

Tests and Understanding of the Virgo+ monolithic suspensions (1)

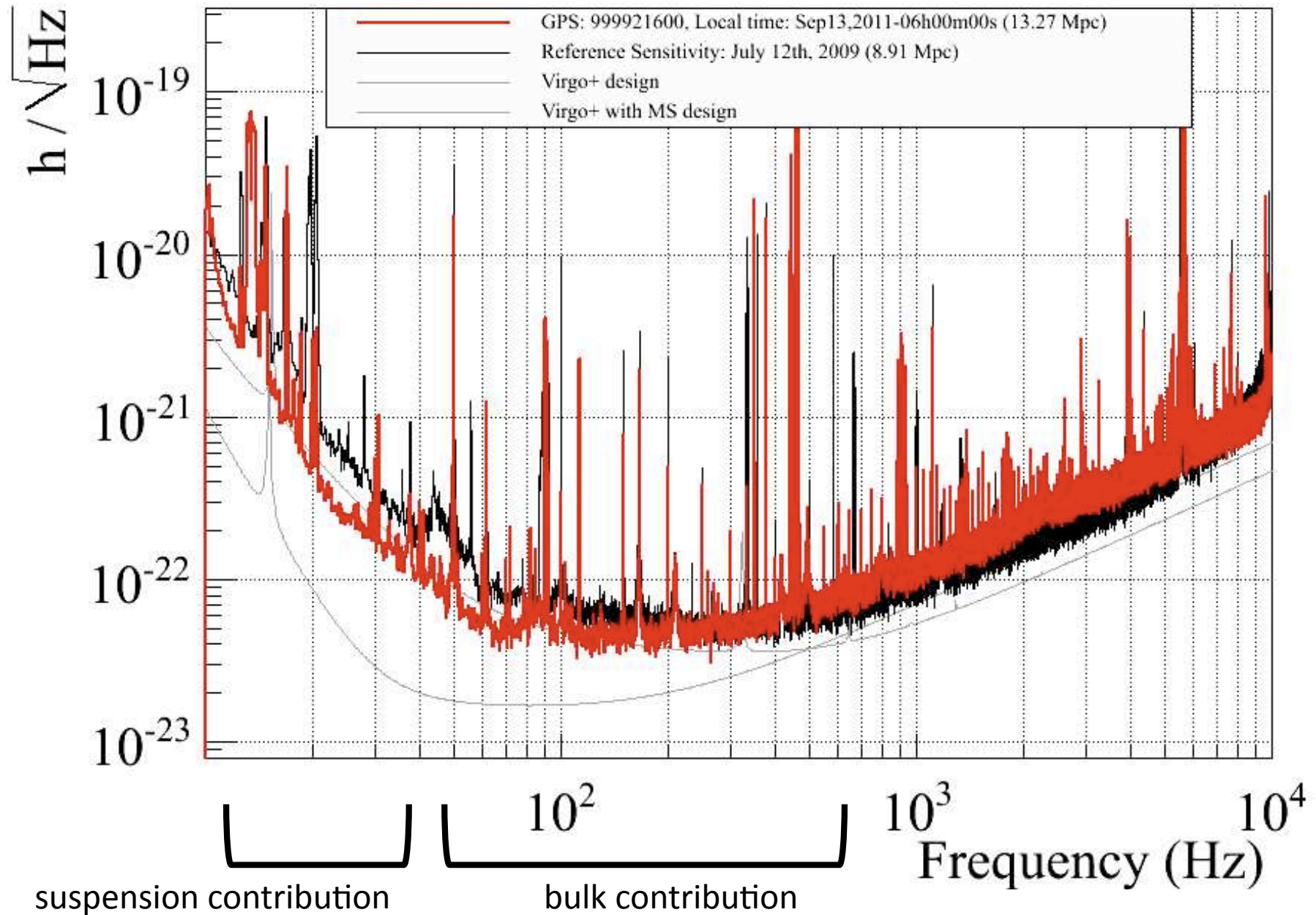
Marzia Colombini

Thermal Noise Workshop
February 23-24 2012

Outline

- Quality Factor measurements:
purpose and procedures
- experimental results:
 - pendulum
 - vertical
 - violins
 - bulk
- identification problems and temperature correlation

Virgo+ expected Thermal Noise



Thermal Noise estimation

We can estimate the Thermal Noise measuring the Quality Factor of the internal modes.

When a payload internal mode is excited, its amplitude decay time is related to the dissipation processes

$$A(t) = A_0 e^{-t/\tau} \quad \longrightarrow \quad Q = \pi \nu T$$

Different modes:

- are connected to different losses (superficial, thermoelastic, structural, recoil...)
- give different contributes to the Thermal Noise

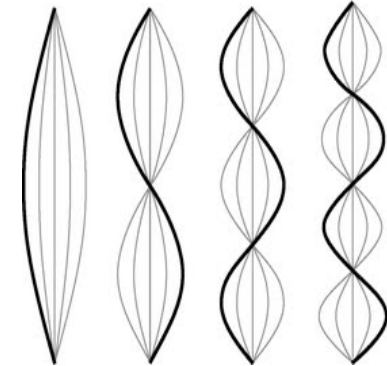
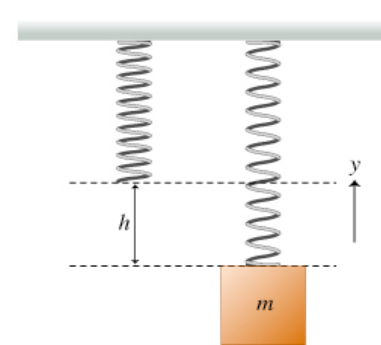
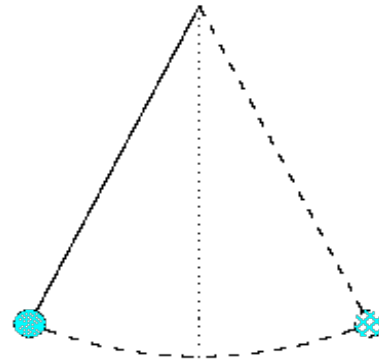


it is crucial to associate correctly each frequency
with its own mode

Measured Internal modes

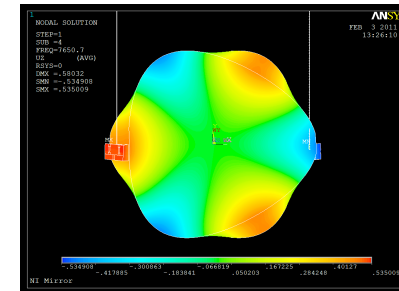
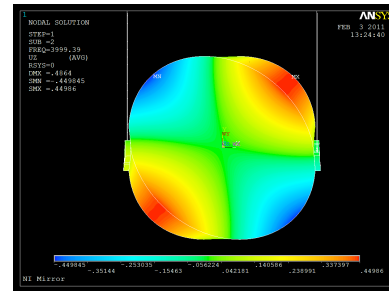
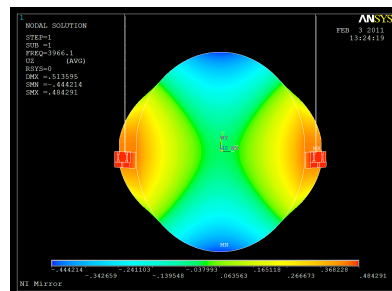
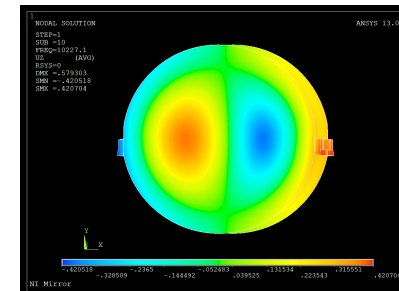
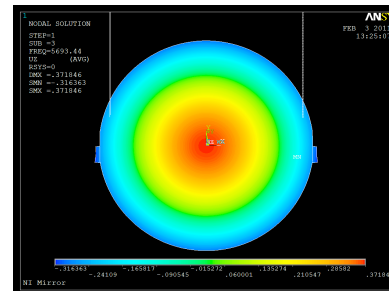
- suspension modes:

- pendulum;
- vertical;
- violins;



- bulk modes:

- drum;
- butterfly;
- radial;



- ...

Measurement procedure (up to 20 kHz)

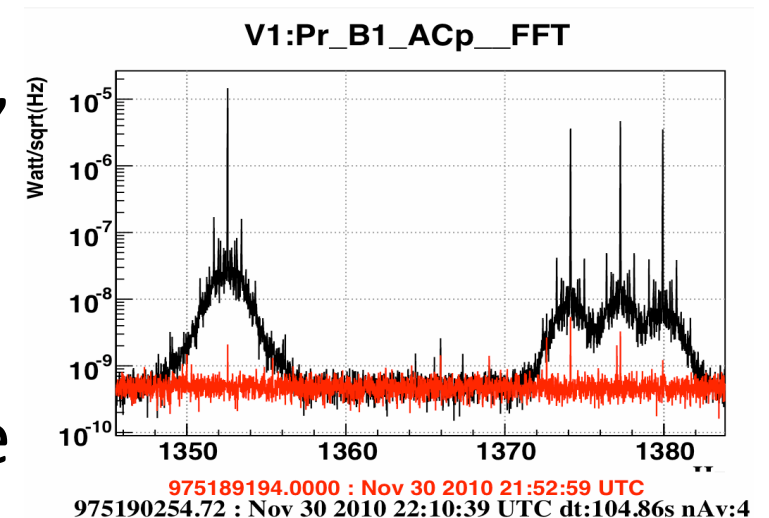
- Excitation → kick (moving the Marionette Balancing Motor by 1 step for each tower)

ITF locked and stable; different days; at least 1 hour of data

- the excitation effect can be observed directly in the Dark Fringe Pr_B1_Acp

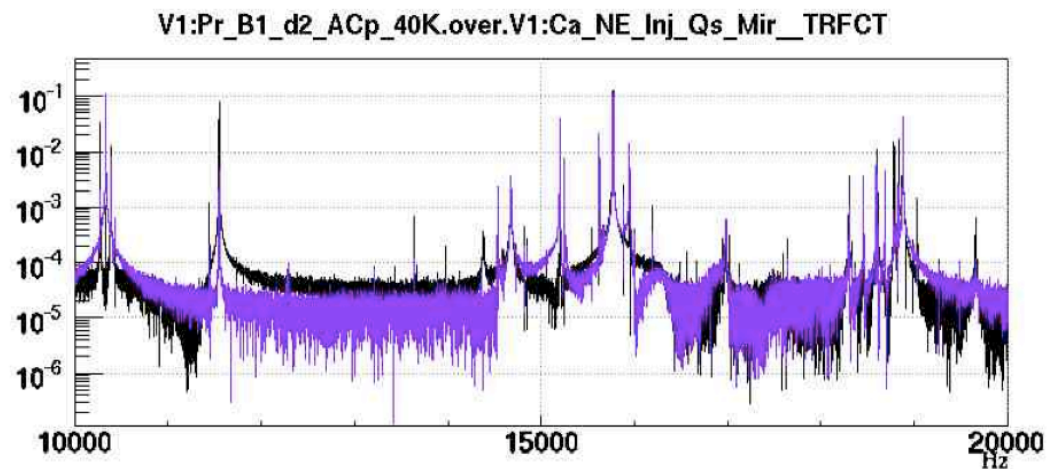
for the pendulum mode we observe the Local Control signals

- we identify every risen frequency, comparing the quiet signal with the spectra after the excitation
- we follow the decaying amplitude of each resonance at different times.



