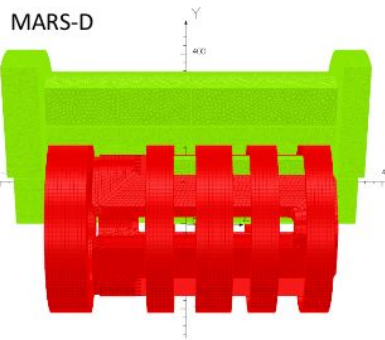
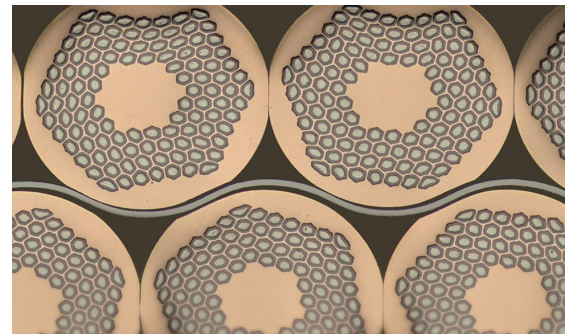
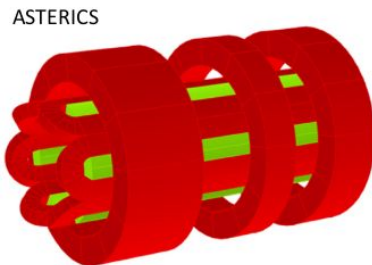


Session: Magnetic Systems for Future ECRIS



Session Agenda

	Topic	Speaker	Talk (minutes)
2:30 PM - 2:35 PM	Introduction	Janilee Benitez	5
2:35 PM - 2:50 PM	FECR - Update	Lianting Sun	15
2:50 PM - 3:05 PM	45 GHz MARS - Update	Janilee Benitez	15
3:05 PM - 3:30 PM	Beyond 45 GHz	Paolo Ferracin	25
3:30 PM	Discussion - Lessons Learned	All	60



MARS

MARS-D

Janilee Benitez

Production of Intense Beams and Highly Charged Ions

April 8, 2025

ECR Development at the 88

1st Generation ECR
1983

Max B-Field: 0.4T

Frequencies: 6.4GHz

Max Power: 0.6kW

2nd Generation AECR-U
1996

Max B-Field: 1.7T

Frequencies: 10, 14GHz

Max Power: 2.6kW

3rd Generation VENUS
2004, 2008 for operations

Max B-Field: 4.0T

Frequencies: 18, 28GHz

Max Power: 12kW

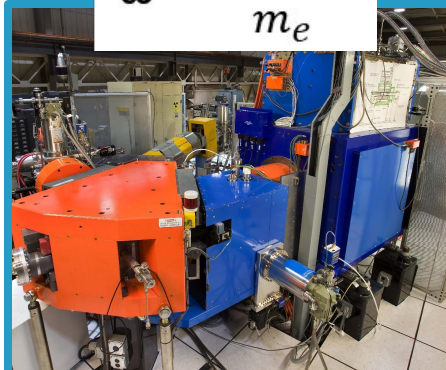
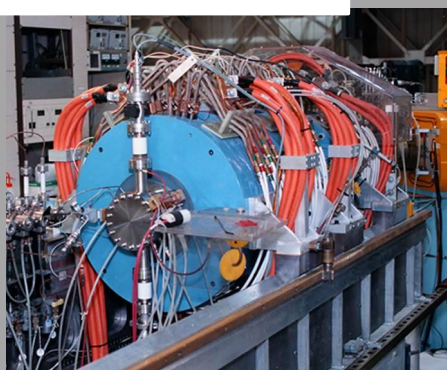
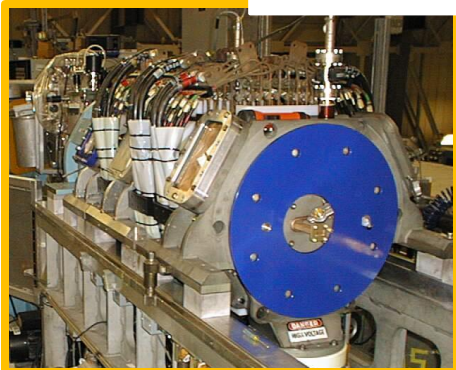
4th Generation MARS-D

