

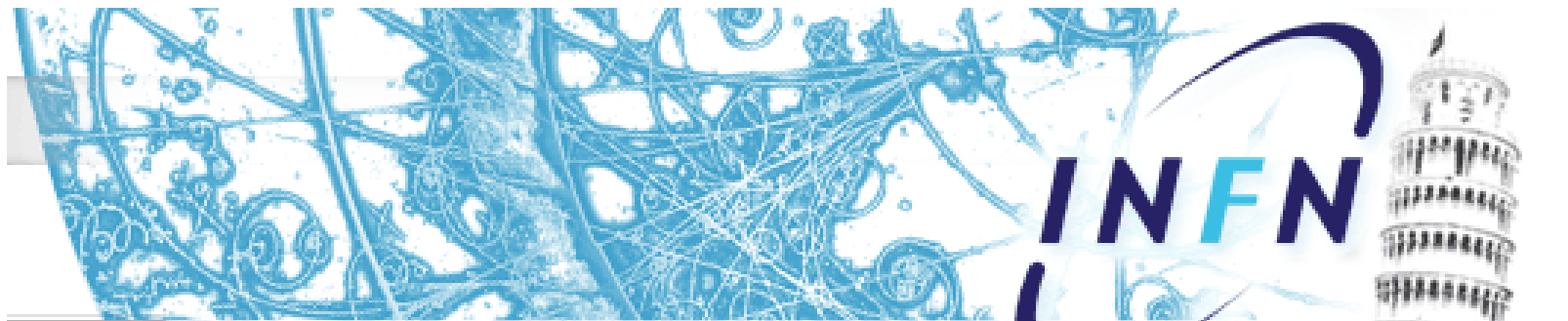


Update on SVT Mechanics

F. Bosi

INFN-Pisa

on behalf of the SuperB SVT Group





Outline



- SVT design on layer 1-5
- L0 StripleTs version
- L0 supports (MAPS version)
- I.R. general layout
- Conclusion



SVT L1-5 Layout design



Update on the L1-L5 design by London workshop :

- 1) defined L1-L5 modules dimensions
- 2) defined modules positions
- 3) defined gimbal ring positions
- 4) defined cooling ring position
 - this components definition has been usefull to QMUL to proceed on the design of C.F. supporting cones and Space-Frame
- 5) Moved L1-2 in outer z position respect BaBar position

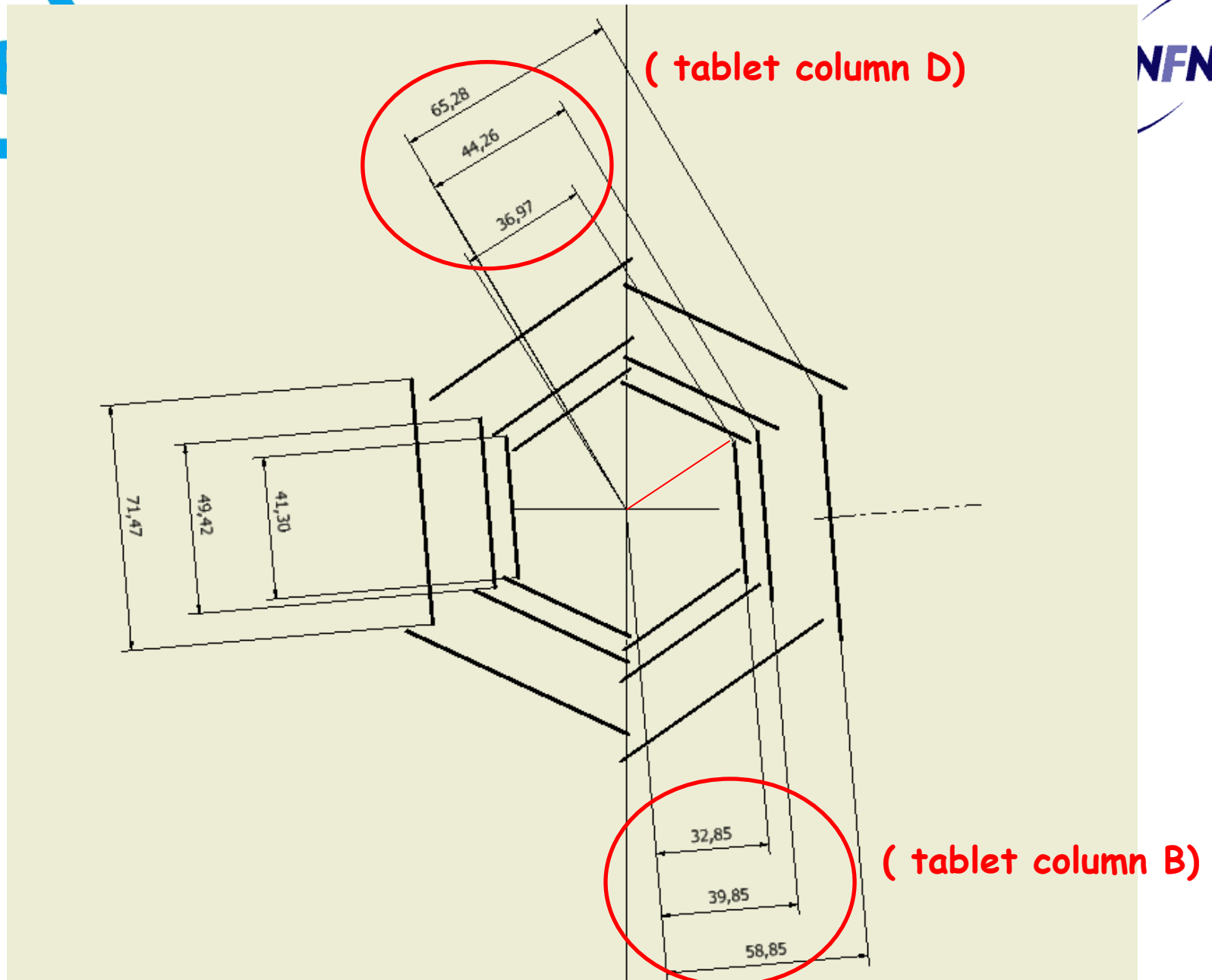
SVT - Dimensioni e copertura angolare sensori

| A | B | C | D | E | F | G | H | I | J | K | L | M | N | O |
|-------|--|---|--|---|--|--|---------------------------------|---|---|--|---|-------------------------|--|---|
| Layer | Radius piano y-z sensore barrel SuperB | Radius piano y-z punto estremo sensore wedge SuperB | Radius punto estremo laterale sensore SuperB | Lunghezza orizzontale sensore tangente cono 300 mrad SuperB | Lunghezza sensore barrel SuperB (tabella Londra) | Lunghezza totale sensore barrel SuperB | Lunghezza totale sensore SuperB | Lunghezza estensione sensore oltre 300 mrad SuperB column (G-E)/2 | Lunghezza estensione sensore oltre 350 mrad BaBar | Angolo interrettato nel punto ingombro estremo sensore con piano y-z (rad) | Angolo interrettato nel punto ingombro estremo laterale sensore (rad) | Shift Layer asse Z (mm) | Angolo interrettato nel punto ingombro estremo sensore con piano y-z+shift (rad) | Angolo interrettato ingombro fisico sensore estremo laterale +shift (rad) |
| 0 | 15,10 | - | 17,30 | 97,63 | - | 104,00 | 104,00 | 3,19 | - | 0,283 | 0,321 | 0 | - | - |
| 1 | 32,85 | - | 36,97 | 212,39 | 214,78 | 223,36 | 223,36 | 5,48 | 21,69 | 0,286 | 0,320 | +2 | 0,284 | 0,325 |
| 2 | 39,85 | - | 44,26 | 257,65 | 262,78 | 265,78 | 265,78 | 4,06 | 2,51 | 0,291 | 0,322 | -2 | 0,293 | 0,326 |
| 3 | 58,85 | - | 65,28 | 380,49 | 385,70 | 385,70 | 385,70 | 2,60 | 1,41 | 0,296 | 0,326 | 0 | - | - |
| 4A | 119,85 | 87,91 | 90,54 | 574,60 | 457,95 | 457,95 | 578,23 | 2,05 | 1,96 | 0,295 | 0,303 | +2 | 0,293 | 0,293 |
| 4B | 123,85 | 91,91 | 94,42 | 597,69 | 479,42 | 479,42 | 599,70 | 1,14 | 1,07 | 0,297 | 0,305 | +2 | 0,296 | 0,296 |
| 5A | 139,85 | 112,18 | 114,25 | 732,47 | 613,04 | 613,04 | 737,46 | 2,72 | 2,58 | 0,295 | 0,300 | -2 | 0,297 | 0,297 |
| 5B | 143,85 | 116,18 | 118,18 | 756,53 | 635,84 | 635,84 | 760,26 | 2,05 | 1,93 | 0,297 | 0,301 | -2 | 0,298 | 0,298 |

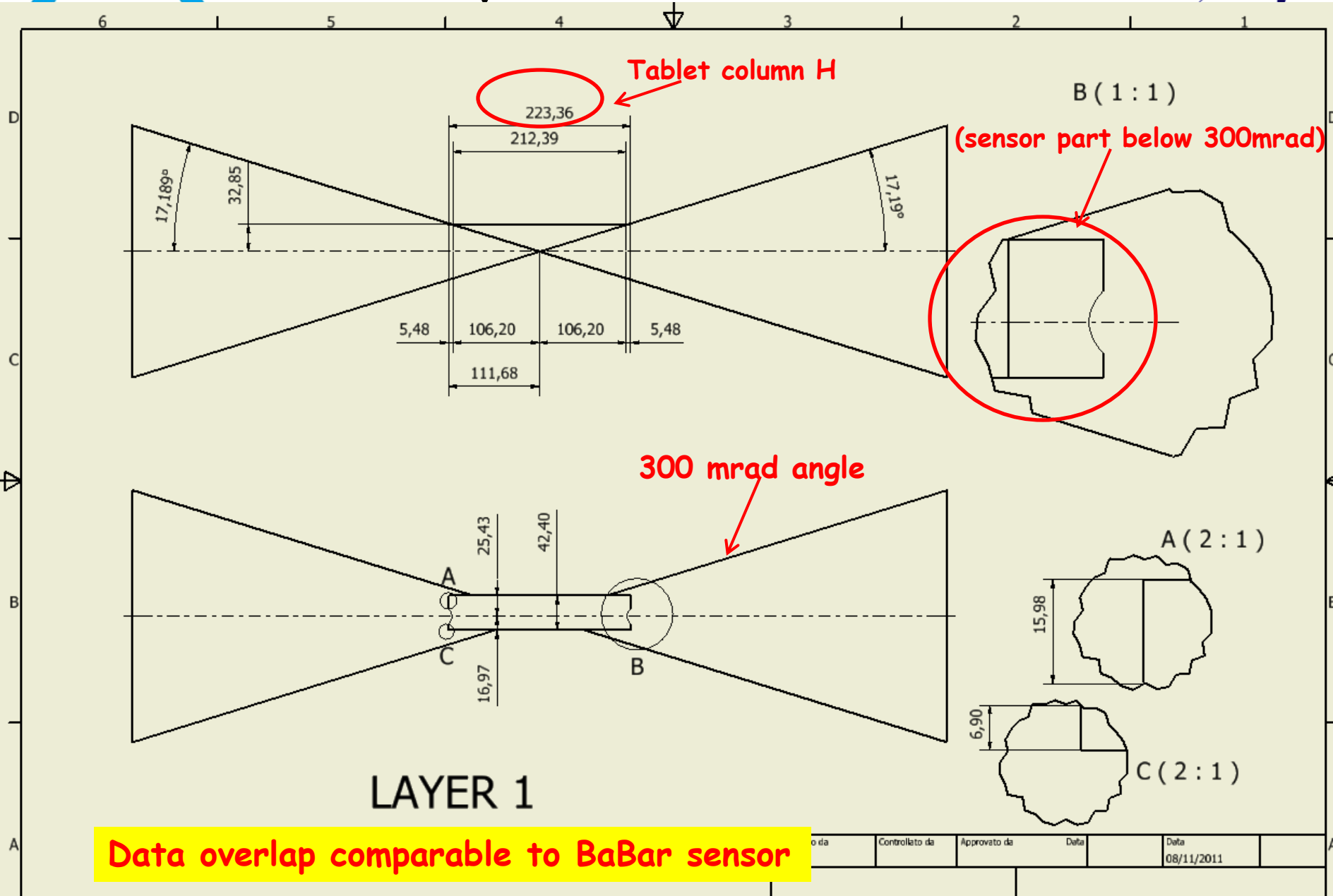
Tablet usefull for trieste group to fix **sensor** and **fanout** dimensions

Modules have sensor in symmetric position respect I.P. but are shifted along z direction to avoid middle dead space

Layer 1-2-3 module radius



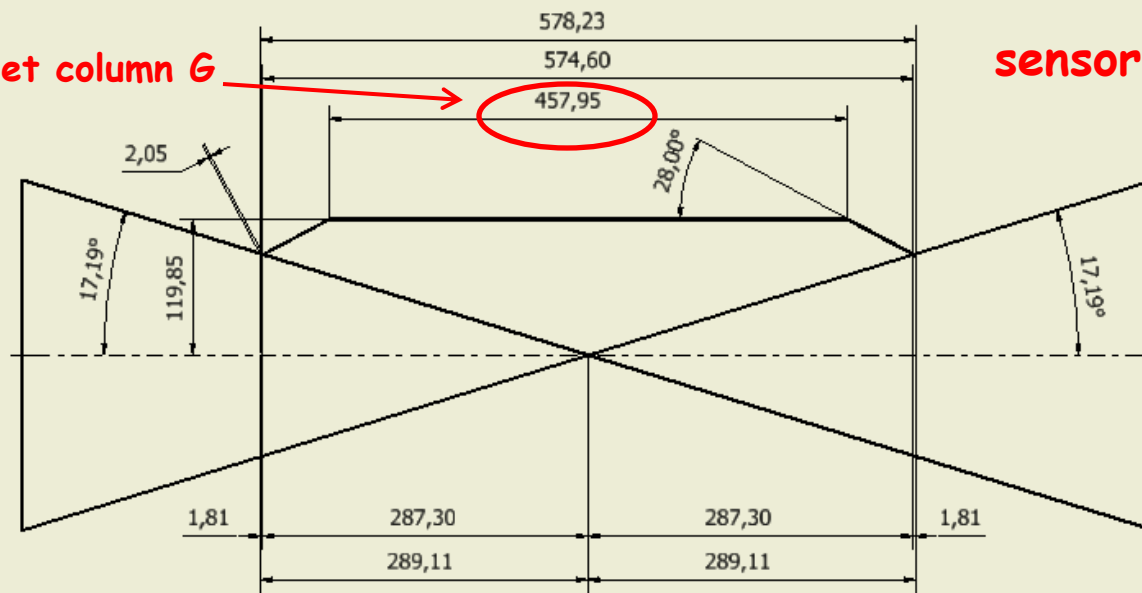
Layer 1 module



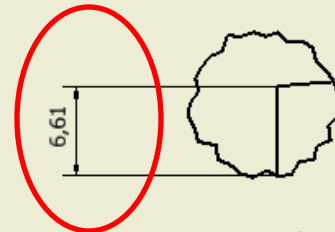
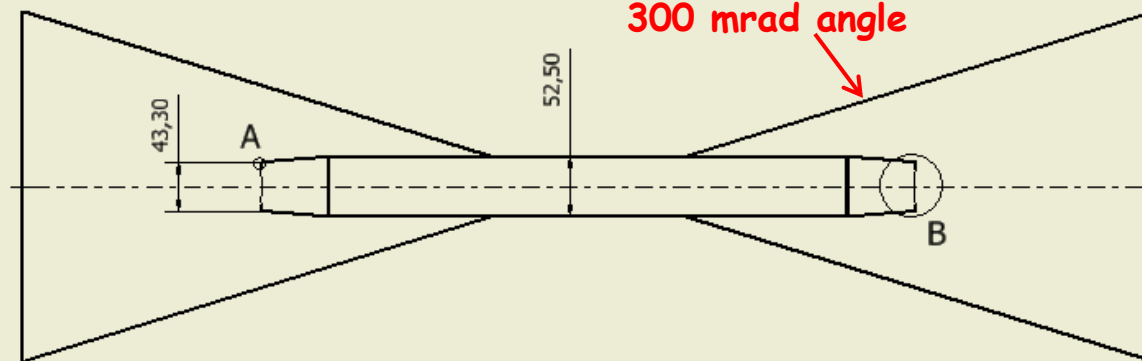
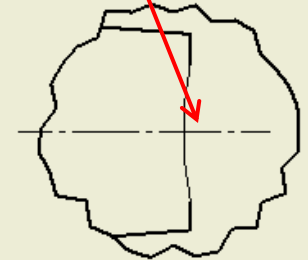
Layer 4 A module

Tablet column G

sensor part below 300mrad



B (1 : 1)



A (3 : 1)

LAYER 4A

Data overlap comparable to BaBar sensor

| | | | | |
|-----------------------------------|--------------|------|------------|--------|
| Controllato da | Approvato da | Data | Data | |
| | | | 08/11/2011 | |
| Assieme_modulo_4A_overlap_300mrad | | | Edizione | Foglio |
| | | | 1 | 1 |

Tablet column H

104,00

97,63

17,189°

15,10

17,189°

3,19

48,81

48,81

52,00

52,00

A (2:1)

13,90

300 mrad acceptance angle

8,45

B

A

C

13,90

5,45

B (4:1)

