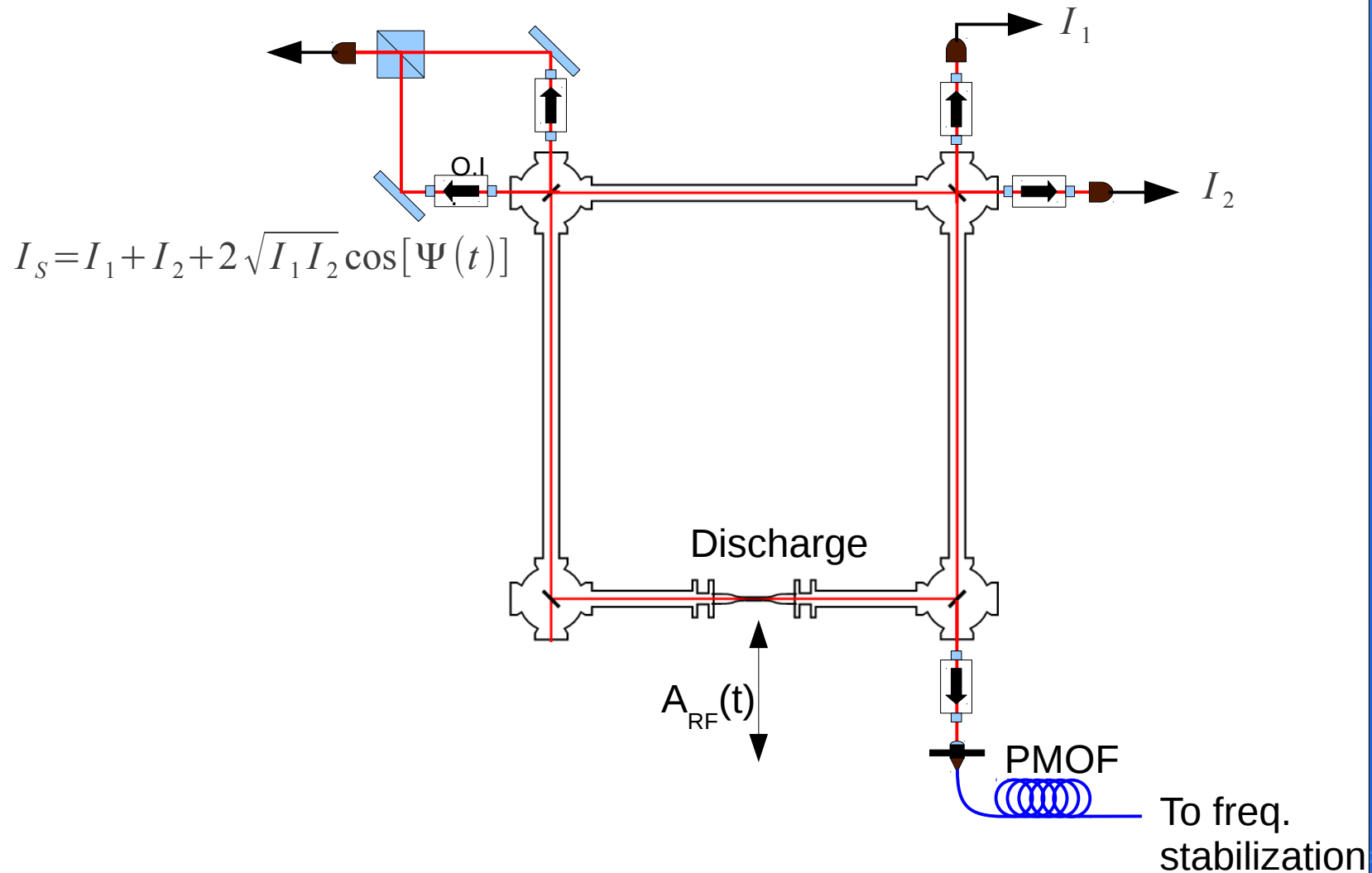