Max B-Field ~ 6T

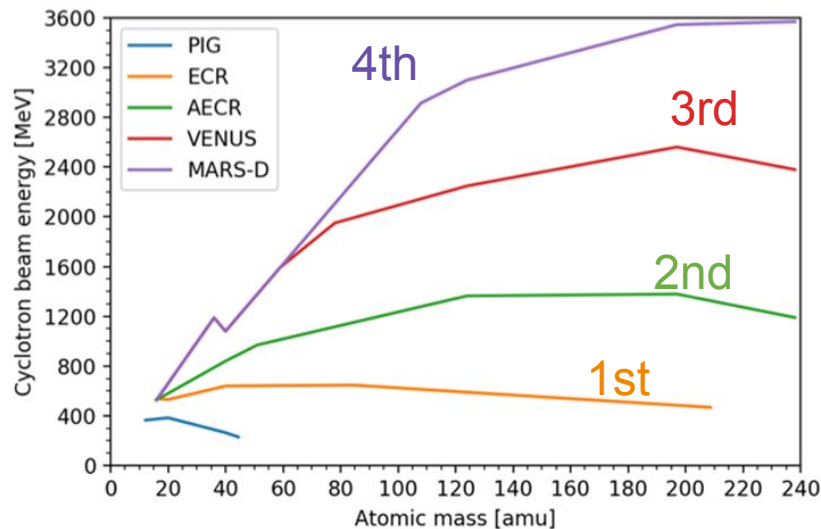
Max Frequency: 45GHz

Beam Intensity $\propto \omega^2$

$$\omega = \frac{e \cdot B_{ECR}}{m_e}$$

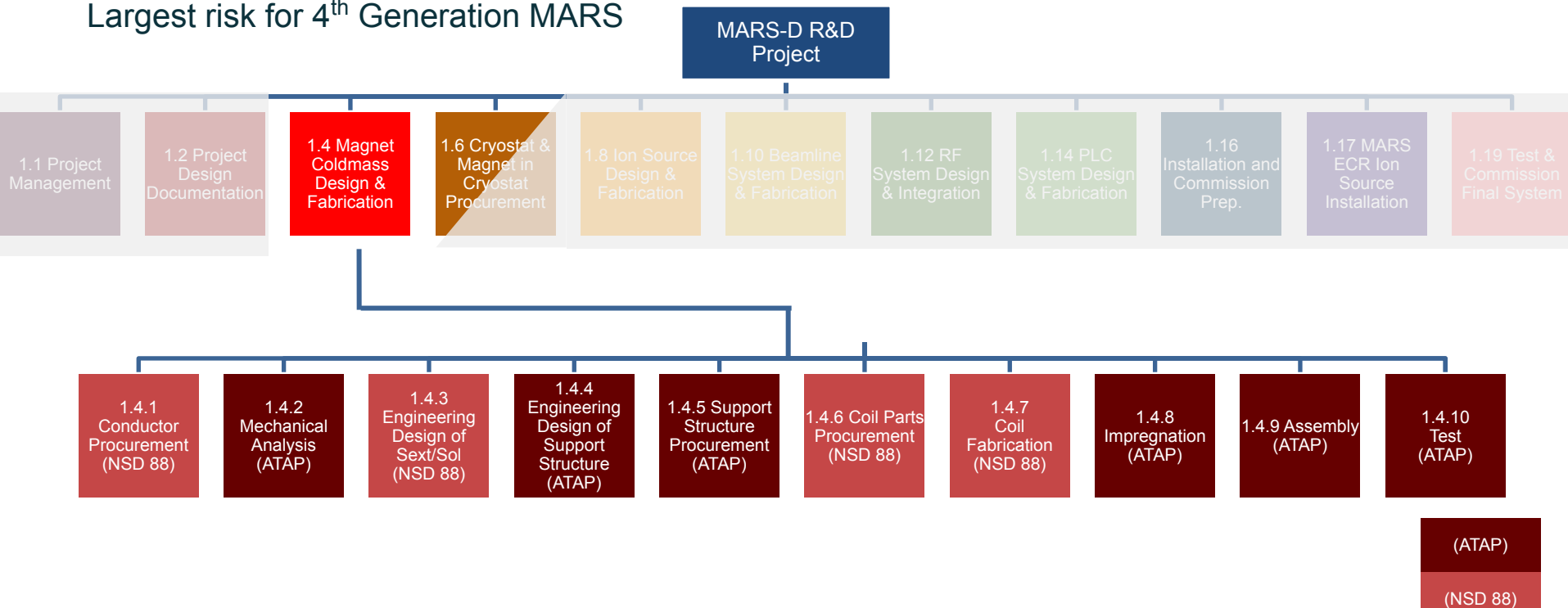


4th Generation 45 GHz MARS-D will produce higher intensities and higher charge states, leading to higher energy beam

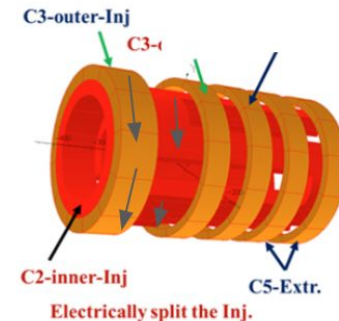
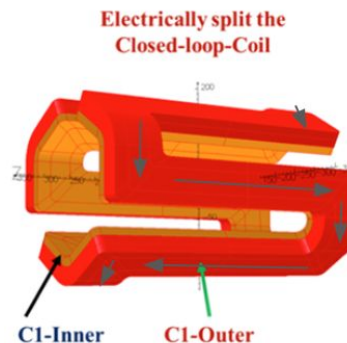
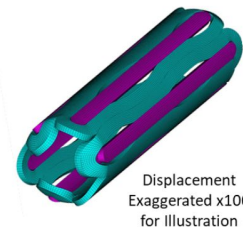