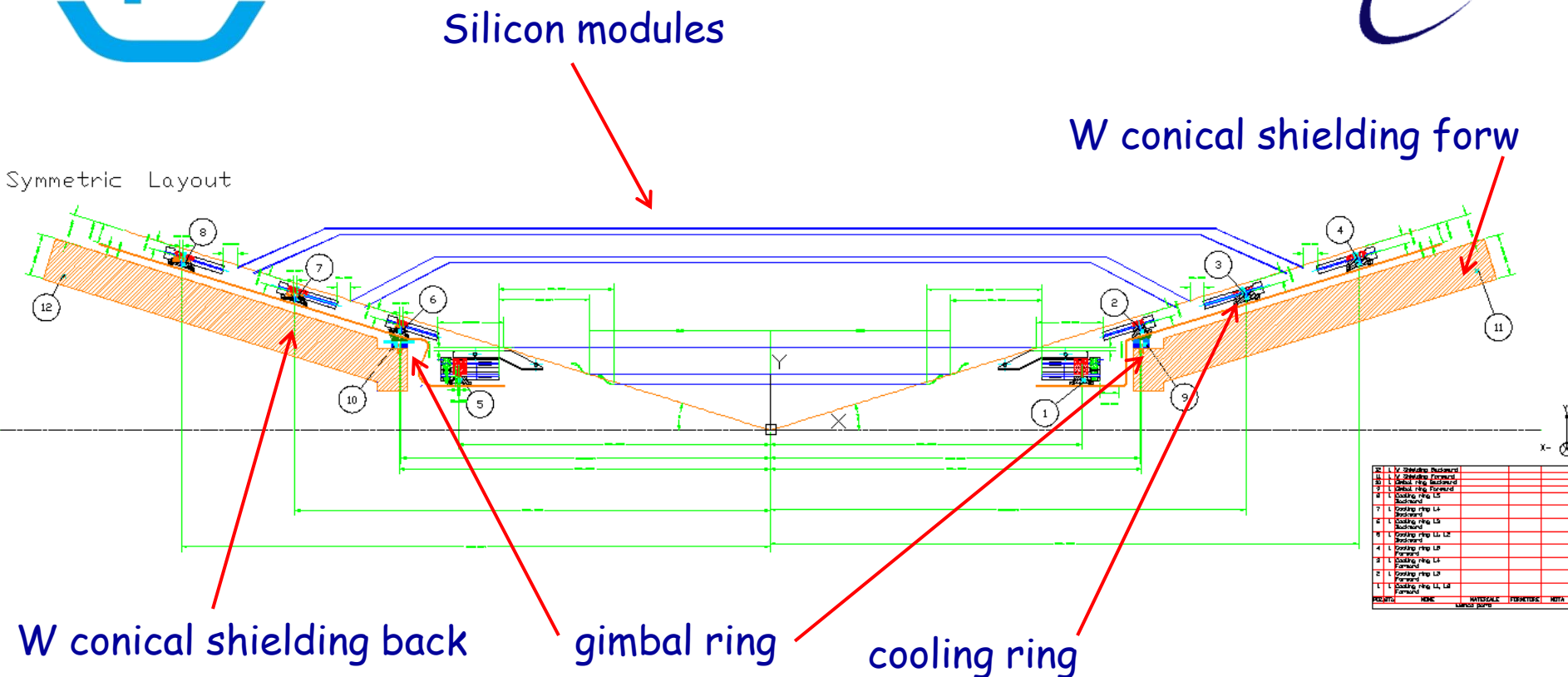
3,38

0,50

C (4:1)

LAYER 0

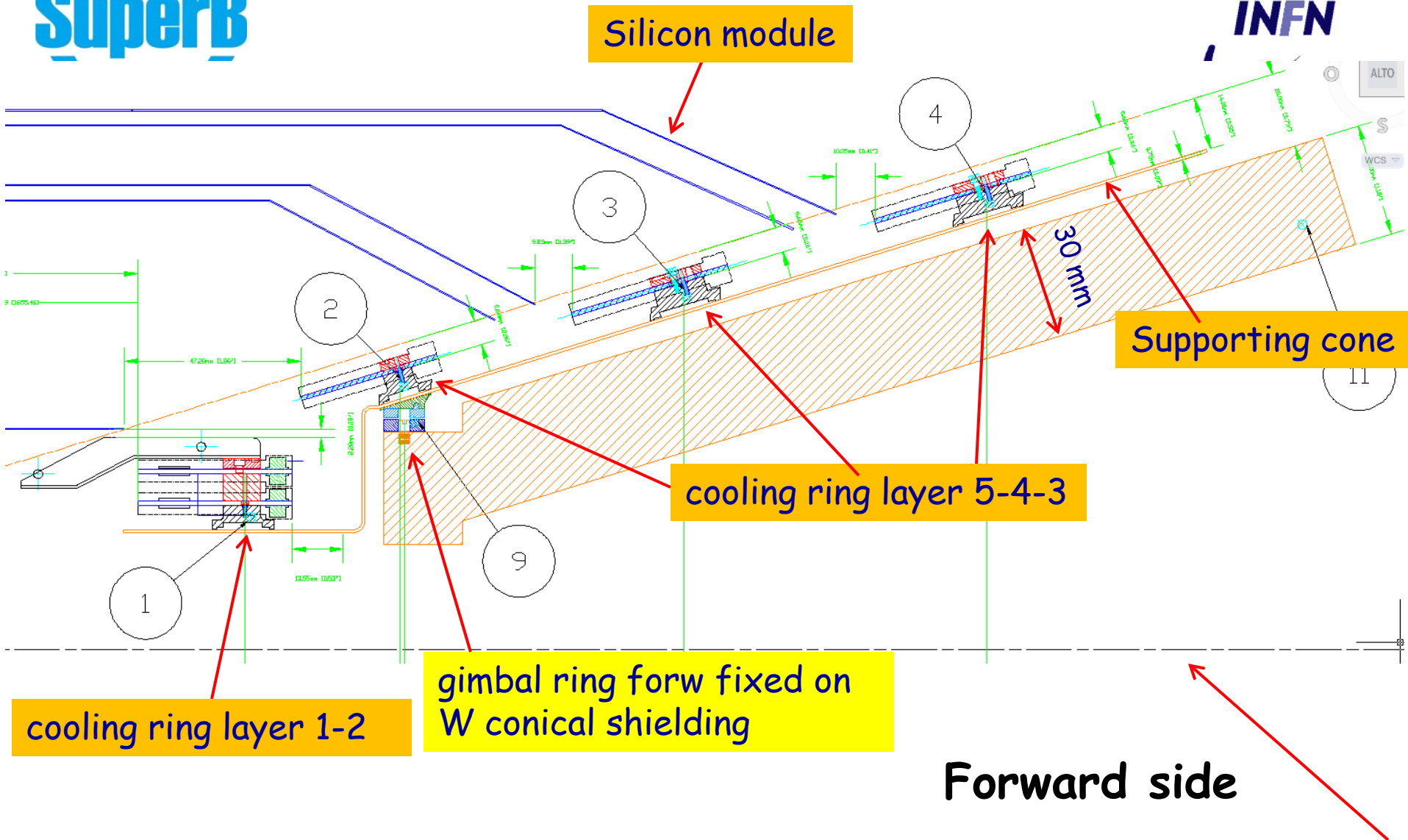
| | | | |
|--|---------------|--|--------------------|
| Progettato da F. Bosi | Controlato da | Approvato da | Data 21/11/2011 |
| Istituto Nazionale di Fisica Nucleare-Sezione di Pisa | | Assieme_modulo_0_overlap_300mrad SuperB | |
| | | Edizione | Foglio 1 / 1 |

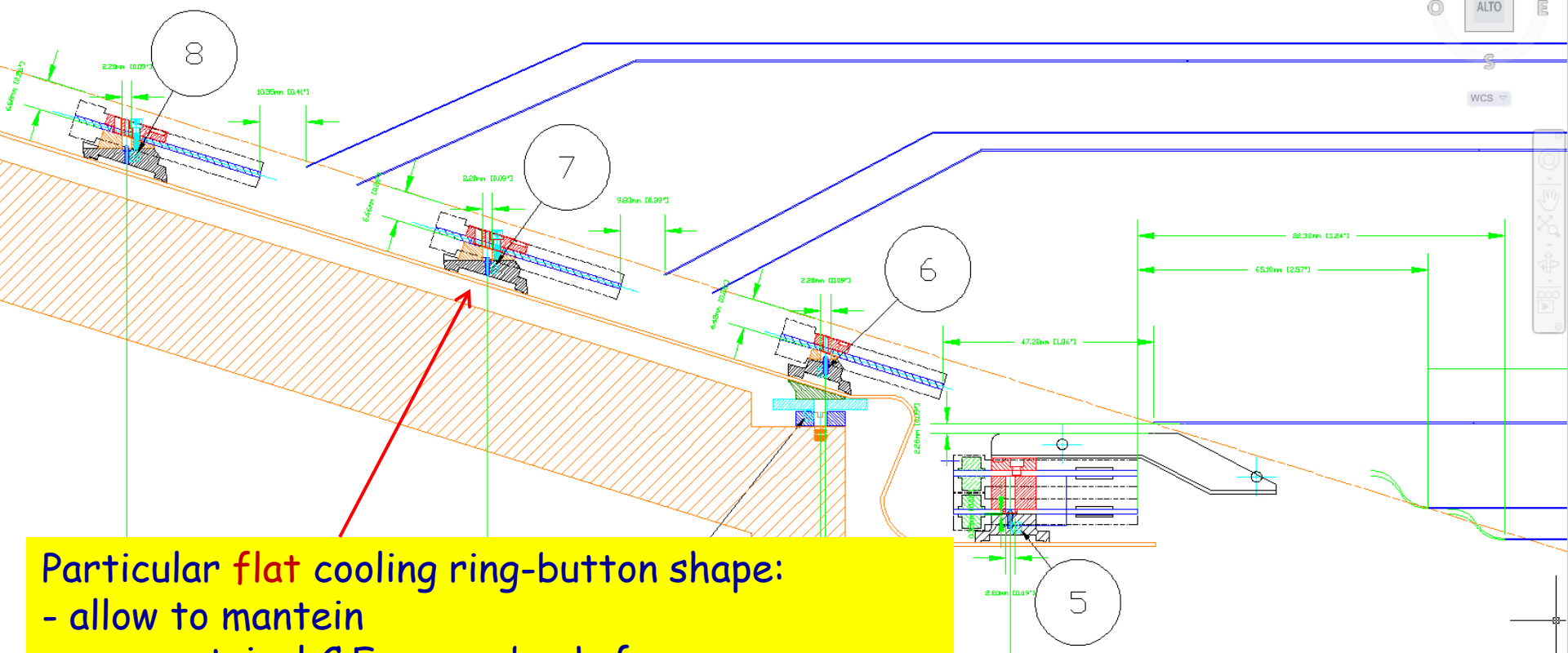


This design provides :

- symmetrical C.F. supporting cones forw-back
- symmetrical cooling ring forw-back
- W conical shielding coupled to gimbal ring and supporting SVT

We used the same BaBar HDI dimension for L 1-2-3-4-5



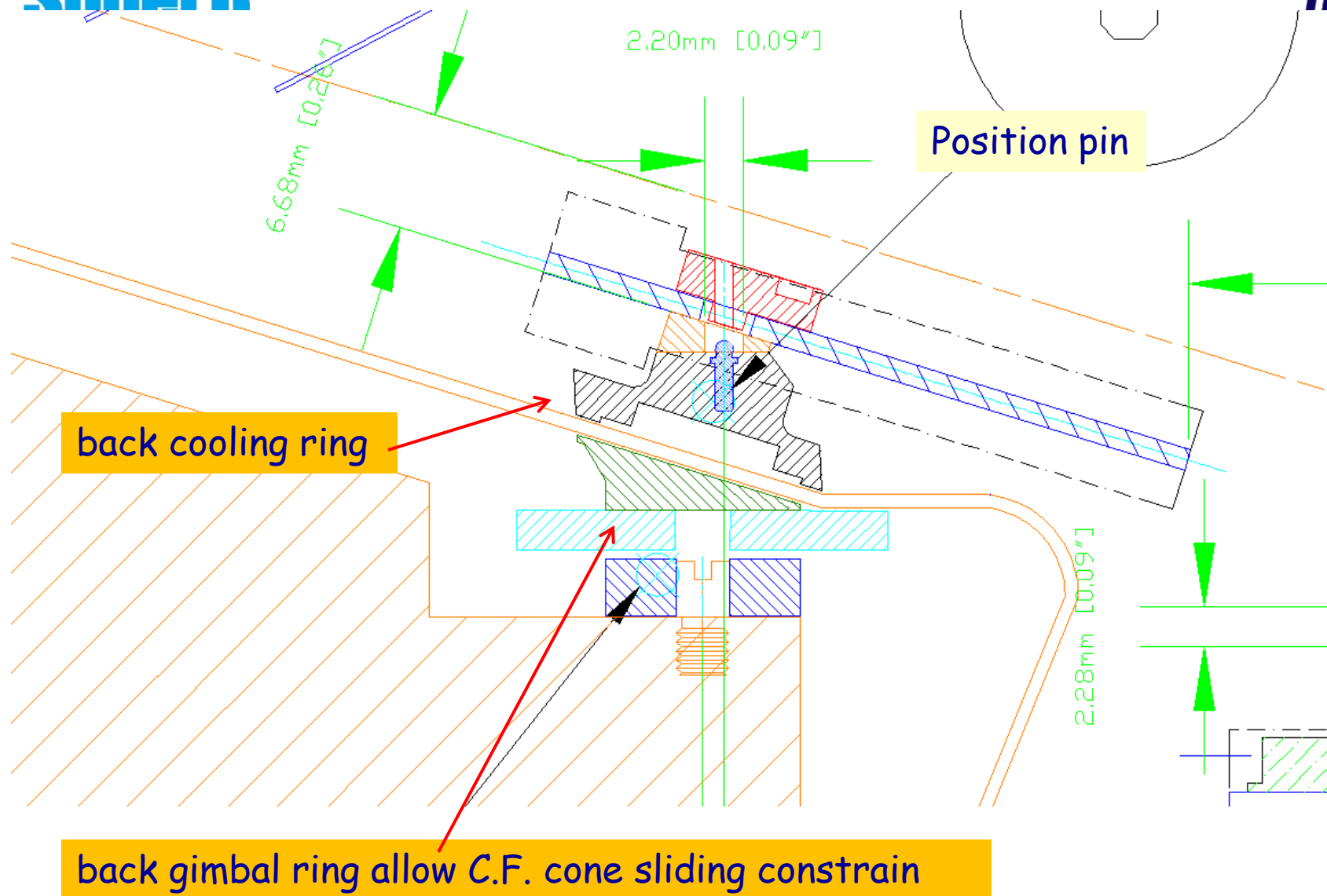


Particular **flat** cooling ring-button shape:

- allow to maintain a symmetrical C.F. cones back-forw (less mask for production)
- avoid an over-constrain of the module fixing

backward side

General Layout SVT





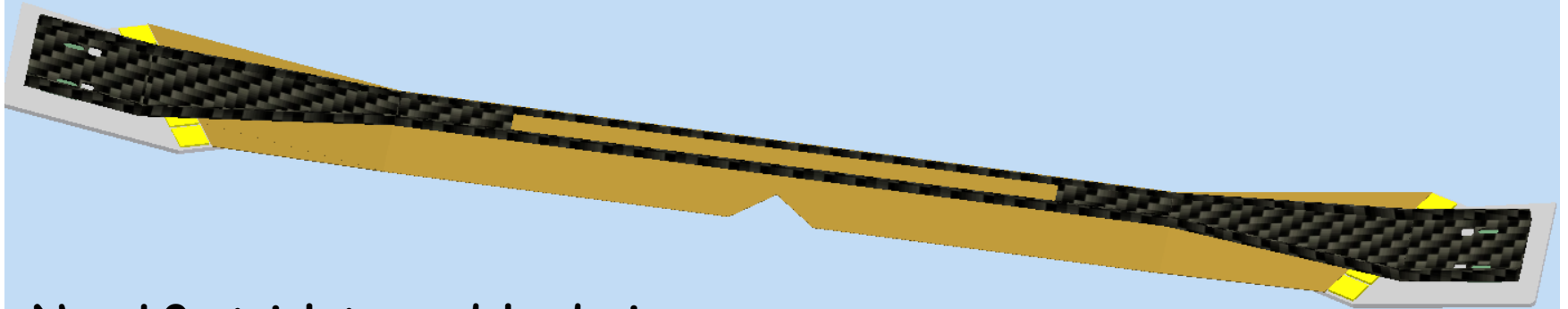
L0 design



Update on the L1-L5 design by London workshop :

- New L0 triplets design with Hdi/kapton inclined 10°
- Changed length and component Be beampipe
- Still some adjustment needed to optimize modules relative clearance
- Possible to gain still in diameter distance from beam-pipe
- No conflict with L1-2 SVT modules

L0 striplets design



New L0 striplets module design

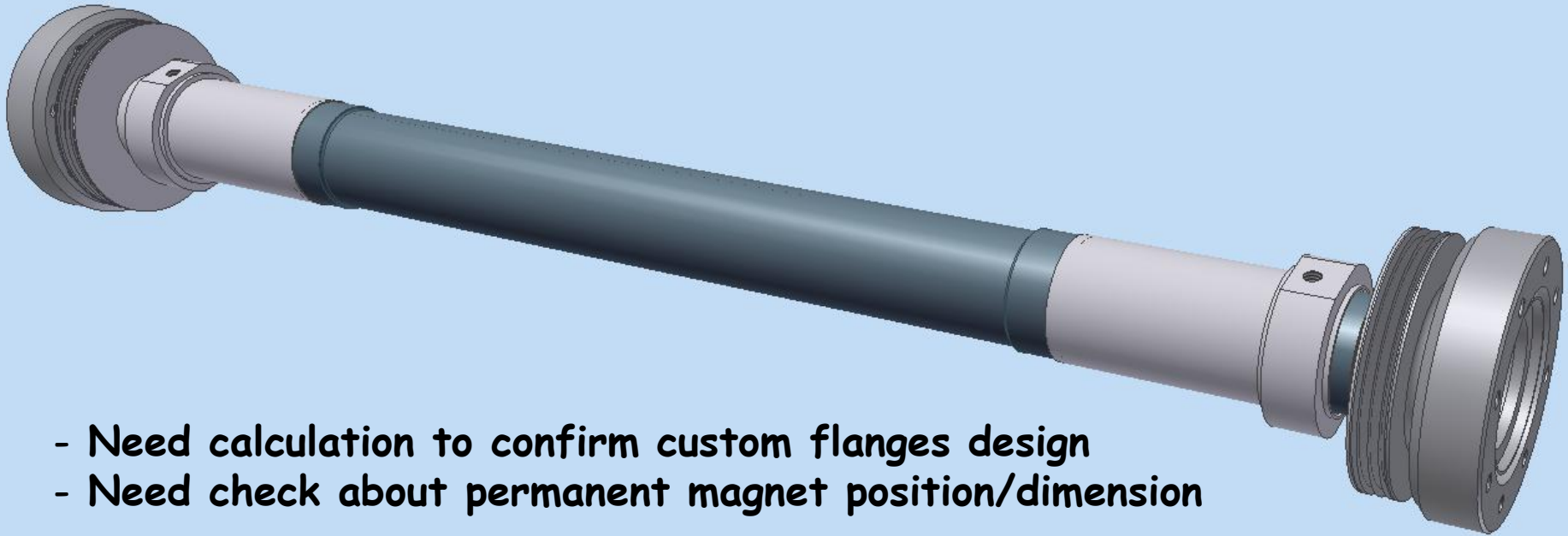
HDI/kapton inclined 10° (17.8° previous design)