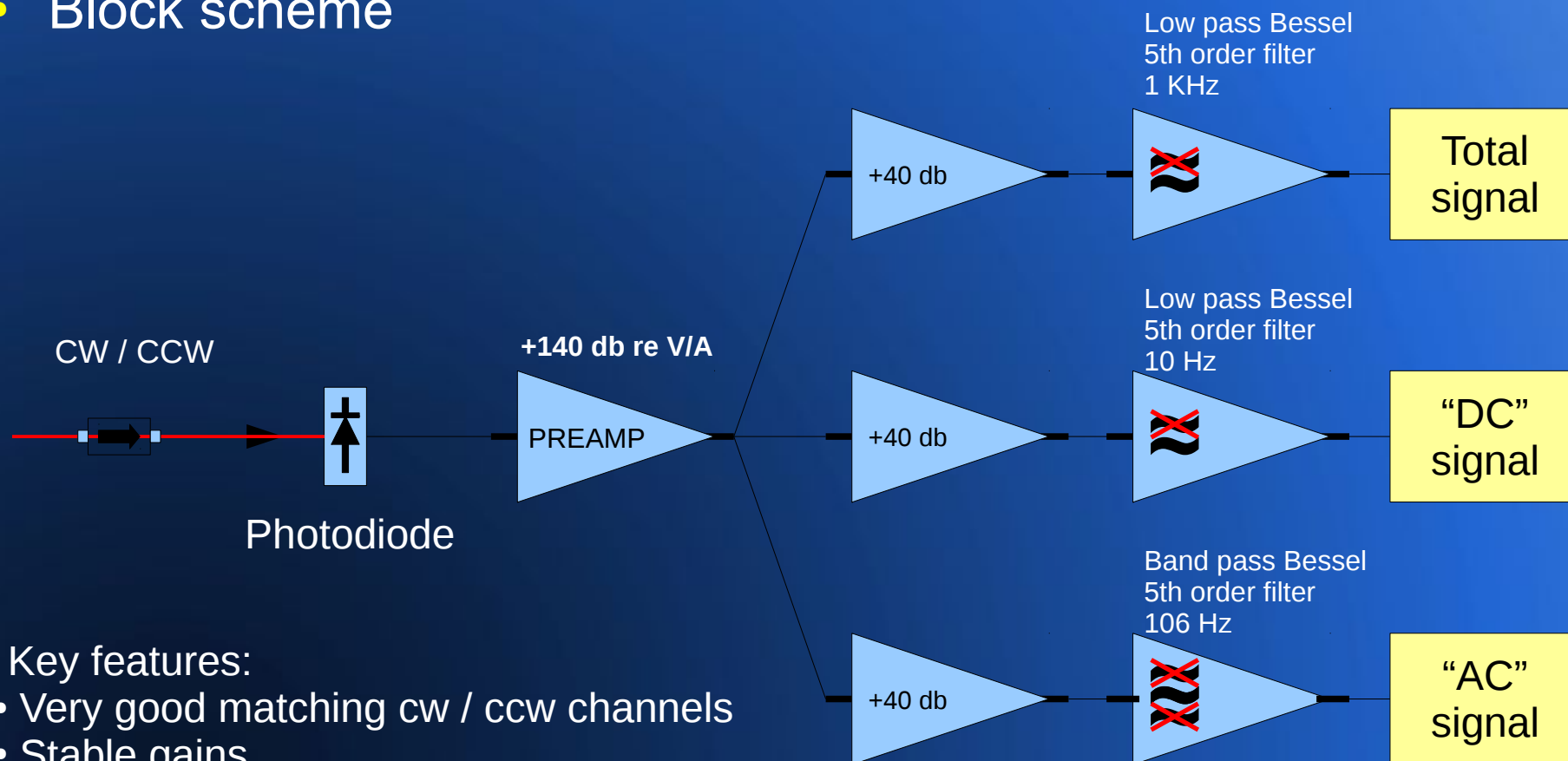


