



SAPIENZA
UNIVERSITÀ DI ROMA

Development of superconducting magnets for the future Muon Collider

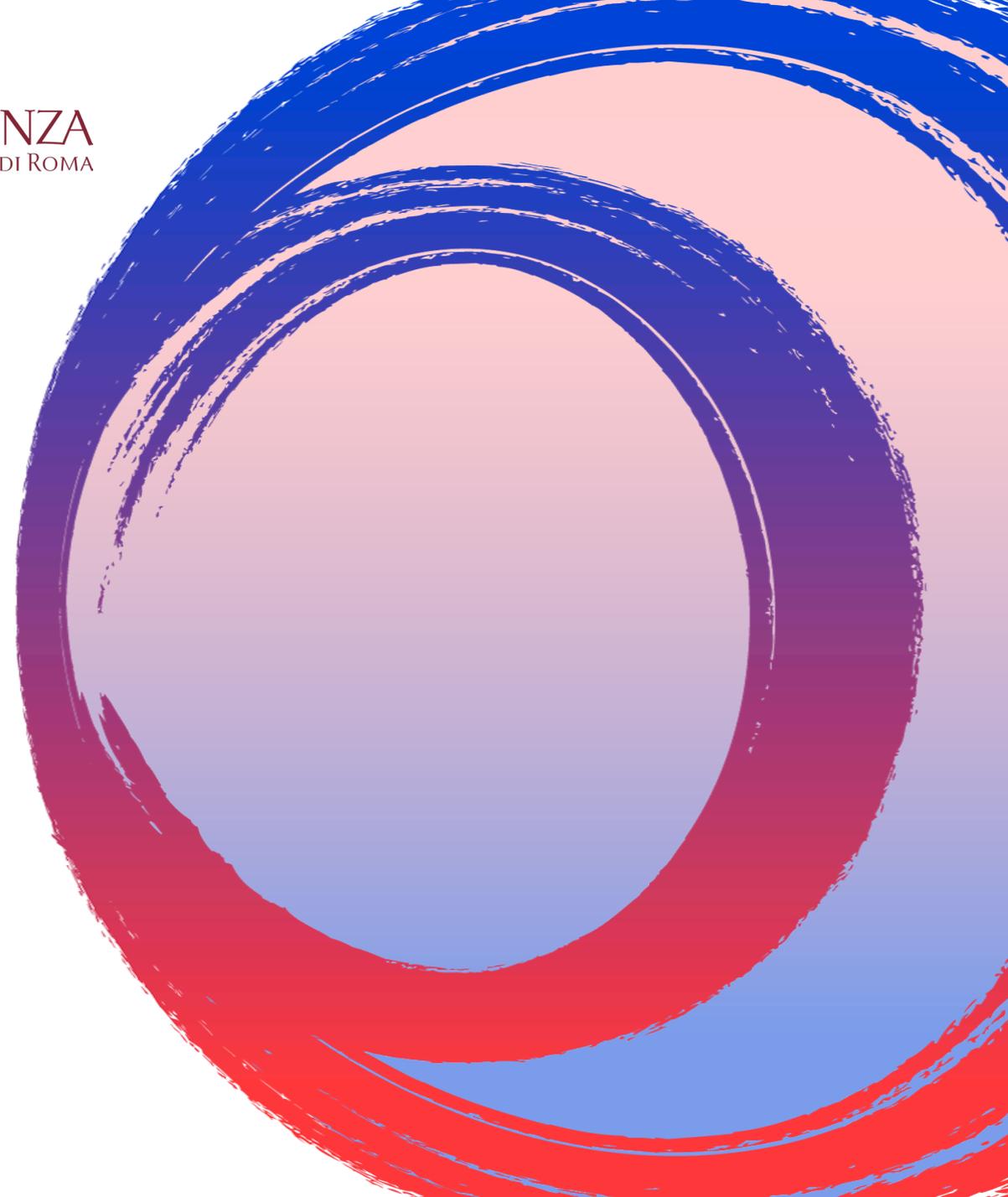
Daniel Novelli

Ph.D. in Accelerator Physics – XXXVIII cycle

24 October 2024



Funded by the European Union (EU). Views and opinions expressed are however those of the author only and do not necessarily reflect those of the EU or European Research Executive Agency (REA). Neither the EU nor the REA can be held responsible for them.





Why a Muon Collider?

IMCC (International Muon Collider Collaboration) aims at studying the feasibility of a 10 km, 10 TeV center of mass energy **Muon Collider**, as indicated by the European Strategy for Particle Physics.

The Muon Collider is a very promising post-LHC high physics facility:

- μ 200 times heavier than electron ($m_\mu = 105.7 \text{ MeV}/c^2$, $m_e = 0.511 \text{ MeV}/c^2$) $\rightarrow 10^9$ times less radiation loss.
- μ elementary particle: all COM energy available for the collision, contrary to hadron machines.

BUT μ decays in $2.2 \mu\text{s}$ in rest frame:

- must be produced, accelerated and collided ASAP
- decay products must be shielded to avoid damage to the machine or radiation

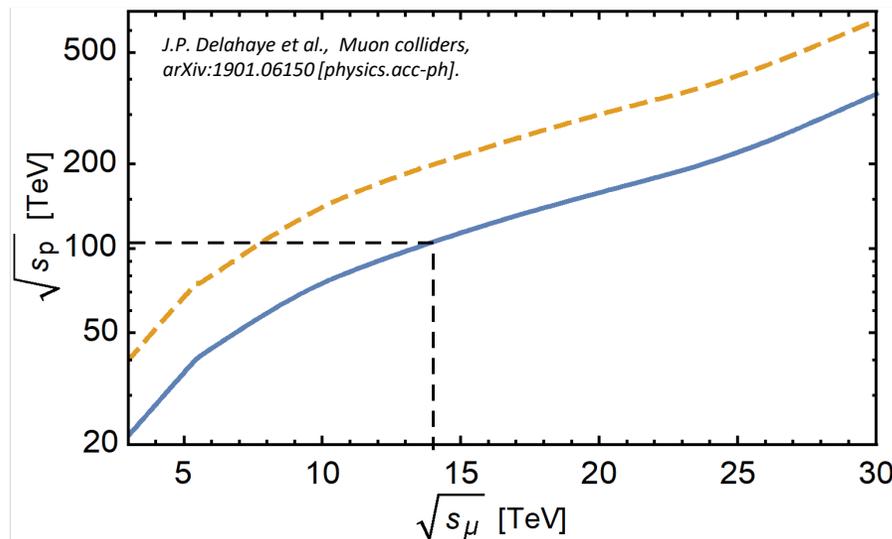
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Physics?

Muon collisions in the range of 14 TeV have comparable discovery potential to hadron (proton) collisions in the range of 100 TeV

- Comparable Feynman amplitudes for the muon and the proton production processes.
- A factor of ten enhancement of the proton production amplitude squared, possibly due to QCD production, is considered.