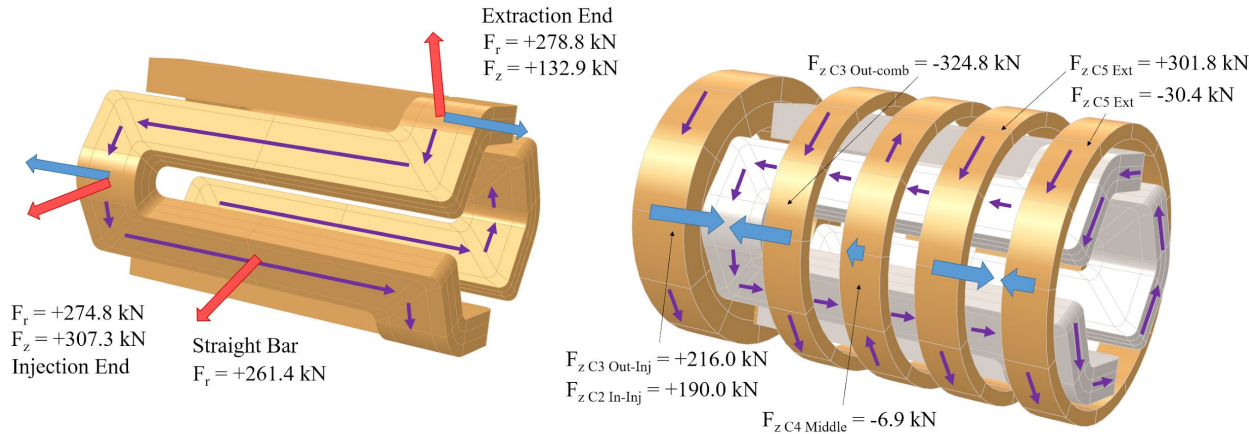
$$E = K \frac{q^2}{m}$$

- DOE funded winding of the coldmass (sextupole + solenoids) & cryostat design through an FOAs
- Largest risk for 4th Generation MARS

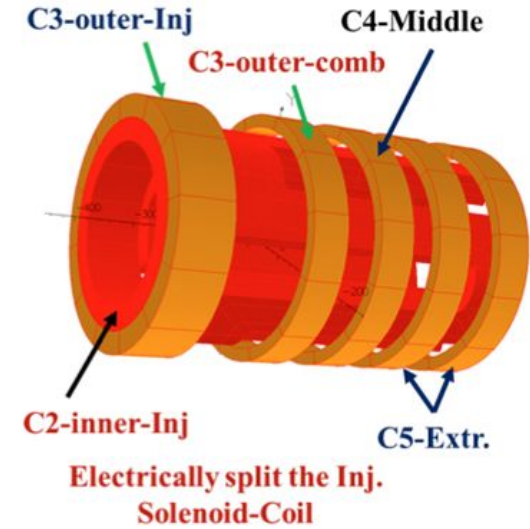
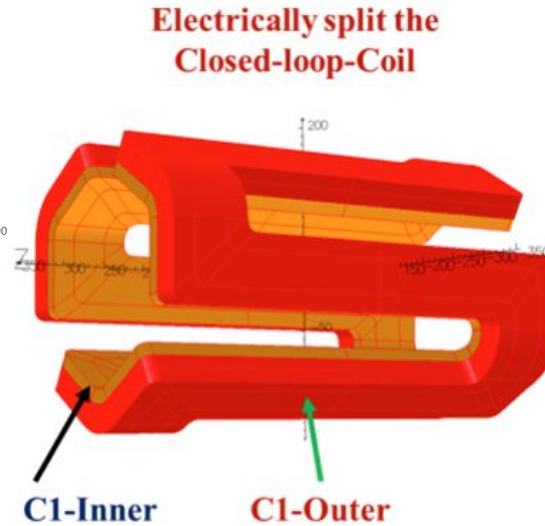
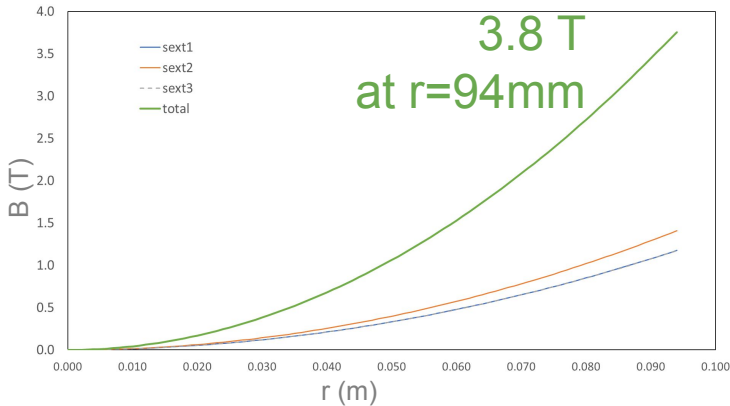
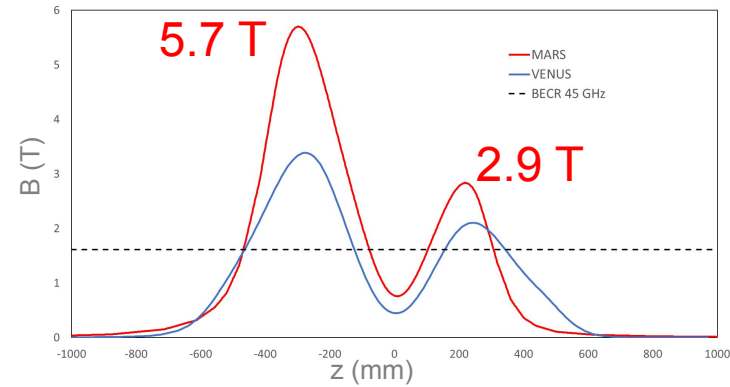


- 3rd generation VENUS uses NbTi in conventional structure
- 4th generation Nb₃Sn in conventional structure difficult to clamp
- 4th generation MARS-D allows continued use of NbTi
 - Optimized geometry provides 50% greater fields