Gyrolaser Optical design: STD op.



3-ways analog cw/ccw signal processing

- Block scheme

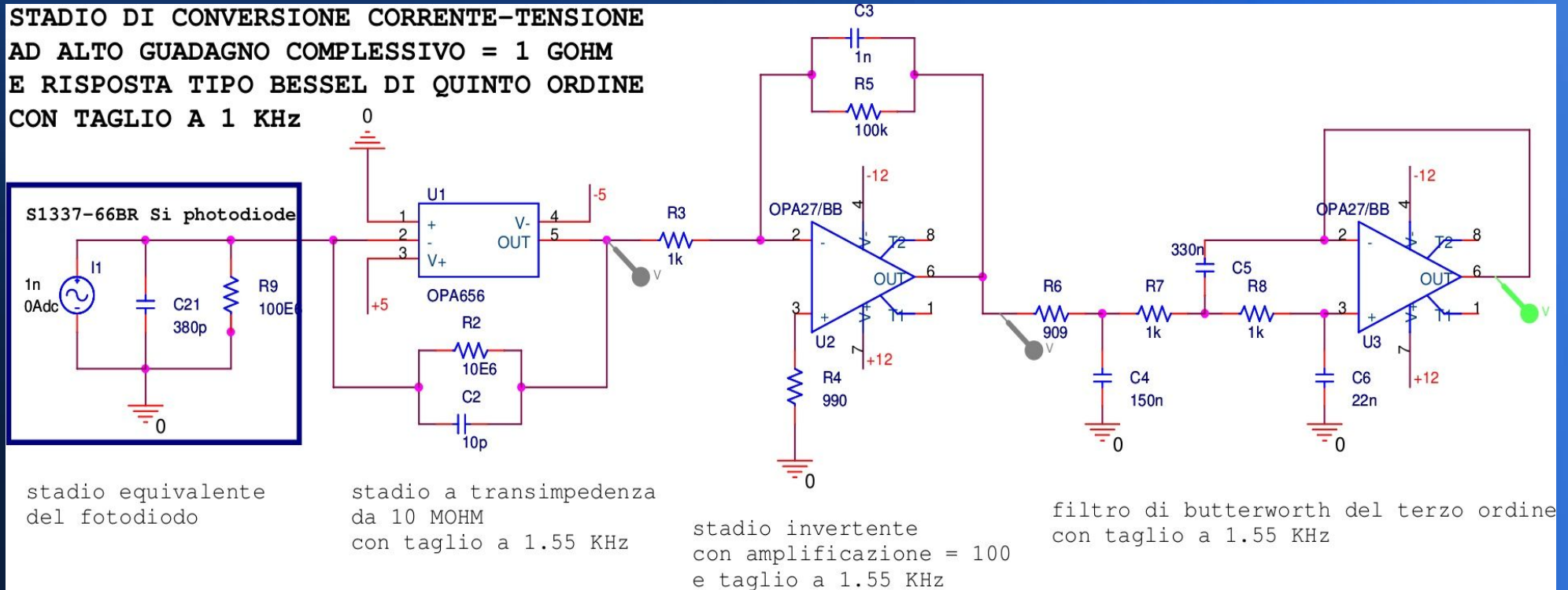


Key features:

- Very good matching cw / ccw channels
- Stable gains
- Noise performances over commercial amplifiers

3-ways analog cw/ccw signal processing

- Electrical scheme of the upper branch



3-ways analog cw/ccw signal processing

- Noise performances vs commercial preamp with equivalent gain

Red line: commercial amp preamp
(femto LCA-4k-1G)
Blue line: h.m. module (iccw)

Further improvements on noise performances of our modules are still (hopefully) possibles