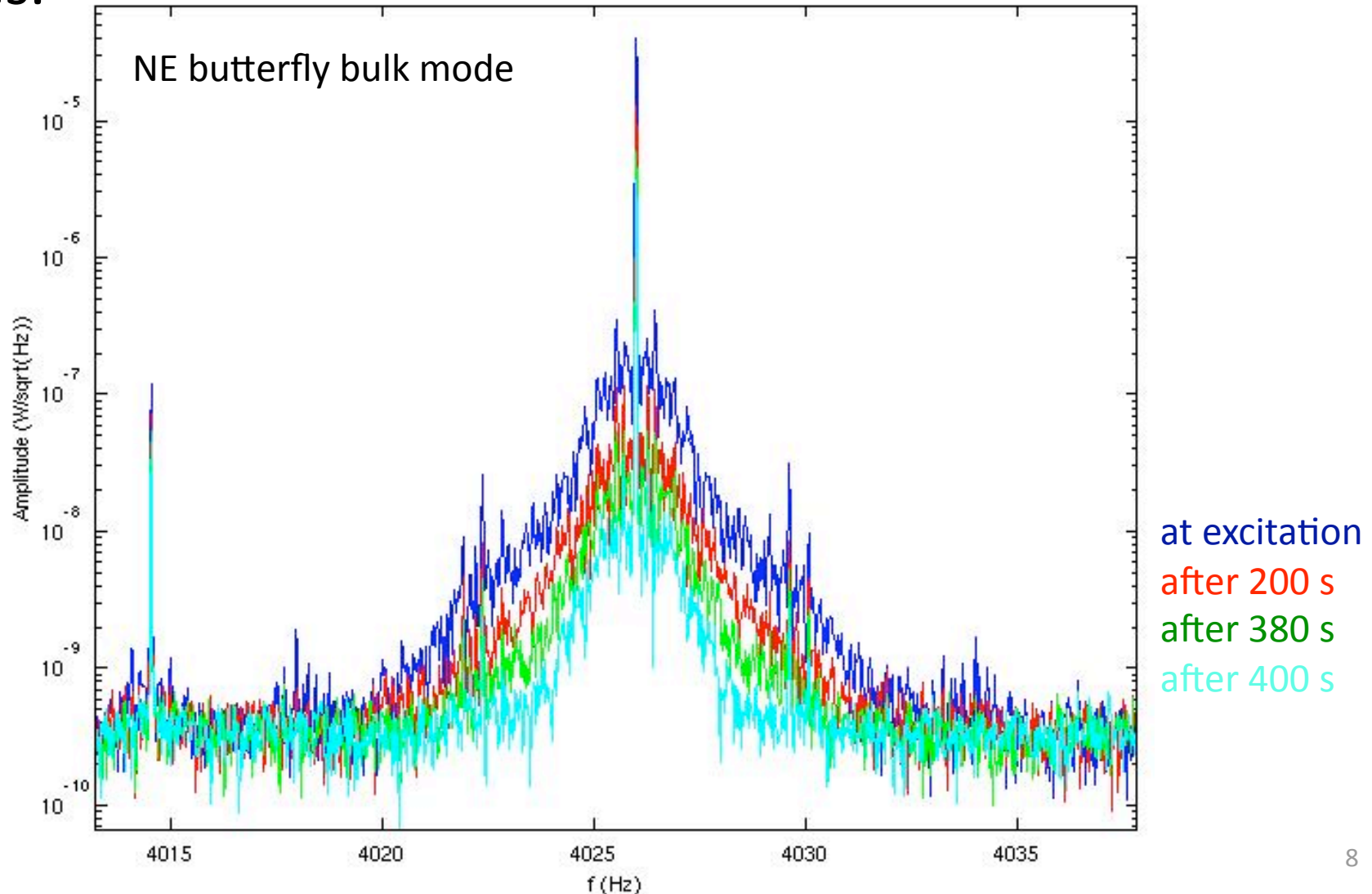
Measurement procedure (up to 40 kHz)

- Excitation → band-limited noise to RM coils (using the Spectrum Analyzer for each tower)
ITF locked and stable; different days; at least 1 hour of data
- the excitation effect can be observed in the Pr_B1_d2_ACp_40K
- we identify resonances using the transfer functions
- we follow the decaying amplitude of the spectra for each resonance.



Quality Factor Measurement (1)

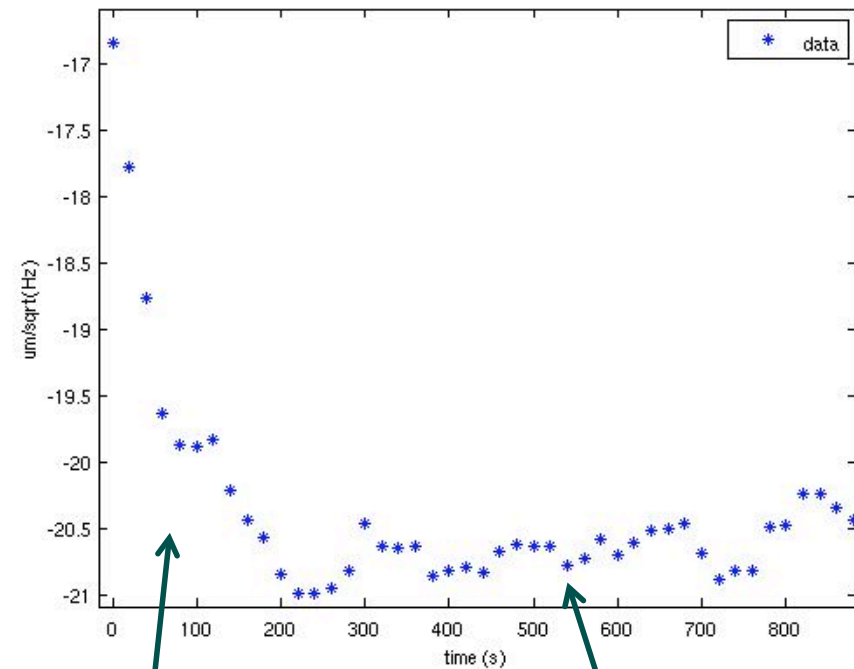
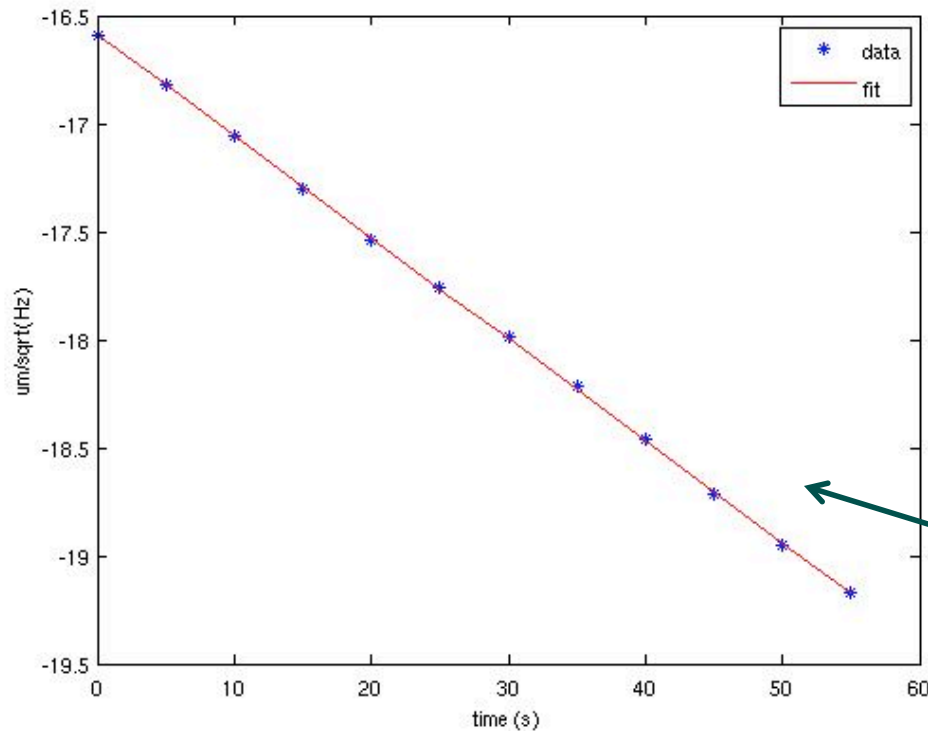
For each frequency we take its amplitude at different times.



Quality Factor Measurement (2)

We fit the linearized data using a Matlab script.