- Close-loop coil provides radial + solenoid field
- Simpler Lorentz force distribution
- Higher field in hexagon "Corners"
- Complex and labor-intensive winding



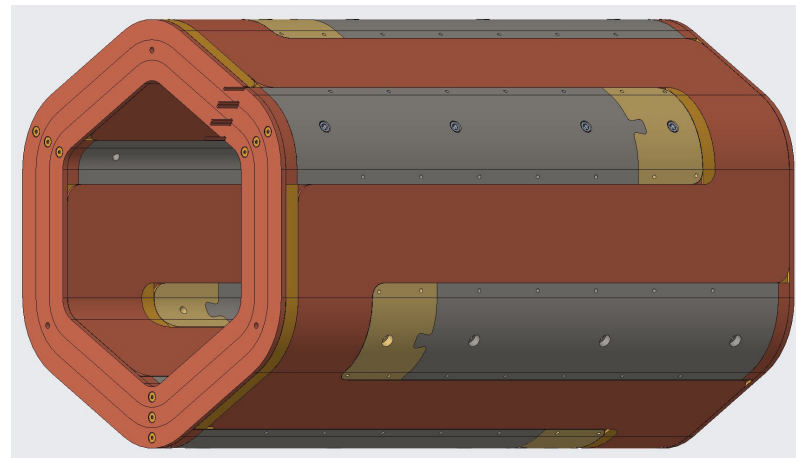
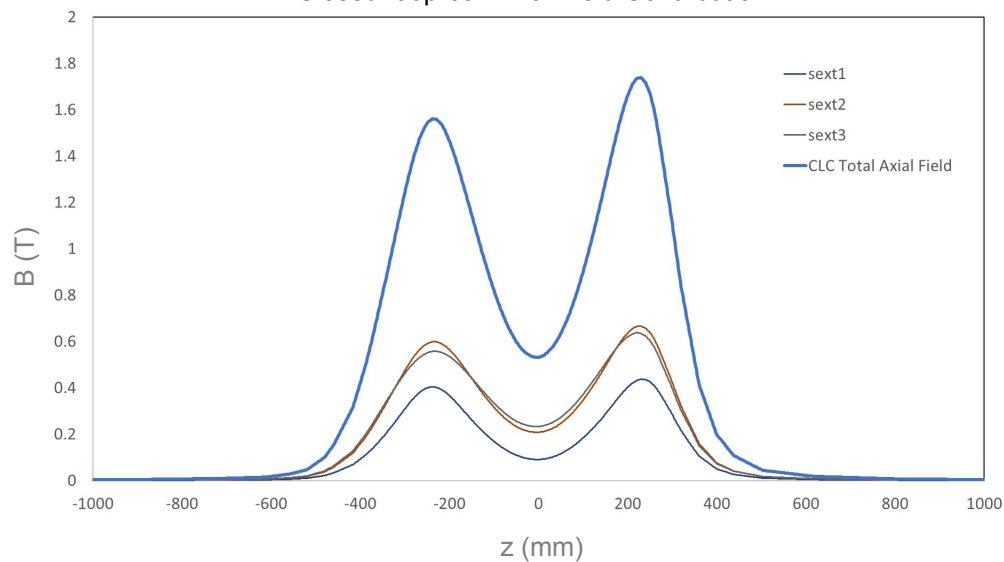
MARS-D Specifications*		
	Closed-loop coil	Solenoid
Conductor size (mm ²)	1.45 x 0.71	1.91 x 1.23
Copper ratio	1.3	1.4
Conductor length (km)	5.6	10.9
Load line (%)	88.6	83.3
Stored energy (kJ)	560	



* Y. Yang *et al.*, "Design Margin Comparison of a Sextupole-in-Solenoid and a Closed-Loop-Coil Type Nb-Ti Superconducting ECR Magnets," in *IEEE Transactions on Applied Superconductivity*, vol. 35, no. 5, pp. 1-5, Aug. 2025, Art no. 4100605, doi: 10.1109/TASC.2025.3527961.