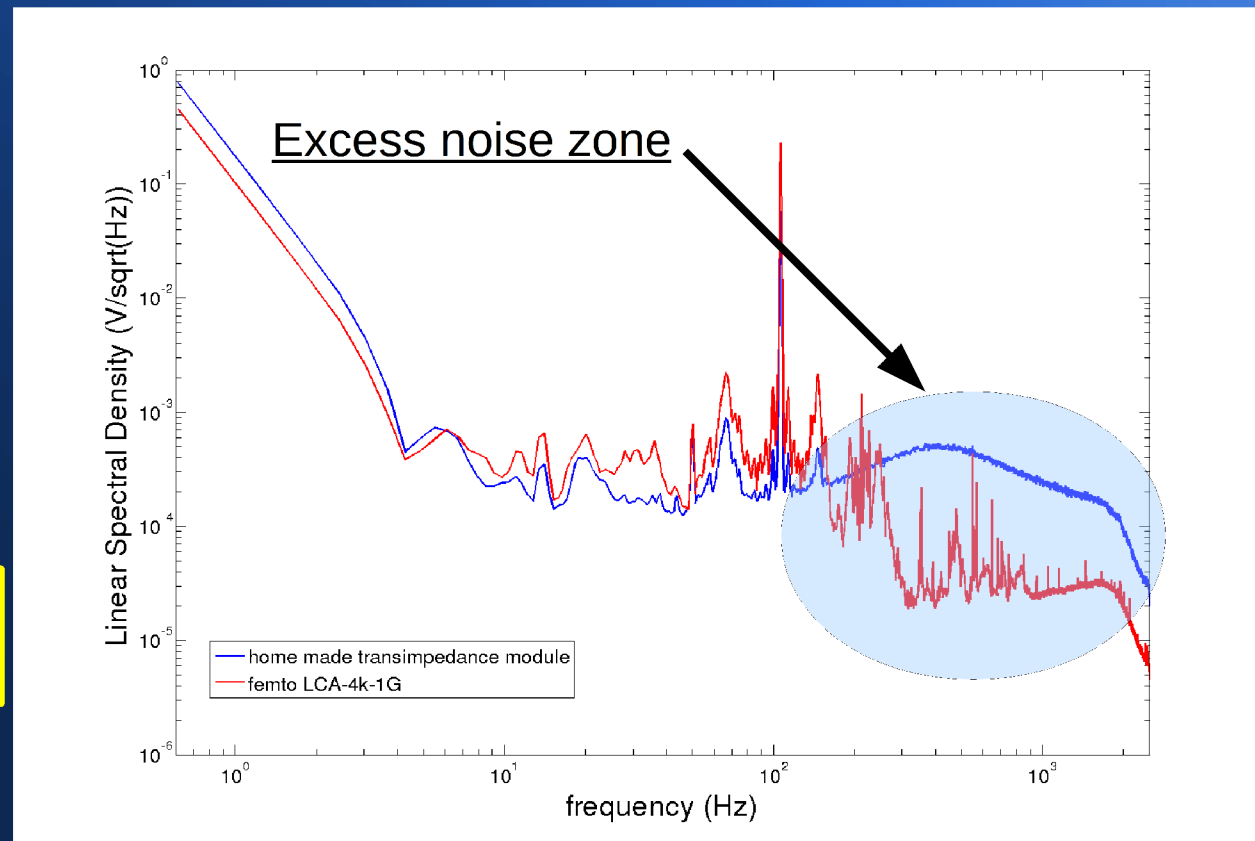
Simulated noise



An unexpected parasitic capacitance is responsible for the noise peaking



Measured noise



3-ways analog cw/ccw signal processing

- An explanation from circuit theory

$C_s = 10 \text{ pF}$
 $C_d = 380 \text{ pF}$

$C_d = 10 \text{ nF} !!$

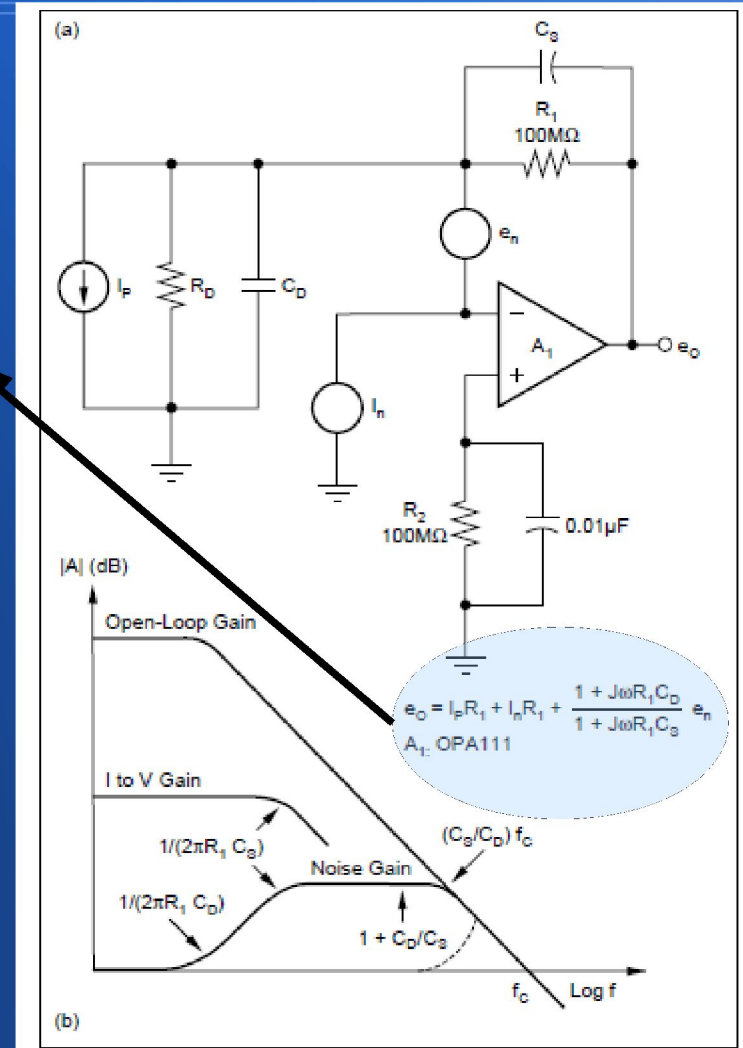
$$e_o = I_p R_1 + I_n R_1 + \frac{1 + j\omega R_1 C_D}{1 + j\omega R_1 C_S} e_n$$