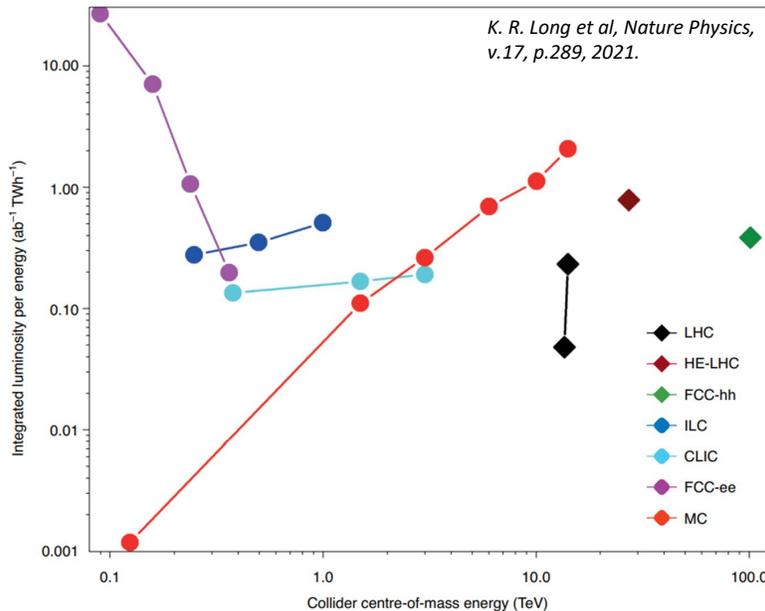
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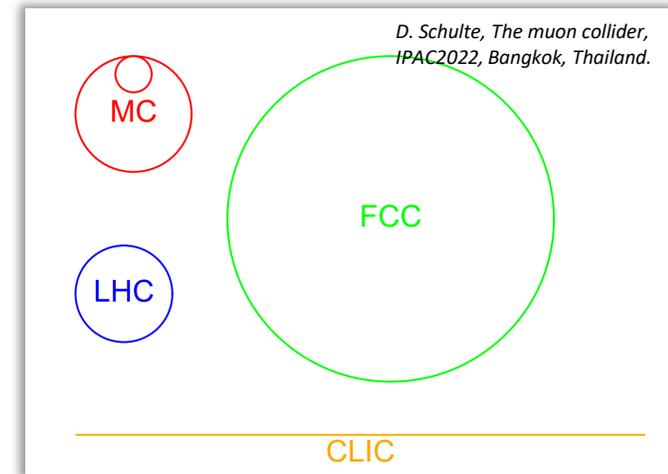
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Sustainability?

A 10 TeV muon collider
can provide the highest integrated luminosity
per unit of energy consumption.

Collider size comparison



Why a Muon Collider?

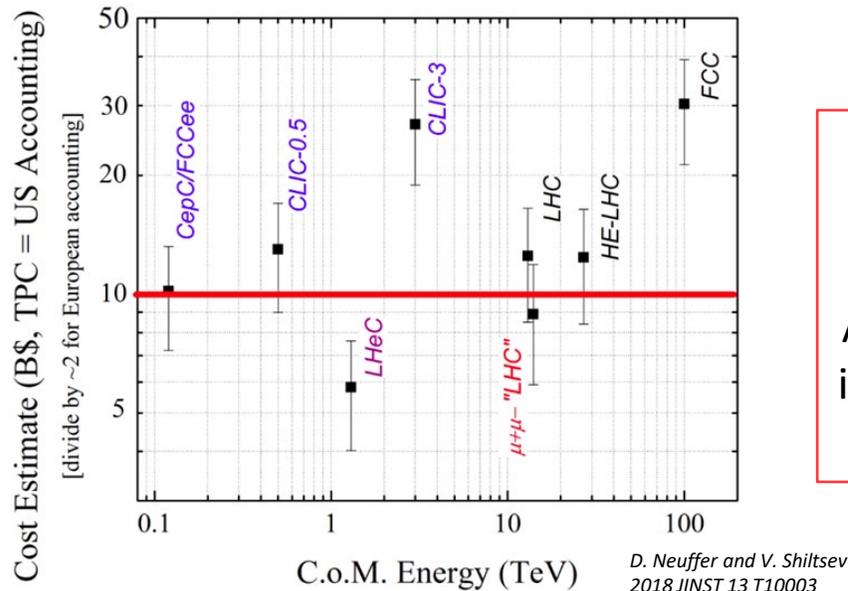
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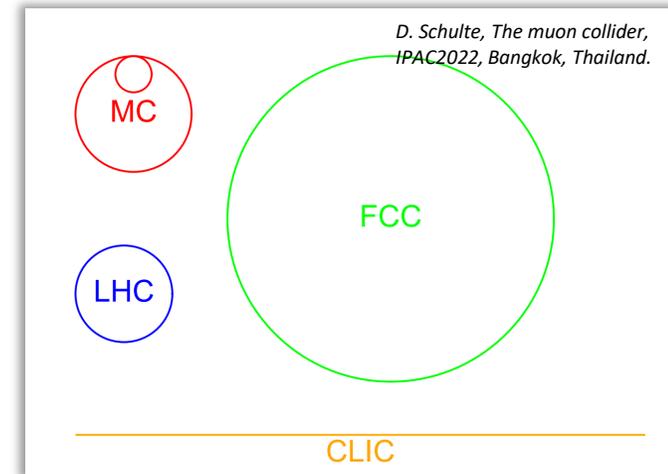
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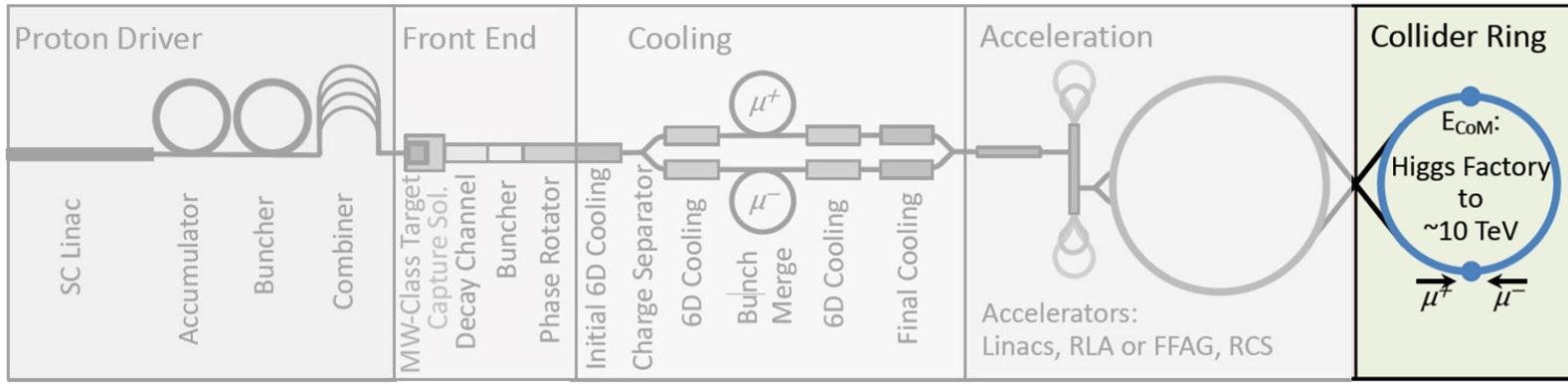
Affordability?