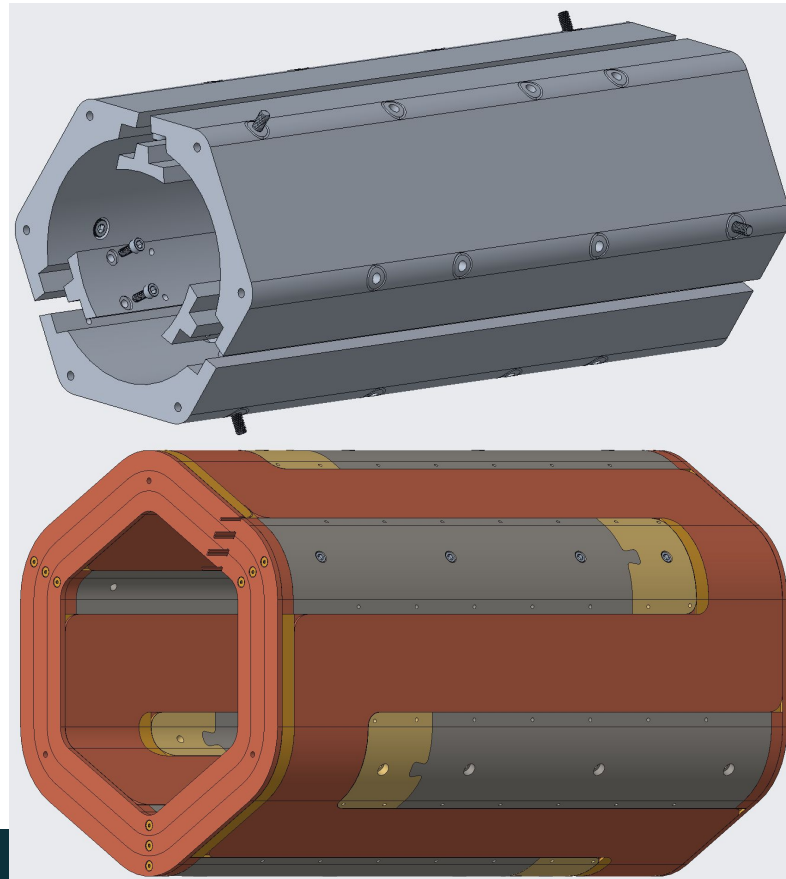
Closed-loop-Coil Structure

Closed-loop-coil Axial Field Contribution



Coil Structure

- The coil is wound on a removable mandrel (to maximize the use of the magnetic field)
- Divide the sextupole coil into 3 coil layers. (optimized field with different currents)
- Each coil layer has 8 wire-layers. (24 total layers)
- Each wire-layer has maximum 64 turns of SC wire.



4 layer NbTi Test Coil:

1. Pre-overbending

- a. bend tests showed no broken wires
 - i. R12.5 mm 90° bend at the easy way
 - ii. R20.0 mm 120° bend the hard way

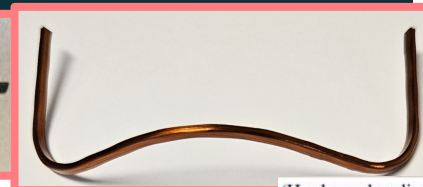
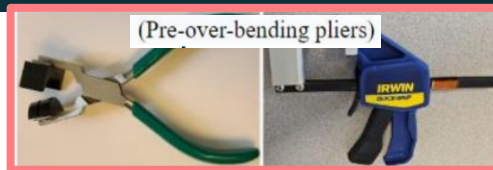
2. Winding Procedures

3. Impregnation

- a. CTD-101K epoxy in vacuum at 135 °C
- b. Cold test 2 cycles to 77K
 - i. Found changes in superglue, minimize
 - ii. Epoxy ok

4. Removable Mandrel

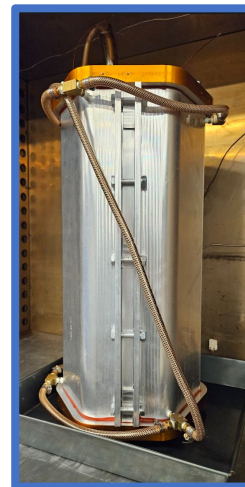
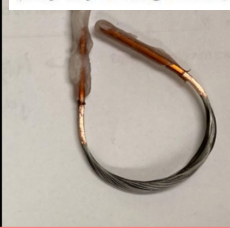
- a. Mold release to facilitate demolding



(Hard way bending R12.5 mm)



(Easy way bending R8 mm)

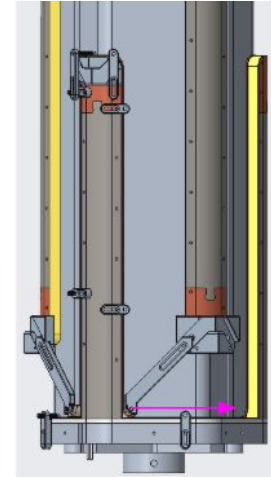
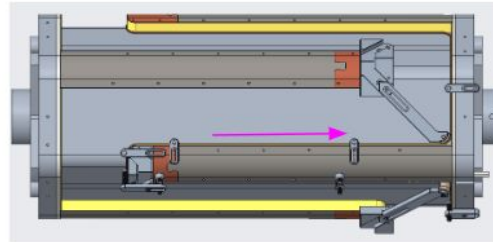
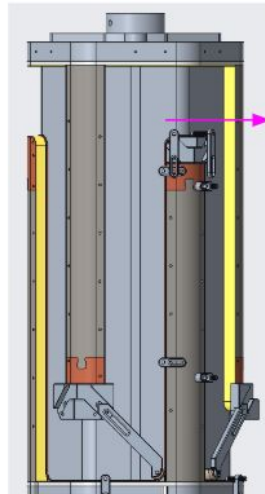
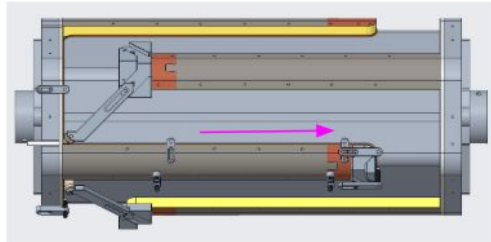