Possible cause: parasitic from breadboard
 We can try with a PCB board

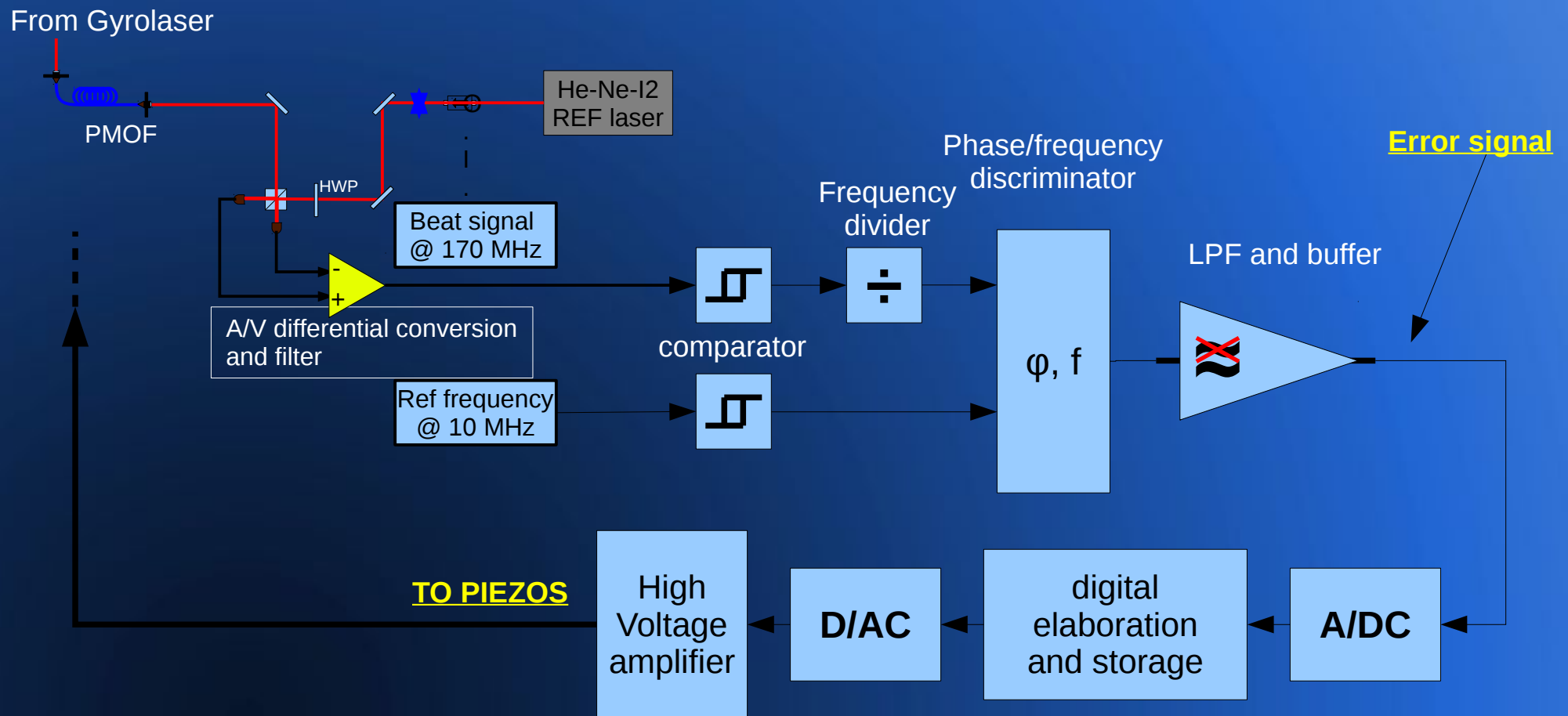
Simulated noise

An unexpected parasitic capacitance is responsible for the noise peaking

Measured noise



Perimeter lock: PLL phase and frequency lock



Perimeter lock: some considerations on SNR / 1

- “Best case”: FEMTO- pre amplifier:
let $100 \text{ uW} = \text{power of stabilized laser} = P_s$
 $1 \text{ nW} = \text{power of gyrolaser} = P_g$ ($P > 1 \text{ nW} \rightarrow \text{multi mode}$)
power of beat = $2 \cdot \sqrt{P_s \cdot P_g}$ (peak value) = 600 nW peak
- After the P.D. and the pre-amplification we get $1,1 \text{ mVrms}$ of signal
- Preamp data sheet:
 - equivalent input noise current @ $100 \text{ MHz} = 21 \text{ pA}/\sqrt{\text{Hz}}$
 - Standard deviation of output noise = 300 uV rms

