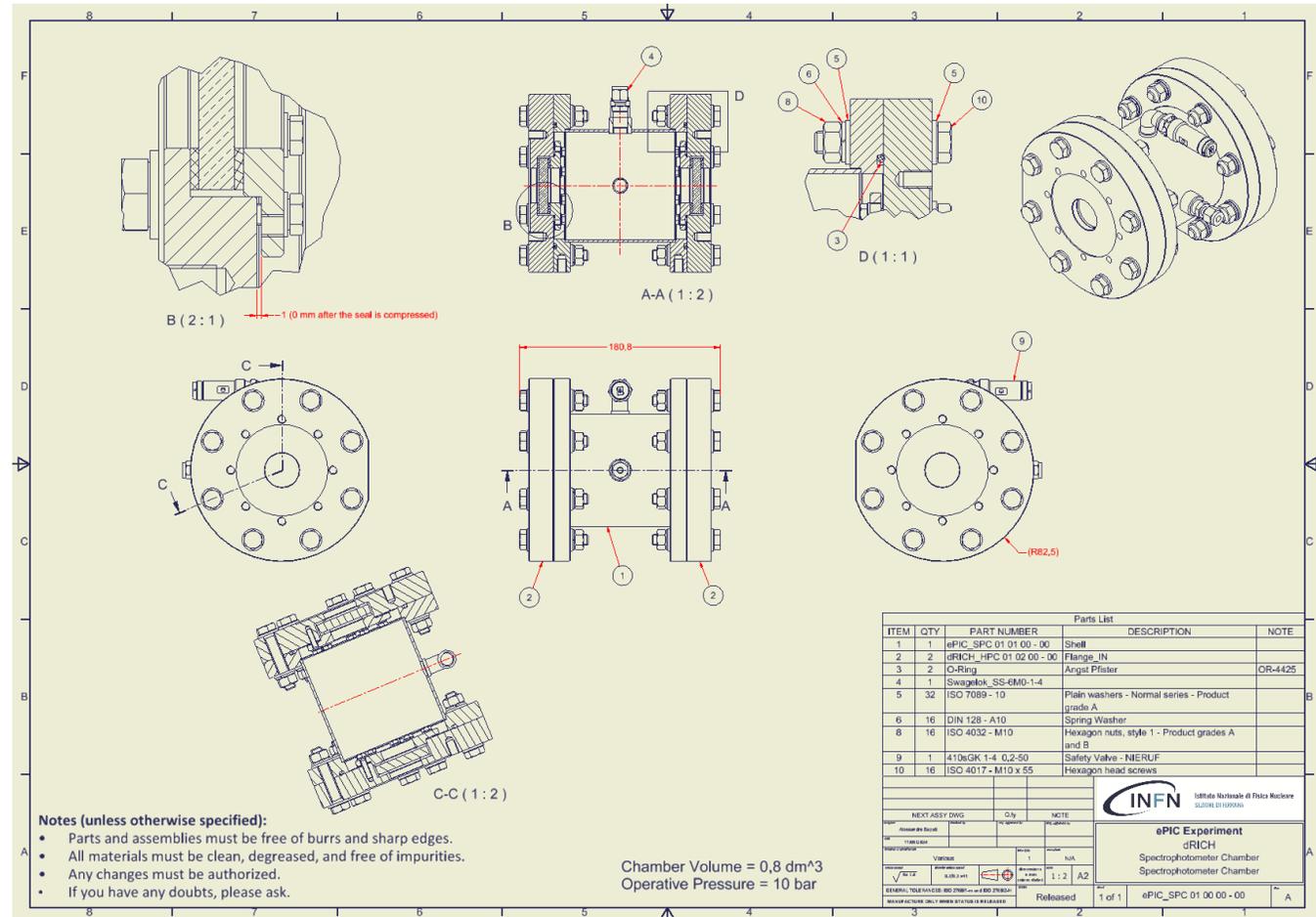