Winding Procedure



Winding Procedure

Starting



Maximum wire tension 5 kg

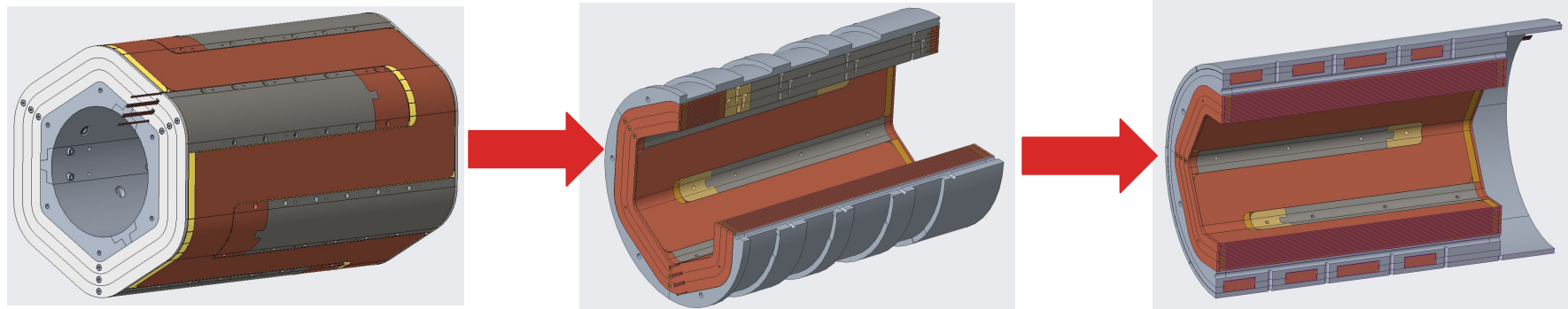
Current & Next Steps

Each turn ~ 45 minutes to 1 hour
Each layer ~ 2.5 weeks

Closed-loop coil is $\frac{2}{3}$ complete

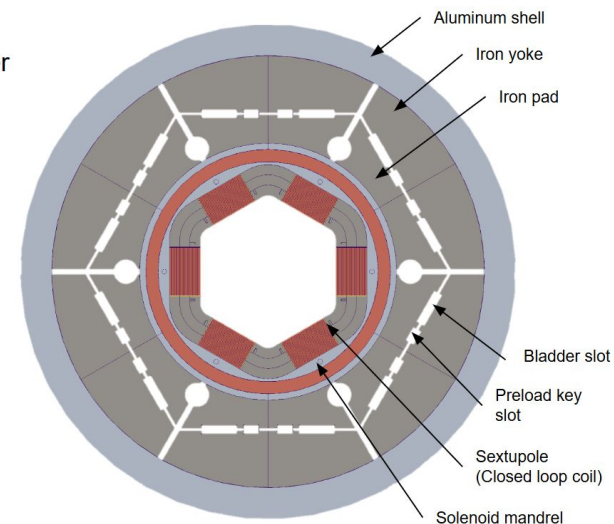
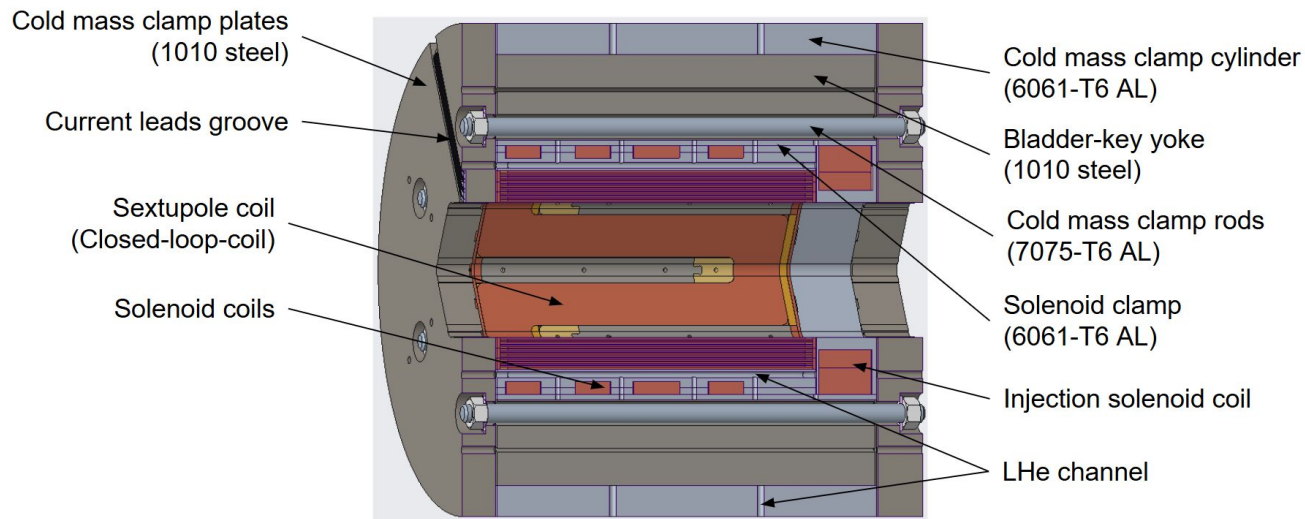
100% this summer