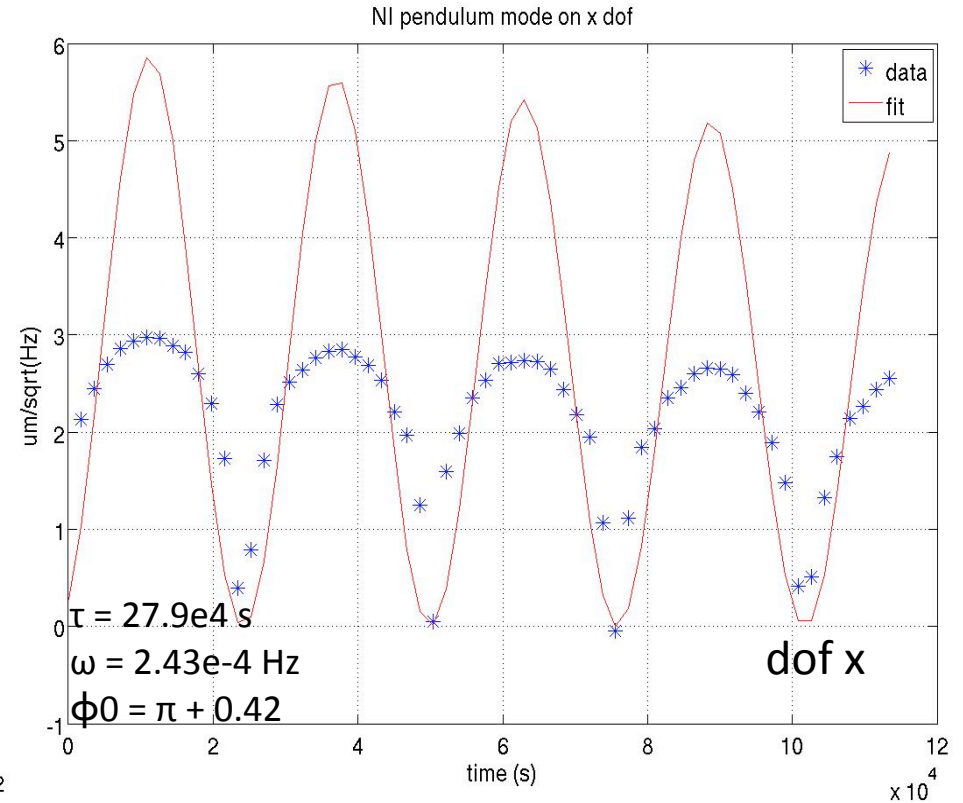
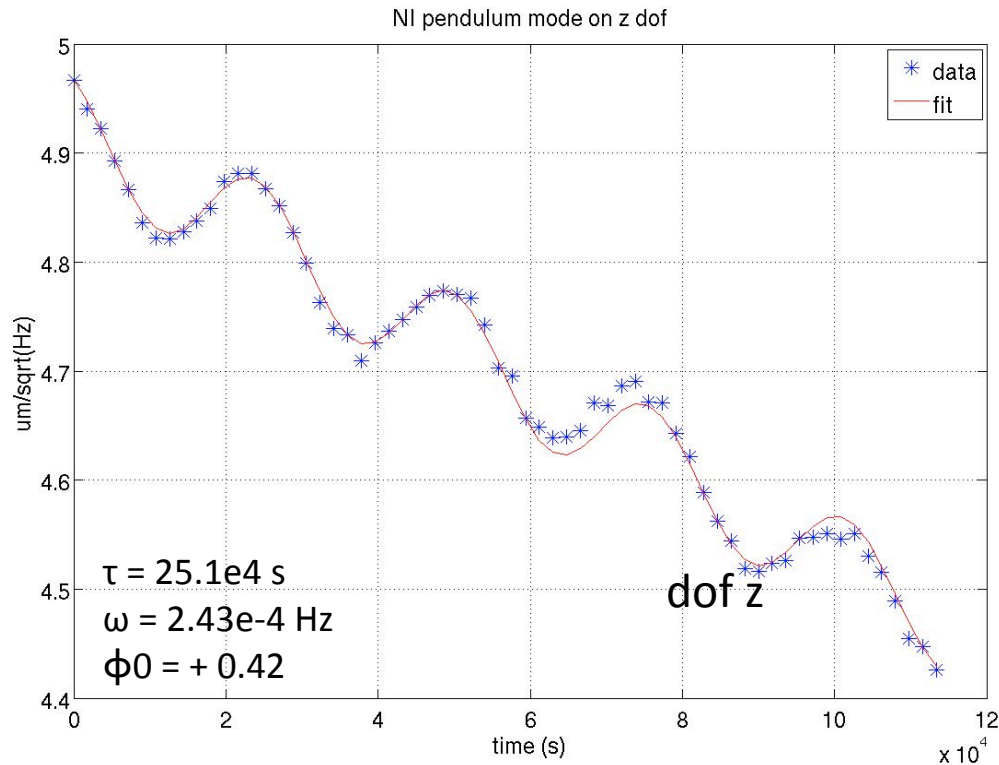
Example:
 WE $f = 4537.17$ Hz (X violin)
 $Q = 3.03 \text{ e}5$



decaying amplitude
 noise
 (the peak is not recognizable anymore)

fitted data:
 we take only the data with a linear behaviour

Pendulum Mode



NI

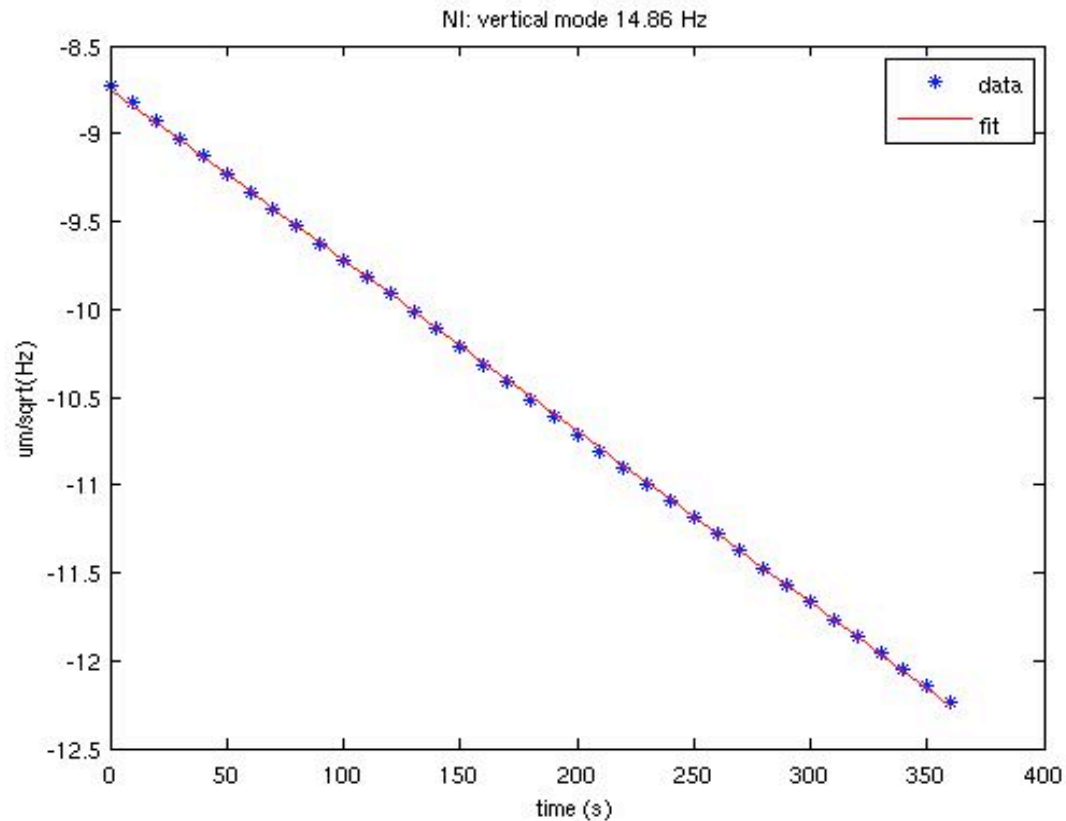
$f = 0.59 \text{ Hz}$

There is a coupling between the z dof and the x; furthermore the PSD on the x dof saturates.

	$\tau(s) \cdot 10^5$	$Q \cdot 10^5$
NI z	2.55	4.80
NI x	2.35	4.43
WI z	5.74	10.8
WI x	6.82	12.8
NE z	1.05	1.98
NE x	1.69	3.18
WE z	7.17	13.5
WE x	3.77	7.11