Si sensor :
W=13.9 mm
L=104 mm
R=15.1 mm

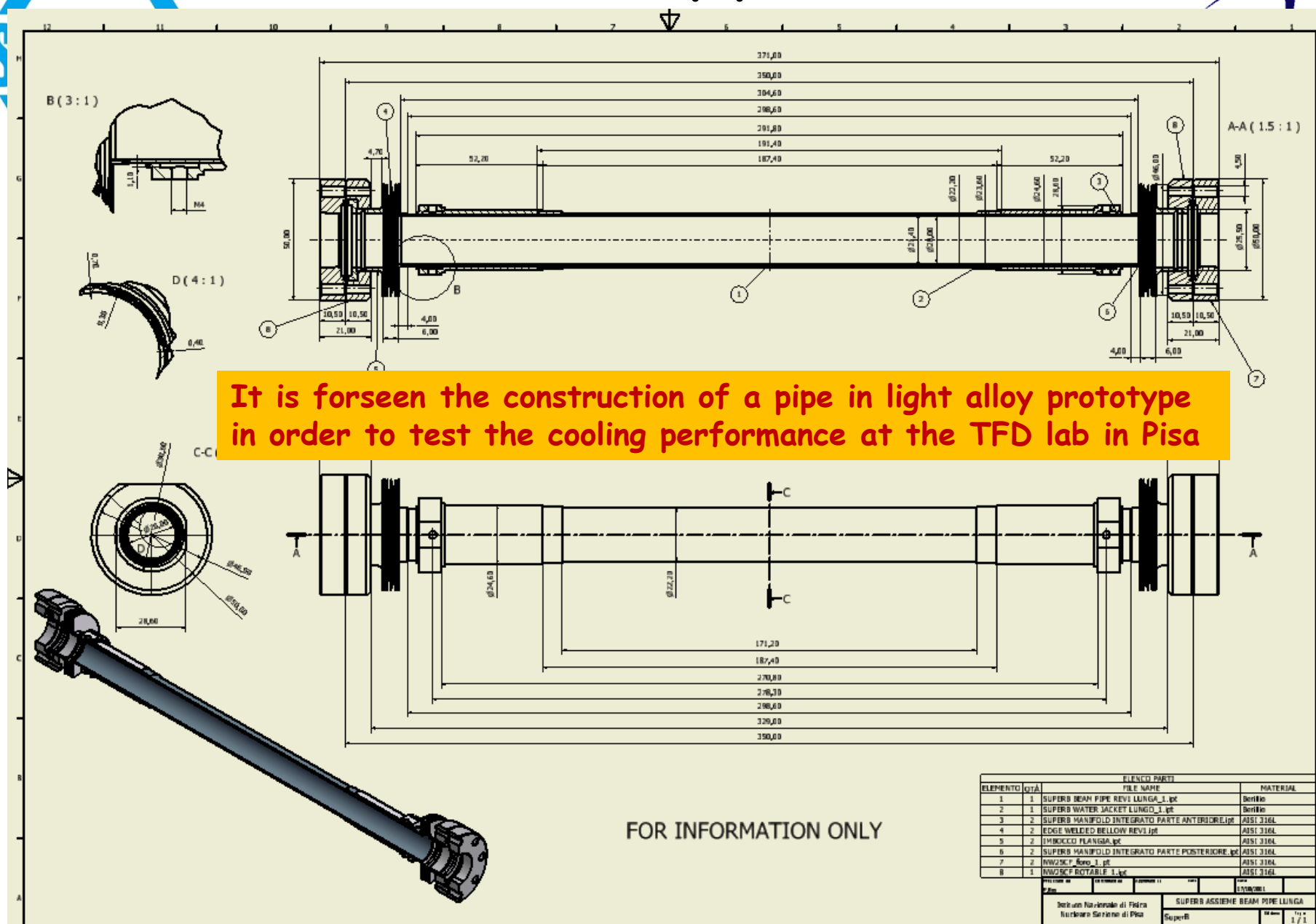
Possible larger width
of 0,3mm
for safer overlap in
the actual design

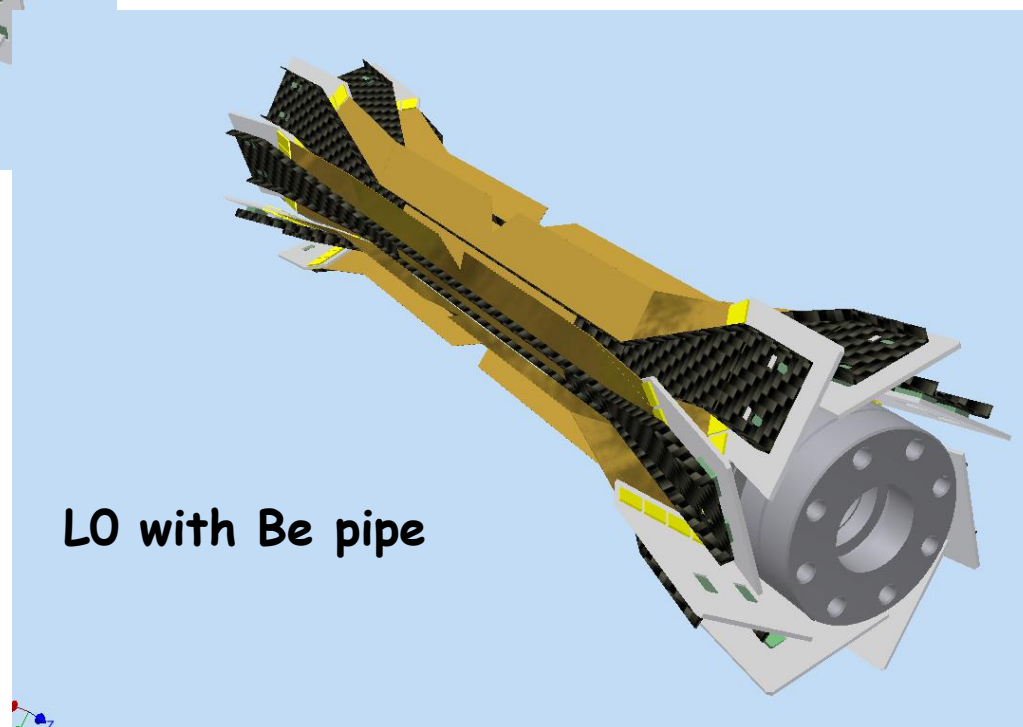
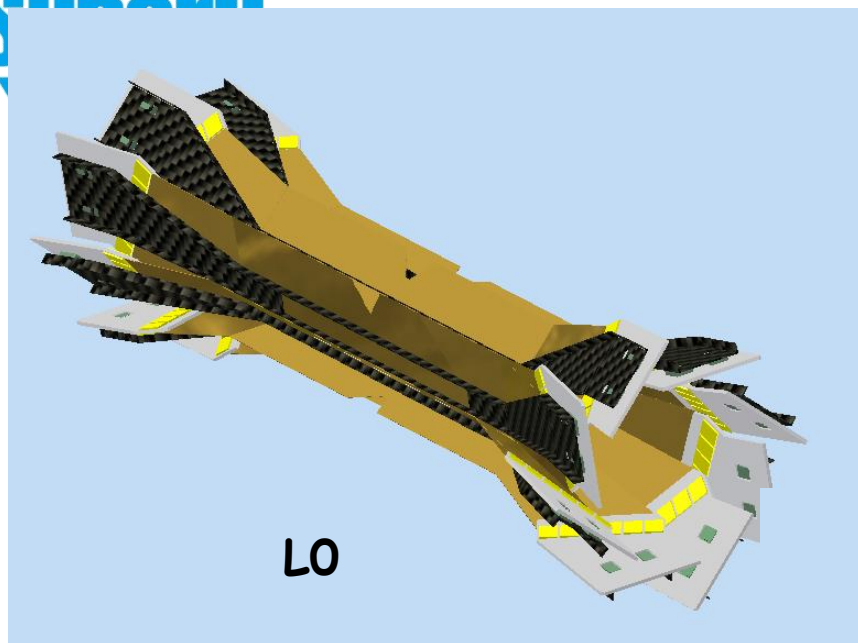
- New length to match L0 striplets design $L=304 \rightarrow 350$ mm :
(+23 mm/side, M.Sullivan has to approved.....)
- CF flanges not standard :
 - reduced in diameter (4 mm)
 - reduced in thickness (1.5 mm)
 - more screw with reduced diameter



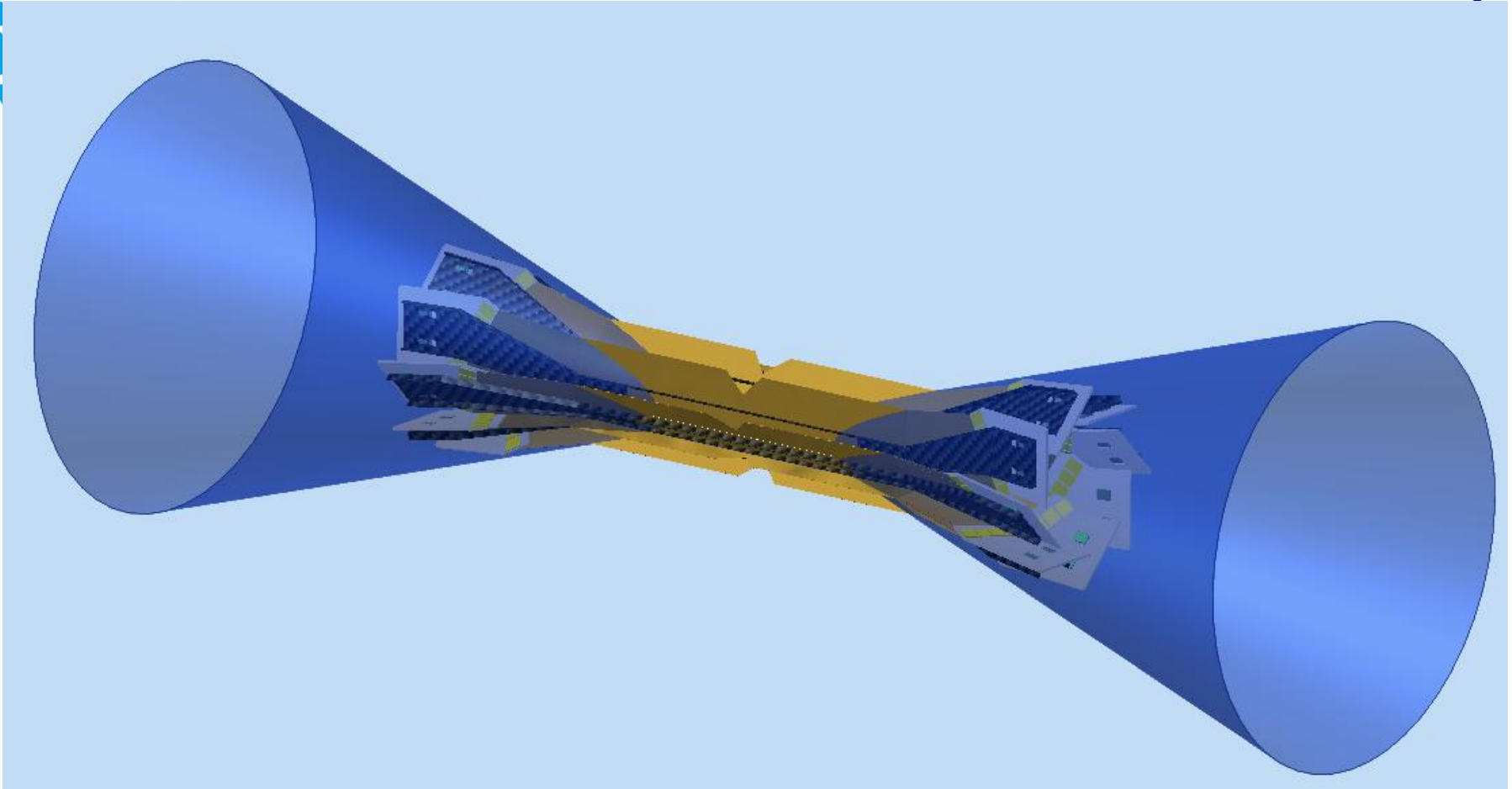
- Need calculation to confirm custom flanges design
- Need check about permanent magnet position/dimension

