

# Measurements of the PSB LLRF multi-harmonic beam loading compensation system

## Mariangela Marchi, Simon Albright, Diego Barrientos, Marco Niccolini



**LLRF Topical Workshop on** Timing, Synchronization, Measurements and Calibration 28-30 October 2024<br>INFN-LNF, Frascati





## **Contents**

### CONTEXT

- •PSB Finemet System
- •Beam Stability
- •Finemet Cavity Servo-Loops

### HARDWARE CHARACTERIZATION

- •Test-Stand measurements
- •Comparison with previous measurements

### MODELING

- •Resonator model
- •Beam-Based measurements observations

## CONCLUSIONS

29/10/2024 LLRF Topical Workshop | M.Marchi 2







## CONTEXT - CERN ACCELERATOR COMPLEX



## CONTEXT - PSB FINEMET SYSTEM

Ring4

Ring3

Ring<sub>2</sub>

Ring1

### 29/10/2024 LLRF Topical Workshop | M.Marchi 4

## Proton Synchrotron Booster



- 4 super-posed rings
- Accelerating from 160 MeV to 1.4 - 2 GeV
- Large revolution frequency sweep: 0.994 kHz-1.81 MHz (factor of 2 increase)







- 3 sectors per ring (S5, S7, S13)
- 12 cells per sector ⇒ 36 cells per ring
- Max  $VPK = 8$  kV per sector
- Multi-Harmonic operation ⇒ operational flexibility

## Modular RF System: Finemet Magnetic Alloy (MA) wide-band cavities









# CONTEXT - BEAM STABILITY

### Wide-Band response of the Finemet loaded cells require actions on many harmonics



## Longitudinal impedance:

- Mainly resistive in the operational range
- $f_{RF} = h \times f_{REV}$  (  $h = 1,...,16$ )
- Fast RF feedback applied

At carrier frequency: Stationary beam loading Side-Bands at fREV: transient beam loading Side-Bands at synchrotron frequency : f<sub>REV</sub> with phase modulation at fs

 $PSB: f_{RF} = f_{REV} \rightarrow \text{Narrow-Band Multi-Harmonic}$ feedback wit fREV side-bands treated individually

General: induced voltage by a beam undergoing longitudinal oscillations has power at the discrete frequencies:

Further impedance reduction on the revolution frequency lines by **long delay feedback**

$$
f = f_{RF} + nf_{REV} + mf_S
$$



# CONTEXT - BEAM STABILITY

Longitudinal stability dependent on LLRF system configuration.

**→ Characterization of the LLRF for** model implementation in macroparticle simulator BLonD (Beam Longitudinal Dynamics) [2].

One example: When servo-loops active observation of instabilities in Single RF operation starting at low intensities.

### PSB 2 GeV cycle









## One servo-loop per each revolution harmonic:







### One servo-loop per each revolution harmonic:



*Finemet cavity*











## HARDWARE CHARACTERIZATION - TEST-STAND MEASUREMENTS

### **Measurement setup[3][4]**





## Measurements on a Test-Stand of the LLRF cavity control system isolated from the cavity.

### Configuration:

- Cavity emulated by cable
- Induced voltage to be compensated emulated by excitation given by the VNA
- VNA Port 1 gives the excitation
- VNA Port 2 detects the excitation
- Cavity loops suppress the excitation close to the revolution harmonic
- Set-Point to 0



## HARDWARE CHARACTERIZATION - TEST-STAND MEASUREMENTS



Harmonic 8 at 1 MHz (Flat-Bottom): • Attenuation: ~ - 60, - 65 dB •-3 dB Band-Width: 7.67 kHz

Harmonic 8 at 1.81 MHz (Flat-Top): •Attenuation: ∼ -60 dB

•-3 dB Band-Width: 12.2 kHz

Harmonic 1 at 1 MHz (Flat-Bottom): •Attenuation: ∼ - 60, -65 dB •-3 dB Band-Width: 11.5 kHz

Harmonic 1 at 1.81 MHz (Flat-Top): • Attenuation: ~ - 55, -60 dB •-3 dB Band-Width: 16.4 kHz





## HARDWARE CHARACTERIZATION - TEST-STAND MEASUREMENTS

Evaluation of filter response in a frequency range around the resonant frequency spanning a fs of 2 kHz (pink span) and 6 multiples of it (blue span).