see VIR-0622A-10

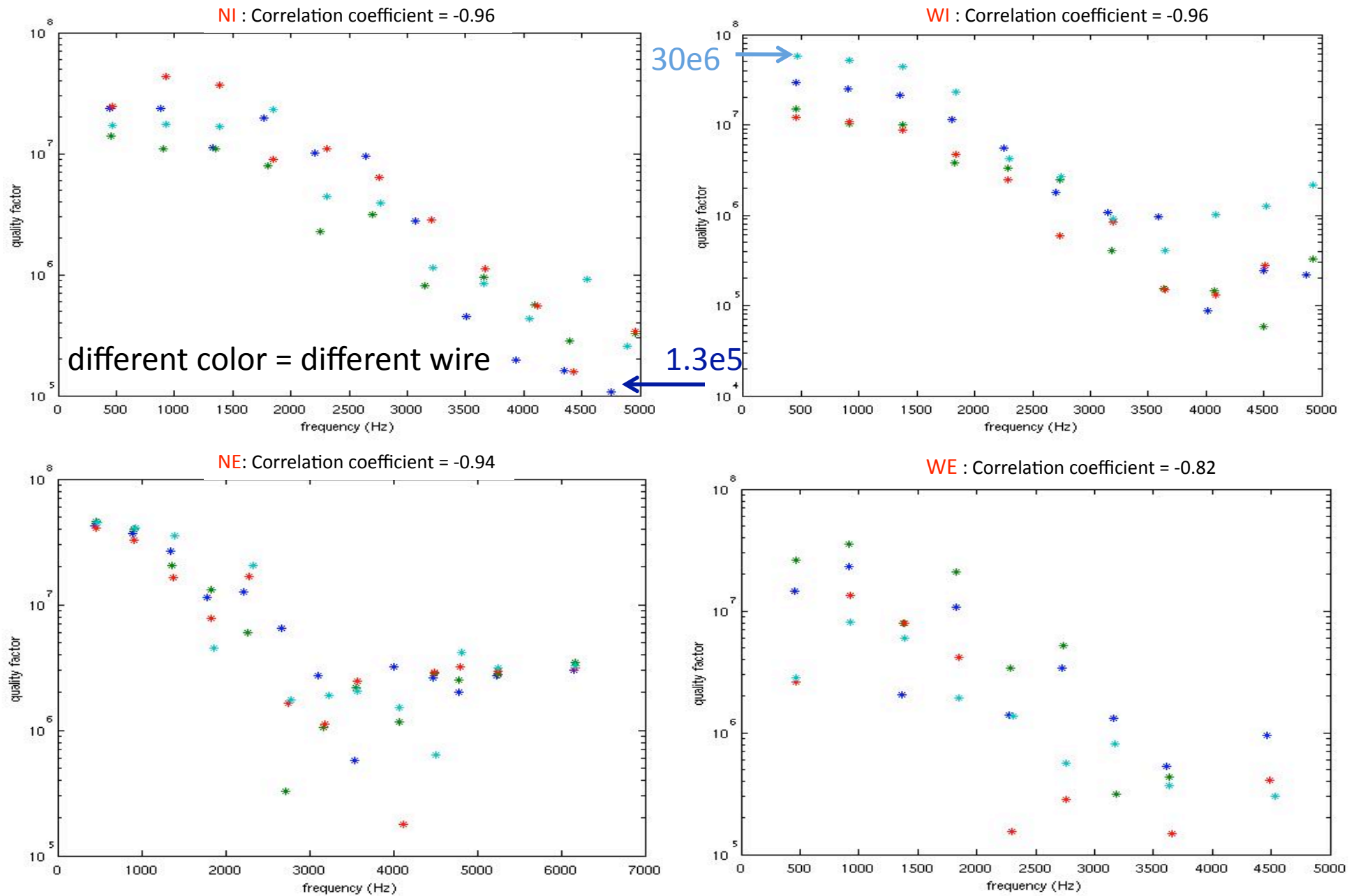
Vertical Modes



NI
dof y
 $f = 14.86 \text{ Hz}$

	f (Hz)	τ (s)	$Q \cdot 10^4$
NI	5.97	4450	8.36
	14.86	103	0.48
WI	5.90	1570	2.90
	14.78	101	0.47
NE	5.97	560	1.05
	14.88	65.8	0.31
WE	5.92	134	0.25
	14.78	63.1	0.29