Its size is competitive because it is compact.
A 10 TeV muon collider making use of the LHC infrastructure could be the most cost-effective energy frontier collider

Collider size comparison



Main stages of a muon collider complex



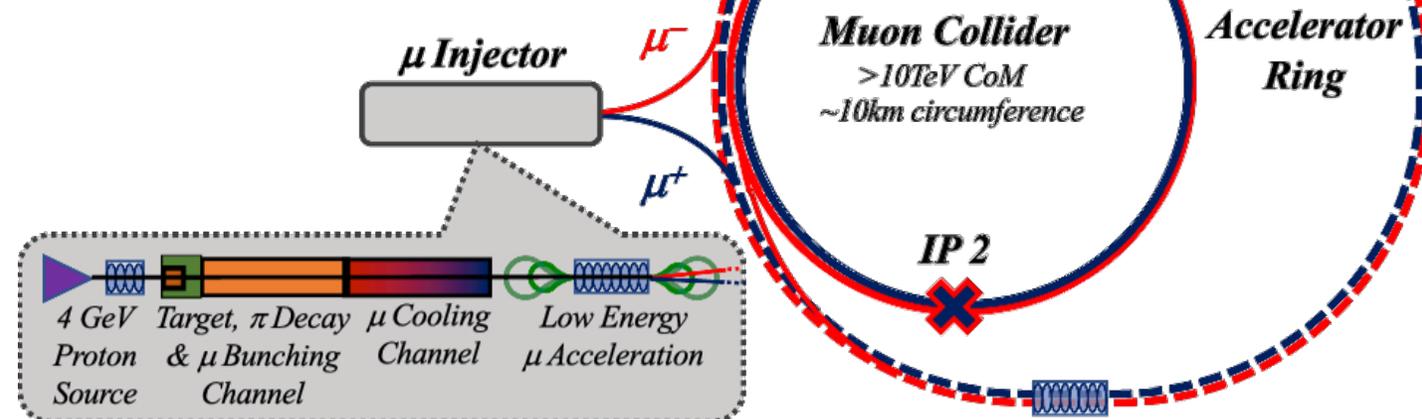
Task 7.4

Magnets:

- **Dipoles**
- **Quadrupoles**
- Sextupoles

Purpose:

- Evaluate realistic performance targets for the collider magnets, in close collaboration with studies of beam physics, cryogenics, and energy storage.
- Produce a credible and affordable design study (contain costs, energy efficiency, sustainable operation).

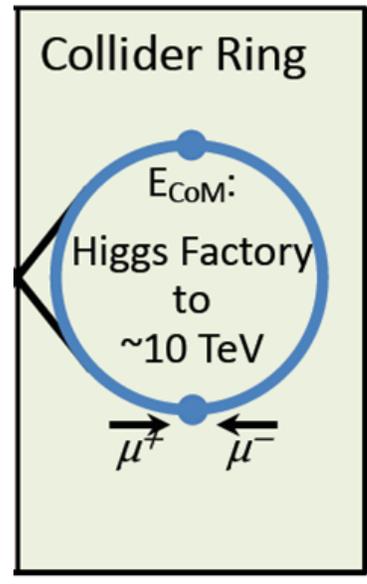


3 TeV collider (5 km ring):

- Close to state of the art
- $\sim 11\text{T}/150\text{mm}$ (Nb_3Sn)
- 600 magnets, 5 m length
- Operating temperature: 4.5 K

10+ TeV collider (10 km ring):

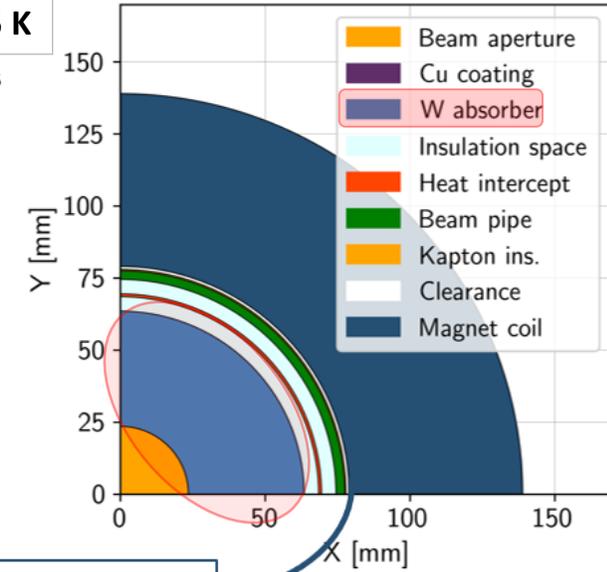
- HTS magnets, R&D is required
- $\sim 15\text{T}/150\text{mm}$ (ReBCO, hybrid)
- 1200 magnets, 5 m length
- Operating temperature: 4.5...20 K



Assuming 10 TeV machine and coil at 4.5 K

- Beam aperture (5σ) 23.5 mm radius
 - Cu layer beam screen 0.01 mm thick
 - Tungsten absorber 40 mm thick
 - Insulation space 5 mm thick
 - Heat intercept 1 mm thick
 - Insulation space 5 mm thick
 - Beam pipe 3 mm thick
 - Kapton insulation 0.5 mm thick
 - Clearance 1 mm thick
 - Coil pack* (60 mm thick)
- *thickness TBD, placeholder

Courtesy of Patricia Borges de Sousa
<https://indico.cern.ch/event/1250075/contributions/5357594/>



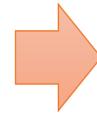
Coil aperture 158 mm

with HTS @20K the absorber can be thinner

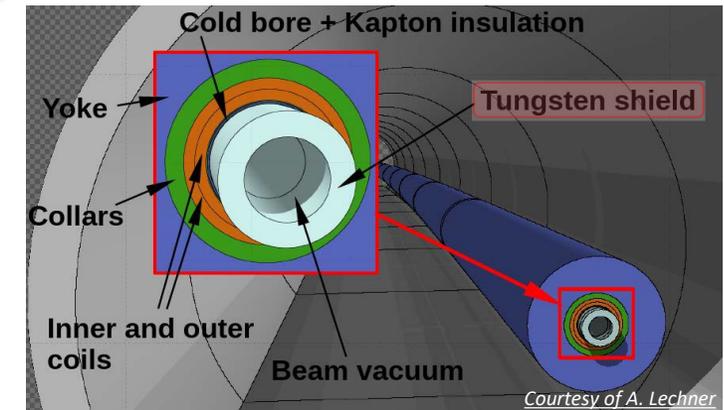
➤ **High field** dipoles to minimize collider ring size and maximize luminosity.

