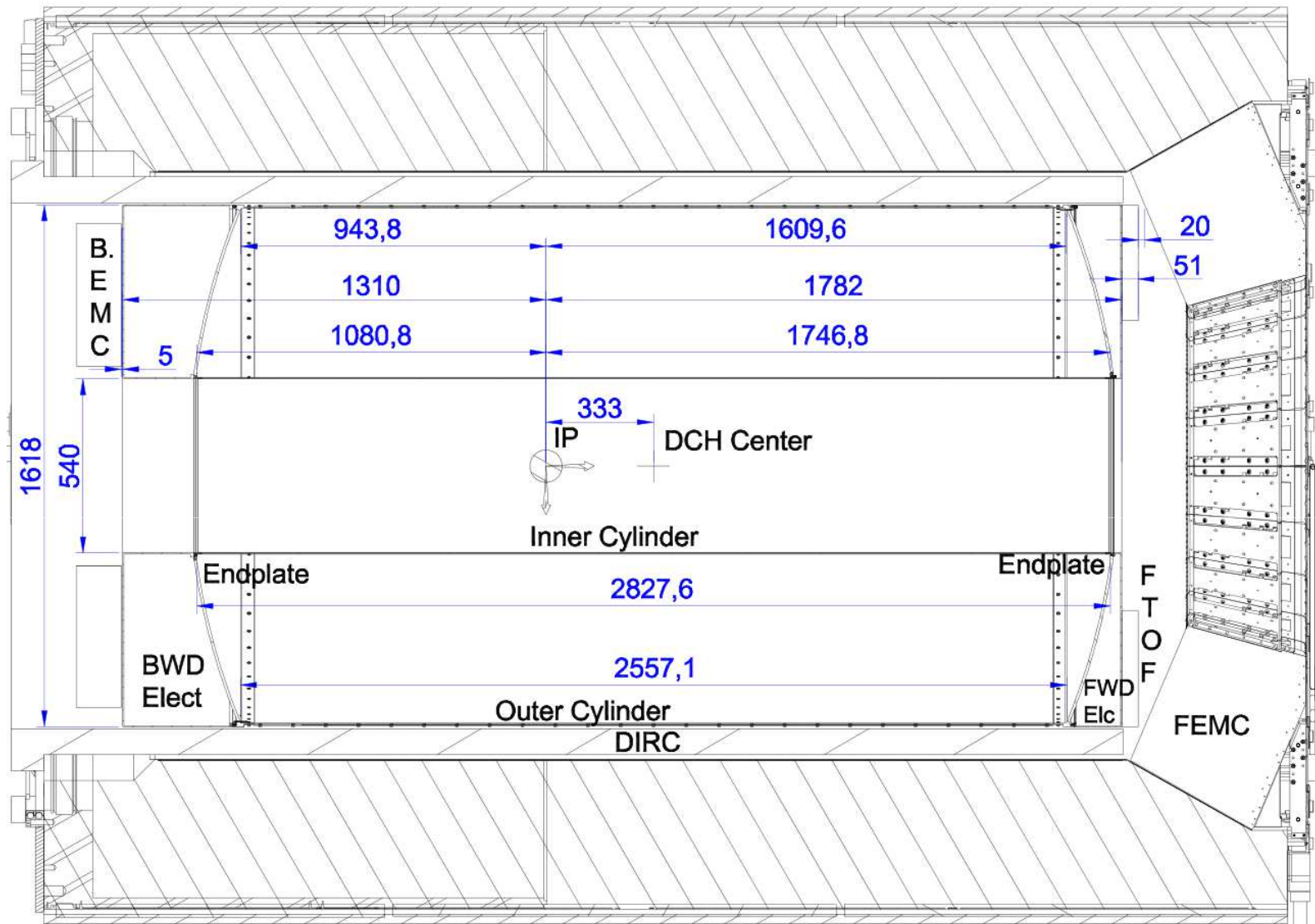




# DCH mechanics

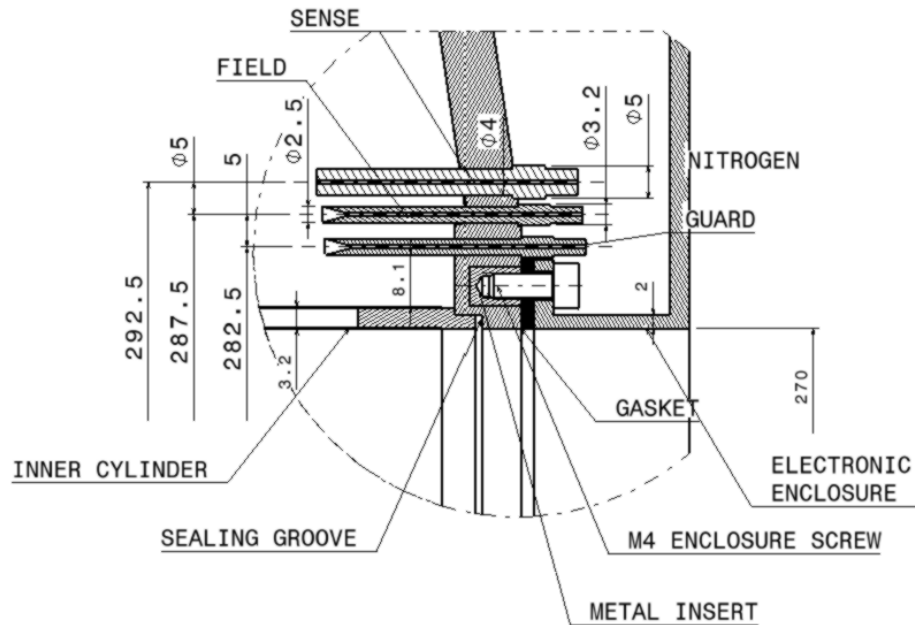
- **DCH final configuration**
- **Safety factor analysis**
  - Endplate
  - Outer cylinder
  - Inner Cylinder

# DCH Final Configuration



- +100mm BWD side
- -11mm FWD side
- 5mm clearance BEMC
- 20mm clearance FEMC

# Endplate



## Inner radius

First guard layer: 282.5mm

First field layer: 287.5mm

First sense layer: 292.5mm

22.5 -> from outer radius (270mm)