Be Beam pipe





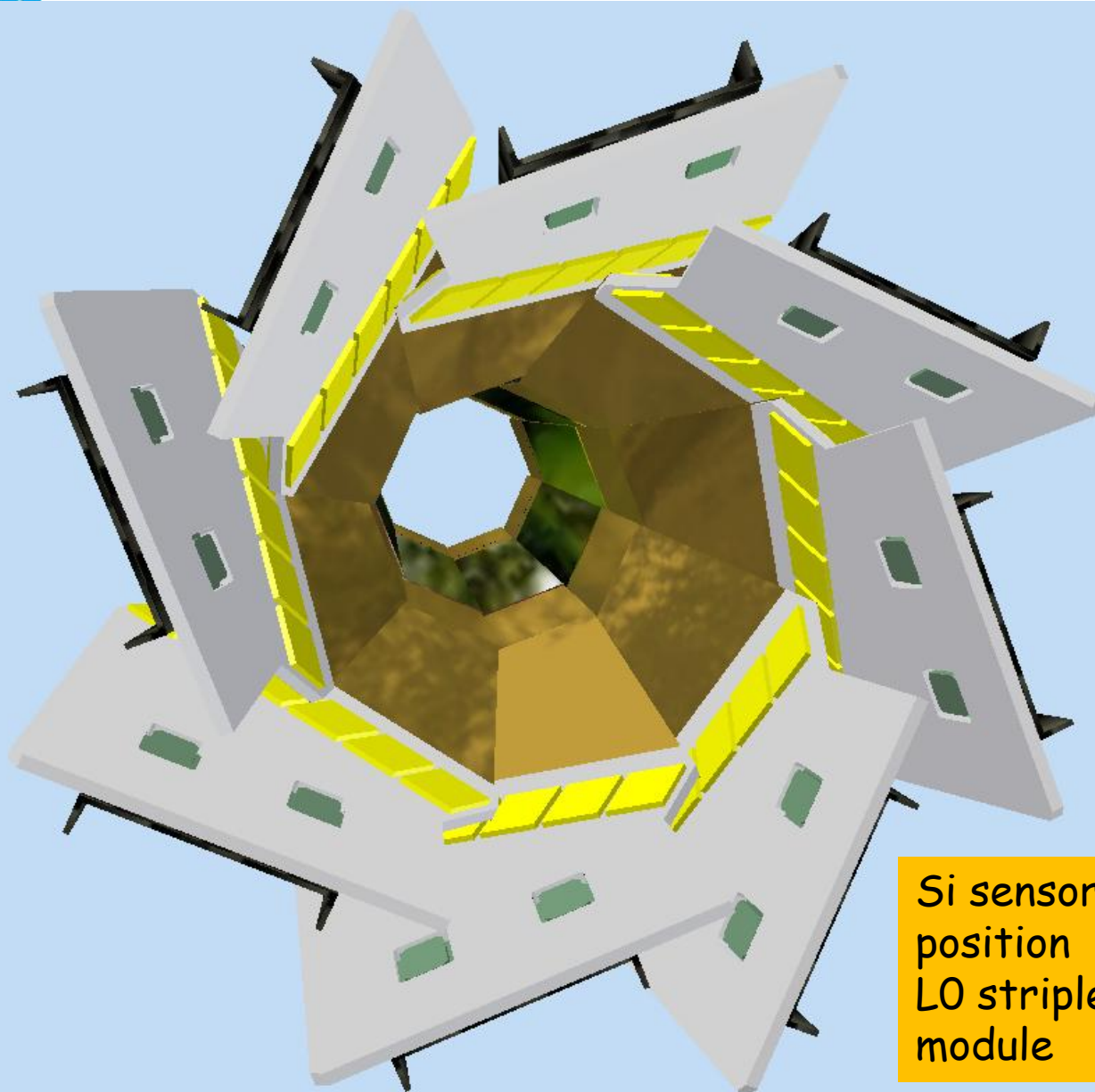
L0 stripjets new design



All L0 HDI are contained below
the 300 mrad acceptance angle



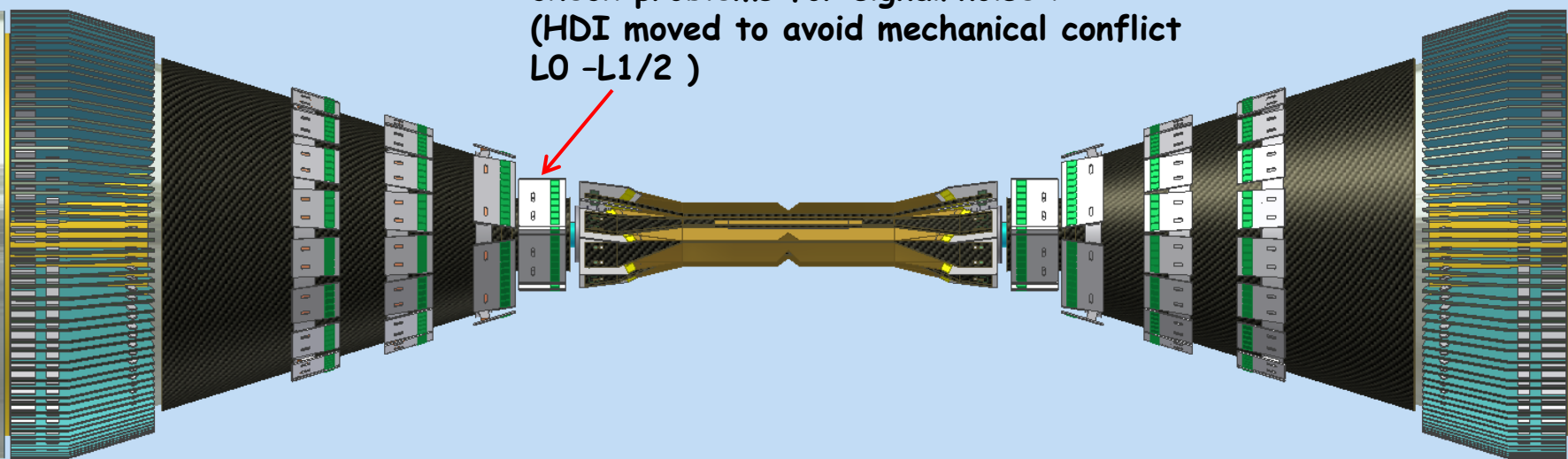
L0 design



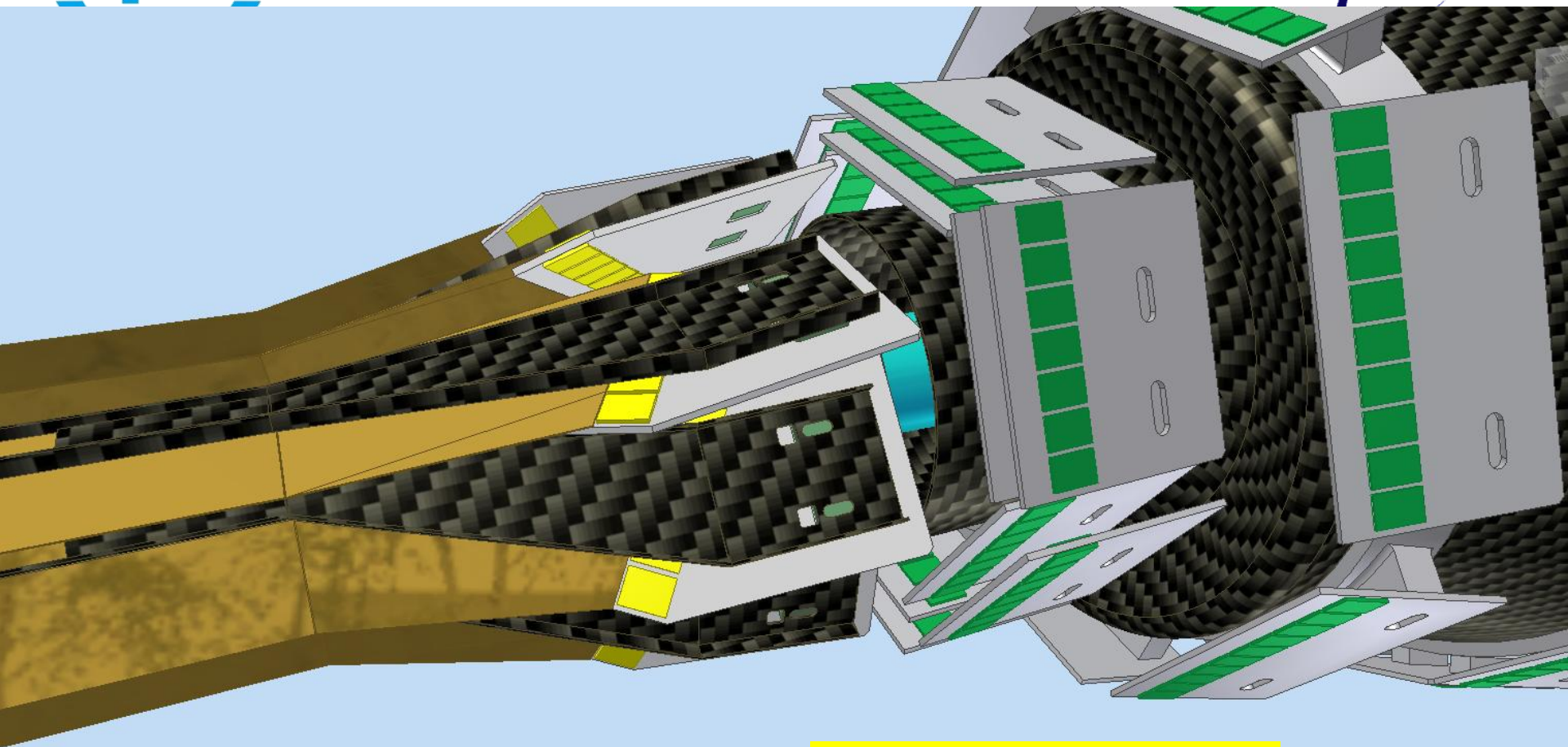
Si sensor
position in the
L0 striplet
module



Layer 1-2 fanout longer (max 80mm):
check problems for signal/noise !
(HDI moved to avoid mechanical conflict
LO -L1/2)



Relative positions between SVT HDI and LO HDI



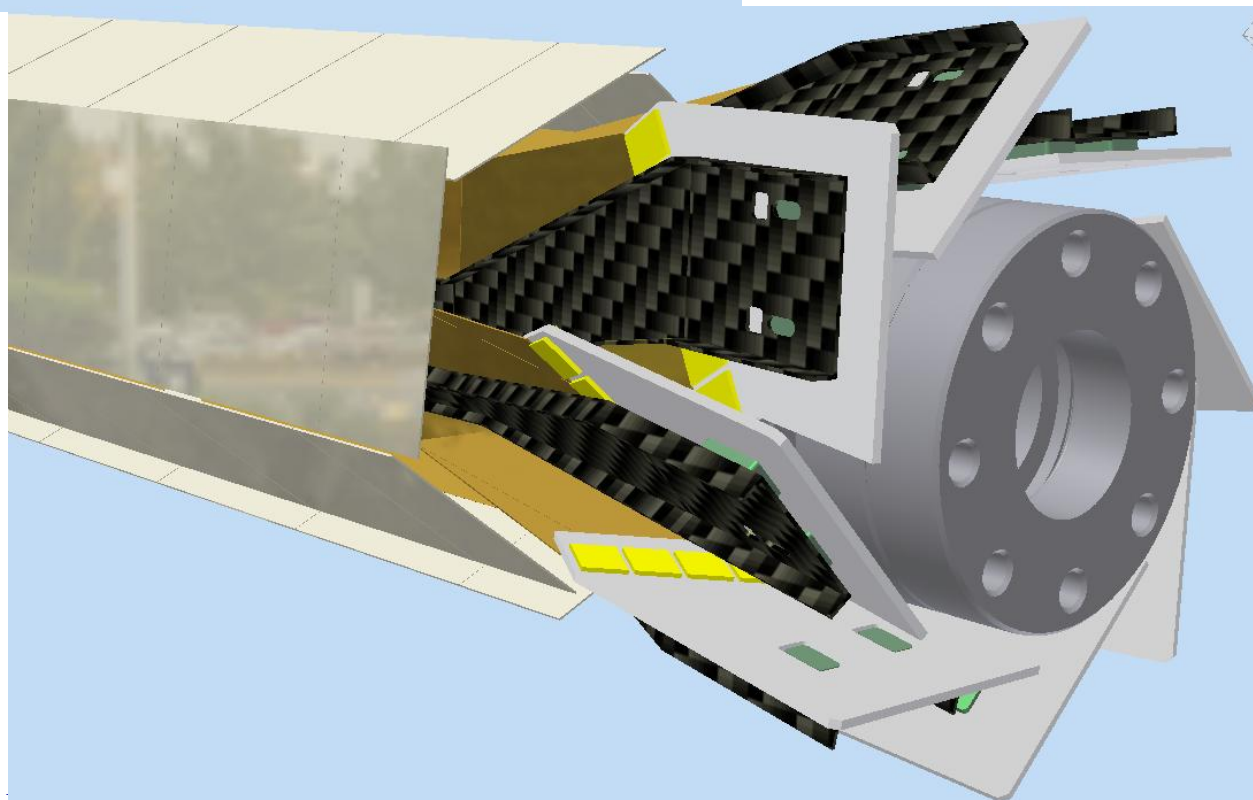
Crowded region !

**L 1-2-3 HDI
and LO HDI**

New L0 striplets design

Layer0/Layer1

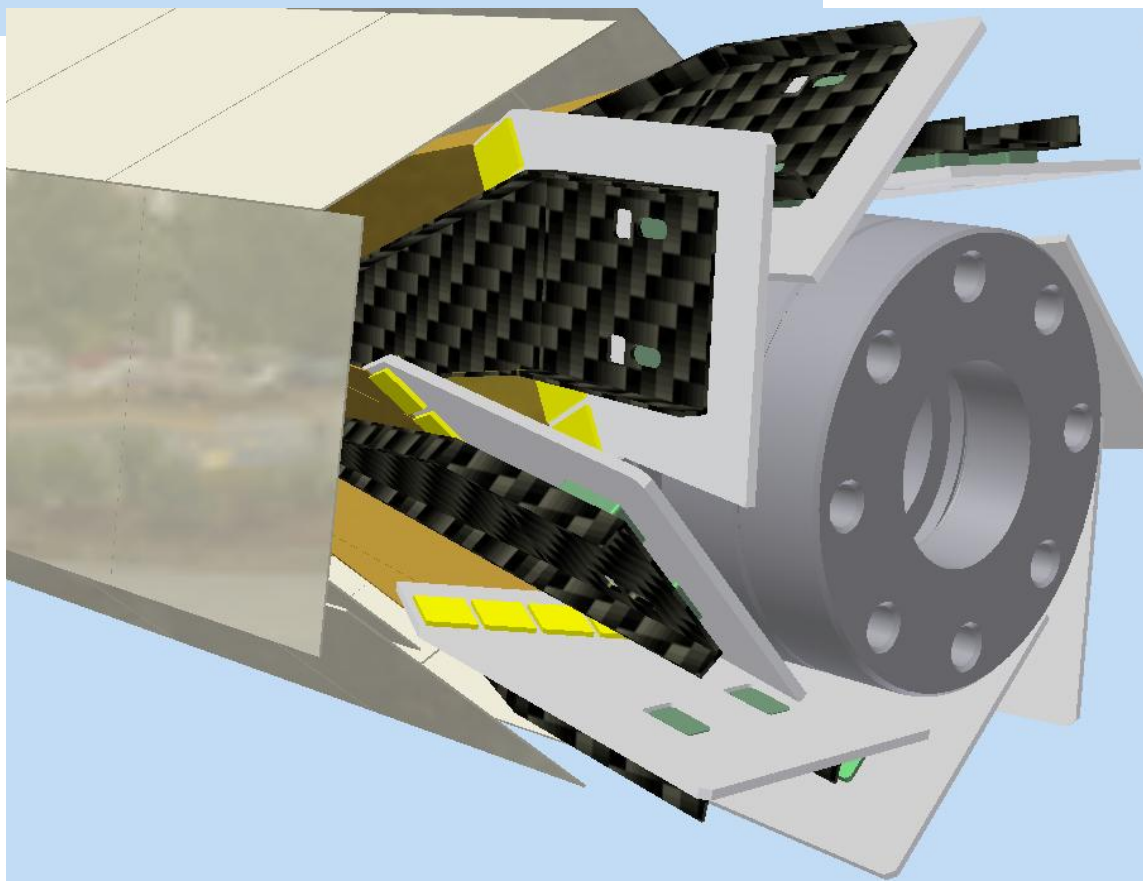
No conflict !



L0 striplets design

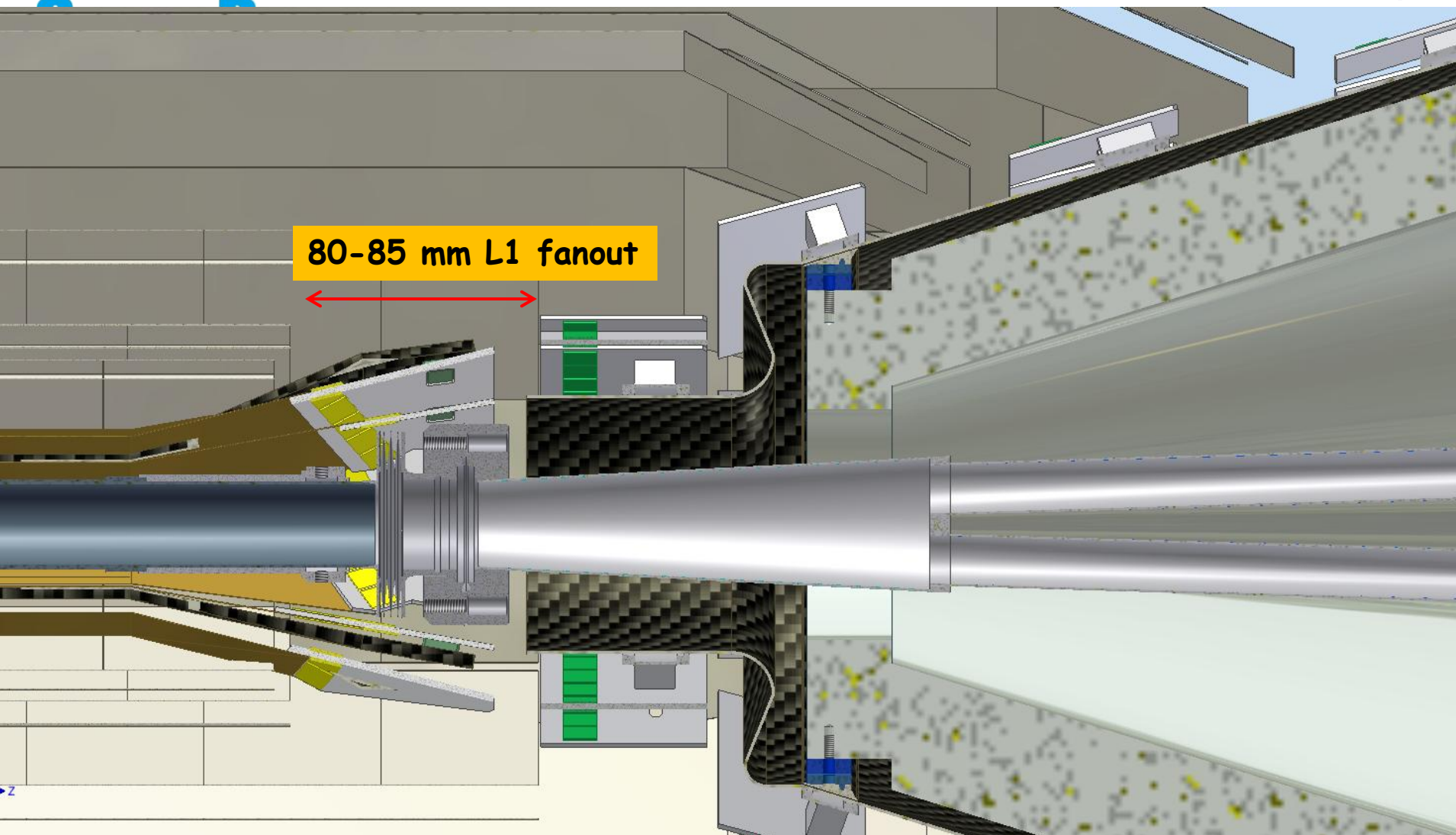
Layer0/Layer2

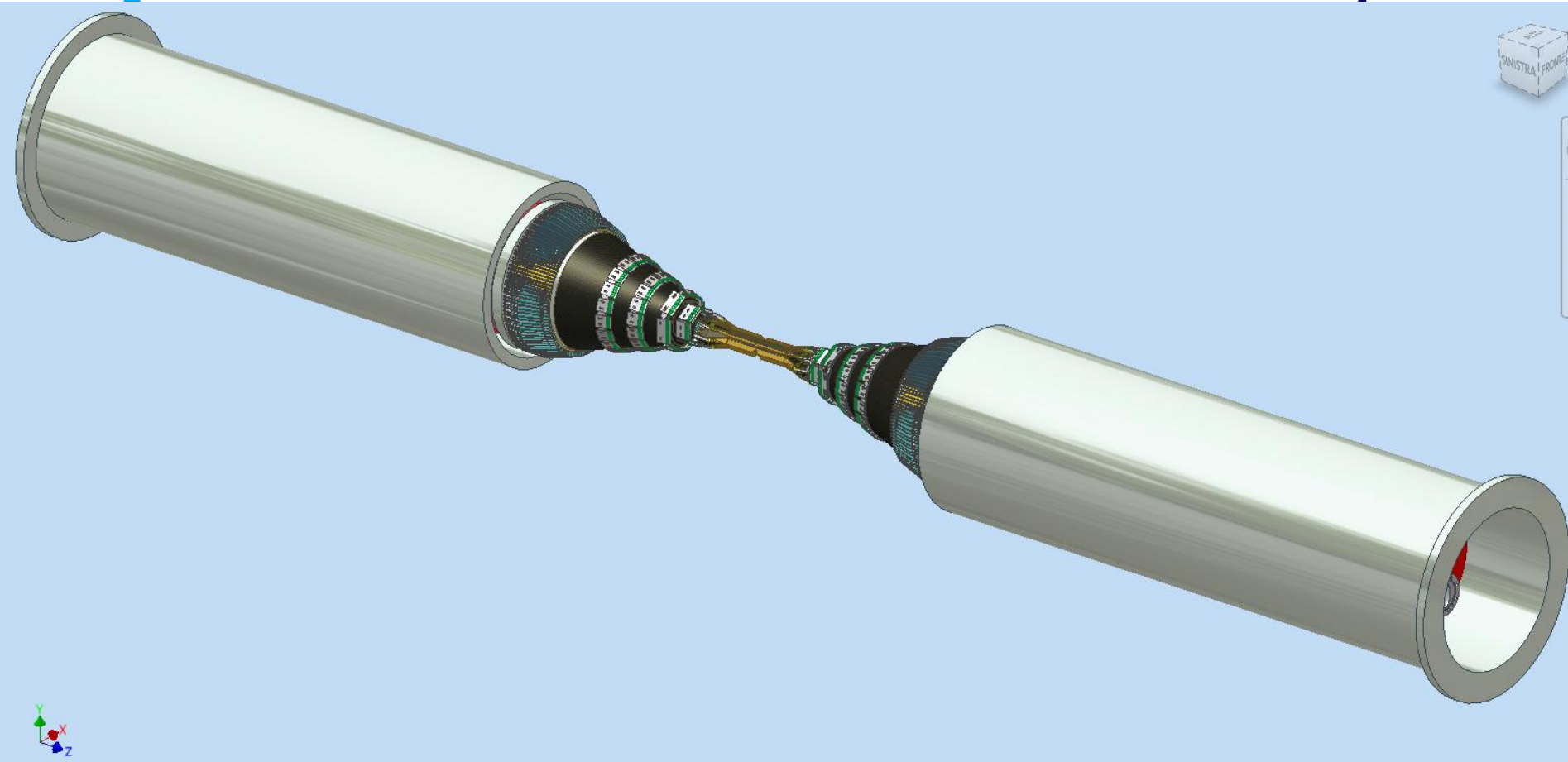
No conflict !

