

E. Peluso<sup>1,2</sup>, G. M. Apruzzese<sup>1</sup>, A. Belpane<sup>3</sup>, S. Palomba<sup>4</sup>, L. Senni<sup>5</sup>, E. Giovannozzi<sup>1</sup>, V. D'Agostino<sup>2</sup>, T. Craciunescu<sup>6</sup>, M. Gelfusa<sup>2</sup>, P. Gaudio<sup>2</sup> and L. Boncagni<sup>1</sup>

<sup>(1)</sup> ENEA, Nuclear Department, C.R. ENEA-Frascati, Via E. Fermi 45, 00044, Frascati (RM), Italy <sup>(2)</sup> Department of Industrial Engineering, University of Rome, Via del Politecnico 1, 00133, Rome (RM), Italy  
<sup>(3)</sup> Consorzio RFX (CNR, ENEA, INFN, Università di Padova, Acciaierie Venete SpA), Corso Stati, Padova, 35127, Italy, <sup>(4)</sup> DTT S.C.a.r.l., Via E. Fermi 45, I-00044, Frascati (RM), Italy  
<sup>(5)</sup> National Institute for Laser, Plasma and Radiation Physics, Magurele-Bucharest, Romania, <sup>(6)</sup> CNR - Institute for applied mathematics 'Mauro Picone' (IAC) Via dei Taurini, 19, 00185 - Roma - Italy

[emmanuele.peluso@enea.it](mailto:emmanuele.peluso@enea.it); [emmanuele.peluso@uniroma2.it](mailto:emmanuele.peluso@uniroma2.it)

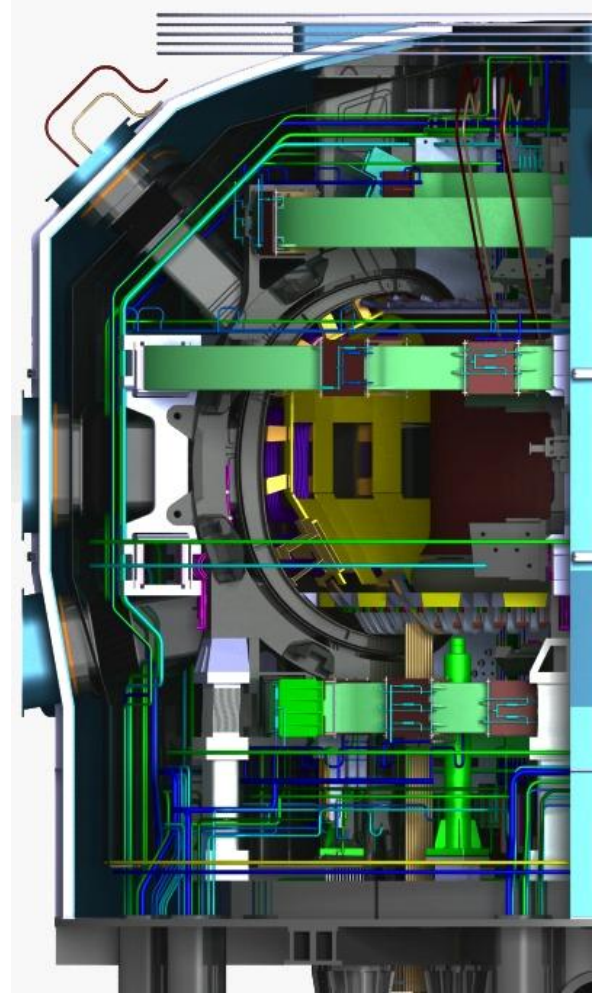
## Background:

The Divertor Tokamak Test (DTT) Facility is an experiment under construction at the ENEA Research Centre in Frascati; its main mission is to test the power extraction strategies for the first nuclear fusion power plant [1].

Currently, a Phase1, a Phase2 and a Phase3 are planned, with different implemented diagnostics and with increased external heating (~19MW, ~28MW and ~45MW respectively[2]).

A preliminary conceptual design of the bolometric diagnostic, requiring 216 lines of sight (LoS), has been completed [3]. The bolometers will be housed in a pinhole box support unit [4]; the thermo-mechanical analysis can be found in [5] instead. Synthetic profiles (phantoms) were considered to validate the overall layout by adapting an expectation maximisation algorithm for a maximum likelihood (ML) approach[6].