➤ **Beam loss protection**

High-energy electrons and positrons arising from muon decay and striking the collider ring magnets can cause radiation damage and unwanted heat load.



- **Shielding**
- **Large aperture**



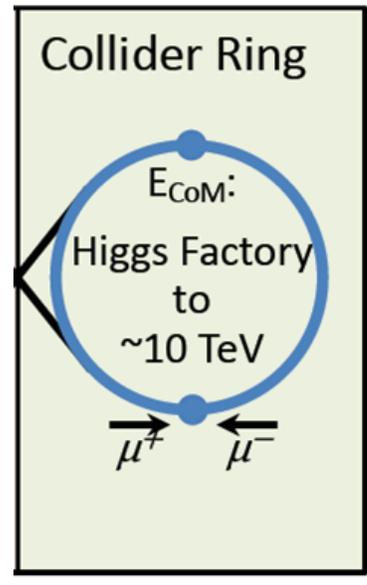
Courtesy of A. Lechner

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10+ TeV collider (10 km ring):

- HTS magnets, R&D is required
- $\sim 15\text{T}/150\text{mm}$ (ReBCO, hybrid)
- 1200 magnets, 5 m length
- Operating temperature: 4.5...20 K



Arc:

- Combined function magnets: B1, B1+B2 and B1+B3
- $B \approx 8...16\text{ T}$; $G \approx 320\text{ T/m}$; $G' \approx 7100\text{ T/m}^2$
- Aperture $\approx 160\text{ mm}$

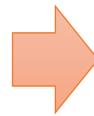
Final focus:

- Combined function magnets: B1, B2, B1+B2, B1+B3
- $B \approx 4...16\text{ T}$; $G \approx 100...300\text{ T/m}$; $G' \approx 12000\text{ T/m}^2$
- Aperture $\approx 150...330\text{ mm}$

➤ **High field** dipoles to minimize collider ring size and maximize luminosity.

➤ **Beam loss protection**

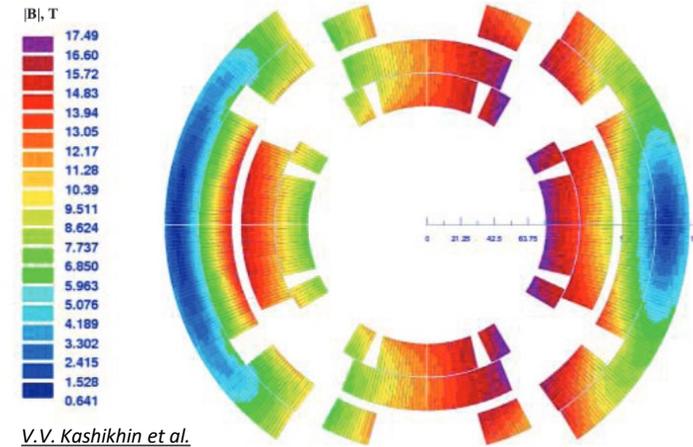
High-energy electrons and positrons arising from muon decay and striking the collider ring magnets can cause radiation damage and unwanted heat load.



➤ **Shielding**

➤ **Large aperture**

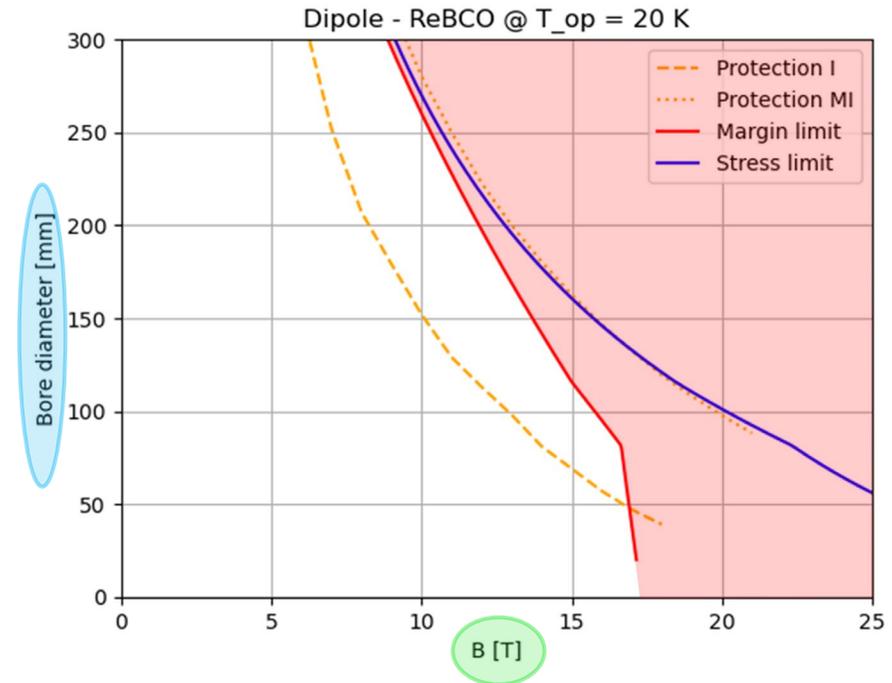
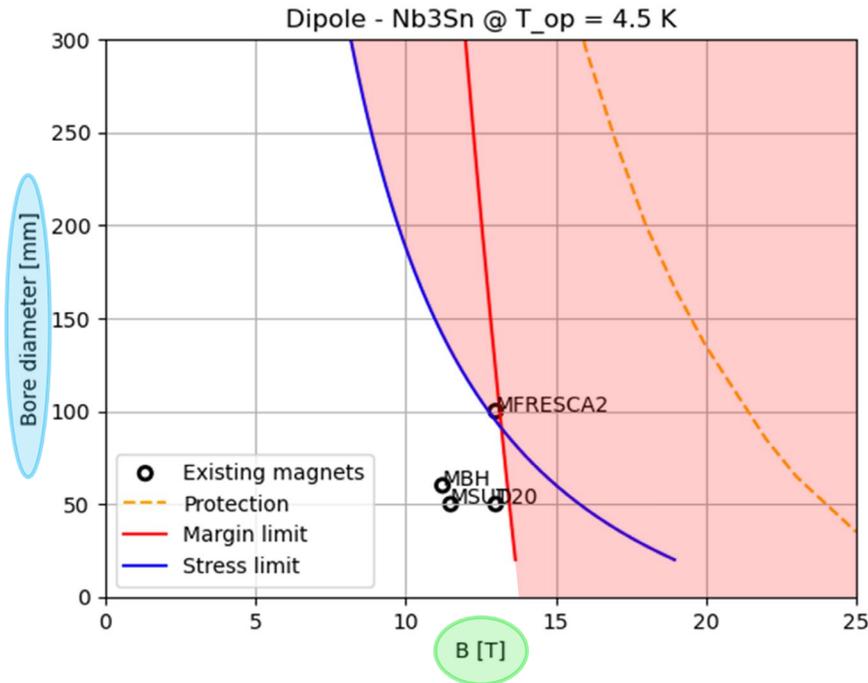
Difficult to define a single magnet specification



Need for high fields in large apertures

- We perform plots that can show the allowed area between aperture diameter (A) and bore field (B).