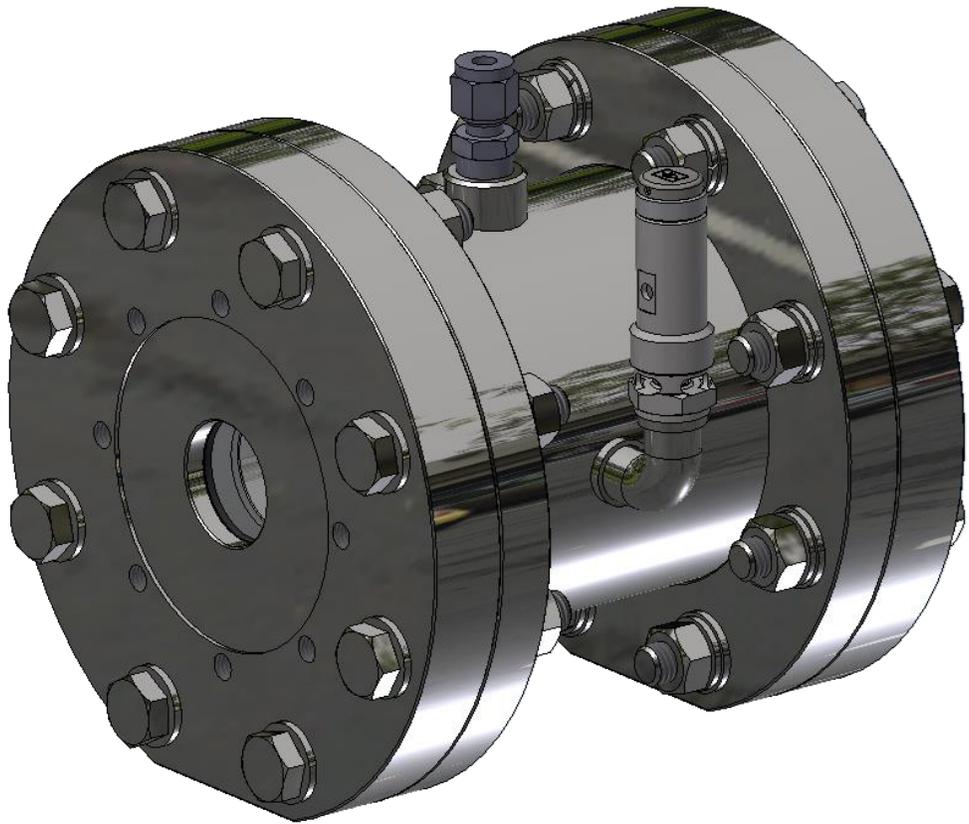
$SF_c > 7$ → checked