# HARDWARE CHARACTERIZATION - COMPARISON

Same setup but LLRF connected to the cavity and



## HARDWARE CHARACTERIZATION - COMPARISON

## Total Transfer Function with external VNA and closed loop response measured with the Embedded VNA.[5]

![](_page_13_Figure_3.jpeg)

![](_page_13_Figure_7.jpeg)

![](_page_13_Picture_8.jpeg)

The embedded Network Analyser sweeps the the RF Drive signal itself. ➔Action of the loop chain on the signal without the compensation 㱺 Pass-band response

![](_page_14_Picture_10.jpeg)

![](_page_14_Picture_0.jpeg)

## HARDWARE CHARACTERIZATION - MODELING

![](_page_14_Figure_2.jpeg)

**→Fit with Resonator** model based on test-stand measurements:

For simulation purposes: need a model reliably describing the filter action to be used to benchmark measurements and validate impedance model.

Not accurate enough to describe the filter steadystate transfer function.

**Working on a better fit and beam-based measurements to gain information about transient beam loading behaviour.**

![](_page_15_Figure_7.jpeg)

### Single RF Double RF

![](_page_15_Picture_9.jpeg)

![](_page_15_Picture_0.jpeg)

## HARDWARE CHARACTERIZATION - BEAM - BASED MEASUREMENTS

Measurements in Single RF at injection (160 MeV): transient state. Scans in intensity to evaluate beam loading through the demodulated I and Q components. Time needed at injection to compensate beam loading is inversely proportional to the -3 dB BW.

![](_page_15_Figure_3.jpeg)

- •PSB Finemet RF System introduces large broad-band longitudinal impedance
- •Fast and slow RF feedback action required to reduce beam loading effects
- •Unstable behaviour at low intensity happening in Closed-Loop and Single RF operation
- •LLRF modular cavity control system acting on multiples of the revolution frequency
- •TEST-STAND MEASUREMENTS
	- •Small effects of harmonics and frequencies on Transfer Function (TF) parameters
	- Consequential change in the TF at higher multiples of fs
- •INJECTION TRANSIENT MEASUREMENTS
	- •No effect from bunch length at *h = 1*
	- •Effect from peak current and bunch length at *h = 2*
- •MODELING
	- •Previous model does not accurately reproduce the steady-state behaviour
	- •Transient behaviour to be included

![](_page_16_Picture_22.jpeg)

![](_page_16_Picture_0.jpeg)

## CONCLUSIONS

![](_page_17_Picture_0.jpeg)

## References

•[4] M.E. Angoletta *et al.*, "Control and Operation of a Wideband RF System in CERN's PS Booster", in *Proc. 8th Int. Particle Accelerator Conf. (IPAC'17)*, Copenhagen, Denmark, May 2017, paper THPAB141, pp. 4050-4053,

- •[1] Courtesy of Mauro Paoluzzi, CERN
- •[2] H. Timko et al., Phys. Rev. Accel. Beams, vol. 26, 2023.
- •[3] Courtesy of Marco Niccolini, CERN
- ISBN: 978-3-95450-182-3.
- Proton Synchrotron Booster", in *Proc. IPAC'22*, Bangkok, Thailand, Jun. 2022, pp. 907-910.
- •[6] Courtesy of Diego Barrientos, CERN
- •[7] Courtesy of John C. Molendijk, CERN

•[5] D. Barrientos, S. C. P. Albright, M. E. Angoletta, A. Findlay, M. Jaussi, and J. C. Molendijk, "A New Beam Loading Compensation and Blowup Control System Using Multi-Harmonic Digital Feedback Loops in the CERN

29/10/2024 LLRF Topical Workshop | M.Marchi 18

![](_page_17_Picture_15.jpeg)

![](_page_17_Picture_16.jpeg)

![](_page_18_Picture_0.jpeg)

## Back-Up Slides

29/10/2024 LLRF Topical Workshop | M.Marchi 19

![](_page_18_Picture_5.jpeg)

![](_page_19_Picture_7.jpeg)