SNR= 10 dB

SNR very close to 0 dB even in “ideal” conditions

Perimeter lock: some considerations on SNR / 2

- A significantly lower SNR can be expected:
 - *Many others sources of noise than the input equivalent noise current:*
 - Voltage input noise
 - Transimpedance thermal noise
 - Op-amp voltage and current noise noise
 - Shot noise
 - *The signal is lower*
 - Light losses
 - Non-ideal light coupling with the photodiode
 - Non-ideal polarization of incident beams

Perimeter lock: some considerations on SNR / 3

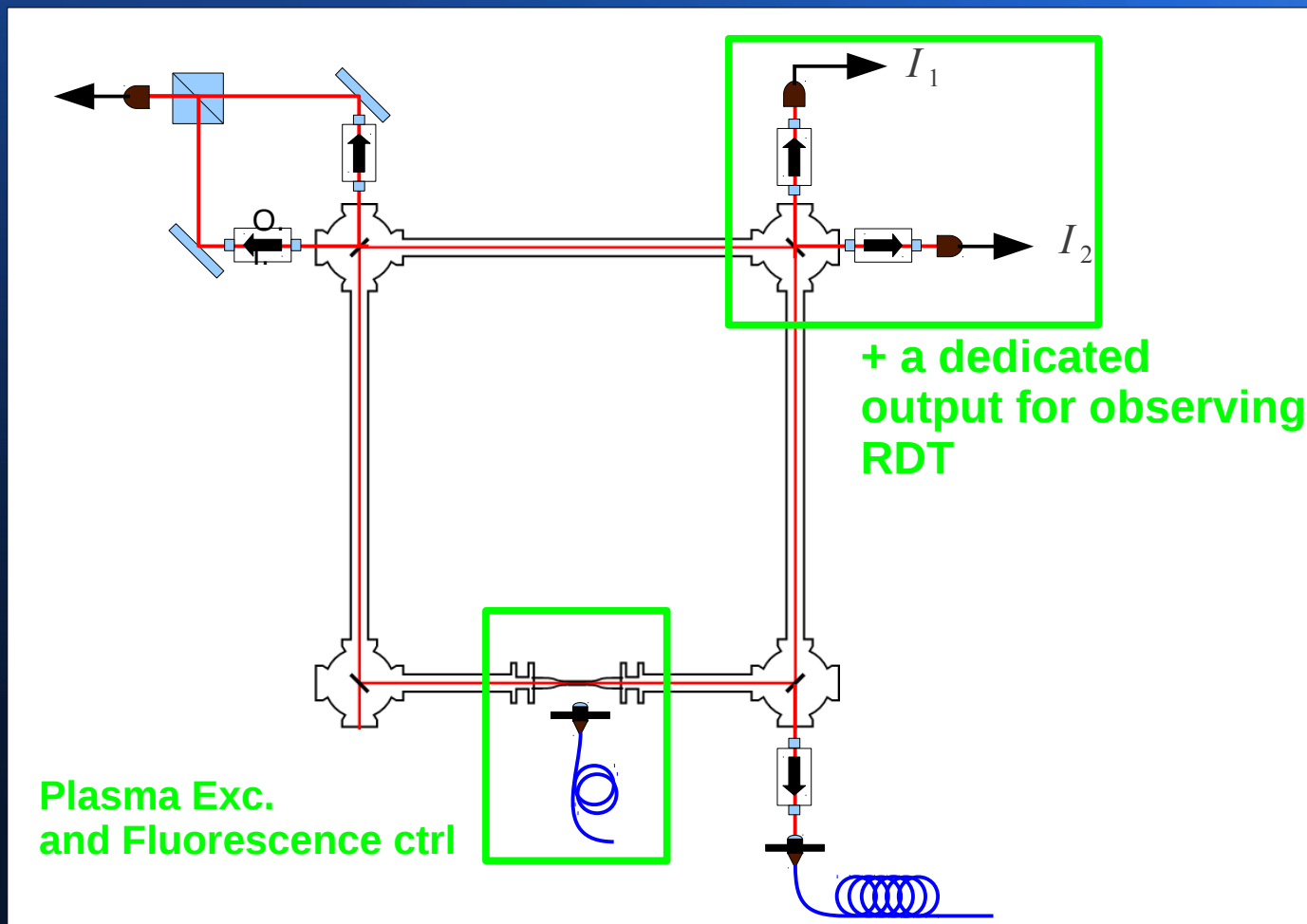
Measurements of SNR on “real” working conditions:

