

## Elettra Sincrotrone Trieste



## Improving long-term stability and 1/f amplitude noise using pilot-tone compensation technique in Beam Position Monitors

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G. Brajnik, 29/10/2024



- Introduction
- Pilot tone compensation technique
- eBPM system at Elettra
- Noise considerations
- Results and conclusions





- Beam induces EM field on pickups
- Information is encoded in signal amplitude (AM)

 $a(t) = A\cos(2\pi f_{RF}t)$ 

Amplitude signals mapped into positions by DoS equation

$$x = K_{\chi} \frac{(A+D) - (B+C)}{A+B+C+D}$$

Resolution target for 4<sup>th</sup> gen. lightsources (ppm/bit/SNR):

 $\frac{\delta A}{A} \approx \frac{2\sigma_x}{K_x} \rightarrow \quad \text{~~100 nm resolution over 10 mm scale factor: 20 ppm} \\ 94 \text{ dB of SNR} - 16 \text{~~real" bits} - BW \text{~~10/20 kHz}$ 

 Calibration/compensation is needed to discriminate between real beam movements and electronics' drifts

 $\rightarrow$  Possible techniques: switching matrix, <u>pilot tone</u>

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### Pilot tone: implementation by Elettra

- A fixed sinusoidal tone (*pilot*) is added to the original signal coming from the beam (*carrier*)
- The 4 channels use the same tone as reference
- The pilot tone frequency has to fall near the carrier one without interfering with the latter

Typical spectrum of a eBPM button plus the pilot tone: Spaces between revolution harmonics are valid locations





## **Pilot tone:** implementation by Elettra

Hypothesis: every channel variation affects in the same way both carrier and pilot



Compensated position in classical Difference-over-Sum (DoS) equation "Deconvolution" between carrier and pilot





### Advantages of this technique:

- Compensation of cables
  - Possible when the tone is injected near to the pick-ups
- No need for thermoregulation
  - Thermal drifts are the same for carrier and pilot
- Reduced current dependence
  - Pilot can be also used as a "dithering" with low beam currents
- The pilot position returns continuously a diagnostic of the system status
  - Hardware faults can be identified
- No switching harmonics compared to switching matrix



## Block diagram of Elettra 2.0 eBPM system

- Result of a partnership signed between Elettra and Instrumentation Technologies
- Modular system: analog front end plus digitizer





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#### Elettra Sincrotrone Pilot tone front end (PTFE)



Trieste

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## **Digital board (DAQ)**

- Board based on Intel Arria 10 SoC FPGA with ARM processor inside
- Onboard memory: 8 GB of DDR3 (buffers, postmortem, collection of raw adc data, etc)
- Connectivity: control system ethernet plus 6 SFP+ capable up to 10 Gb/s (feedbacks)
- Mezzanine support: two FMC HPC slots with 400 pins each
- Double DDC converter in FPGA (carrier + pilot) for each channel
- Position calculation at different data rates (TbT, 100 kHz, 10 kHz, 10 Hz, etc)









### Temperature compensation (ADC, PTFE)



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- Drifts reduction by a factor of 4 (from ~200 to ~50 nm)
- No thermoregulation initial heating of the electronics



Compensated vs Uncompensated positions

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UNI EN ISO 9001:201 UNUSO 45001:2018

![](_page_13_Picture_0.jpeg)

- Can pilot tone compensation be useful not only in mitigating long-term drifts, but also in noise reduction?
- Answer: yes, if we are talking about 1/f noise (flicker)
- PSD of 1/f noise is not flat, there's correlation between consecutive samples
- Techniques for 1/f noise cancellation: modulation (lock-in amps, sigma-delta ADCs)

![](_page_13_Figure_5.jpeg)

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![](_page_14_Picture_0.jpeg)

- Test setup: RF gen + splitter (emulate a stable beam)
- Significant 1/f noise on our BPM system
- Pilot tone compensation can cancel it out
  - Good correlation between amplitude variations due to 1/f on pilot and carrier
- Noise source: coming from ADCs?
  - No difference w & w/o front end  $\rightarrow$  PTFE has white noise
  - No difference at different frequencies  $\rightarrow$  not related to sampling clock jitter
  - Probably caused by sample & hold stage inside ADC

![](_page_14_Picture_9.jpeg)

![](_page_15_Picture_0.jpeg)

- Easier to refer to noise on calculated positions
- graphs: cumulative sum of PSD vs frequency
- Example with white noise (flat PSD integrated over bandwidth):

![](_page_15_Figure_4.jpeg)

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![](_page_16_Picture_0.jpeg)

![](_page_16_Figure_1.jpeg)

Positions @ 100 kS/s

Red trace: white noise reference of 3nm/sqrt(Hz)

Blue trace: carrier Orange trace: pilot Green trace: compensated position

### Noise of non-compensated position higher than expected

Compensated position follows theoretical prediction

![](_page_16_Picture_7.jpeg)

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![](_page_17_Picture_0.jpeg)

![](_page_17_Figure_1.jpeg)

Positions @ 1.156 MS/s - TbT

Expanding bandwidth helps to understand the phenomena

Noise PSD is flat above 7/10 kHz

Noise on pilot positions is lower due to enhanced filtering (reduced BW)

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![](_page_18_Picture_0.jpeg)

![](_page_18_Figure_1.jpeg)

![](_page_18_Figure_2.jpeg)

Fit 1/f noise (red trace): PSD:  $S(f) = \frac{k^2 F_c}{f} + k^2$ , k = 3nm/sqrt(Hz) Corner frequency: about 10 kHz

![](_page_18_Picture_4.jpeg)

![](_page_19_Picture_0.jpeg)

### Integration in current machine

- Currently, a complete section of Elettra storage ring (8 BPMs) is working with the new eBPM system since August '24
  - No issues reported
  - Extreme flexibility due to in-house developed firmware
  - Continuous (1 kHz) tune measurements thanks to higher data rate
  - Control system and Global Orbit Feedback integration thanks to DPDK framework (feedback freq. 10 kHz, bpm acq. freq. 1.15 MHz)

![](_page_19_Picture_7.jpeg)

![](_page_19_Picture_8.jpeg)

![](_page_20_Picture_0.jpeg)

- Pilot tone is a useful technique to enhance both long-term stability and 1/f noise performance
- The new system is working well on the present machine
- Fine-tuning enhancements ongoing
- Target: increase reliability and usability for a easier deployment on the new machine

![](_page_20_Picture_5.jpeg)

![](_page_21_Picture_0.jpeg)

# Thank you!

![](_page_21_Picture_2.jpeg)

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