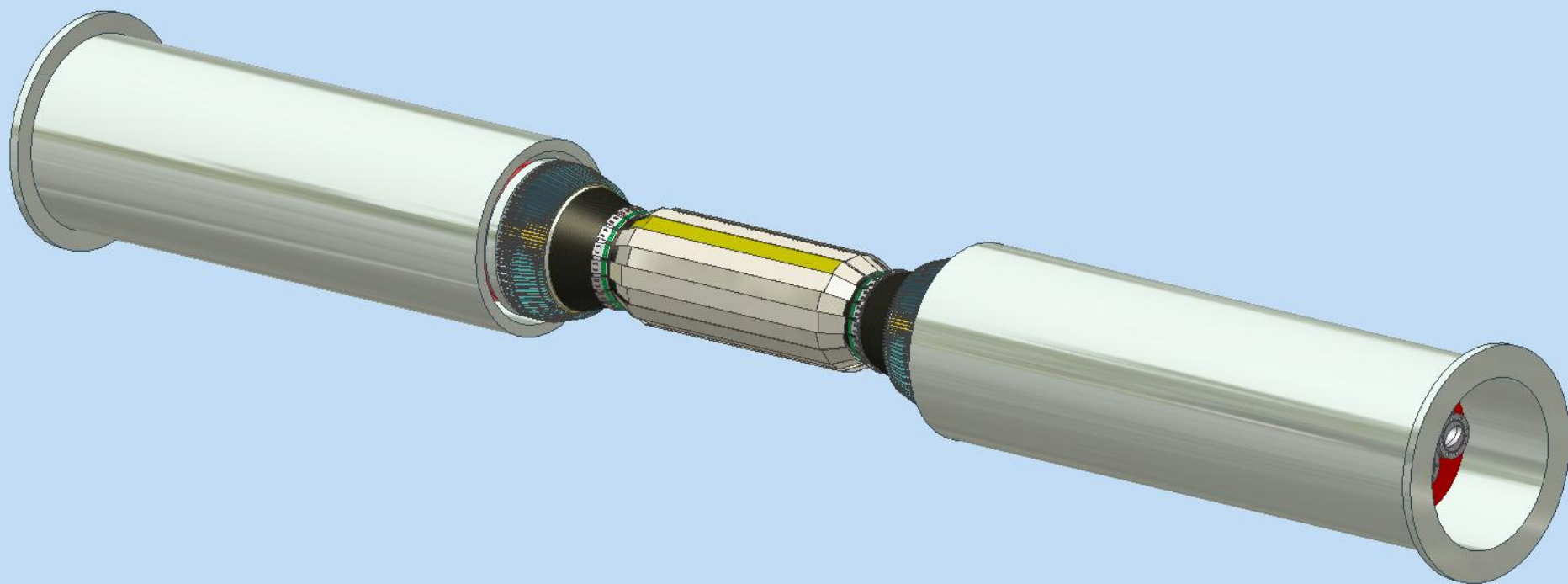




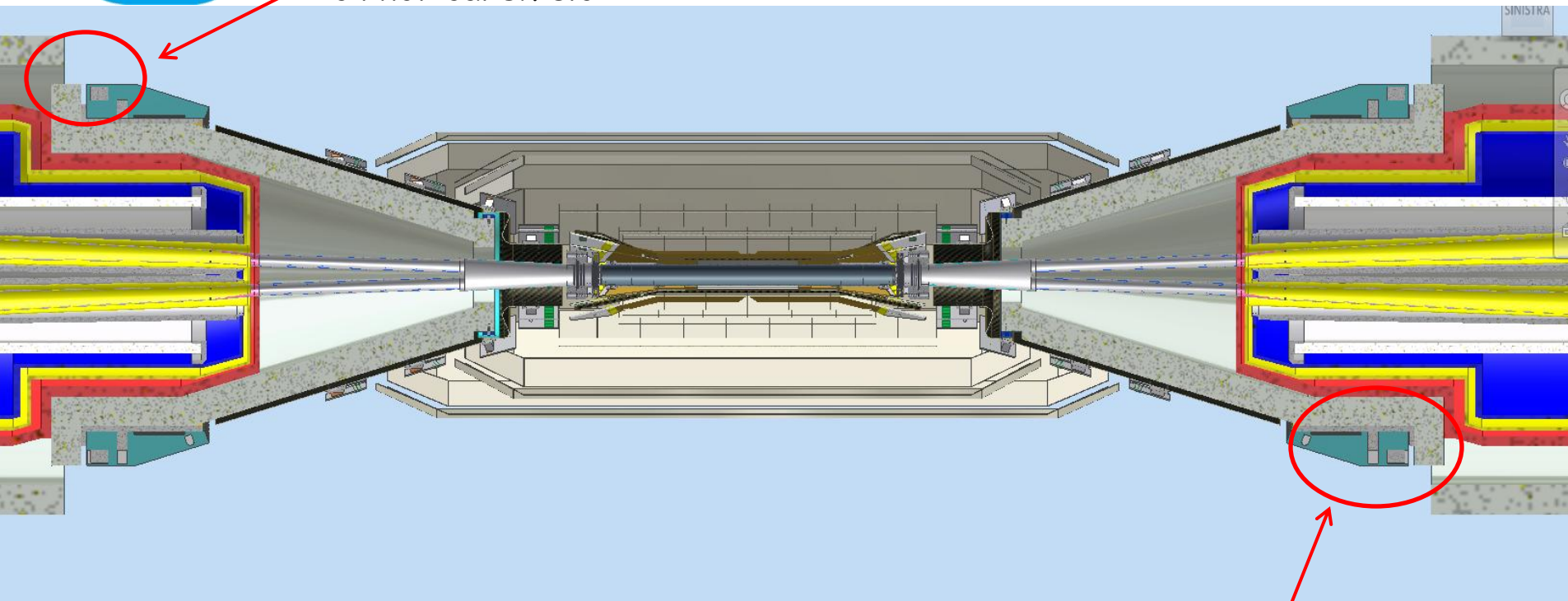
I.R. Layout



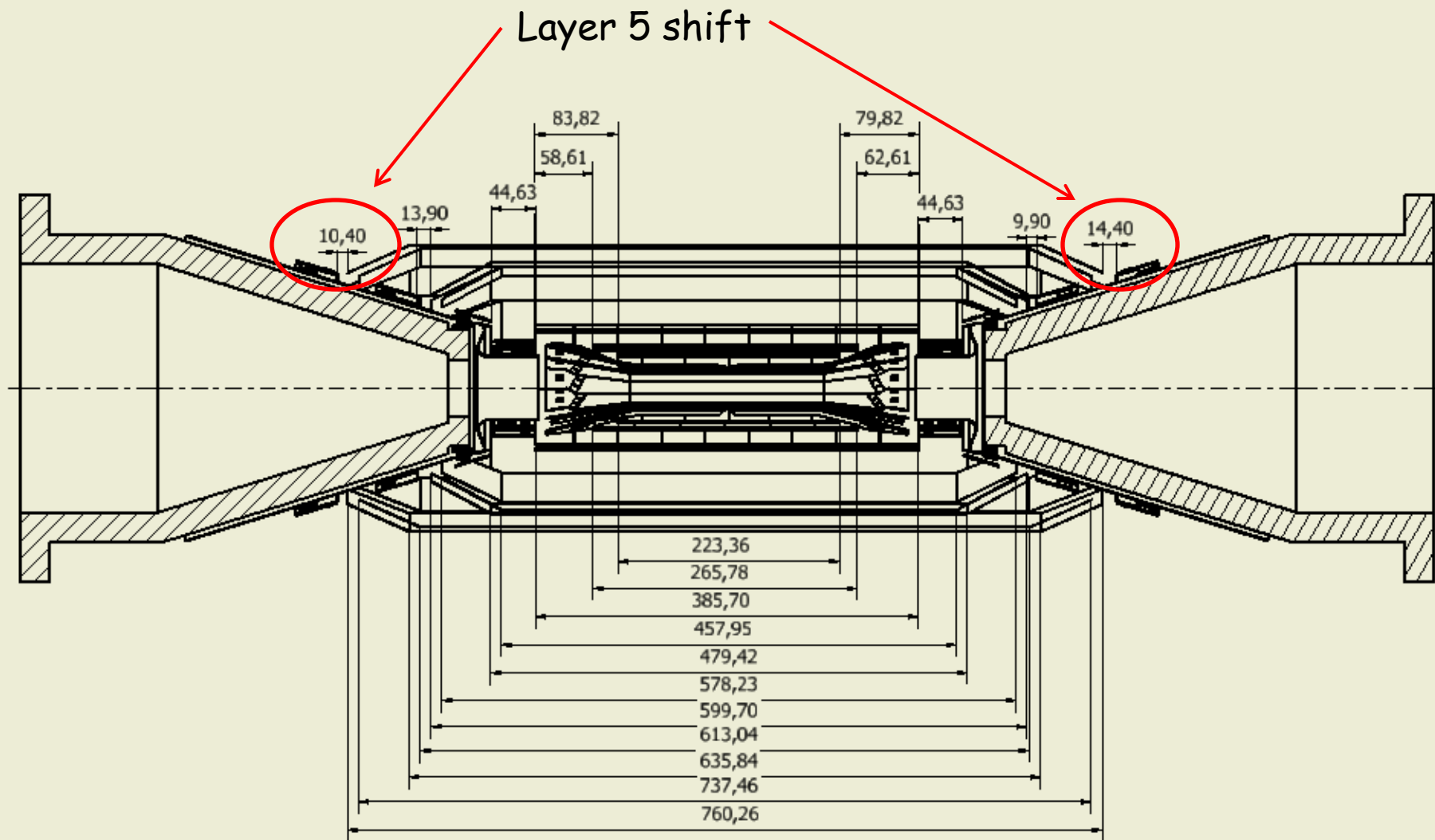


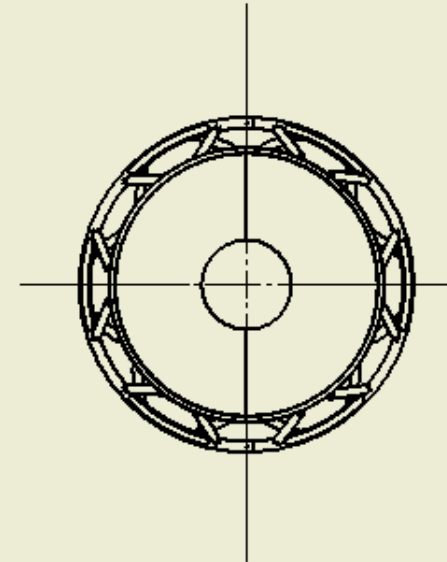
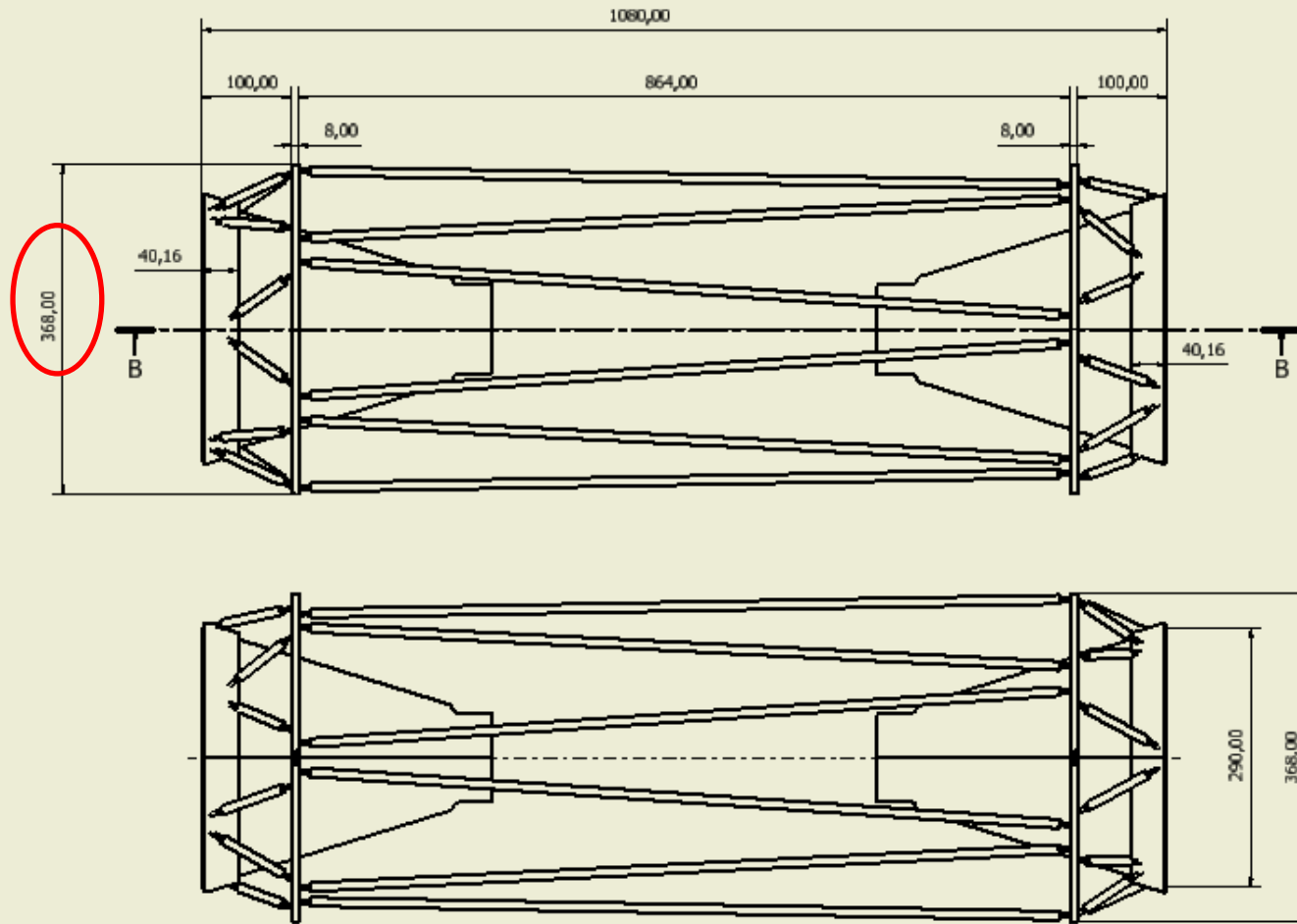


W conical shield
independent from
cilindrical shield



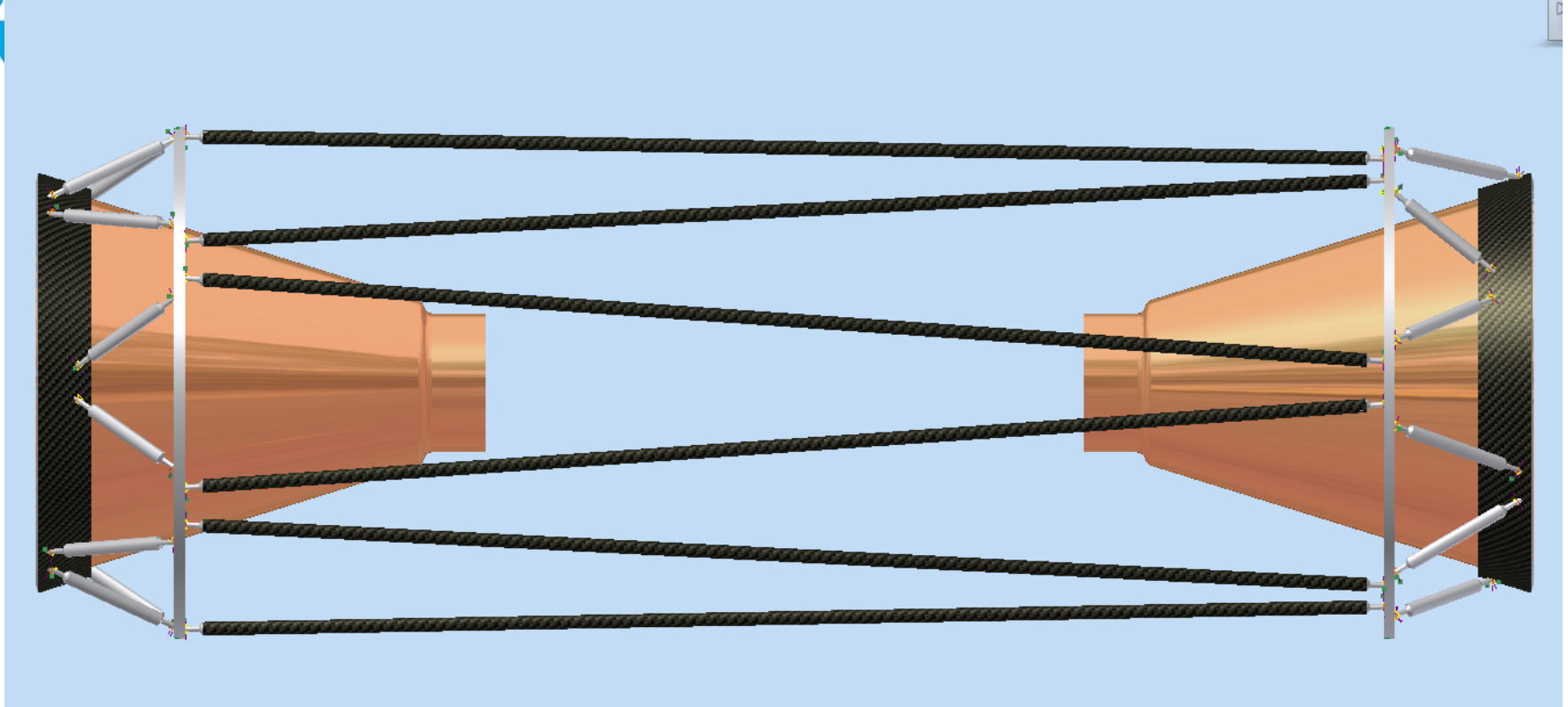
Transition card with radial dimension useful
to remain below ext diam W conical shield to
allow movement respect to cilindrical shield