RBW of the real time spectrum analyzer = 100 KHz

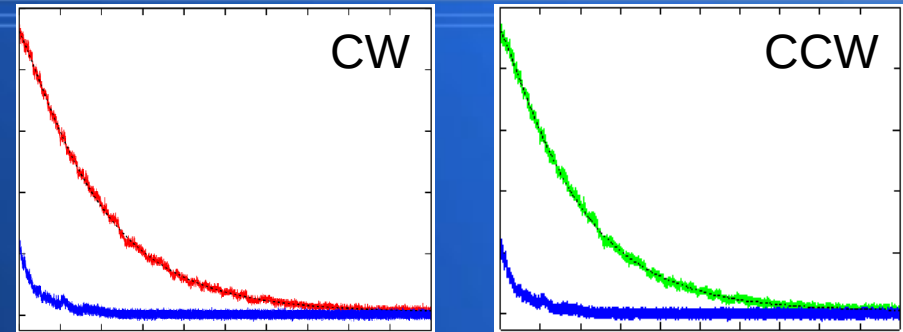
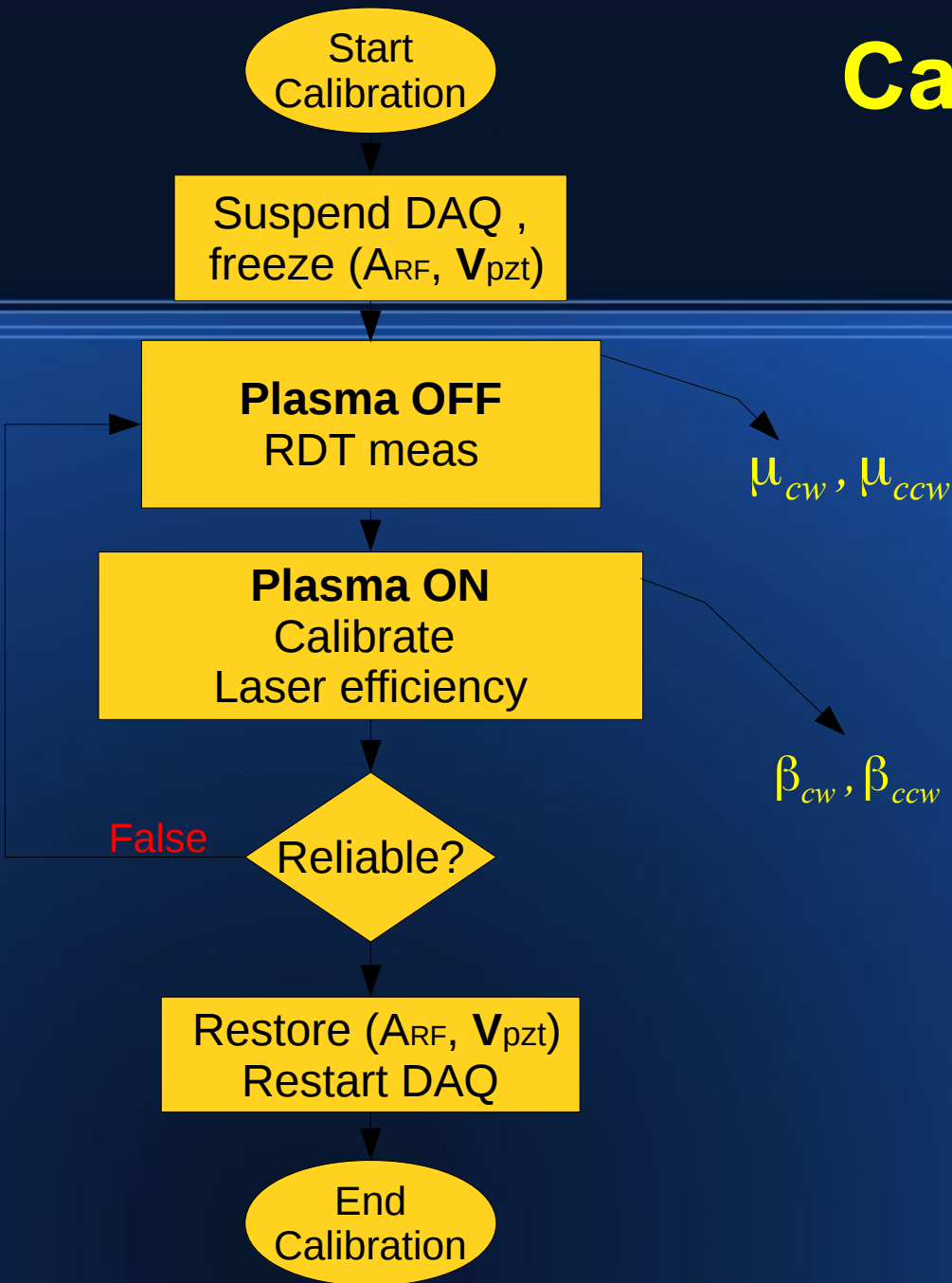
- Noise floor -86 dBV (corresponding to 158 nV/sqrt(Hz), near to the data-sheet value of 100 nV/sqrt(Hz))
- Beat from 31 uW + 10 uW He-Ne beams: **-36 dBV @126 MHz**
- Beat from 31 uW + 10 nW He-Ne beams: **-67 dBV @126 MHz**
- Beat powers are scaling according to the relation $2 * \sqrt{P_1 \cdot P_2}$
but 10 dB (a factors of 10 in power) is missing
- We can take into account those 10 dB considering the non ideal working conditions (for signal and noise) as considered above
 - we measured a loss due to optical coupling of 5dB
 - Beam polarization: work in progress . . .