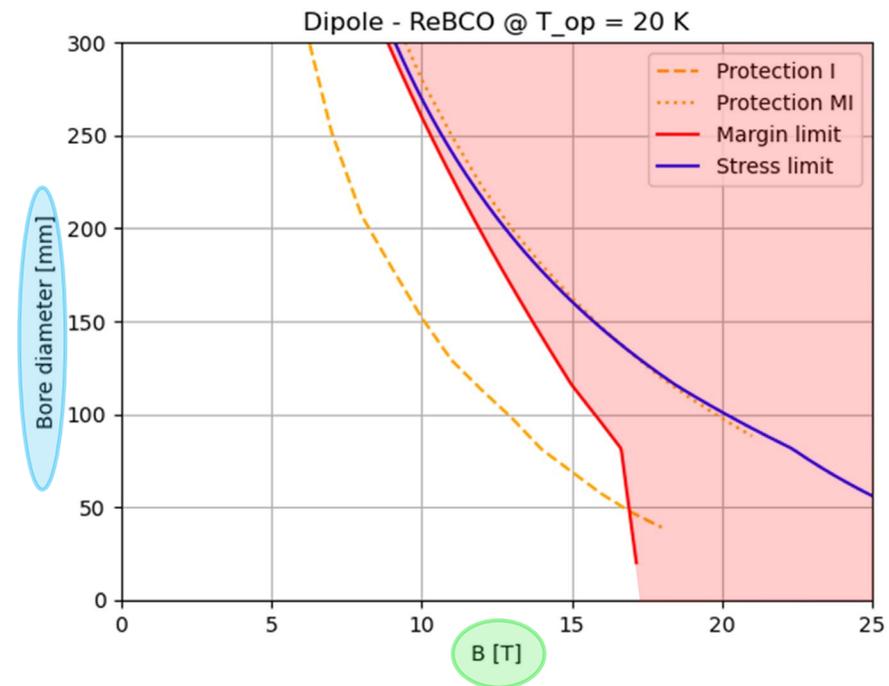
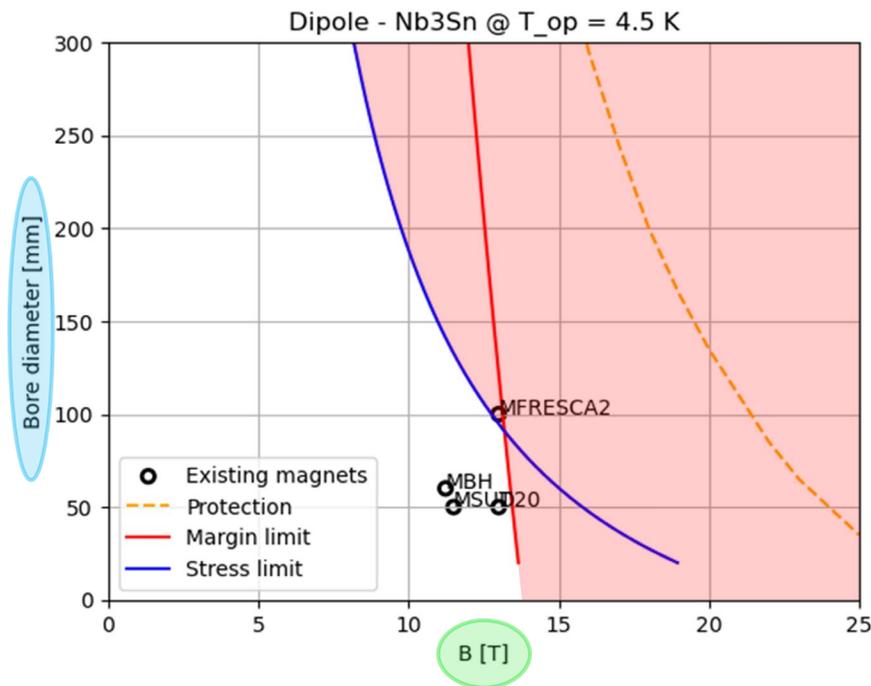
- ✓ Innovative approach, useful for interfacing the needs of beam dynamics with the technological limits (of today and the near future) related to superconducting magnets.
- ✓ Immediate feedback capable of analyzing many possible configurations in a single plot



Need for high fields in large apertures

- We perform plots that can show the allowed area between aperture diameter (A) and bore field (B).
- We consider Nb₃Sn for the 3 TeV machine and HTS (ReBCO) for the 10 TeV collider.

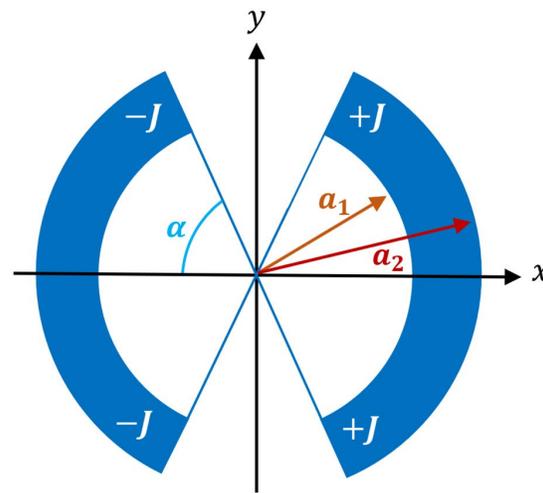
- Limit curves are introduced by mechanical challenges (stress limit), critical current density (margin limit) and stored magnetic energy (quench protection), depending on the superconducting material.



- A Python code is used to implement the **analytic formulas** for the cos-theta magnets in **sector coil** approximation.

(α is 60° for the dipole and 30° for the quadrupole)

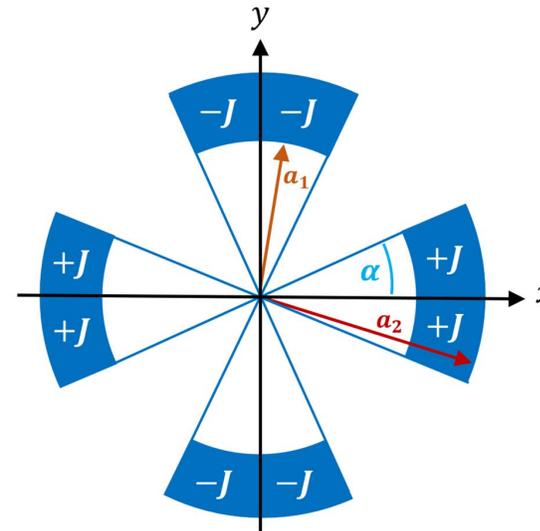
Dipole



$$B(w, J) = \frac{2\mu_0 J (a_2 - a_1) \sin \alpha}{\pi}$$

($w = \text{coil width}$)