CF-sandwich inner cylinder

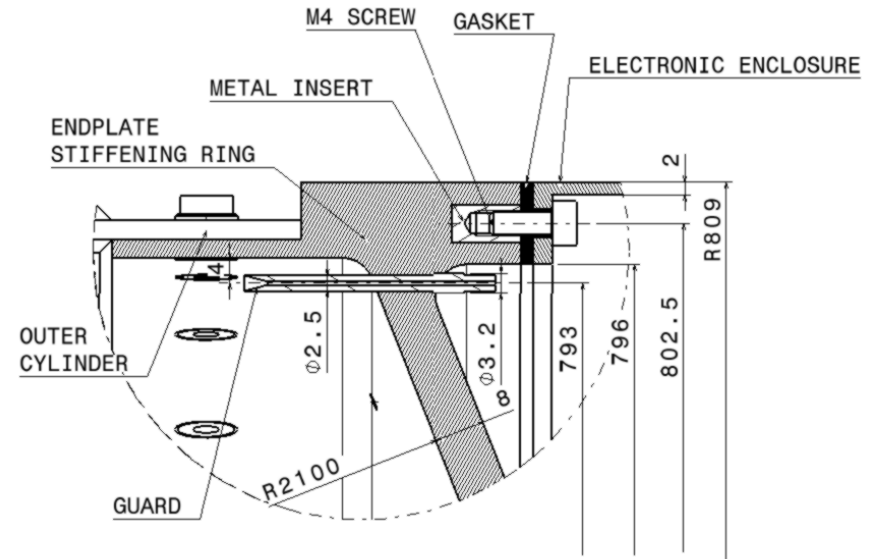
## Outer radius

Last guard layer: 793mm

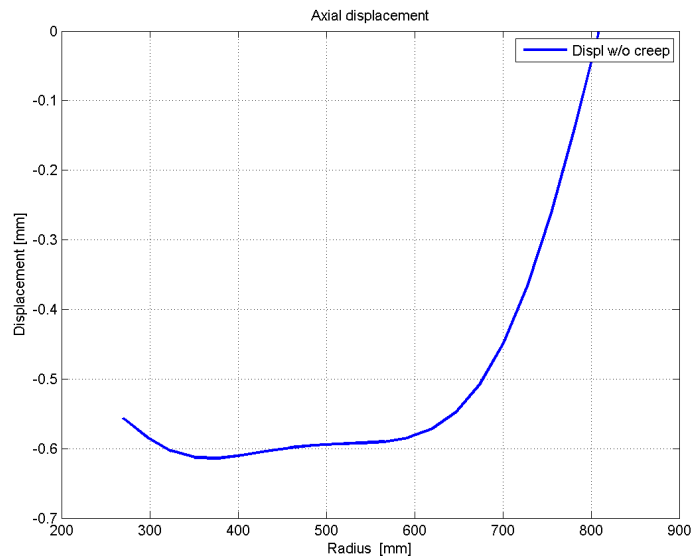
Last field layer: 788.1mm

Last sense layer: 781.7mm

27.3 -> from outer radius (809mm)



# DCH Configurations



Inner and outer stiffening ring have an important effect on endplate behaviour (stiffness of whole structure)

## Load

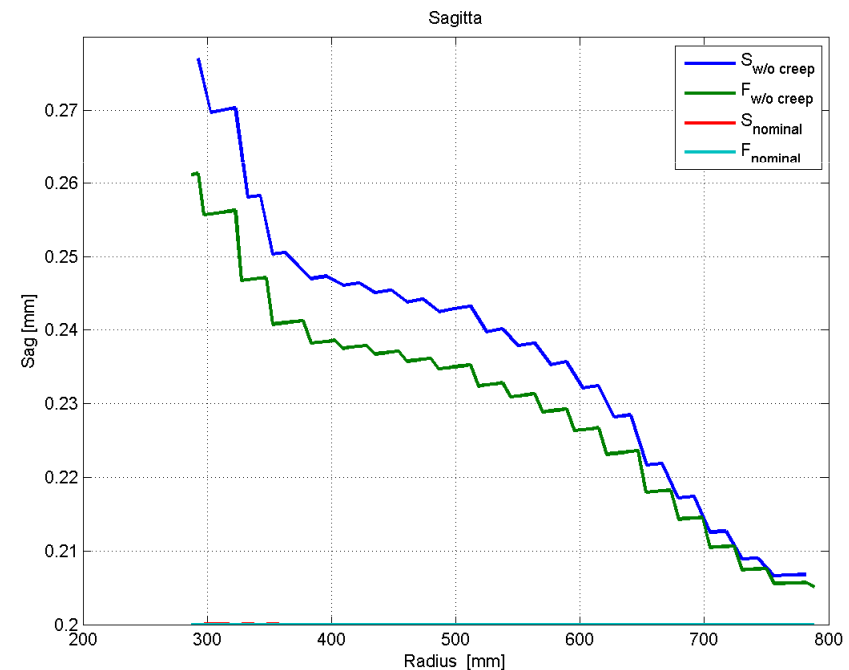
Before stringing: 21400 N

After stringing: 18900 N

Max displ: 0.61 mm

Max Sagitta w/o creep: 0.28mm

Max sagitta difference: 0.02mm



# Safety factor

All the main elements are subjected to compression loads  
An instability analysis is needed

- ENDPLATE
- INNER CYLINDER
- OUTER CYLINDER

Important:

Instability values provided by analytical and FEM analysis are qualitative results

Instability is really sensitive to imperfection in geometry, load and materials  
especially for thin cylindrical shell