## DTT



R [m]	2.19
a [m]	0.70
I <sub>p</sub> [MA]	5.5
B <sub>T</sub> [T]	5.85
P <sub>tot</sub> [MW]	45
Pulse length [s]	100

For Single Null (SN), Flat-Top, Full Power Scenario  
 $T_e \sim 10 \text{ keV}$   
 $n_e \sim 2 \cdot 10^{20} \text{ m}^{-3}$

## Main features of the ML approach implemented

- The variance associated with the reconstructed emissivity and hence the uncertainties in the derived quantities can be obtained [7];
- an anisotropic smoothing has been implemented that can take into account differently oriented directional derivatives for smoothing[8];
- the width of each LoS is considered and both the etendue and the contribution of each truncated pyramidal voxel are estimated[6].

## Objectives of this contribution

Describe the designs or current state of the art of strategies for estimating:

- the radiated power of the plasma,  $P_{rad}$ , using directly arrays of Line Integrals (L.I) for a Real Time (RT) implementation;
- $P_{rad}$  in different regions of the plasma, using Region of Interest (ROIs) in RT for feedback control;
- tomograms from a ML approach during the inter-shot phase to provide more accurate estimates of  $P_{rad}$  in different locations of the device as well as radiation profiles

## Estimation of $P_{rad}$ from arrays of L.I in RT (A objective)

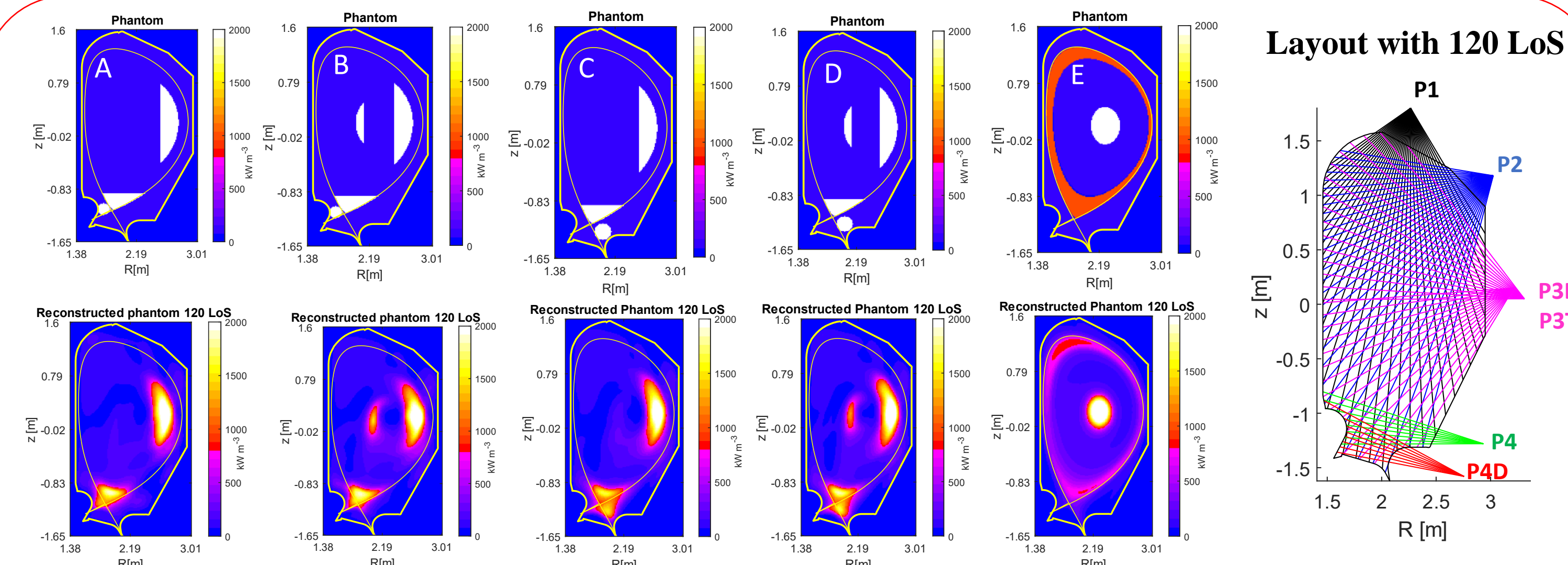
Starting from the absorbed power from a detector,  $P_m$ , the L.I or  $I_m$ , can be derived for a bolometer  $m$ , i.e. :

$$P_m = \sum_p \# \text{ voxel} (\epsilon_p dV_p d\Omega_p)_m = \frac{E_m}{4\pi} I_m \Rightarrow I_m = \sum_p \# \text{ voxel} H_{mp} \epsilon_p = \int \epsilon(r, \theta) dl_m$$

where  $\epsilon$  is the synthetic emissivity profile described by a phantom;  $p$  stands for a truncated pyramidal voxel, seen by the detector with etendue  $E$ , with a volume  $dV$  and emitting by an infinitesimal solid angle  $d\Omega$  towards the bolometer. The radiated power  $P_j$  inside the vacuum vessel can be derived from an array of  $q$  bolometers (i.e. P1, P2 or P3) by a weighted sum of the L.I:

$$P_j = 2\pi R_0 \sum_q \# \text{ L.I.} S_{qj} \left( \frac{I_{qj}}{L_{qj}} \right) c_j$$