Deformation along Z Axis



Spectrophotometer Chamber: target R&D

Design Pressure: 1,43 Mpa
Operative Pressure: 1 MPa

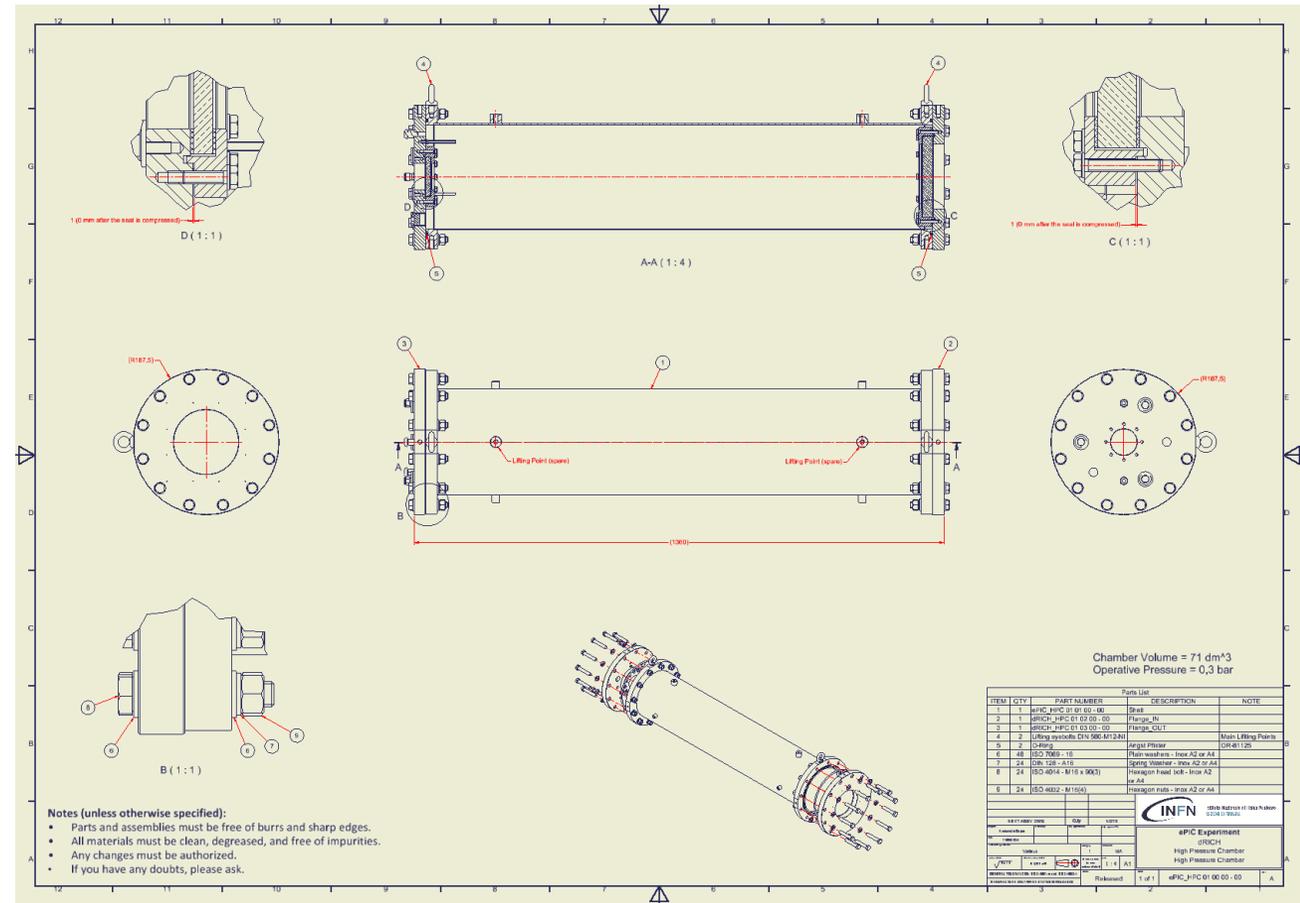


This chamber has been designed to study:

- Gas permeability of carbon fiber
- Gas transparency in the visible spectrum
- Gas-aerogel interactions

High Pressure Chamber: generic R&D

Design Pressure: 0,5 Mpa
Operative Pressure: 0,3 MPa

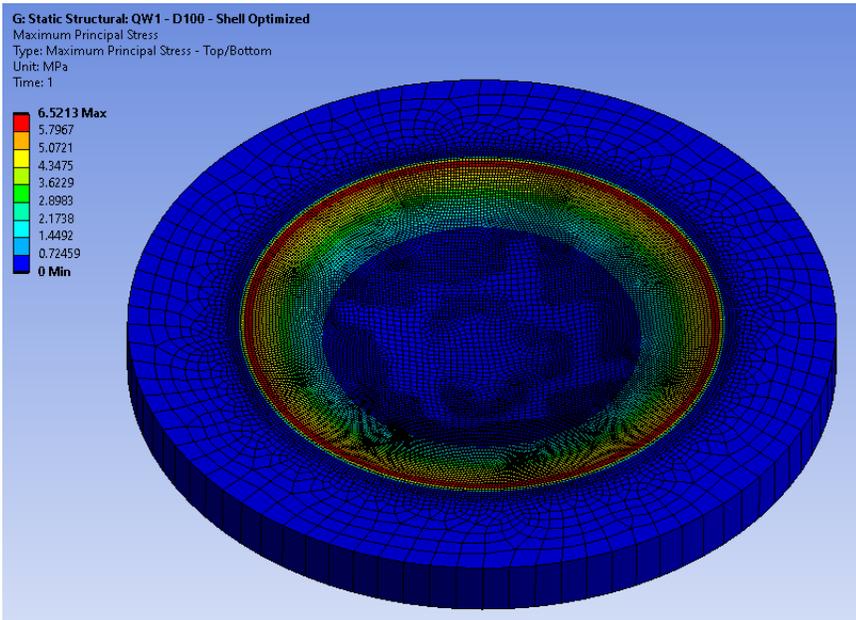


This chamber has been designed to study risk mitigation strategies for greenhouse gases.