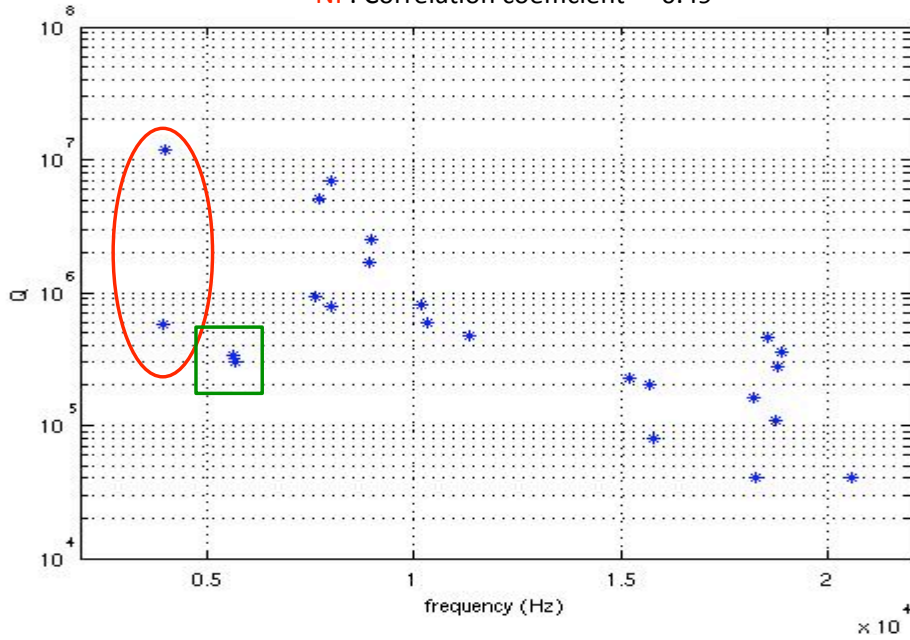
Violin Modes



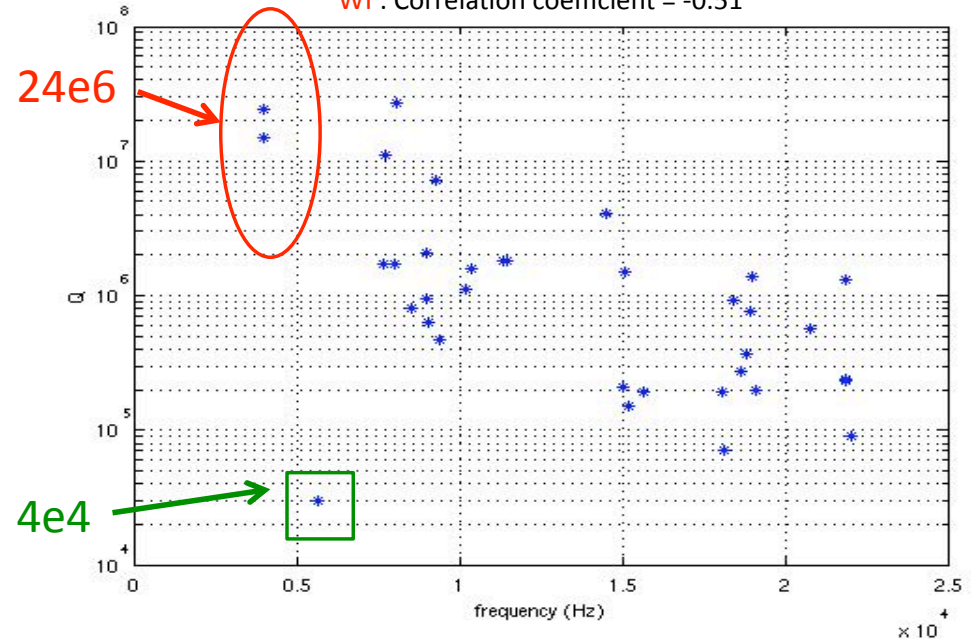
Bulk Modes

butterfly drum

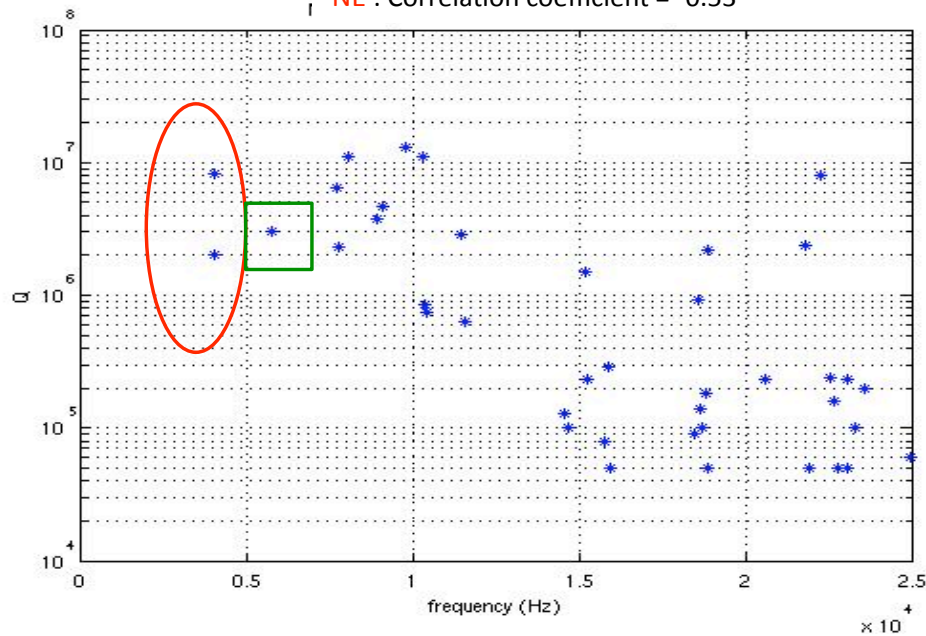
NI : Correlation coefficient = -0.49



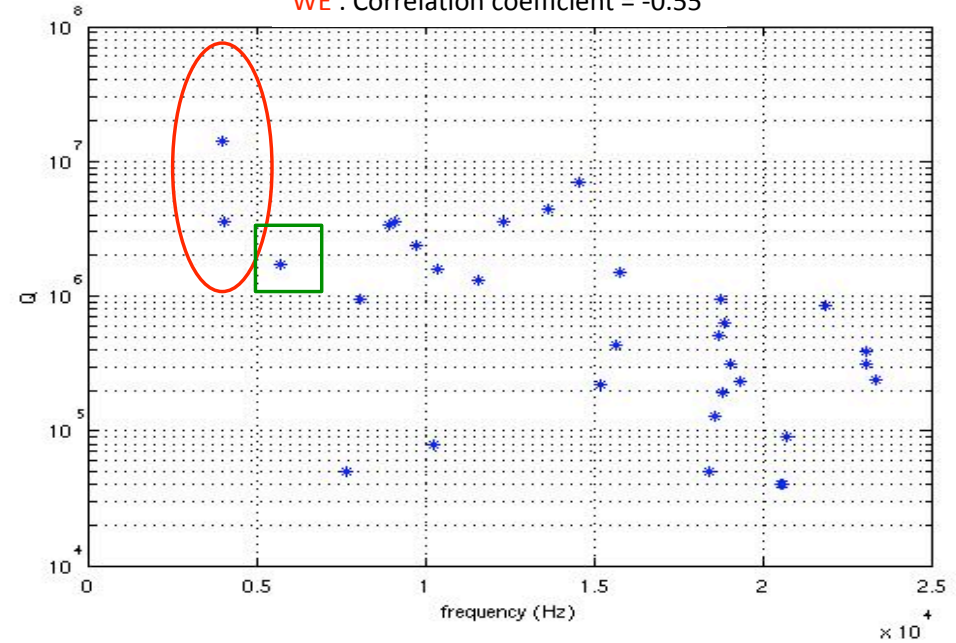
WI : Correlation coefficient = -0.51



NE : Correlation coefficient = -0.53

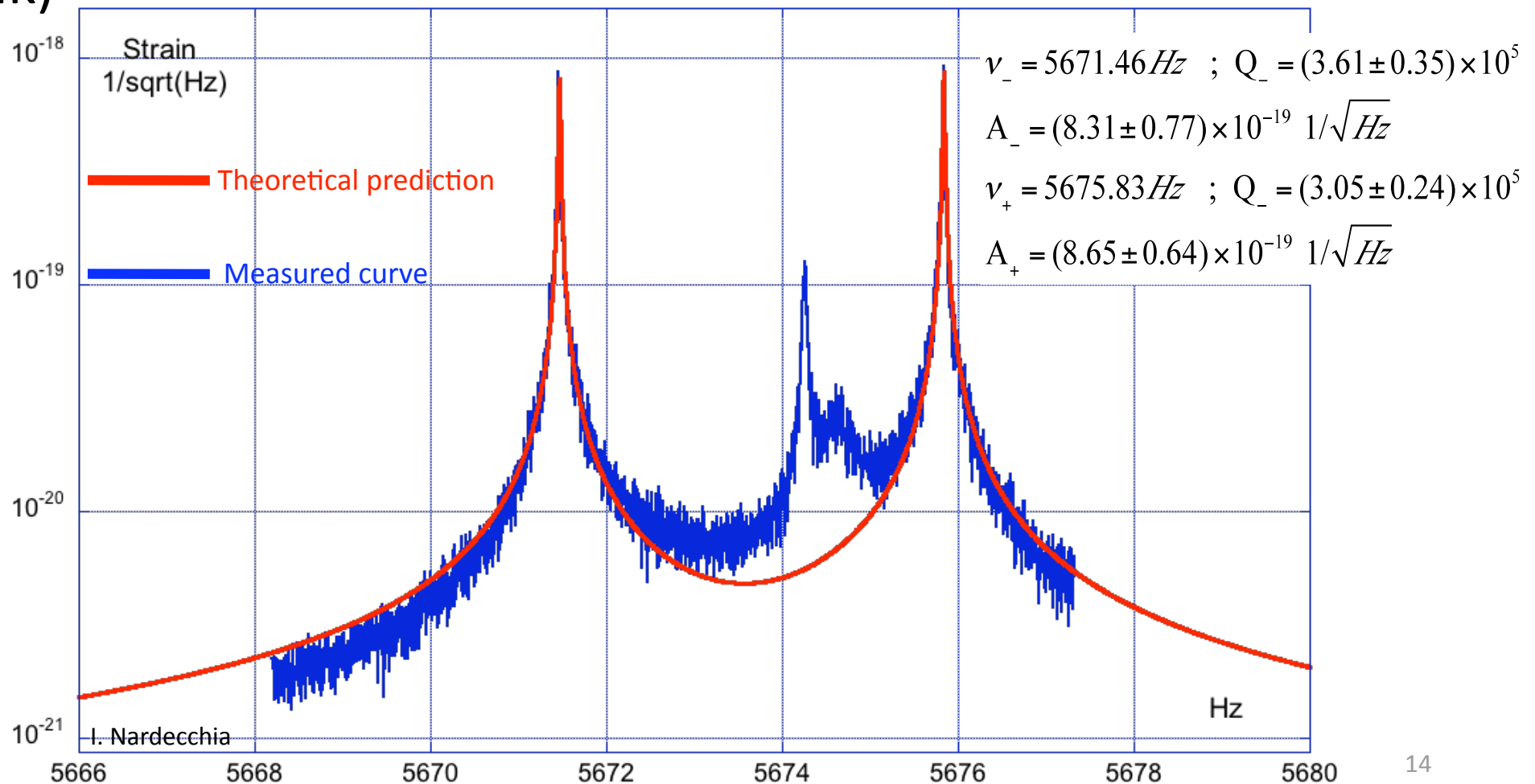


WE : Correlation coefficient = -0.55

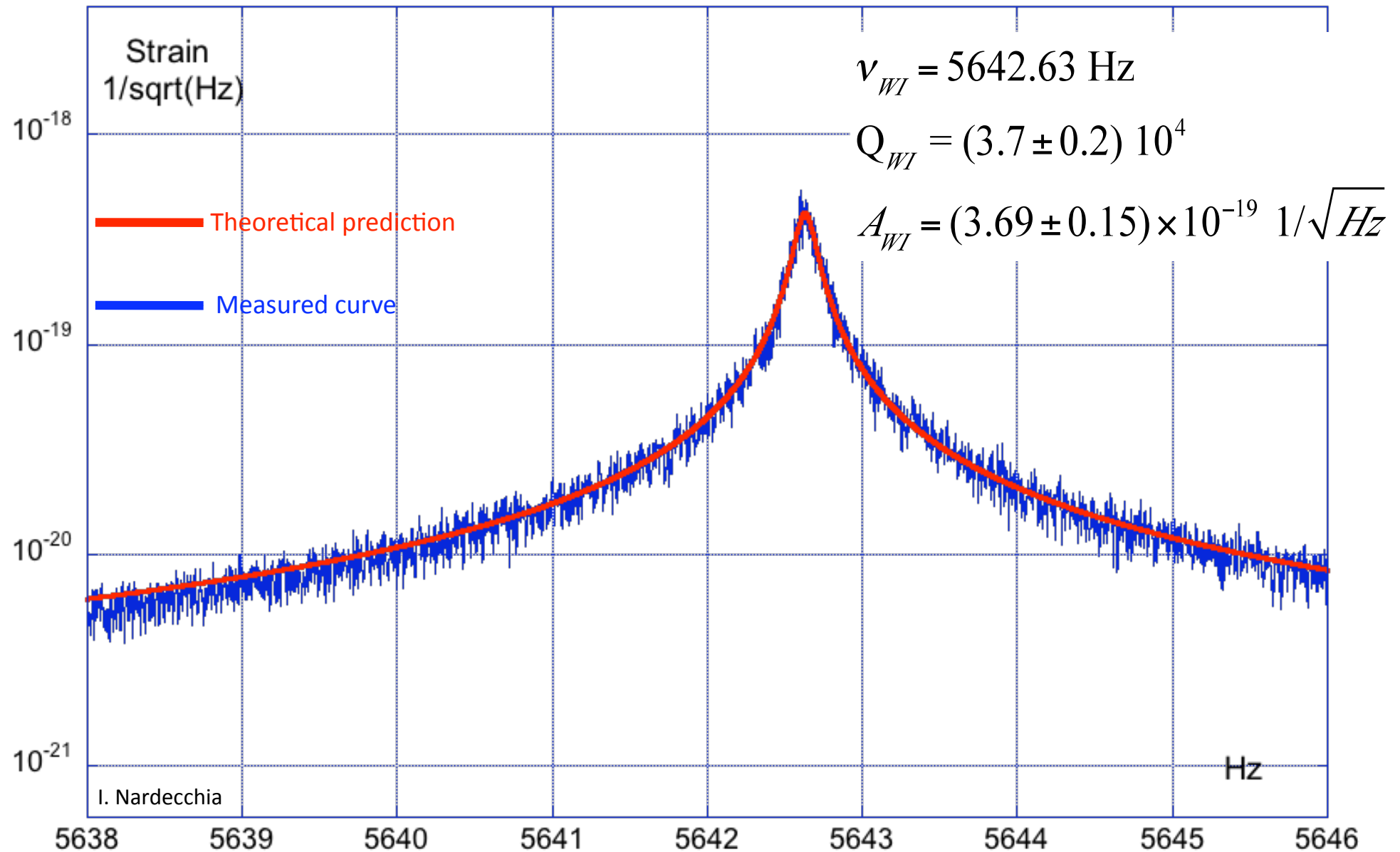


NI Drum modes

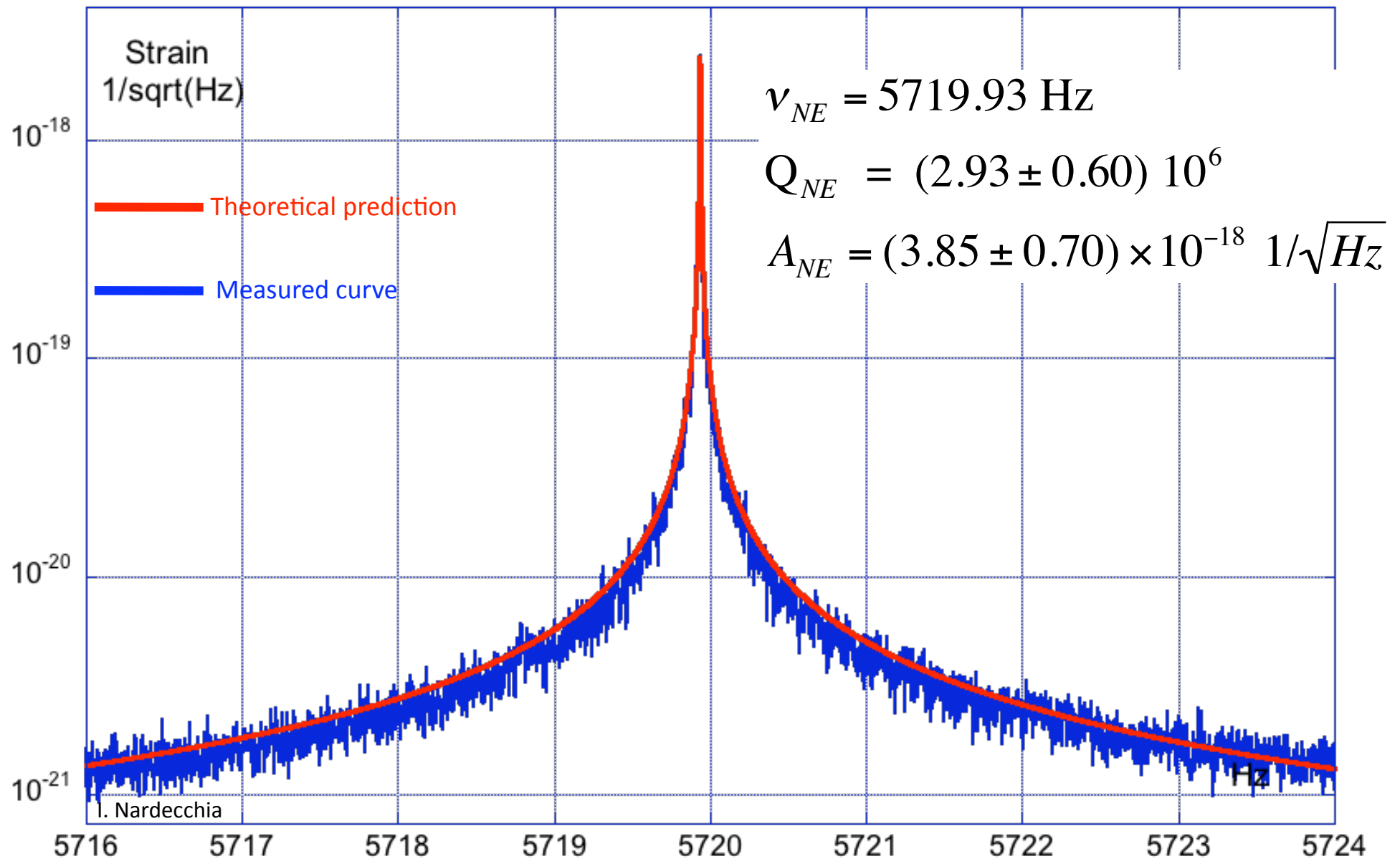
We repeat the Q estimation with a Lorentzian fit taking data from a quiet period (for interpretation and details see Puppó's talk)