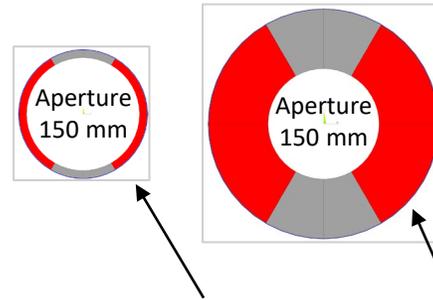
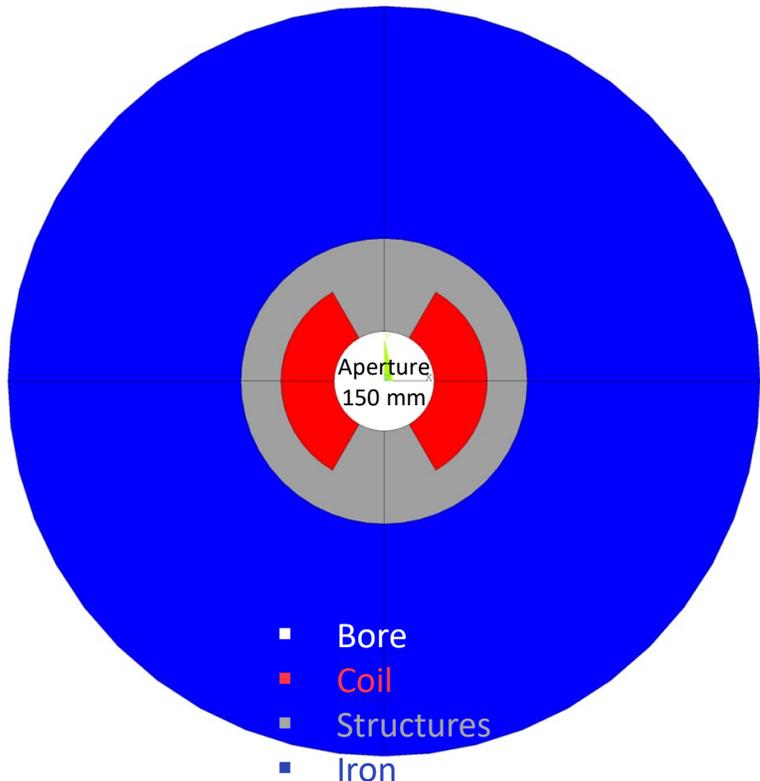
Quadrupole



$$G(w, J) = \frac{2\mu_0 J}{\pi} \ln \left(\frac{a_2}{a_1} \right) \sin(2\alpha)$$

- A Python code is used to implement the **analytic formulas** for the cos-theta magnets in **sector coil** approximation.
- **Cost model:** by setting an upper limit to the cost of the magnet, the maximum coil width can be calculated for each aperture, taking into account the other components.

Example diagram with bore aperture set at 150 mm.



Coil width: $10 \text{ mm} \leq w_c \leq 80 \text{ mm}$
 $\rho_{coil} = 8000 \text{ kg/m}^3$

Structures: $w_s \leq 60 \text{ mm}$
 SS cost: 10 EUR/kg (HL-LHC)
 $\rho_{ss} = 7800 \text{ kg/m}^3$

Iron yoke: $w_i \leq 350 \text{ mm}$
 Fe cost: 8 EUR/kg (HL-LHC)
 $\rho_{Fe} = 7800 \text{ kg/m}^3$

Total cost of the magnet = 400 kEUR/m
 (FCC-hh 175 kEUR/m [ref])

Cost of the labour = 20 kEUR/m (LHC)

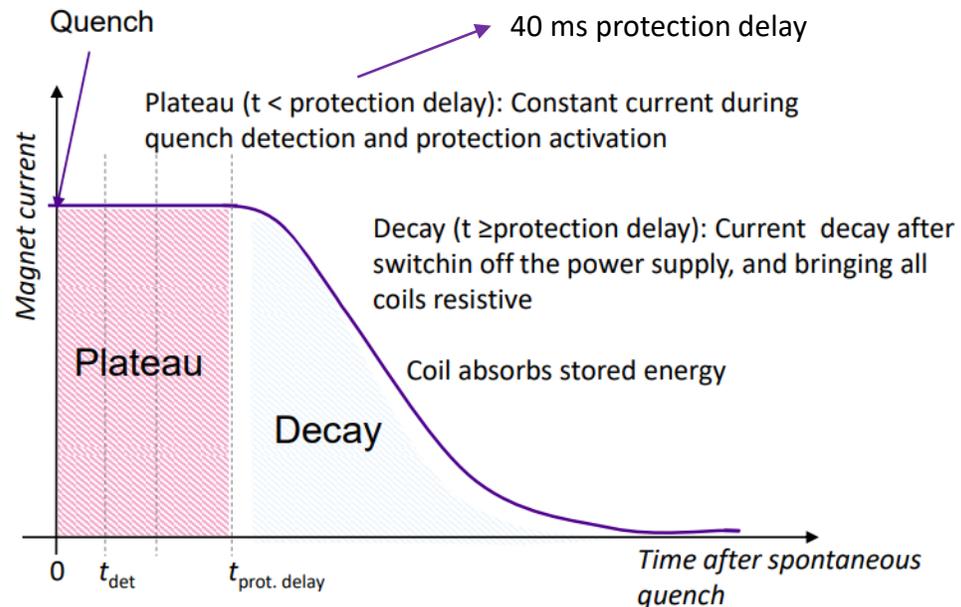
Materials	SC cost [EUR/kg]	Aspirational SC cost [EUR/kg]
Nb ₃ Sn	2000	700 (FCC target)*
ReBCO	8000	2500 (realistic projection)**

* 7€/kAm, FCC
 target 5€/kAm

** 50 €/kAm: 1/3 of today prize (150€/kAm)
 Also based on projection of ref
 A. Molodyk and C. LARBALÉSTIER, Science, 2023

The maximum total cost of the magnet is the same for both materials.

- A Python code is used to implement the **analytic formulas** for the cos-theta magnets in **sector coil** approximation.
- **Cost model:** by setting an upper limit to the cost of the magnet, the maximum coil width can be calculated for each aperture, taking into account the other components.
- The **protection scheme** consists in QH (or CLIQ) for classical insulated coils, limiting the hotspot temperature and the stored energy in the coils.



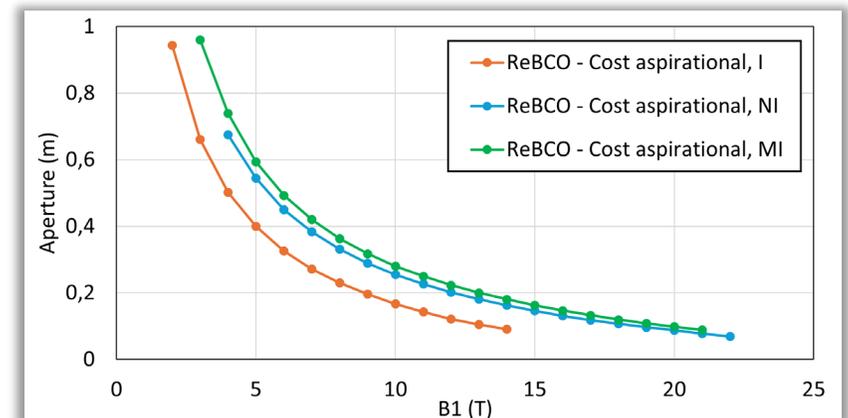
For the ReBCO, high cost requires small coil and very high current density → Protection will be a limiting factor

Need to devise alternative protection schemes!