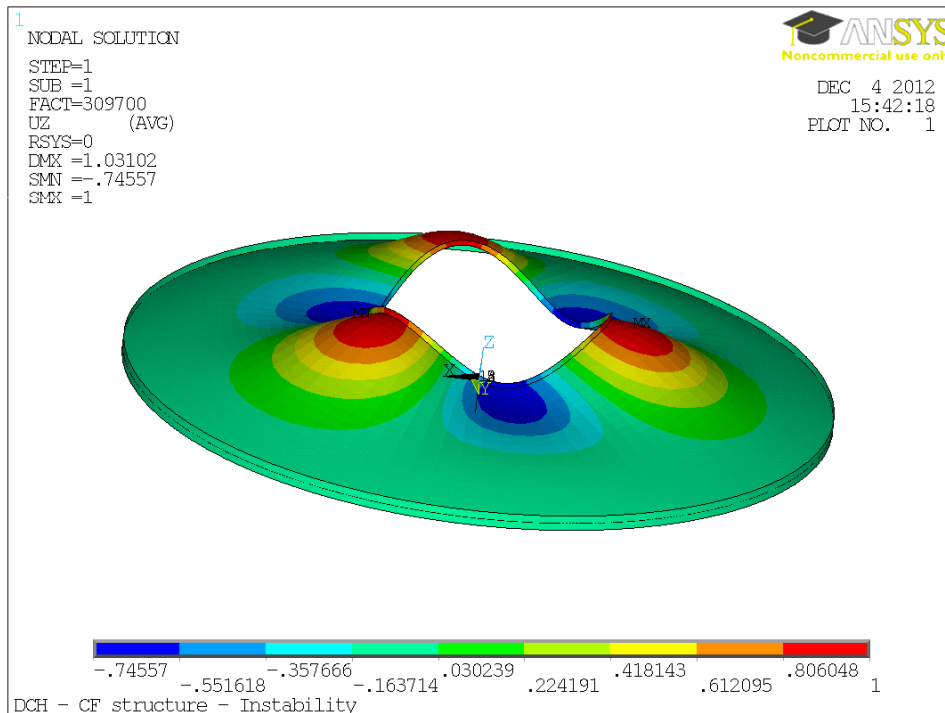
ASME and UNI standards suggest to use a  $SF > 4$  for pressure vessel (steel, aluminum)

Uncertainty in carbon fiber material properties lead to choose  $SF > 10$

# Endplate SF\*

R_ep	Thickness (mm)	Max displ (mm)	Buckling SF
2100	8	0.614	16
3000	8	1.15	8
4000	8	1.77	4.8

8mm CF – quasi isotropic layup  
~~[0°/45°/45°/0°]\_8 ]\_8 - 0.25mm~~  
 Plain weave