Where the length of each LoS is  $L$  and the poloidal section of the LoS is  $S$



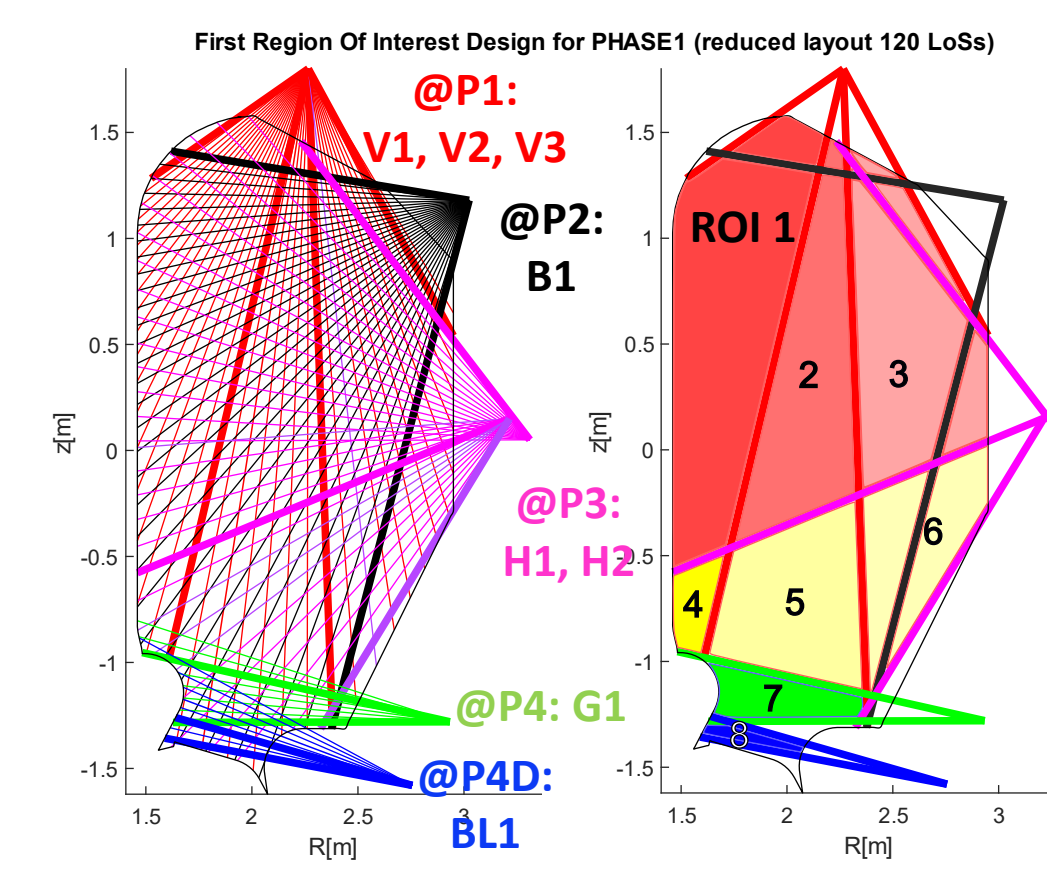
Phantom	ML		Array P1		Array P2		Array P3		P1 and P2		P1,P2 and P3	
	$P_{rad}$ [MW]	$\epsilon\%$	$P_{rad}$ [MW]	$\delta\%$	$P_{rad}$ [MW]	$\delta\%$	$P_{rad}$ [MW]	$\delta\%$	$P_{rad}$ [MW]	$\delta\%$	$P_{rad}$ [MW]	$\delta\%$
A	13.44	13.43	12.96	-3.92	13.72	1.86	14.18	5.06	13.34	-0.94	13.62	1.14
B	14.63	14.62	14.49	-0.86	14.96	2.26	15.18	3.69	14.73	0.72	14.87	1.73
C	13.93	13.91	13.32	-4.55	14.00	0.54	14.49	3.87	13.66	-1.95	13.93	0.070
D	15.13	15.15	14.79	-2.35	15.22	0.48	15.48	2.16	15.00	-0.91	15.16	0.12
E	16.72	16.41	18.59	11.72	15.62	-5.15	14.30	-14.77	17.10	4.02	16.17	-1.52

Where  $\epsilon$  stands for the percentage error estimated using the ML approach from a set of projections with normal added Gaussian noise[6];  $\delta$  stands for the discrepancy in percentage between the L.I estimates of  $P_{rad}$  and the expected one.