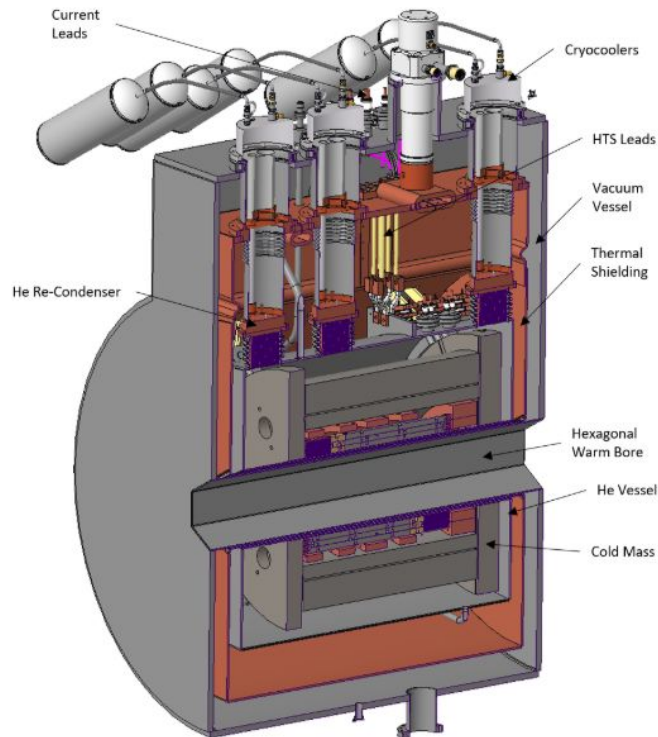


- Divide the solenoid mandrel into **3 sections**, alignment and assembly using **pins** and **shrink-fit reinforcement rings**
- **No gap** between the sextupole coil and the solenoid mandrels, CNC machine enclosures
- one-time impregnation
- After cool down from RT to 4.2K, the solenoid mandrel will shrink more than the sextupole coil, ~0.46 mm.

Cold Mass Structure

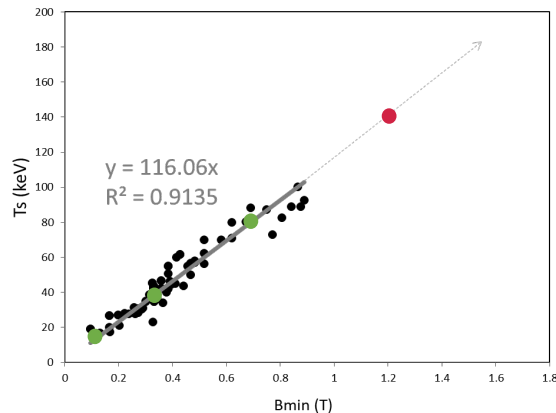


Cryostat Design



- **1 PT Cryocoolers. AL330**
 - 135W at 40K
 - Thermal shielding
 - RT Leads
- **4 PT Cryocoolers. PT450**
 - 60 W at 45K. First Stage
 - HTS
 - Thermal shielding
 - 5 W at 4.2K. Second Stage
 - Low temperature superconductors.
- **Static load: ~2-3W**

Credit: Li Wang
& Lianrong Xu



Impacts:
 Personnel safety
 Cryostat design
 Plasma chamber design

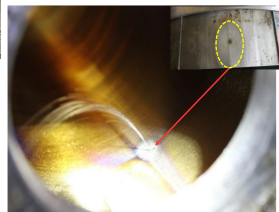
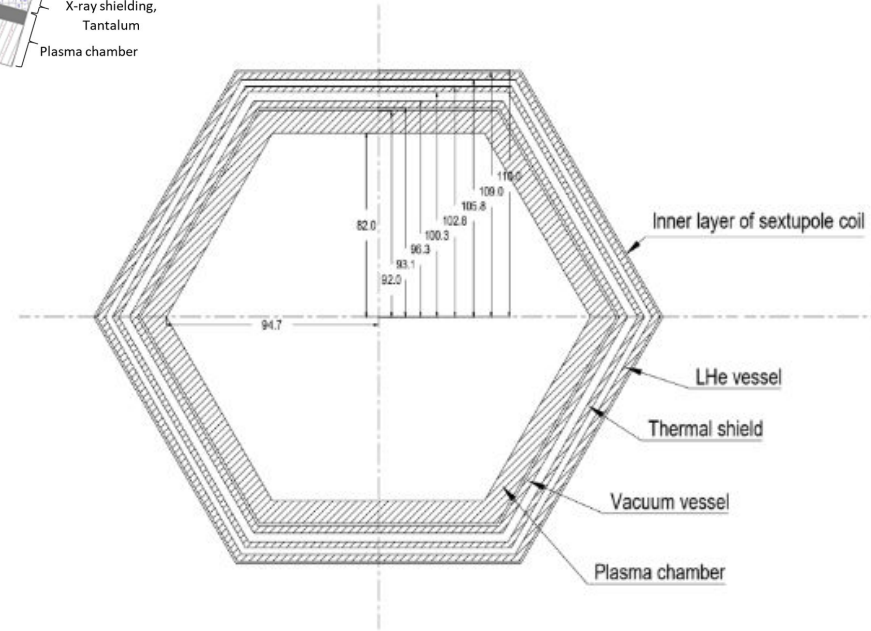
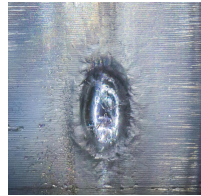
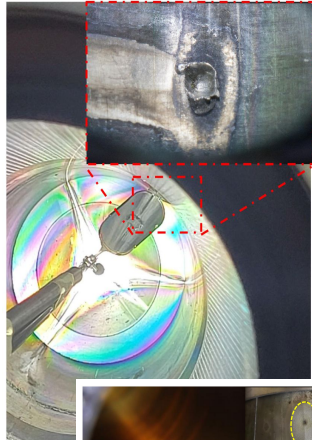
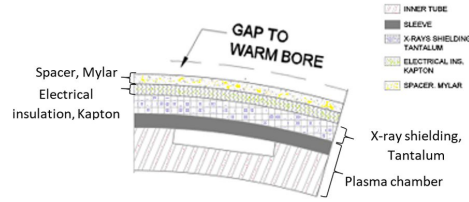
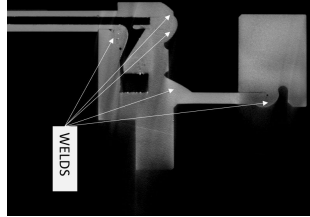
We expect 4th Generation MARS to have much higher electron temperatures!