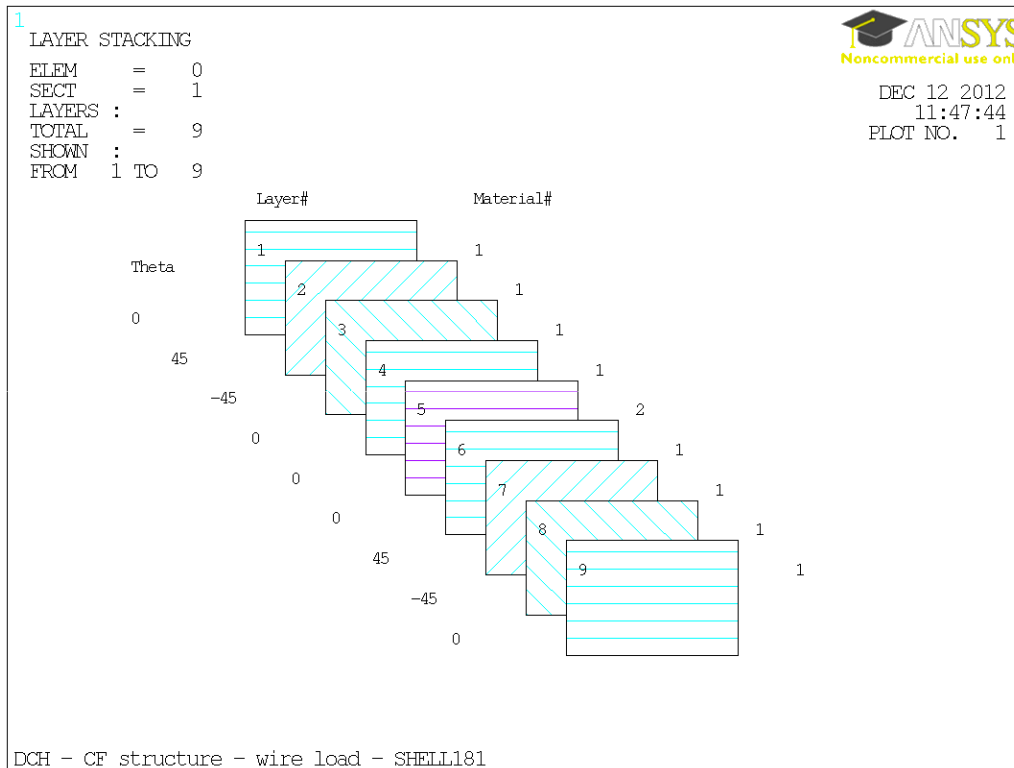


2100 Conf :  
 Small displ -> small sagitta (>0.3) ->  
 probably no need to consider  
 overtension

Higher Safety factor

\*21 KN load

# Outer Cylinder - structure



1mm CF – quasi isotropic layup  
 0°/45°/45°/0° - 0.25/0.25mm  
 Plain weave

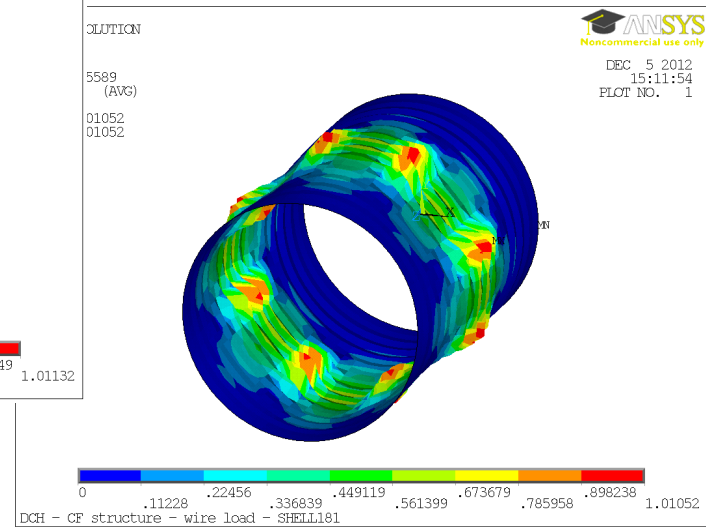
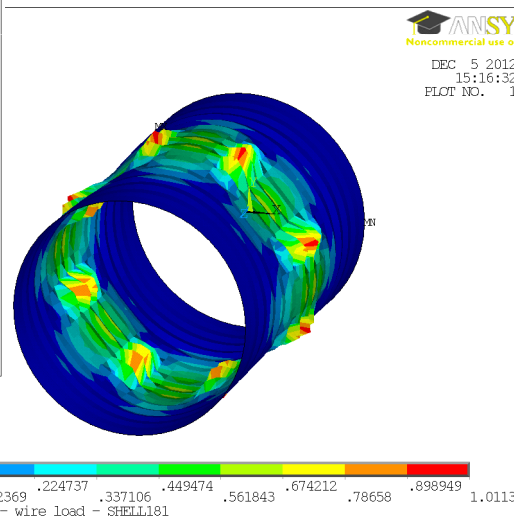
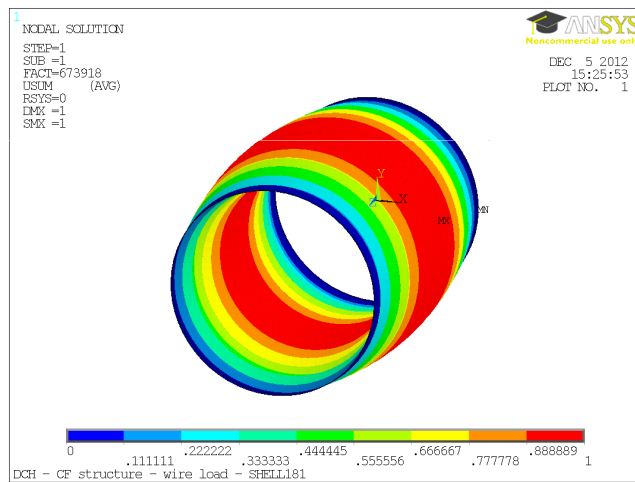
6mm Honeycomb