## Estimation of $P_{rad}$ from ROIs for RT feedback control (B objective)

The RT feedback control of the radiation pattern for prevention is a delicate matter. In seeding experiments, an unstable X-point radiator could lead to a Multifaceted Asymmetric Radiation From the Edge (MARFE) [9] and then to a so-called density limit disruption. Another example of a possible perturbation pathway would be the growth and dynamics of Tearing Modes (TM), which have recently been linked to impurity fluxes and their accumulation[10][11].

A wise approach would be to monitor not only the total radiated power, but also the power radiated from different regions of the device. A fast, but approximate method can be found in [12]. Here it has been adapted for DTT by defining the following closed system composed of eight initial ROIs.



Measurements	ROIs #
V1	1,4
V2	2,5,7,8
V3	3,6
H1	1,2,3
H2	4,5,6,7,8
P4	7
P4D	8
B1	1,2,3,4,5,6,7,8

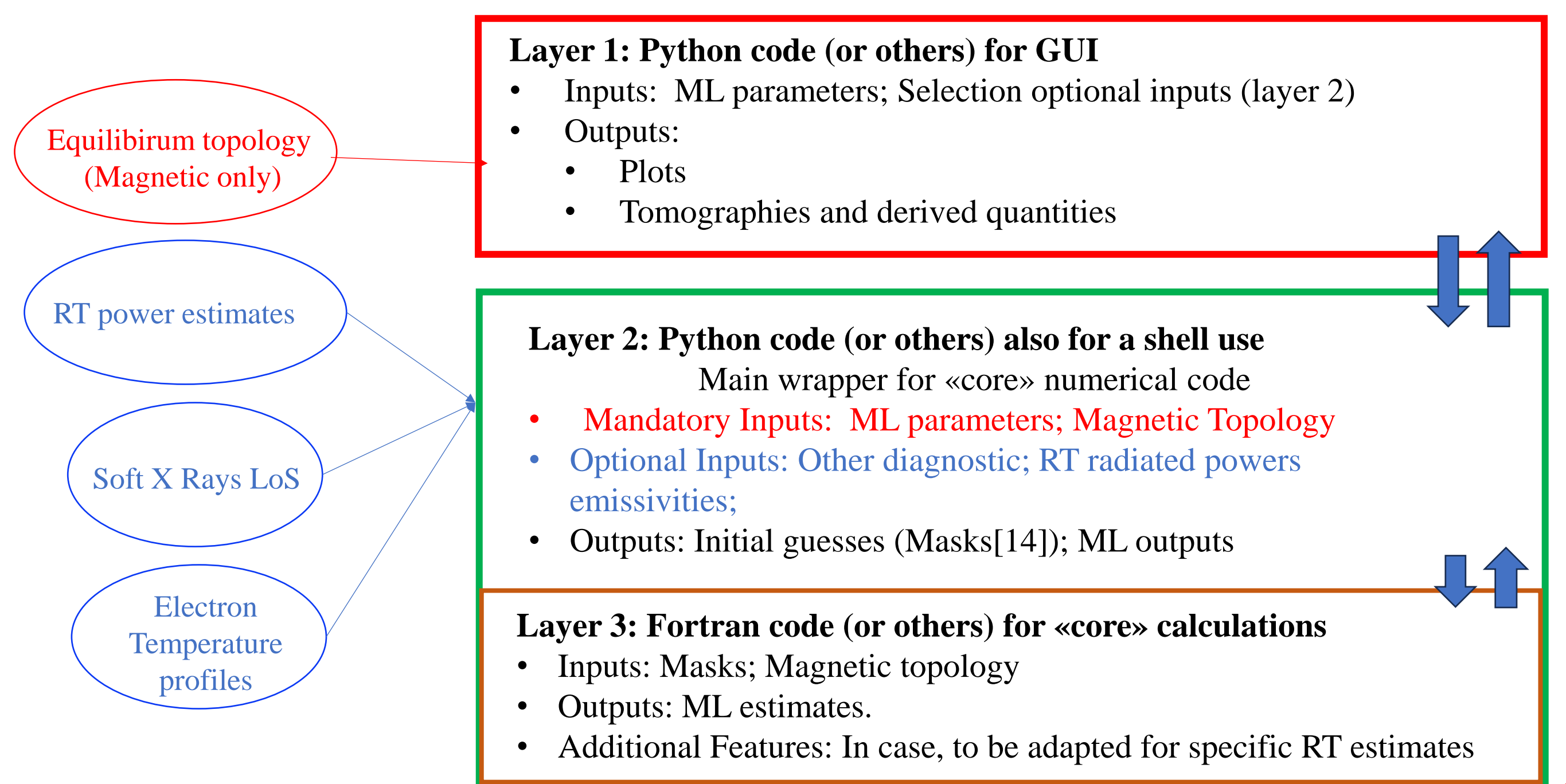
$$\begin{cases} V_1 = 2\pi R_0 \sum_q \# \text{ L.I.} \in V1 S_{q1} \left( \frac{I_{q1}}{L_{q1}} \right) = \frac{S_{ROI1}}{S_{V1}} P_{ROI1} + \frac{S_{ROI4}}{S_{V1}} P_{ROI4} \\ B1 = 2\pi R_0 \sum_q \# \text{ L.I.} \in B1 \dots = \sum_r \frac{S_{ROI r}}{S_{B1}} P_{ROI r} \end{cases} \Rightarrow \begin{pmatrix} V_1 \\ V_2 \\ V_3 \\ H_1 \\ H_2 \\ G_1 \\ B1 \end{pmatrix} = \mathbb{G} \begin{pmatrix} P_{ROI1} \\ P_{ROI2} \\ P_{ROI3} \\ P_{ROI4} \\ P_{ROI5} \\ P_{ROI6} \\ P_{ROI7} \\ P_{ROI8} \end{pmatrix}$$