**ERN** 

## CONTEXT - FINEMET CAVITY SERVO-LOOPS

 $N \approx 19$ **Setppint**  $M \Rightarrow 20$  $M = 20$ [6]m = 20<br>FS Swing -> 4.25 ms<br>Per cavity FS = 8kV \* sqrt(2)  $C42$ C18 SoftRFSwitch  $H1-typ = 8kV$  total H T-typ = 6k V total<br>H 1 / cav = 8/3 kV ~FS/4<br>8kV-step -> 4.25 / 4 ~1 ms. **IQres WrSP MHz100** SP\_I (18:0) lout (18:0) SP\_lin (18:0)  $SP_0$  (18:0) Qout (18:0)  $C24$   $T \rightarrow C2$ SP\_Q (18:0) c25 0 rownd cy testl (18:0) testQ (18:0) loopCtrl:<br>0 = No Drive<br>1 = Test Drive oopControl ( OpenLoop Demodulator 2 = Setpoint Drive (Open Loop) DSP\_RF\_Ena **DriveZero** 3 = Closed Loop  $C2$ control\_bypassDSPE na timOnWhileDSPOff timOnWhileDSPOff RF\_Rst control\_bypassTiming info\_timingOn  $RF\_Clk$ FirmTiming (31:0) firmTimSel\_on (12:8) TimingSel or vectorDeMod\_RdData (31:0) firmTimSel\_off(4:0) mTimingSel\_off vectorDeMod\_Addr (5:2) vectorDeMod\_RdDon RFOutO Range **RFDisByOOR** FOutOfRange RFDisByOOR **MAE R dD** vectorDeMod WrDone н. vectorDeMod\_WrData ( **CLoopPe** CLN otP ermFault VME Wr vectorDeMod\_RdMe vectorDeMod\_RdE rro **VMER dE** vectorDeMod\_WrMer vectorDeMod\_WrE rror **VMFWrF** RF\_CII 4 DSP48 **ADCAtt** RFin (15:0) l\_n (18:0) enableCIC  $Q_{n}$  (18:0) in k  $C26$ RateOut **Epixymy** ∧ f\_MO FrevM (31:0) Hxl (15:0)  $LO$   $HxQ (15:0)$ 많<mark>다\_Rs</mark><br>중  $N \geq 16$  $C<sub>21</sub>$ **IQres Cavity Rotate Control** WrCavRot cavRotCos (15:0) locCavRotCos (15:0) cavRotSin (15:0) locCavRotSin (15:0) **DspSample**  $N \Rightarrow 16$ C<sub>17</sub> **IQreg Loop Rotate Control** WrLoopRot loopRotCos (15:0) locLoopRotCos (15:0) loopRotSin (15:0) locLoopRotSin (15:0) RF\_Clk  $RF_Rst$  $N = > 16$ <br>C34  $\overline{\phantom{a}}$ VME Addr (7:2) VME WrData (31:

**VMERdMem** 

![](_page_19_Figure_5.jpeg)

![](_page_20_Figure_7.jpeg)

![](_page_20_Picture_8.jpeg)

![](_page_20_Picture_9.jpeg)

Electrical delay : < 1 us between LLRF and Finemet Field regulation using DSP with  $T = 10$  us Fixed frequency Clock with  $f_{fix}$  = 122.7 MHz

![](_page_20_Picture_0.jpeg)

# CONTEXT - FINEMET CAVITY SERVO-LOOPS

![](_page_20_Figure_3.jpeg)

![](_page_21_Picture_11.jpeg)

![](_page_21_Picture_12.jpeg)

![](_page_21_Figure_0.jpeg)

## HARDWARE CHARACTERIZATION - TEST-STAND MEASUREMENTS

- •Optimised span around each revolution harmonic: → Resolution Band-Width = 104 Hz
- •Excitation signal sweep time : 600 ms
- •Notch filter like frequency response

When the VNA sweep passes by the set revolution frequency the servoloop response is maximal and the RF drive output increases to compensate the emulated beam loading.

![](_page_21_Figure_2.jpeg)

![](_page_21_Picture_67.jpeg)

![](_page_22_Figure_5.jpeg)

![](_page_22_Picture_6.jpeg)

# HARDWARE CHARACTERIZATION - BEAM - BASED MEASUREMENTS

Measurements in Double RF at Flat-Top (1.4 GeV cycle): sector with accelerating RF off and servoloops not active. Static induced voltage.

![](_page_22_Figure_2.jpeg)