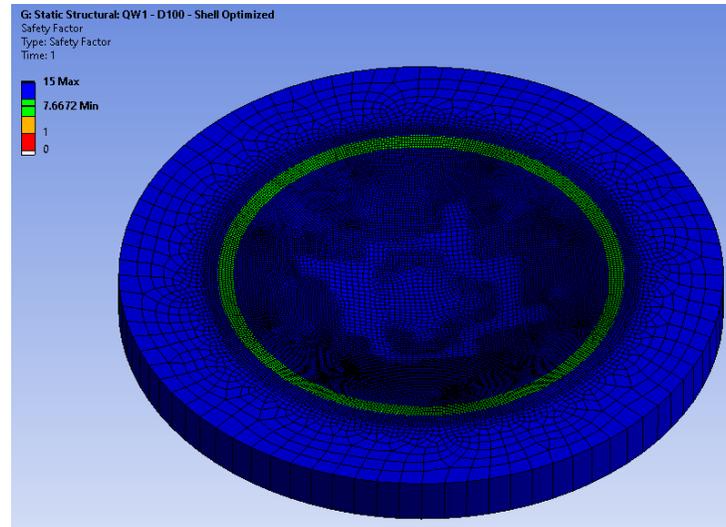
Quartz Window: stress&strain calculation - $t_1=8$ mm

- Thickness: $t_1=8$ mm;
- External diameter: $D_1=100$ mm
- Uniformly distributed (absolute) pressure over the entire surface ($d_1=68$ mm): 0,5 MPa
- Constrains: Fixed along the edge surface

Maximum Principal Stress (S1)



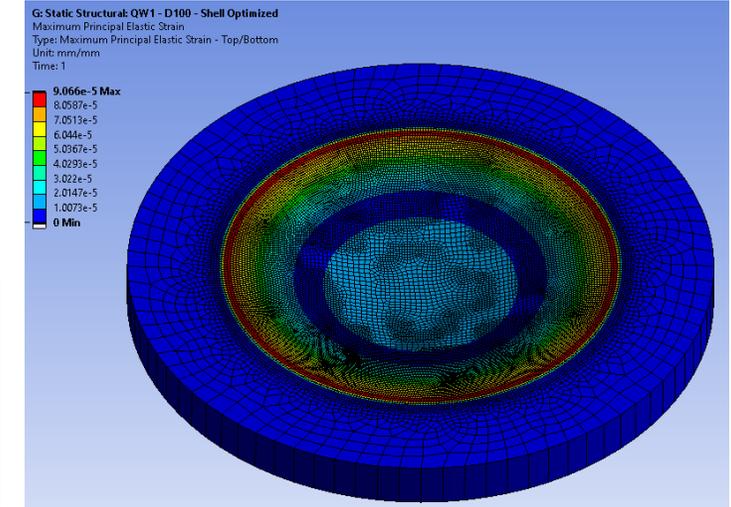
Safety Factor



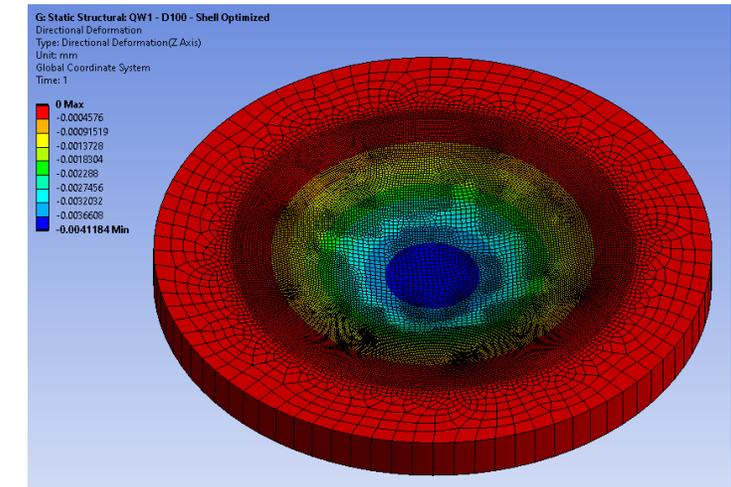
- Maximum Principal Stress $S1=6,5$ MPa;
- Maximum Principal Strain = 0,00009
- Maximum Deformation along Z Axis = -0,004 mm
- Minimum Calculated Safety Factor $SF_c = 7,6$

$SF_c > 7$ → checked

Maximum Principal Strain



Deformation along Z Axis



Conclusions and NEXT Steps

- **Consolidation of the dRICH mechanical design and cooling design:** refining and finalizing the mechanical design of the dRICH.....
- **Integration study of dRICH into the ePIC Apparatus:** fixing system, service integration.....
- **Study of the Extraction and Insertion System (Moving System):** design and optimization of the moving system used for the extraction and insertion of the dRICH detector within the ePIC apparatus
- **Structural Study of dRICH:** A detailed structural analysis of the dRICH detector will be conducted using Finite Element Method (FEM) simulations.

Thank You!!