The matrix  $\mathbb{G}$  contains the imposed geometric weights representing the fraction of the poloidal areas for each ROI. Using a non-negative least-squares fit, the radiated power  $P_{ROI1, \dots, 8}$  in each region can be estimated in RT.

## $P_{rad}$ from ML tomograms for intershot analysis (C objective)

The error-free estimation of the ML code can in principle run in RT, as it is based on standard low-dimensional matrix computations [13]; however, such an option could in principle lead to a possible misuse of the results.

A better approach would be to optimise the algorithm and implement a layered code, including a GUI, for inter-shot analysis aimed at providing tomograms and the derived quantities with their uncertainties from the ML approach.



## Work in progress (STAY TUNED!)

- The designed strategies need to be extensively tested on different configurations (SN, X-Divertor and Negative Triangularity) and mimicking some time slices of a pulse with phantoms.
- Efforts must be made to:
  - obtain a consolidated set of weights ( $c_j$ ) by studying more synthetic profiles;
  - both study and further define a layout of the ROIs for RT, also taking into account a possible modification of the layout for Phase 1;
  - realise the described inter-shot analysis tool and build the actual interfaces with CODAS.

## References and Acknowledgment

- [1] F. Romanelli 2024 Nuclear Fusion. IOP Publishing on behalf of the IAEA
- [2] F. Crisanti, G. Giruzzi and P. Martin, 2024, DIVERTOR TOKAMAK TEST facility Research Plan
- [3] G. M. Apruzzese, submitted to 50th EPS Conference, Salamanca, Spain (08th-12th July 2024)
- [4] A. Belpane, ICFDT7, Frascati, Italy, (21st-28th October 2024)
- [5] V. D'Agostino 33rd SOFT, Dublin, Ireland (22nd -27th September 2024)
- [6] E. Peluso, 33rd SOFT, Dublin, Ireland (22nd -27th September 2024)
- [7] T. Craciunescu et al., 2018, Rev. Sci. Instrum. 89,053504, <https://doi.org/10.1063/1.5027880>
- [8] T. Craciunescu et al., 2023 Phys. Scr. 98 125603 <https://doi.org/10.1088/1402-4896/ad081e>
- [9] M. Bernert et al. Nuclear Materials and Energy 34 (2023) 101376
- [10] G. Pucella et al. Nucl. Fusion 61 (2021) 046020 (12pp)
- [11] S. Zeng et al., Nucl. Fusion 63 (2023) 046018 (12pp)
- [12] R. Rossi et al. Matter Radiat. Extremes 8, 046903 (2023)
- [13] H.H. Barrett et al., I. Theory, Phys. Med. Biol. 39, 833-846 (1994).
- [14] E. Peluso et al., 2022, Plasma Phys. Control. Fusion 64 045013, <https://doi.org/10.1088/1361-6587/ac4854>

Authors are grateful to:  
Antonio Castaldo (ENEA), Lori Gabelleri (DTT), Matteo Iafraiti (ENEA)