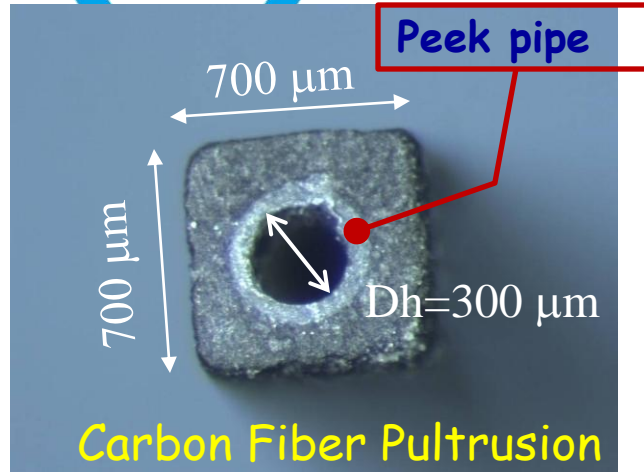
QMUL
J.Morris, F.Gannaway

Space Frame, version 2

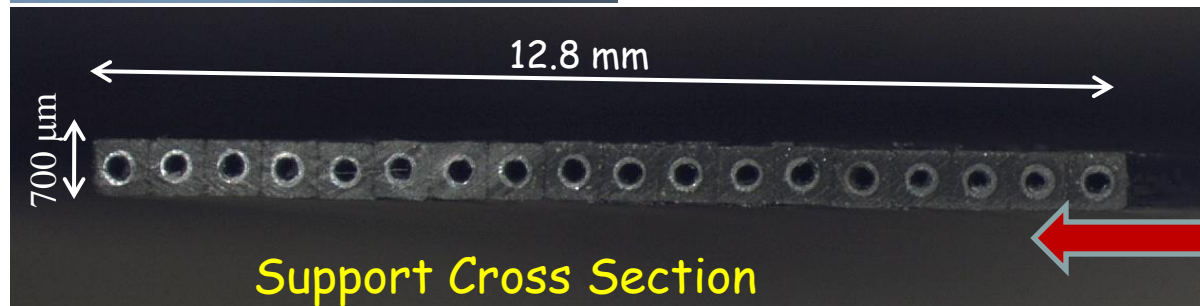


J. Morris and F. Gannaway are working on the version 3 of the C.F. cones and space-frame having the new position of HDI/cooling ring

Space Frame, version 2



The single base microchannel unit
A square CF micro-tube with an internal peek tube 50 μm thick used to avoid moisture on carbon fiber



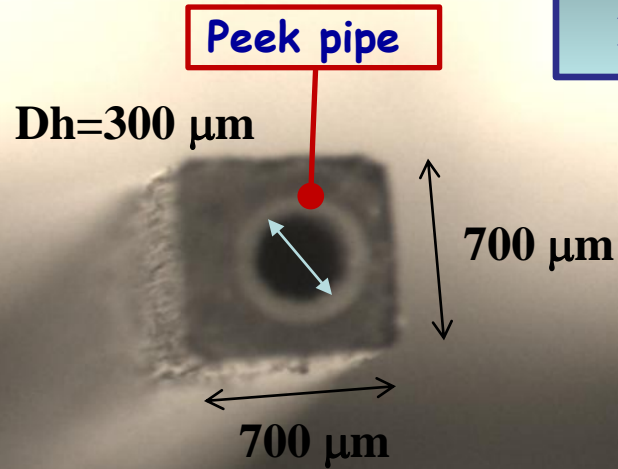
Full micro-channel module
The total radiation length (*) of this support is 0.28 % X_0



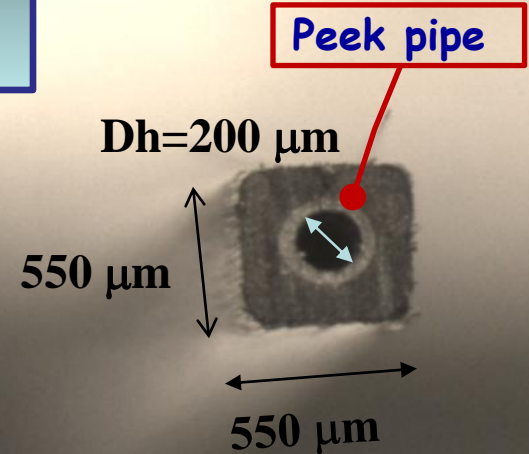
Net micro-channel module
Same dimensions of full micro-channel but vacancies of tubes in the structure.
The total radiation length (*) is 0.15 % X_0

(*): Material of the support structure: (All C.F. material + peek tube + Water)

Further Miniaturization microtube technology



Old Carbon Fiber Pultrusion

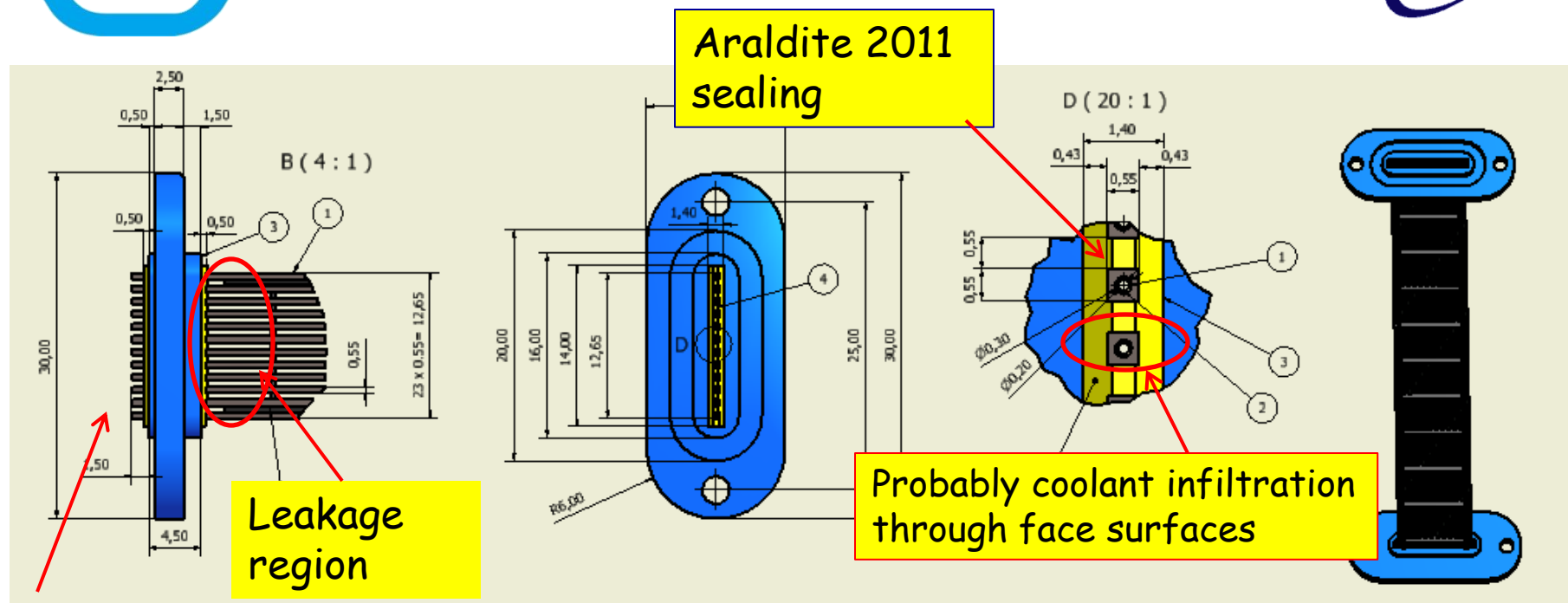


New Carbon Fiber Pultrusion

Full Module $X = 0,28 \% X_0$
Net Module $X = 0,15 \% X_0$

Full Module $X = 0,22 \% X_0$
Net Module $X = 0,11 \% X_0$

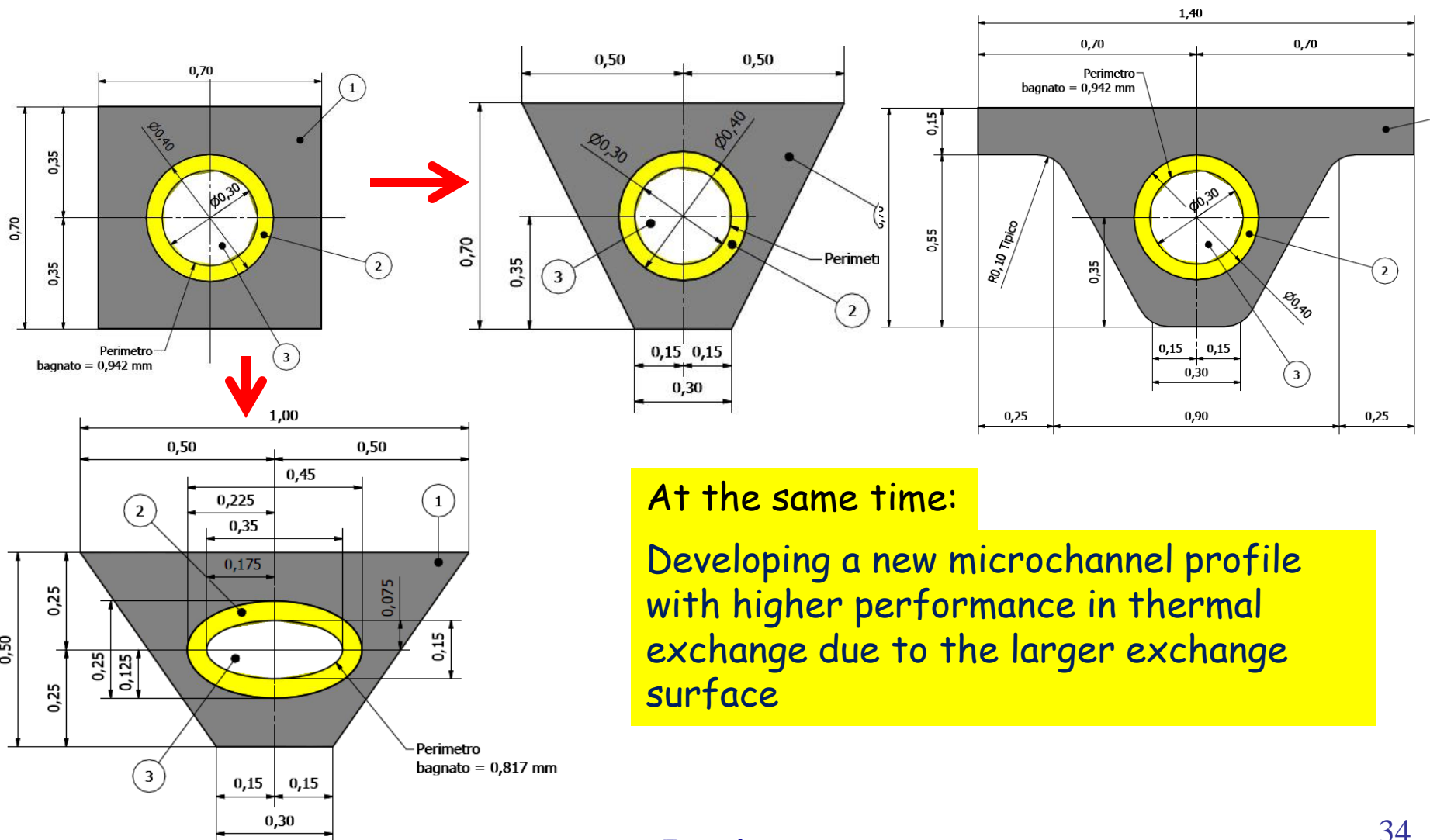
Module Microtubes 550 μm th, Full and Net version tested at the TFD lab



Coolant input

Leakage problem:

The leakage is due to a poor rate of resin respect to the carbon fiber that allow the coolant pass trough the pultrusion at the face plane region of the microchannel ;
NEED A NEW PRODUCTION !

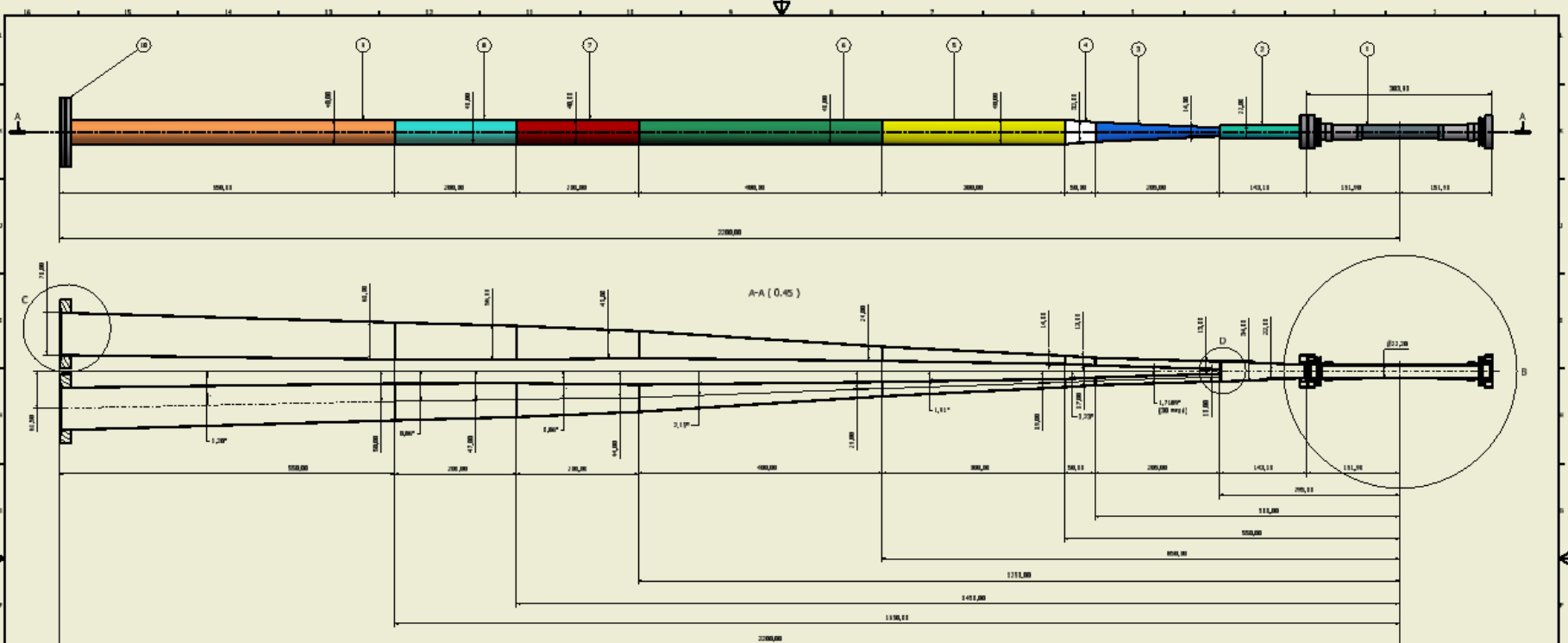


At the same time:

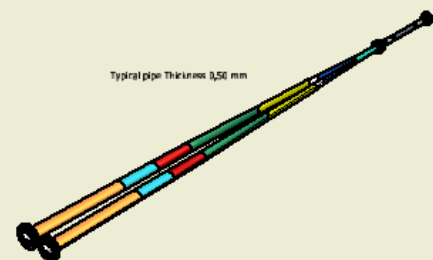
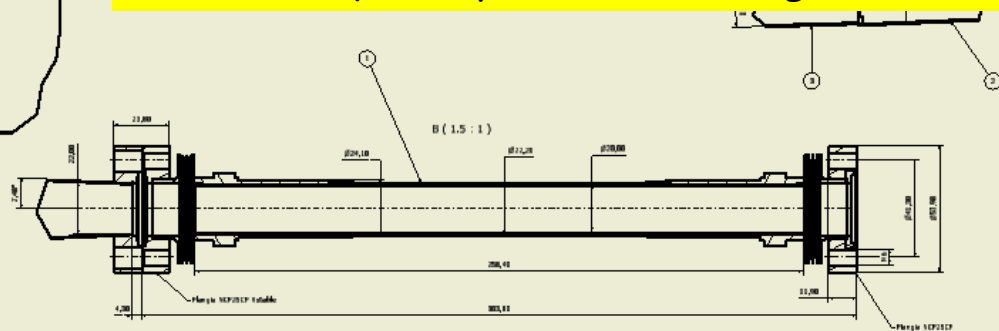
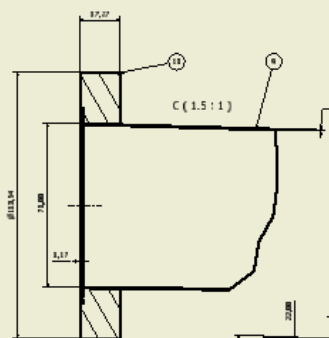
Developing a new microchannel profile with higher performance in thermal exchange due to the larger exchange surface



Beam pipe



Produced solid modeling of criostat beam-pipe to use for quadrupole criostat region



Typical Thickness 0,50 mm

| ELEMENTO | QTA | DESCRIZIONE | REMARKS |
|----------|-----|------------------|---------|
| 1 | 1 | Beam Pipe | |
| 2 | 1 | Flange | |
| 3 | 1 | Flange | |
| 4 | 2 | Flange with Hole | |
| 5 | 2 | Flange with Hole | |
| 6 | 2 | Flange with Hole | |
| 7 | 2 | Flange with Hole | |
| 8 | 2 | Flange with Hole | |
| 9 | 2 | Flange with Hole | |
| 10 | 2 | Flange with Hole | |
| 11 | 1 | Flange | |



I.R. Architecture/quick demounting



- Present I.R. design has the goal to assume W conical shield independent from cylindrical shield to move less mass for quick demounting operation (all SVT components have minor diameter respect to W conical shield int.diam.) .