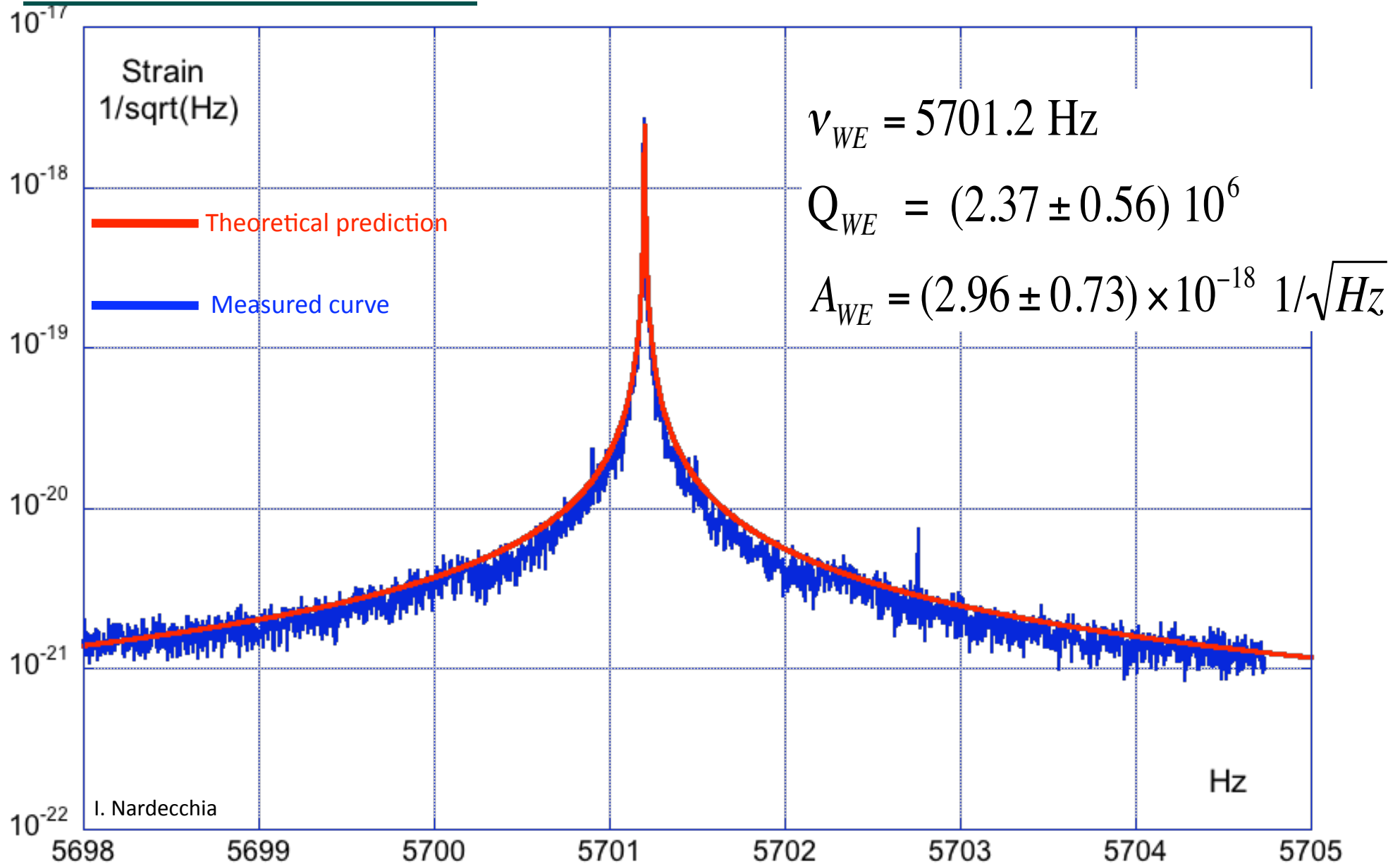
WI Drum mode



NE Drum mode



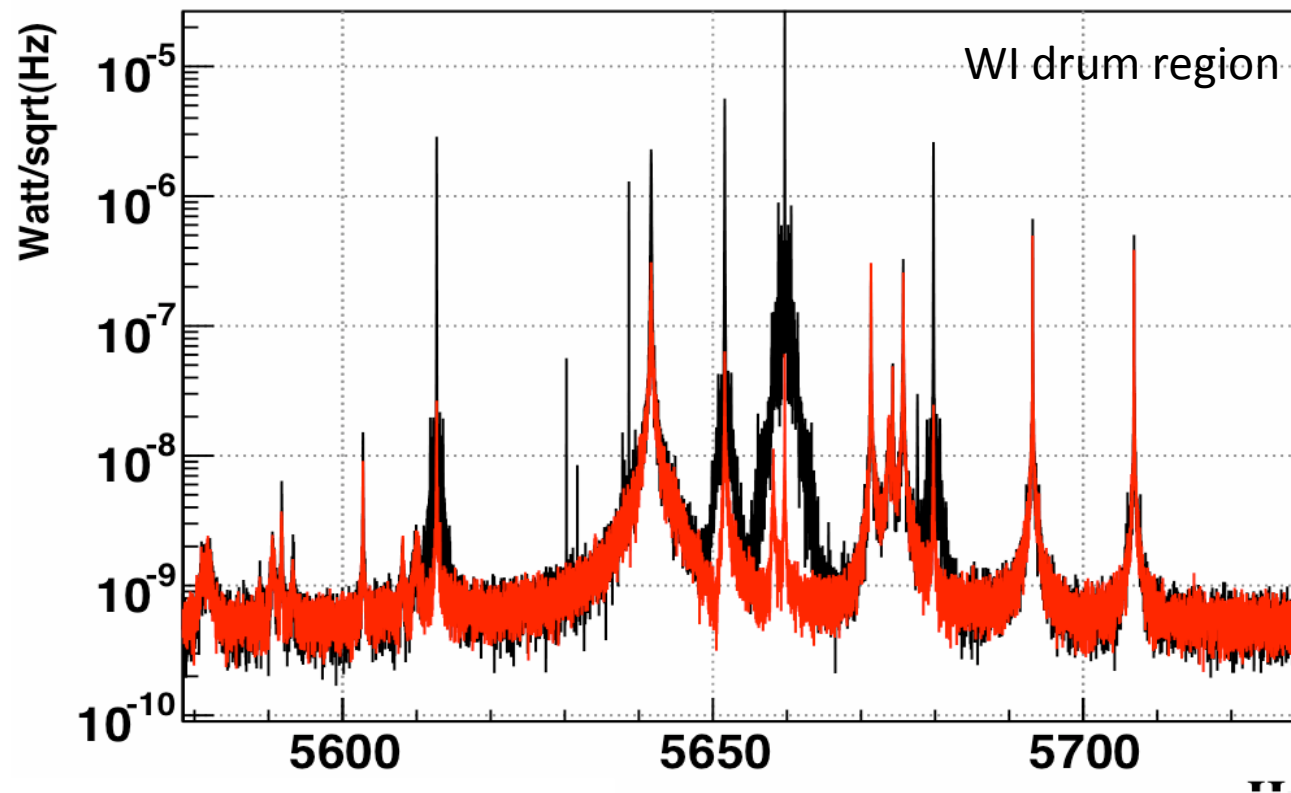
WE Drum mode



Bulk Modes: Identification problems

The problem is that the violin harmonics often fall in the same region of the butterfly/drum modes.

V1:Pr_B1_ACp_FFT



- 1 drum resonance
- all other frequencies are violins

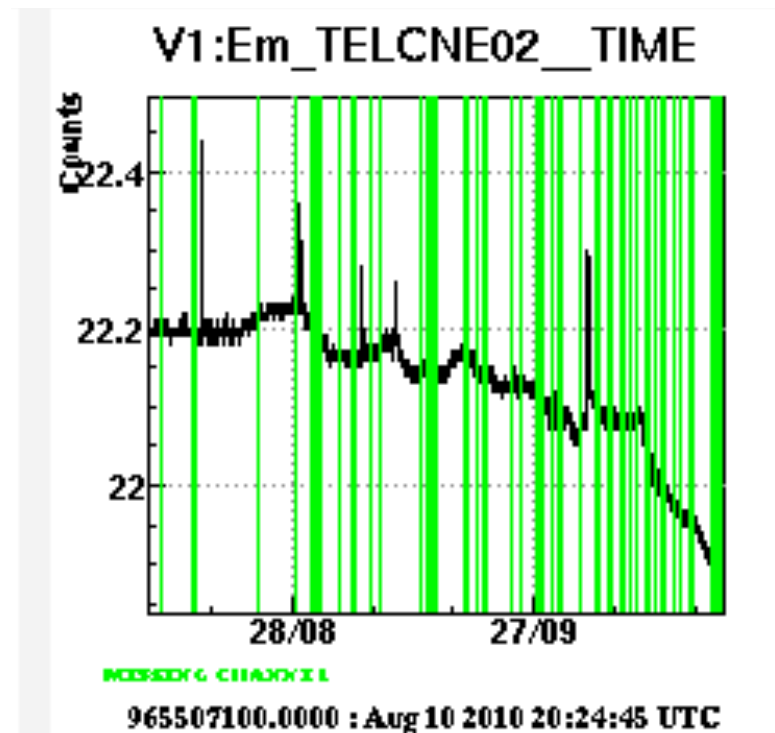
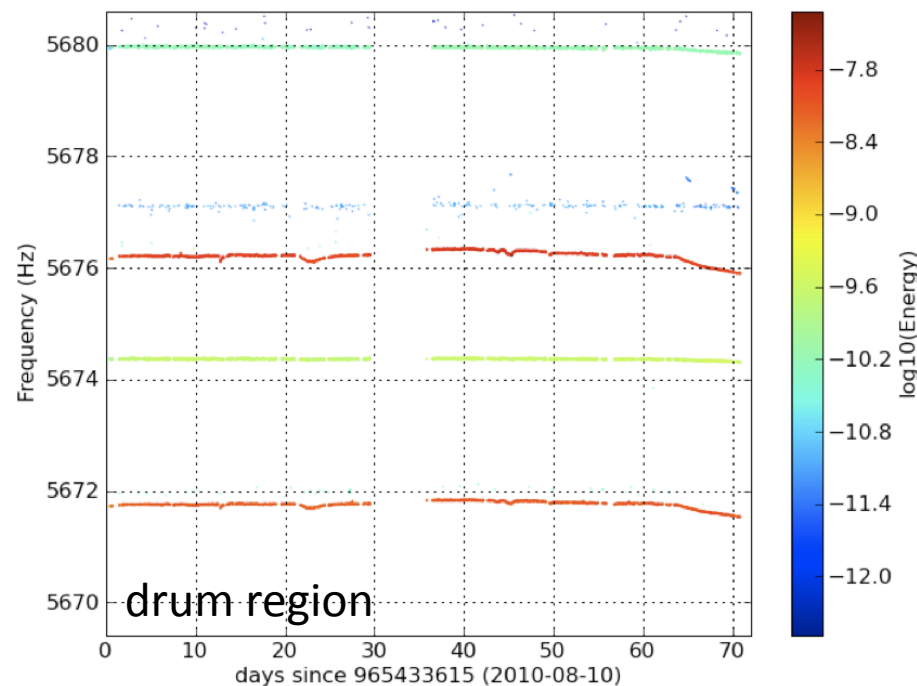
see VIR-0219A-11
VIR-NOT-ROM-1390-262
logbook entry 27158 (M. Punturo)