Scaling Law:

$$B_{min} = 0.5 - 0.8B_{ECR}$$

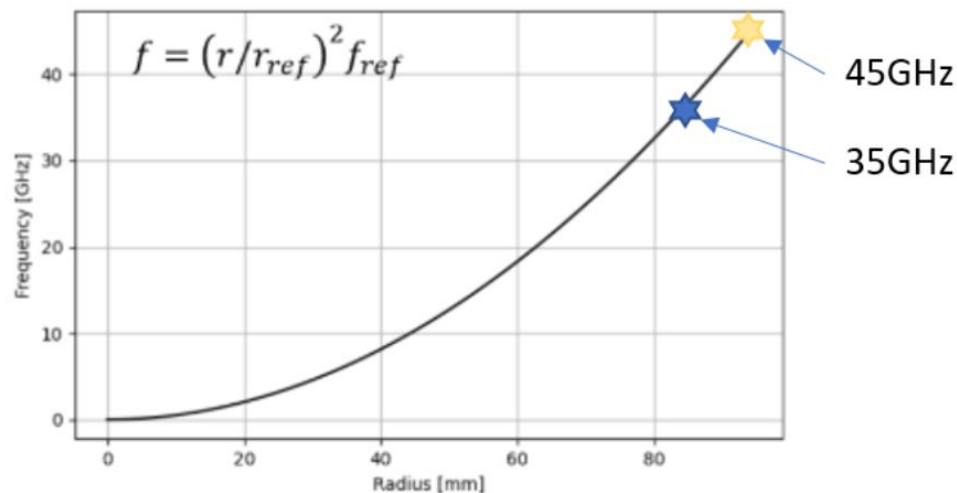
Generation	ω (GHz)	$^{16}\text{O}^{6+}$	B_{ECR} (T)	B_{min} (T)	T_s (keV)
1st (ECR)	6.4 GHz	45	0.23	0.1-0.18	20 keV
2nd (AECE)	14 GHz	800	0.50	0.2-0.4	35 keV
3rd (VENUS)	28 GHz	4,750	1.0	0.5-0.8	80 keV
4th (MARS)	45 GHz	-	1.6	0.5-1.2	140 keV

MARS Challenges



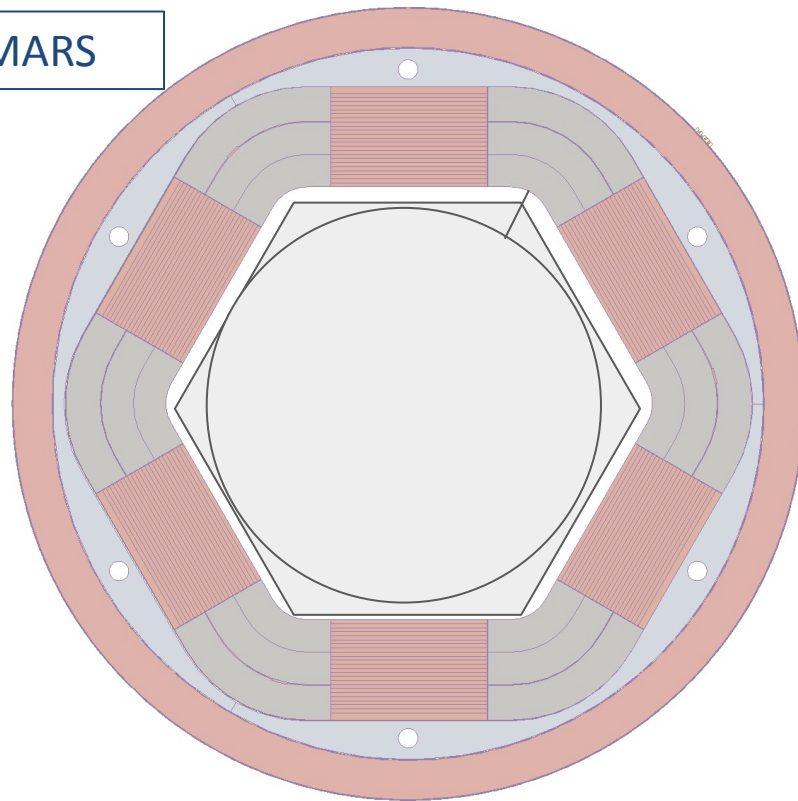
MARS Challenges

- Hexagonal chamber:
 - $B_r = 3.01 \text{ T}$ at 94 mm $\rightarrow$ 45 GHz
- Circular chamber:
 - $B_r = 2.34 \text{ T}$ at $r_{ref} = 82 \text{ mm}$
 - Frequency: 35 GHz



Credit: Ye Yang

MARS



Thank you!

Discussion

Availability of high frequency, high power gyrotrons?

Safety considerations for in-air 45 GHz transport (no waveguides).

Scaling laws and expected heat load into cryostat?

Timeline for long enough cables for HTSC source. Can we use HTSC leads?

Other issues to consider?