1mm CF – quasi isotropic layup  
 0°/45°/45°/0° - 0.25/0.25mm  
 Plain weave



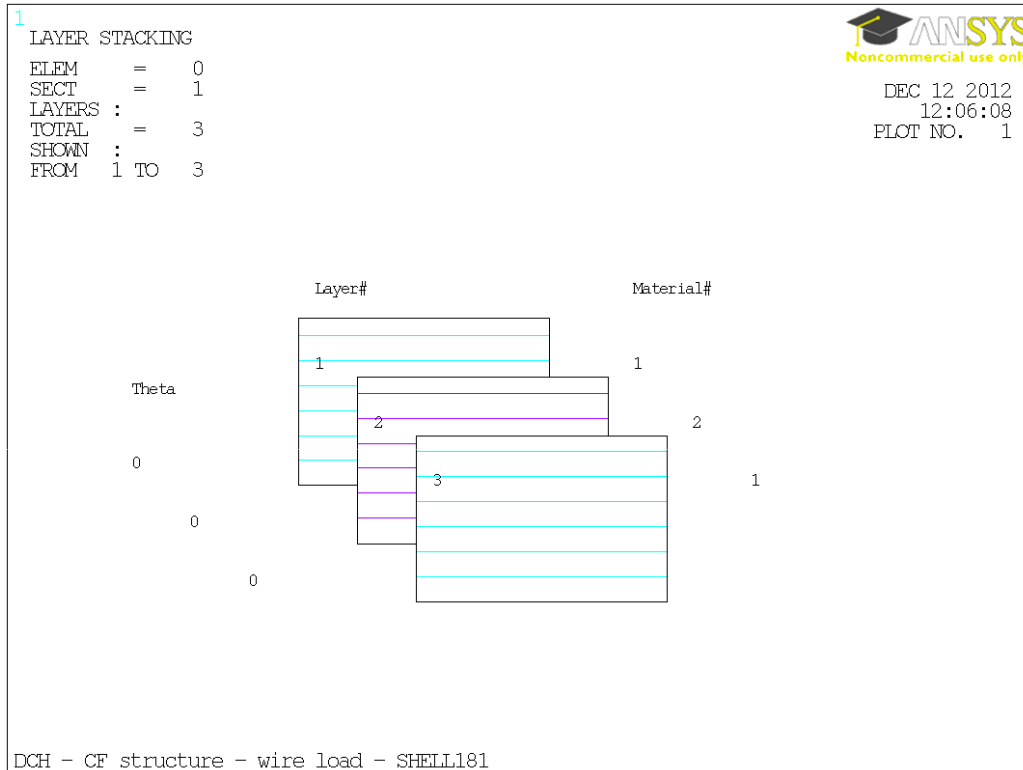
# Outer Cylinder SF\*

Conf	Nom. Geometry	Imp 2mm	Imp 4mm
1_1	24	10.8	8
1_3_1	22	12.8	8.3
1_4_1	25.71	13.5	9
1_6_1	33.6	22.8	18.6