To identify correctly the resonances we use
the temperature correlation.

Temperature dependence

To follow:

- the line frequency in time we use the NoEMi tool, developed by the Pulsar and Noise groups;
- the temperature variation we use the sensor placed on the external wall of the towers.

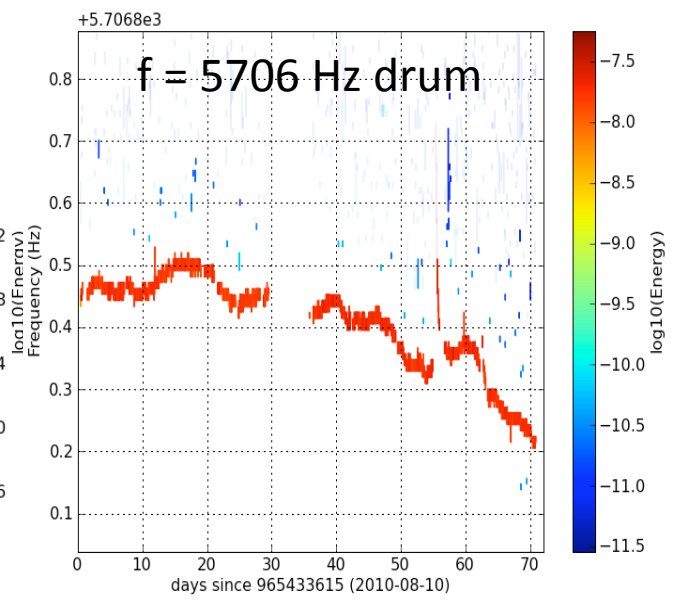
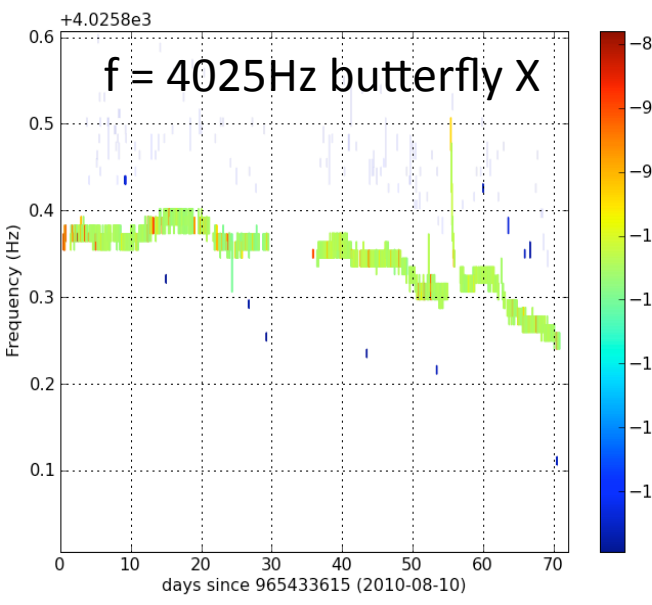
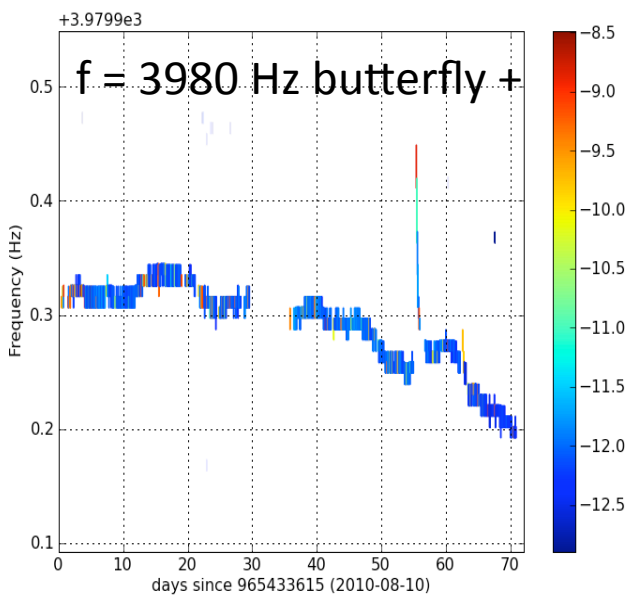
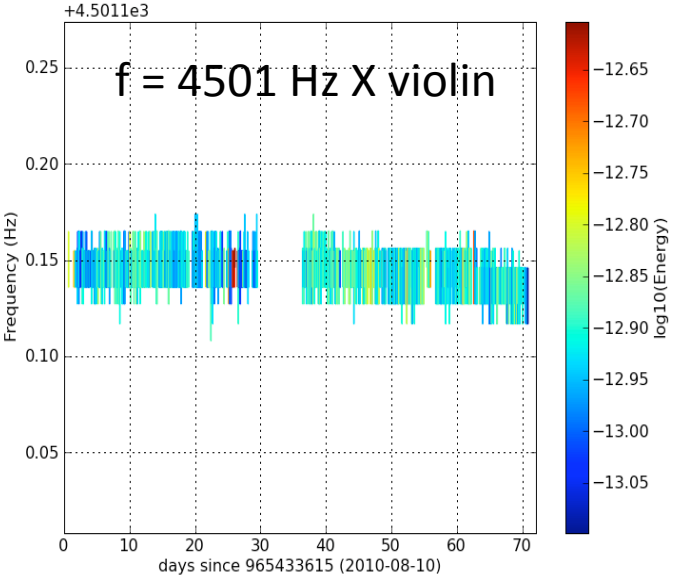
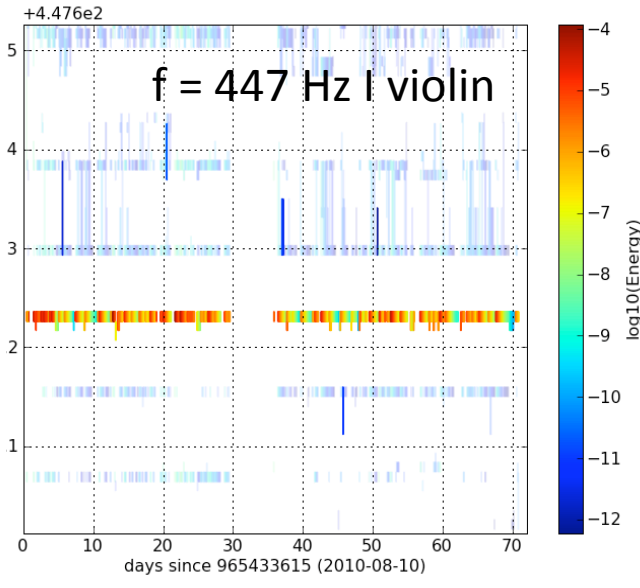
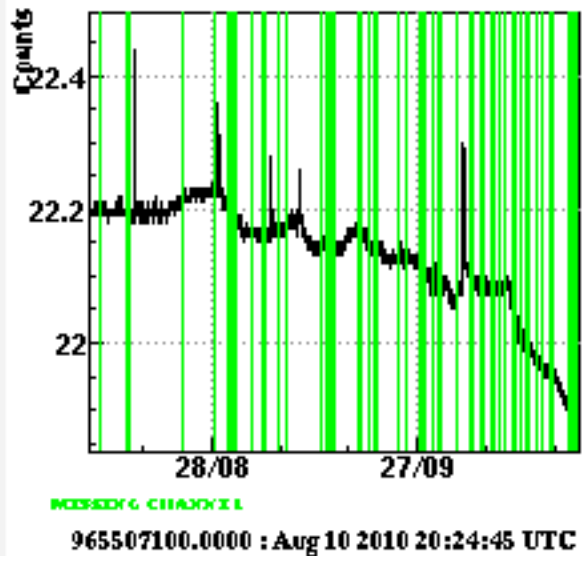