Automated calibration for:

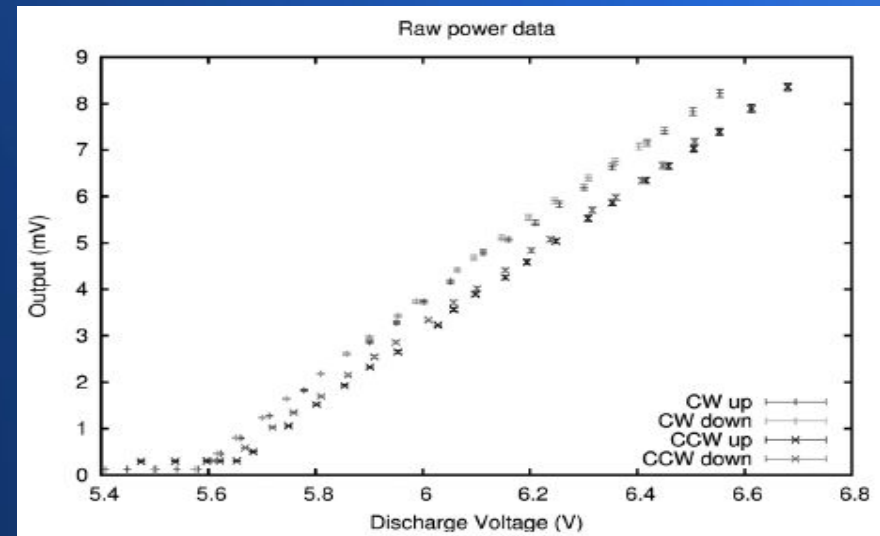
$$\beta_{cw}, \beta_{ccw}, \mu_{cw}, \mu_{ccw}$$



Calibration Logic (PC driven)



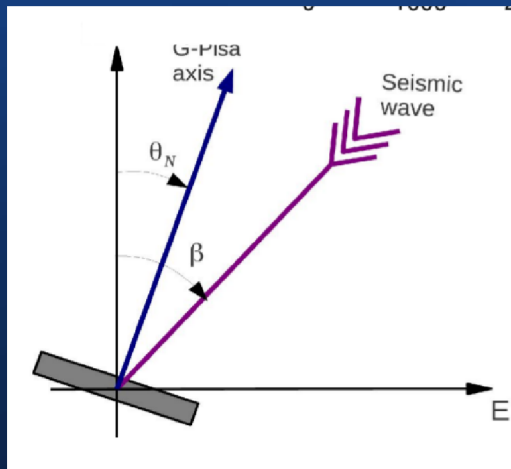
Losses estimation (non reciprocal.)



Laser efficiency

Effects of wind speed and direction on Sagnac frequency

Orientation of G-Pisa:



~ 270 degrees

~ 80 degrees

Same average speed

Further Investigations required