\*21 KN load

# Inner Cylinder - structure



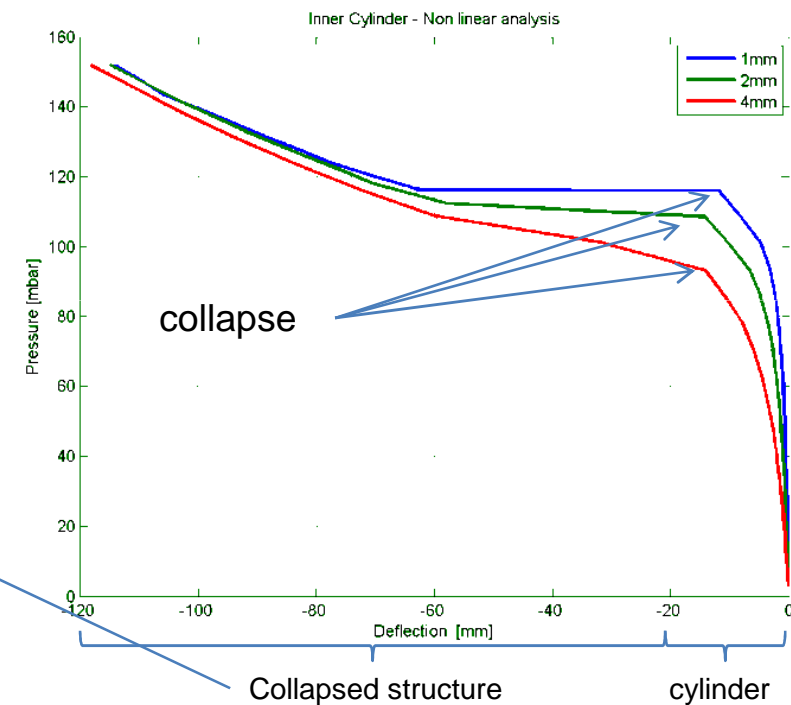
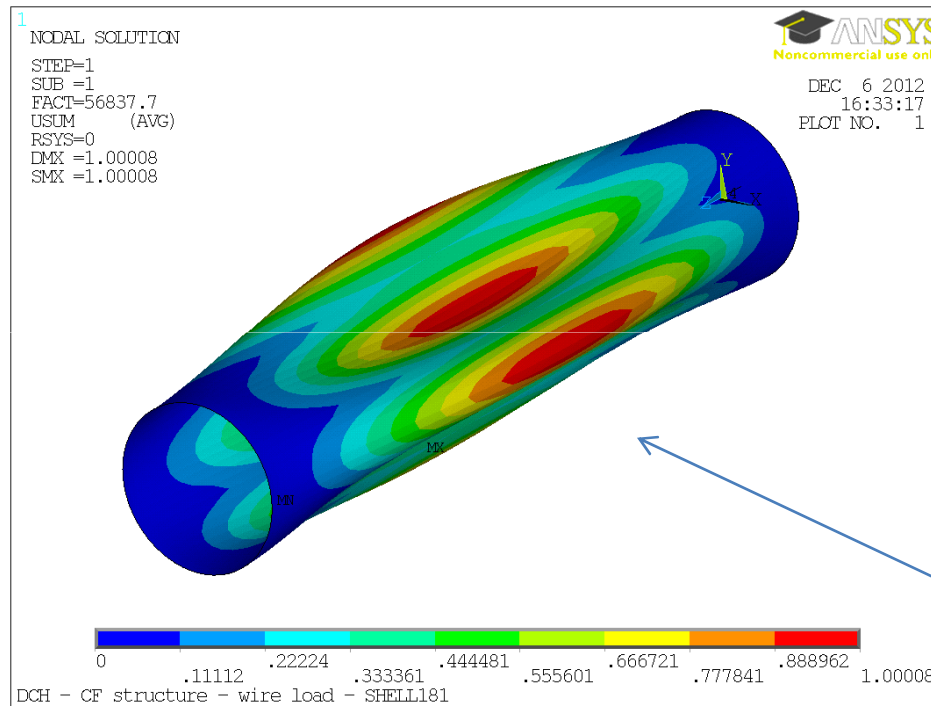
0.09mm CF – 0°  
Plain weave

3mm Honey comb

0.09mm CF – 0°  
Plain weave

# Inner Cylinder

Conf	Nom. Geometry	Imp 1mm	Imp 2mm	Imp 4mm
0.09_3_0.09	120mbar	108mbar	99mbar	86mbar
0.09_0.09	0.84mbar	0.74mbar	0.68mbar	0.56mbar



CF plies thinner than 0.09mm are difficult to handle and are full of microholes (effects on material properties, gas tightening)

## Conclusions

DCH design is almost completed (80%):

To do:

- Enclosure (depend on electronic and supports)
- Fastening DCH-Enclosure Cyl-EP (Number, material and typologies of screw)
- Mechanical drawings

Parametric FEM model (90%):

To do:

- Effects of creep
- Tests (carbon fiber, sandwiches)
- Investigate Kapton-sandwich for inner cylinder (used in KLOE2 CGEM-cathode structure)
- Model can be quite easily adapted to different geometry and materials