see Colla, VIR-0091A-11

Temperature dependence: NE case

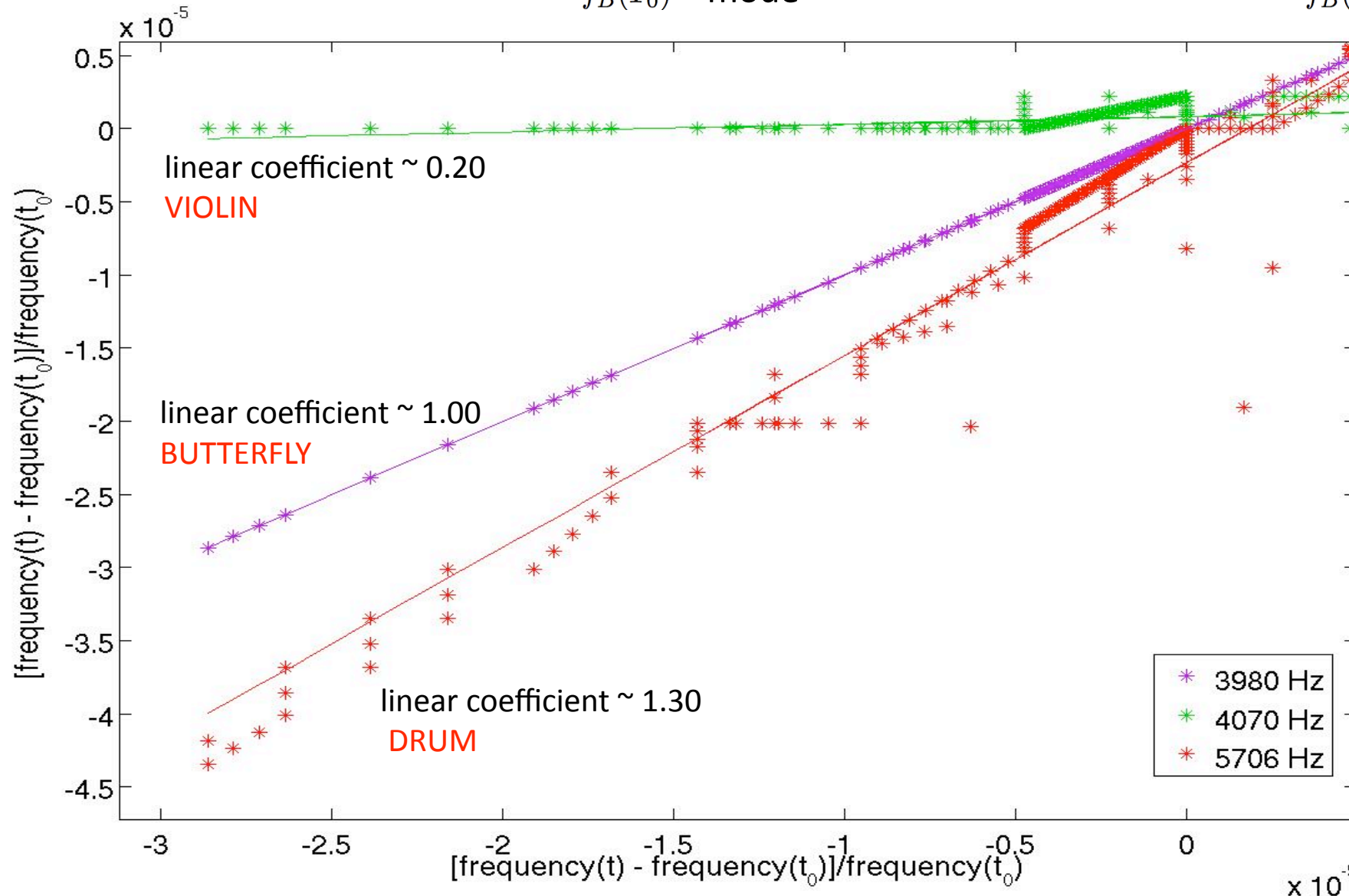
VSR3 data

V1:Em_TELCNE02__TIME



Comparing different modes behaviour

We plot the quantity $\frac{f_B(T) - f_B(T_0)}{f_B(T_0)}$ mode in function of the $\frac{f_B(T) - f_B(T_0)}{f_B(T_0)}$ butt



Conclusion

- we measure the Quality Factor of all the internal resonances of the 4 towers;
- we use the temperature correlation to distinguish between different kind of modes (violins/bulk)
- we obtain Q values lower than the expected ones
- to understand the dissipation processes we need:
 - more simulations and models (see Puppo's and Tacca's talks)
 - more measurements (on the single dismounted payloads)

Temperature dependence (1)

The temperature dependence is contained in the Young Modulus and we can approximate that as:


$$E(T) = E_0 e^{\beta(T-T_0)}$$

For the violin modes:

$$f_{violin} = \sqrt{\frac{T}{\rho}} \frac{n}{2L} \left[1 + \frac{2}{L} \sqrt{\frac{I}{T}} \sqrt{E} \right]$$

For the bulk modes:

$$f_{bulk} = \frac{\alpha_{lm} \sqrt{E}}{\sqrt{(1 + A_{lm} \sigma)(1 - B_{lm} \sigma)}}$$

 f_1 first order correction

Temperature dependence (2)

Using the Taylor expansion at first order we obtain:

- for violin modes

$$R_V = \frac{f_V(T) - f_V(T_0)}{f_V(T_0)} = \frac{f_1 \sqrt{E_0}}{1 + f_1 \sqrt{E_0}} \beta (T - T_0)$$

- for the bulk modes

$$R_B = \frac{f_B(T) - f_B(T_0)}{f_B(T_0)} = \frac{\beta}{2} (T - T_0)$$

$f_1 \ll 1$

If we compute the ratio R between different modes:

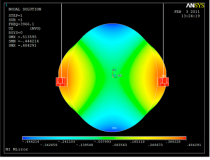
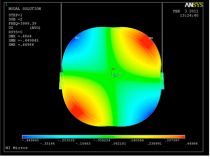
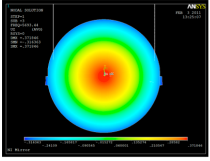
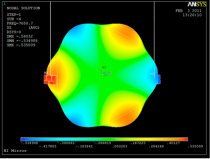
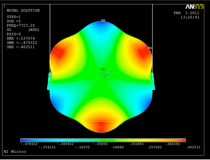
• bulk modes (butterfly or drum) →

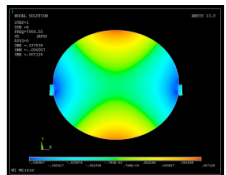
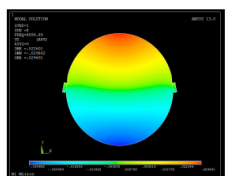
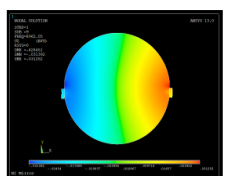
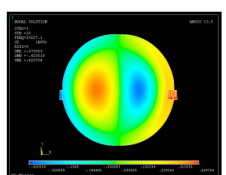
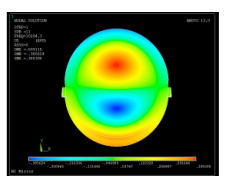
$$R_B(m) / R_B(n) \approx 1$$

• a violin mode and bulk mode →

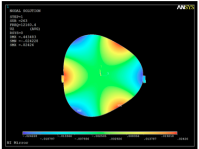
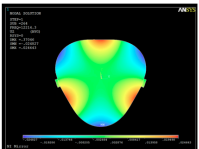
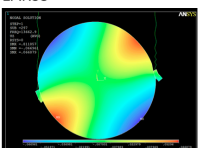
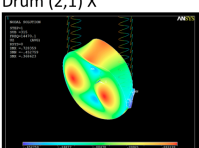
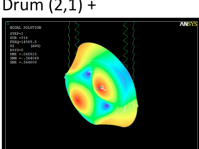
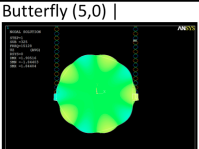
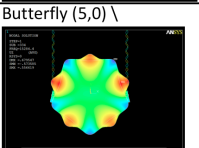
$$R_V / R_B(n) < 1$$

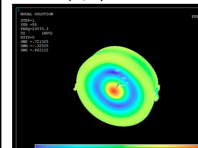
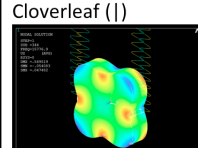
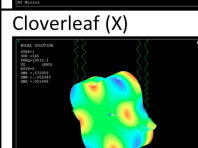
Bulk Mode zoology (1)

Mirror	NI Freq [sym] Q (1e6)	WI Freq [sym] Q (1e6)	NE Freq [sym] Q (1e6)	WE Freq [sym] Q (1e6)
Butterfly (2,0) X 	3964.22Hz [3965.9 Hz] .571	3936.1 15.2	4025->4032 2	4014.6->4018.2 3.6
Butterfly (2,0) + 	3996.7 Hz [3999.2Hz] 12	3969.6 24.3	3980->3986 8	3969.1->3972 13.5
Drum (0,1) 	56751.5-5676 Hz [5689.1 Hz] .34-3	5642 0.04	5707->5719 3	5693->5700 1.72
Butterfly (3,0) + 	7641.27 Hz [7650.7 Hz] .944	7606.3 1.71	7761->7773 2.34	7653->7660 Hz 0.05
Butterfly (3,0) X 	7710.2 Hz [7723.2 Hz] 5.12	7679.9 10.4	7667->7678 6.45	7745->7752 Hz

Egg X 	8022 Hz [7956 Hz] 6.98	8028.9 Hz 27.2		
Ears h 	8926.1 Hz [8897.9 Hz] 1.65	8934.1 Hz 2.15	8899	8895.5 3.36
Ears v 	8984.7 Hz [8959.1 Hz] 2.54	8992 Hz 7	8867.4	9081.7 3.64
Drum (1,1) I 	10191 Hz [10222.0 Hz] 0.798	10165.0 1.57	10331.0	10245 Hz 0.08
Drum (1,1) - 	10323 Hz [10289.0 Hz] .593	10335.0 1.79	10387.0	10313.0 1.64

Bulk Mode zoology (2)

EGG3 	[12160 Hz]			12288 Hz
EGG4 	[12214 Hz]			
EAR33 	13669 Hz [13663 Hz]			13639 Hz
Drum (2,1) X 	14344 Hz [14470 Hz]	14262 Hz		
Drum (2,1) + 	14519 Hz [14684 Hz]	14511 Hz 0.21	14382	14524 Hz 7
Butterfly (5,0) 	15066 Hz [15128 Hz]	15007 Hz 1.46		
Butterfly (5,0) \ 	15223 Hz [15284 Hz] 0.234	15178 Hz 0.14	15209	15183 Hz 2.2

Drum (0,2) 	15673.9 Hz [15726 Hz] 0.205	15659.0 Hz .192	15773	15763 Hz 1.5
Cloverleaf () 	15791.0 Hz [15777 Hz] 0.08			
Cloverleaf (X) 	15898.0 Hz [15833 Hz]			