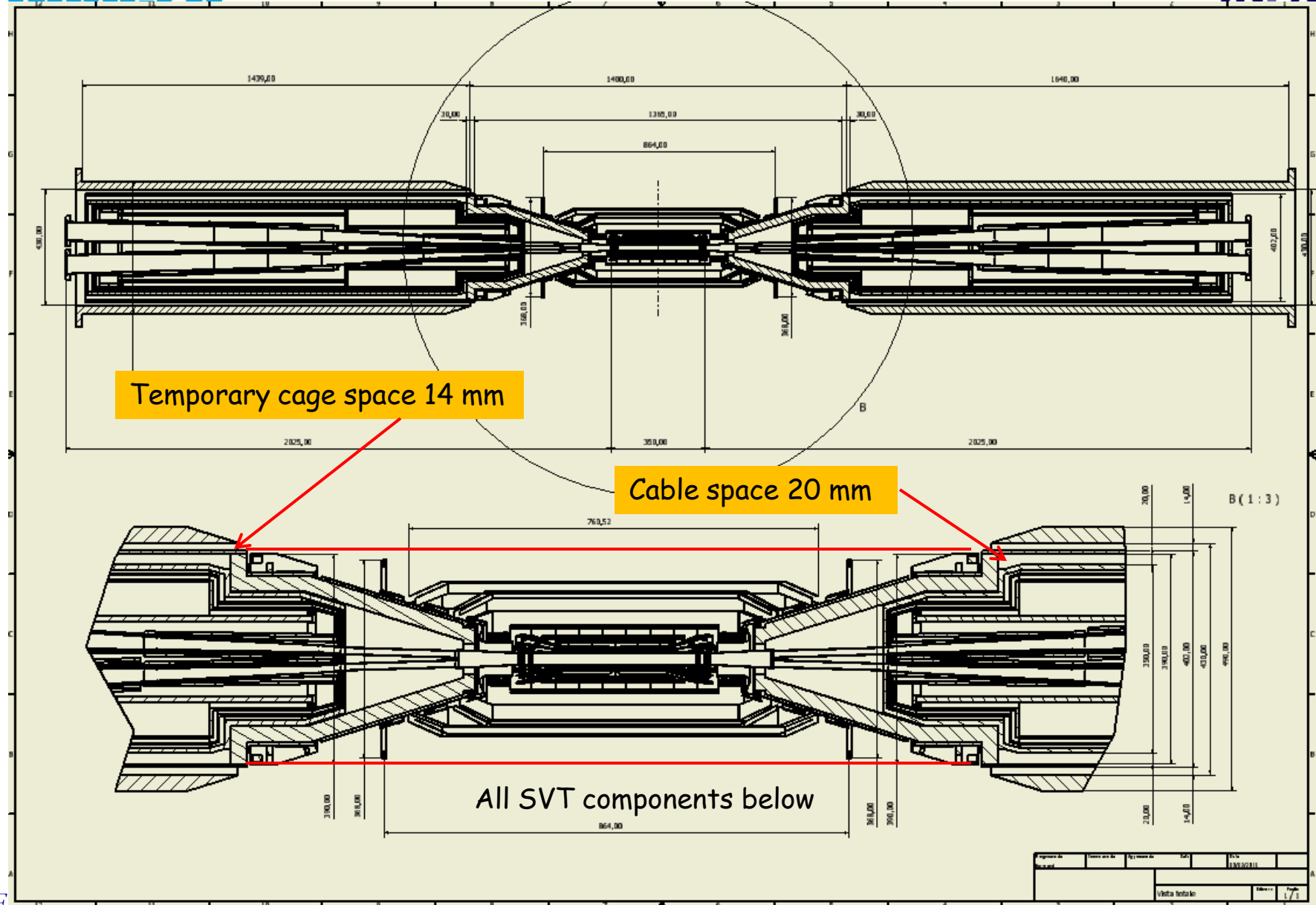
- In this configuration, criostat forw/back+SVT+LO+Be pipe+conical shield forw/back are one body (like in BaBar) but, in SuperB, to gain in X0, is not present the C.F. BaBar supporting tube and the Be pipe and SVT are the weak part of the mechanical chain .

- Quick demounting plans to insert-remove a temporary cage to make rigid SVT /Be pipe during sliding operation to replace LO in short time.

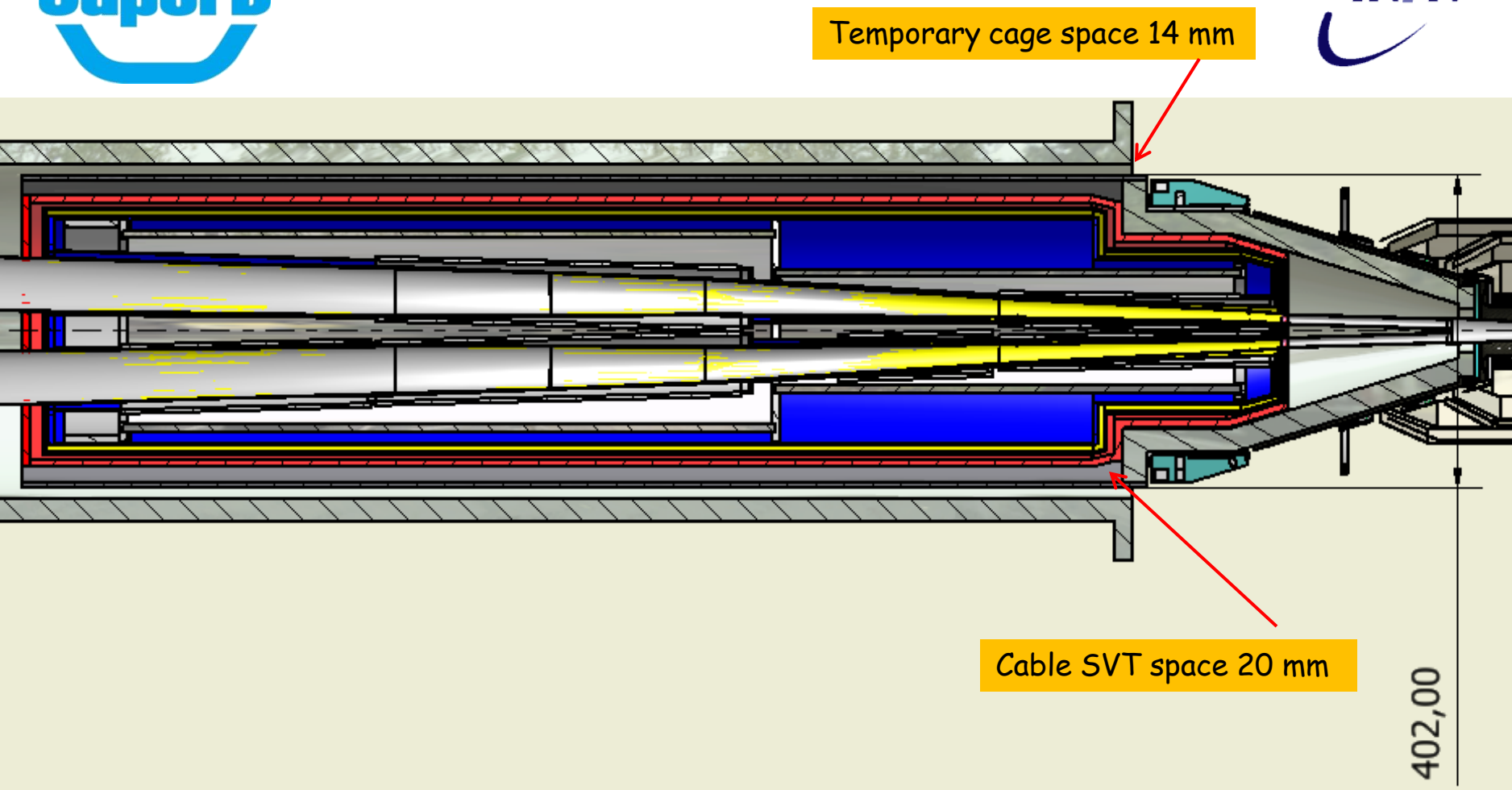
- Has been asked to assume $R=245$ (+10 mm respect now) as internal diameter of D.C. in order to have minimum radial space to design the mechanics of operation.

- The temporary cage should put together the two opposite W conical shield from a remote region (FCAL) previous blocking the external tube forw/back to the internal part of cylindrical W shield.

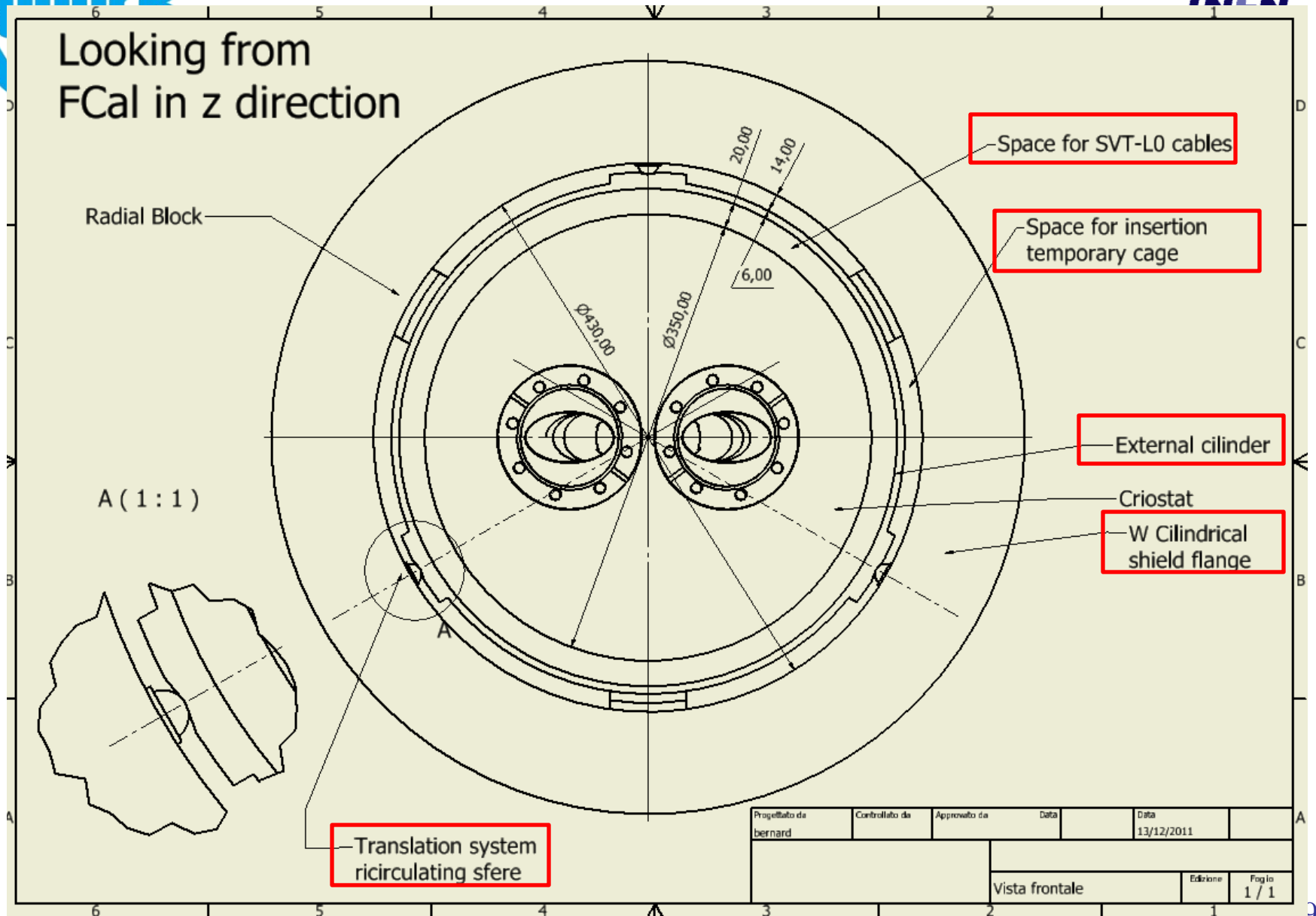
Quick demounting



Quick demounting

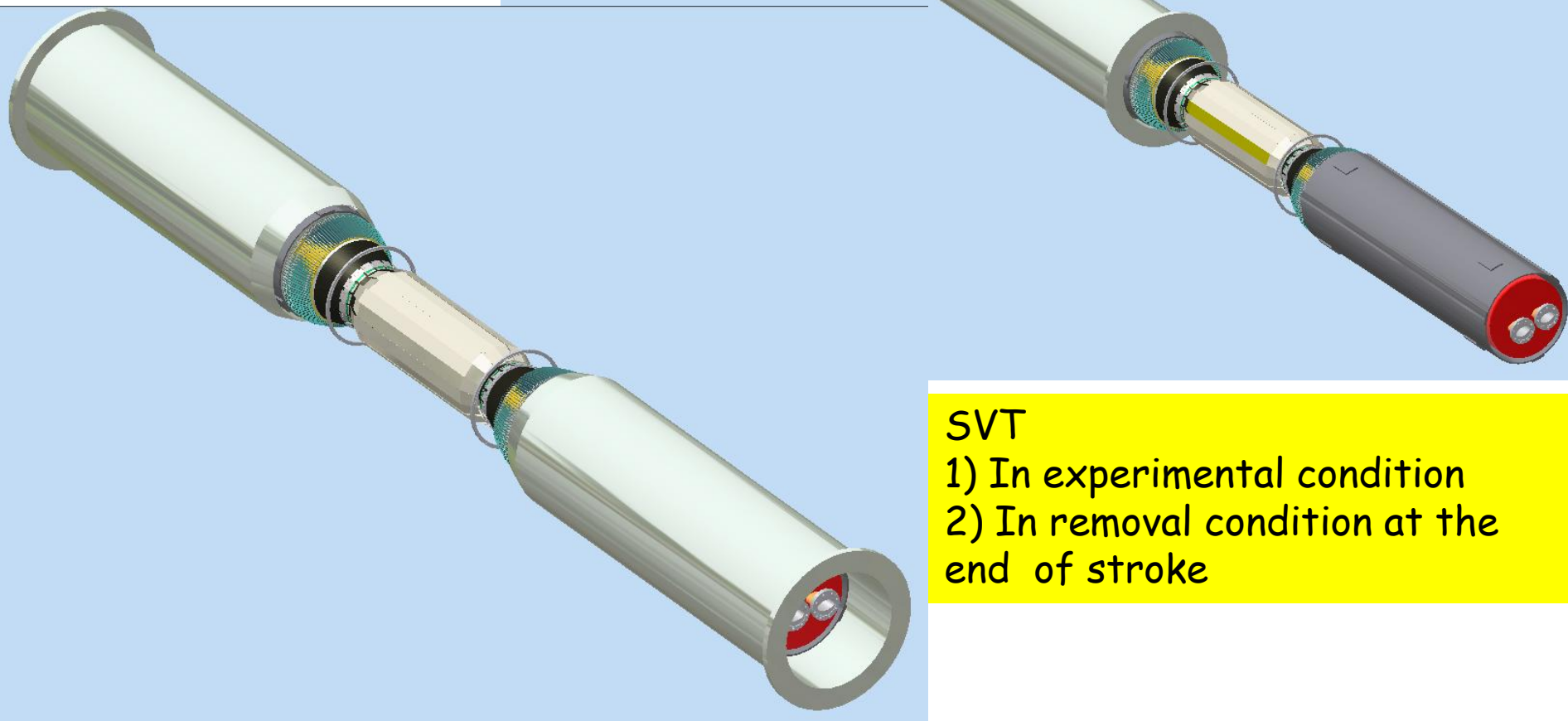


Quick demounting





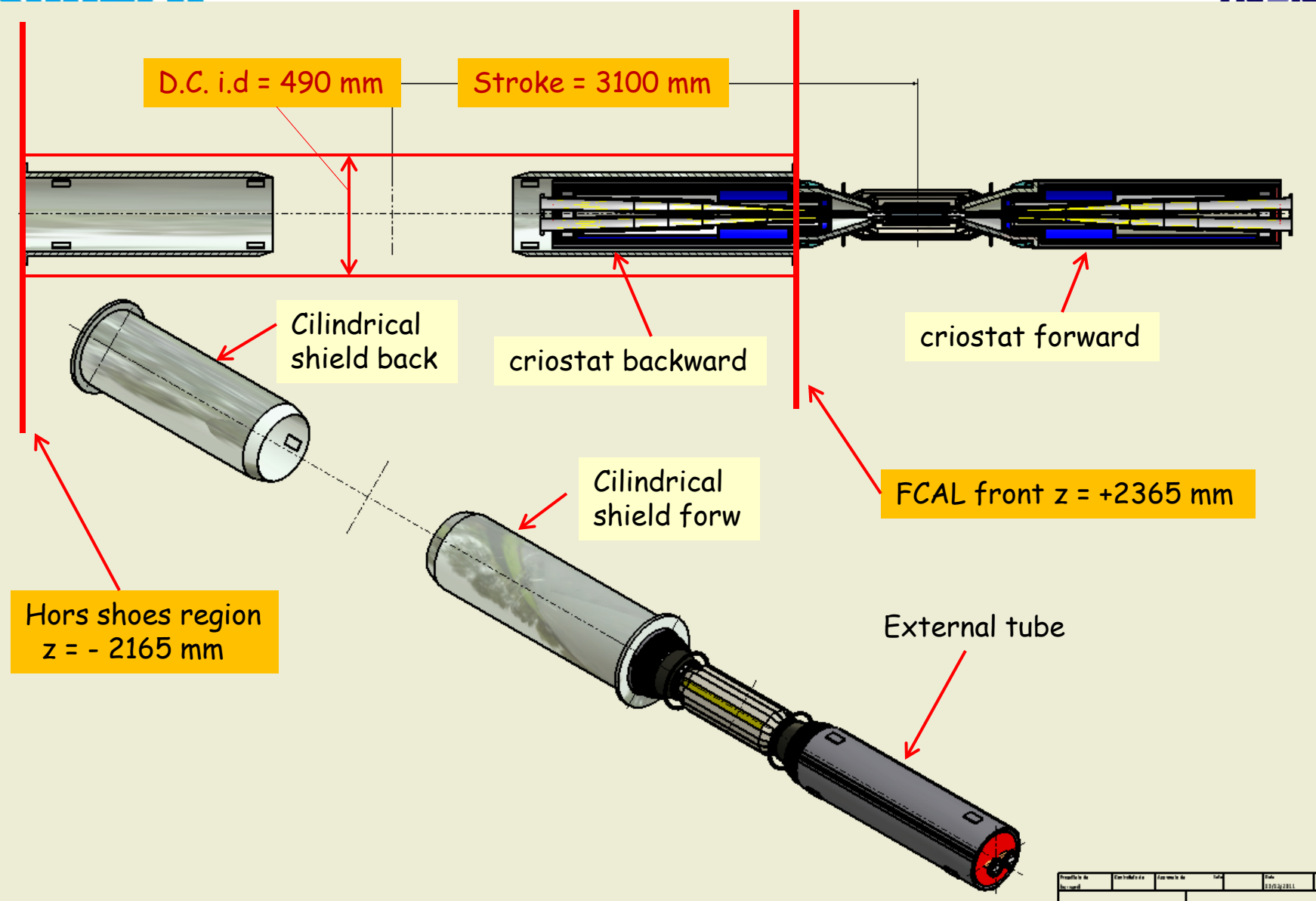
Quick demounting



SVT

- 1) In experimental condition
- 2) In removal condition at the end of stroke

Quick demounting





Conclusion

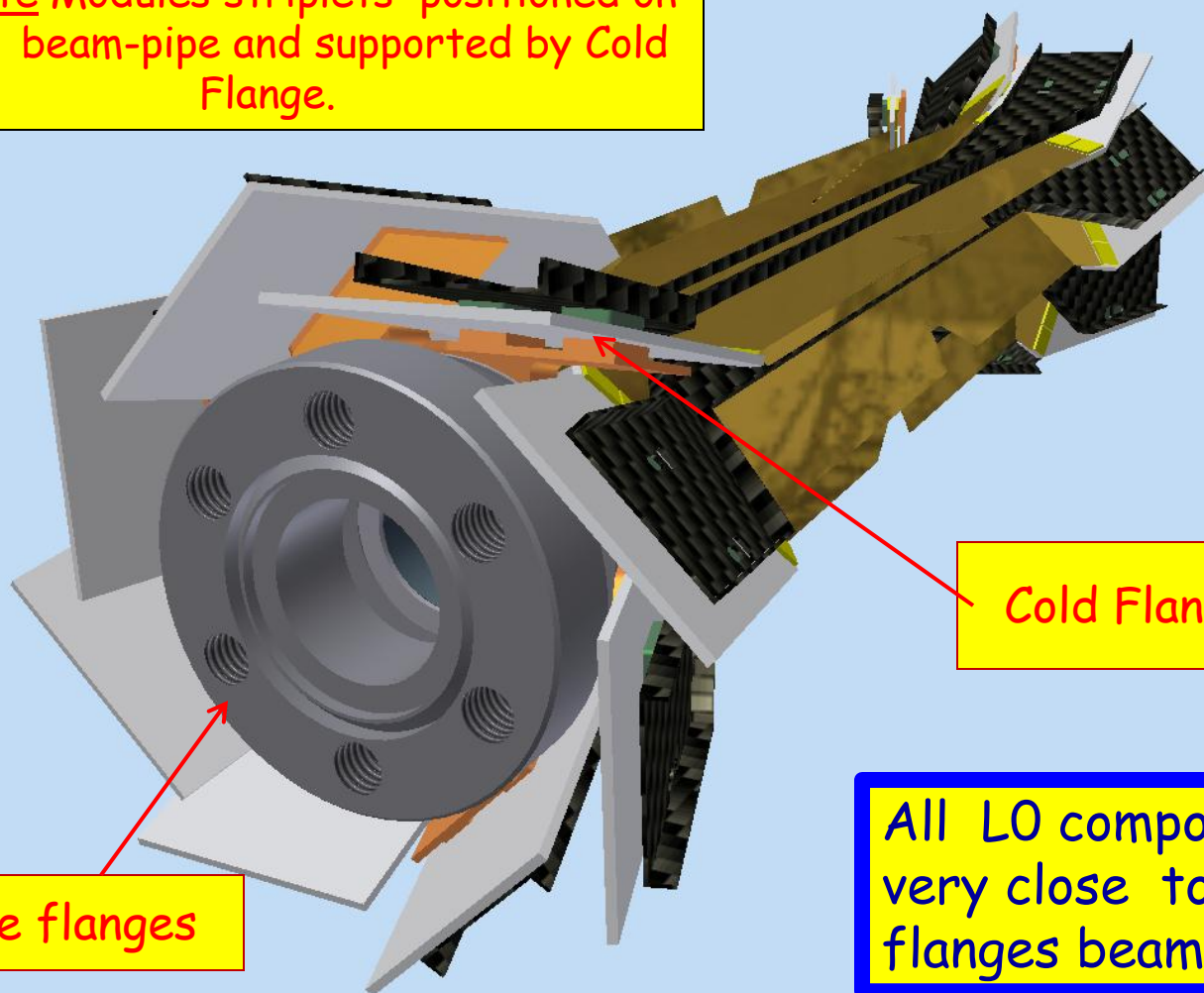


- 1) A lot of work realized on to eliminate SVT-LO conflict and on the architecture of I.R. that allow possible start the preparation of TDR on this issues .
- 2) Strong effort has to be put on the quick demounting operation that is still at beginning study; this issue will be the main effort of next month.
- 2) N.1 new engineer A. Bernardelli working in Pisa on SVT
- 3) N.1 Engineer S.Coelli at 50% will be operative at beginning of next year at INFN Milan to work on trans. card support , cooling simulation etc.
- 4) Good collaborating work with QMUL and real progress on the space-frame and supporting cones design



BACKUP

Complete Modules stripiets positioned on the Be beam-pipe and supported by Cold Flange.



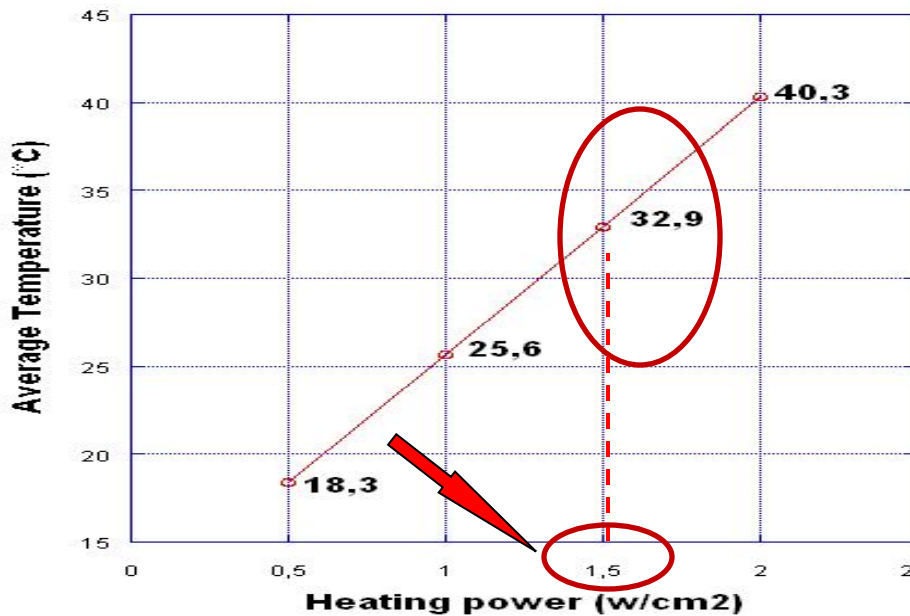
Be pipe flanges

Cold Flanges Buttons

All LO components very close to the flanges beam pipe

Full module H=550 μ m test results

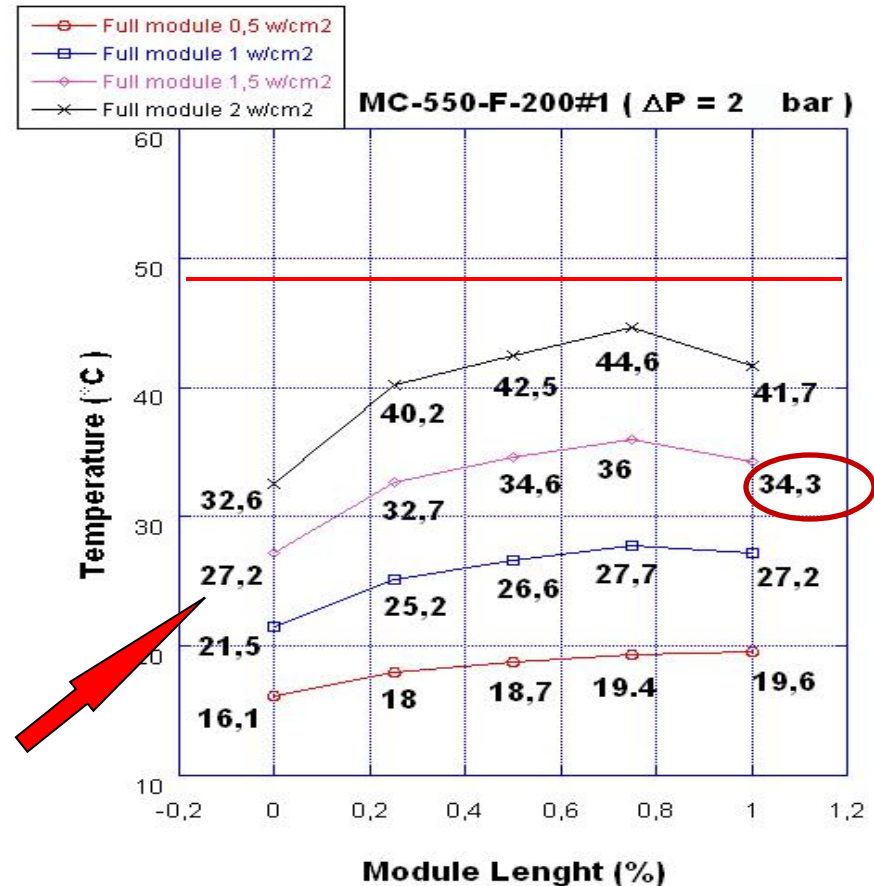
MC-550-F-200#1



Average module Temperature vs Specific Power

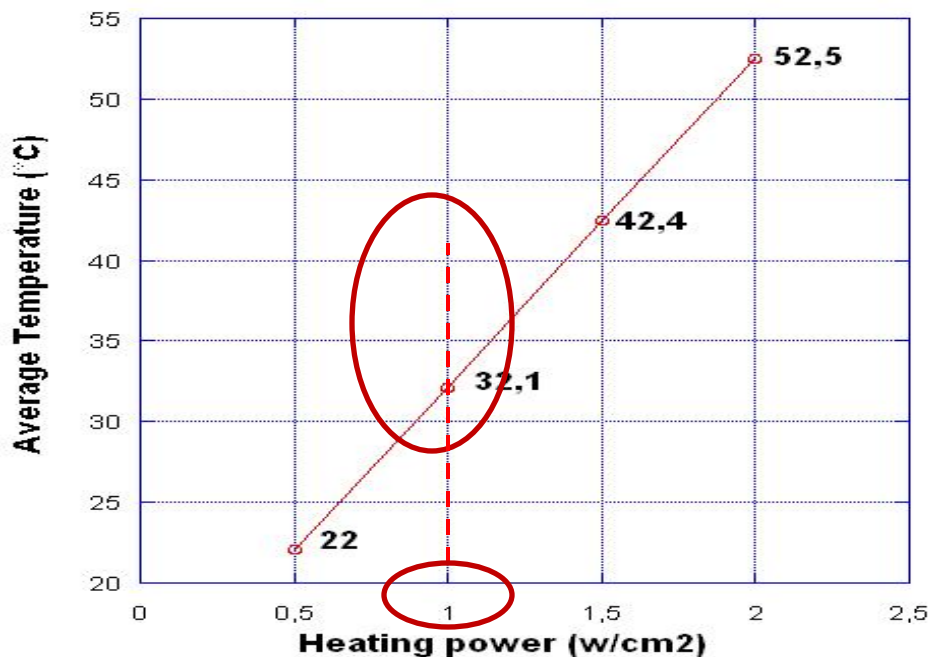
Temperature along the module:
 $\Delta T = 7.1$ °C at 1.5 W/cm² and $\Delta p = 2.0$ atm

Tests performed on full module sample (length = 120 mm) with water-glycol @ 10 °C as coolant ($\Delta p = 2.0$ atm).



Net Module H=550 μ m test results

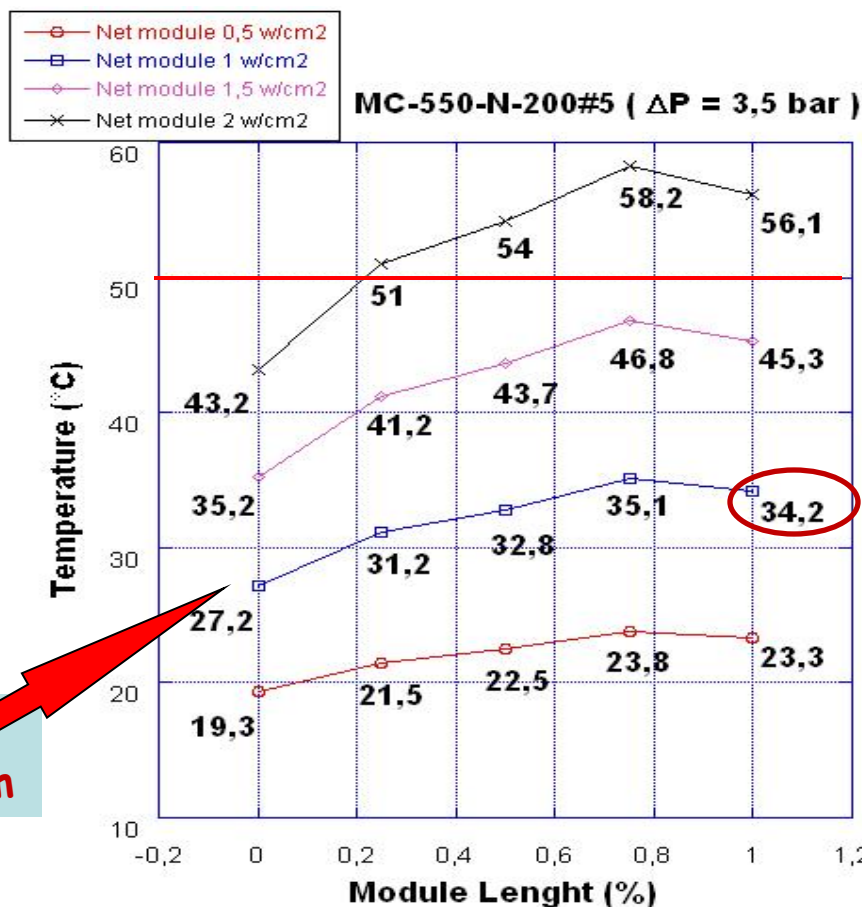
MC-550-N-200#5



Average module Temperature vs Specific Power

Temperature along the module:
 $\Delta T = 7.0$ °C at 1.0 W/cm² $\Delta p = 3.5$ atm

Tests performed on net module sample (length = 120 mm) with water-glycol @ 10 °C as coolant ($\Delta p = 3.5$ atm).



Comparison List

| | | % X0 | T max °C | Specific Power W/cm ² | Hydraulic. Diam. μm | Flow rate g/min | Δ Temperature °C |
|---|--|------|-------------|-------------------------------------|------------------------|--------------------|------------------------|
| 1 | Microchannel FULL Module support H=700 μm | | 35.8 | 2.0 | 300 | 244 | 5.3 |
| 2 | Microchannel NET Module support H=700 μm | 0.15 | 38.3 | 1.5 | 300 | 128 | 6.70.28 |
| 3 | Microchannel Full Module support H=550 μm | 0.22 | 34.3 | 1.5 | 200 | 33* | 7.1* |
| 4 | Microchannel NET Module support H=550 μm | 0.11 | 34.2 | 1.0 | 200 | 24 | 7.0 |

Tests performed on net module sample (length = 120 mm) with water-glycol @ 10 °C as coolant at $\Delta p = 3,5$ atm (Δp not valid for value *).