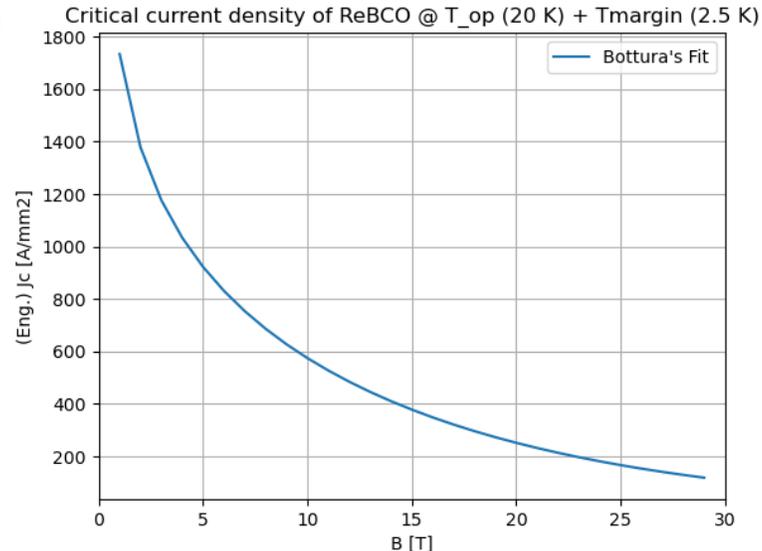
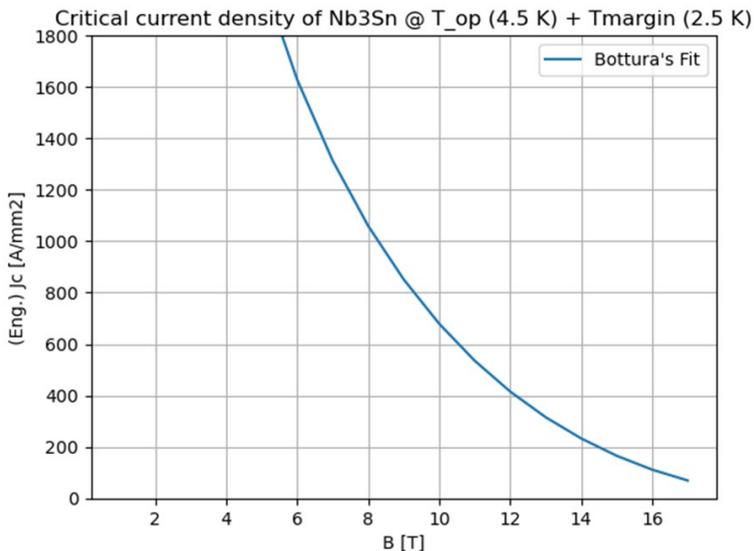
→ **Non-Insulated and Metal-Insulated coils**

Materials	Hotspot T [K]
Nb ₃ Sn	350
ReBCO	200

Courtesy of Tiina Salmi
<https://indico.cern.ch/event/1240045/>



- A Python code is used to implement the **analytic formulas** for the cos-theta magnets in **sector coil** approximation.
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- The **margin limit** is the limit due to the SC material itself, starting from the Bottura's fit for the critical current density.



Materials	Operating T [K]	T margin [K]
Nb ₃ Sn	4.5	2.5 (HL-LHC)
ReBCO	20	2.5

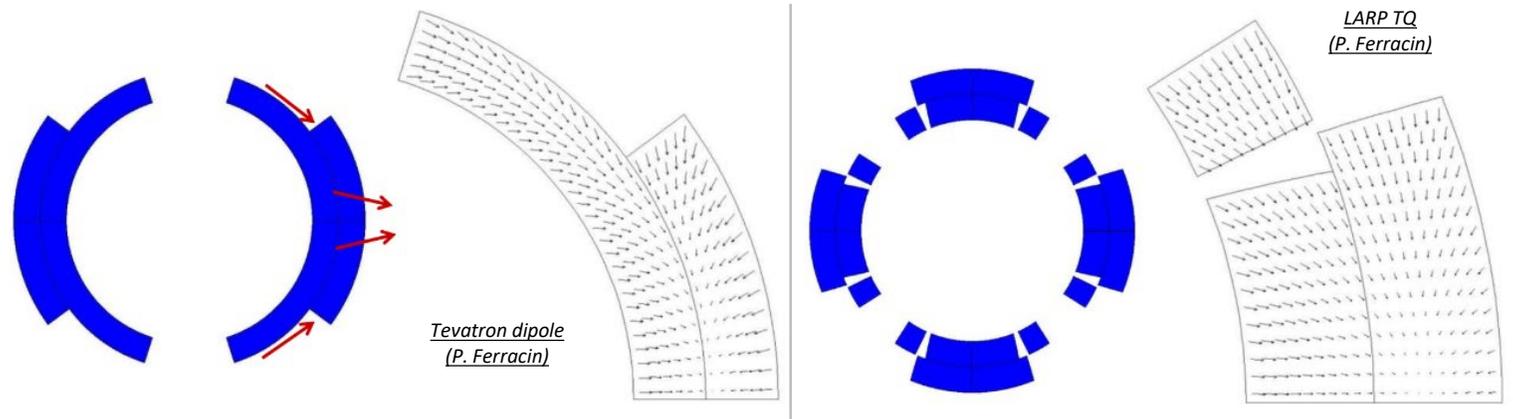
J_c refers to:

- Nb₃Sn: FCC cable target performance
- ReBCO: Fujikura FESC-AP tape

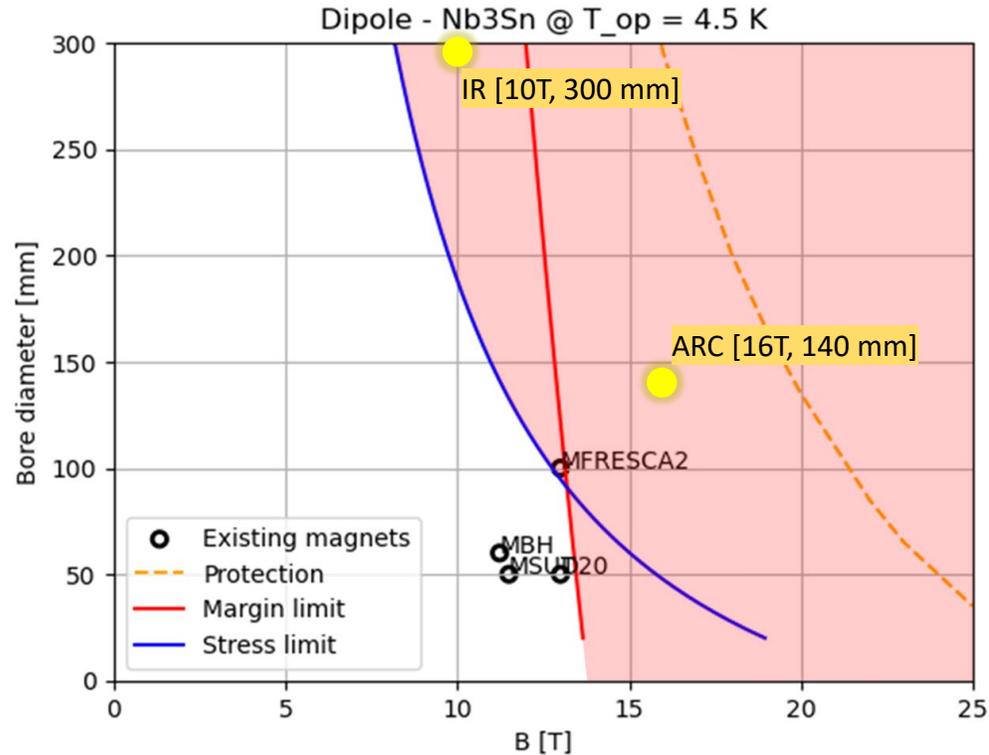
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- The **protection scheme** consists in QH (or CLIQ) for classical insulated coils, limiting the hotspot temperature and the stored energy in the coils.
- The **margin limit** is the limit due to the SC material itself, starting from the Bottura's fit for the critical current density.
- The **stress limit** considers the maximum mechanical stress we can have on the coils, starting from the analytical formula for the midplane pressure of cos-theta magnet in sector coil approx. (Reference: <https://doi.org/10.15161/oar.it/143359>)

Materials	Peak Stress [MPa]
Nb ₃ Sn	150
ReBCO	400

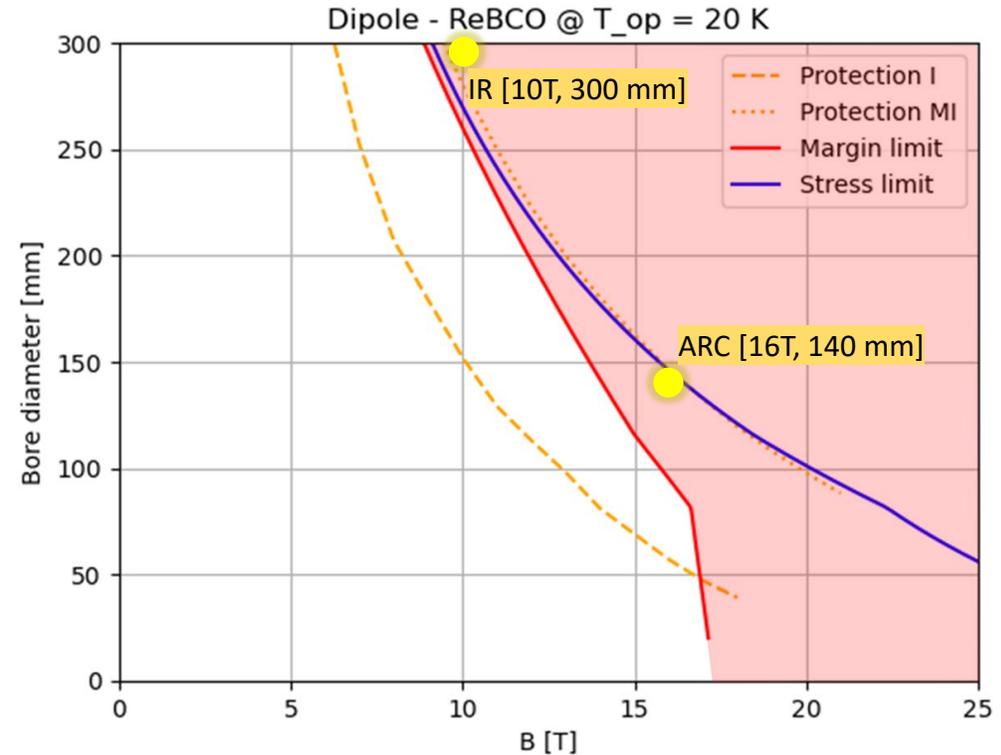
Currently, only stresses generated by Lorentz forces are considered.



Dipole A-B Plots

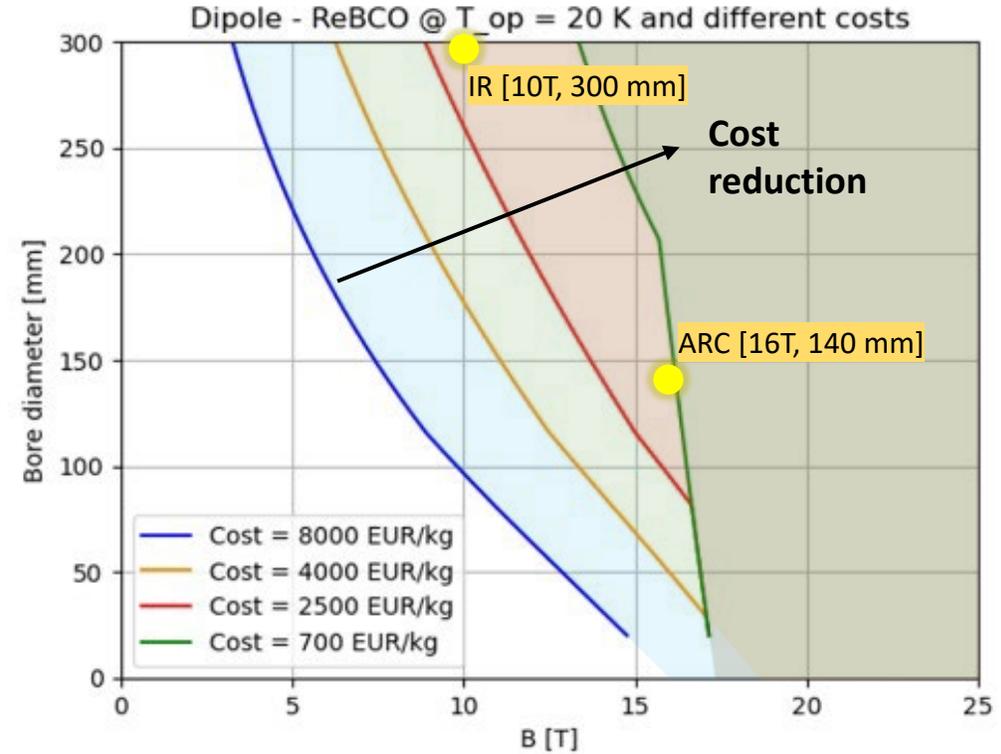
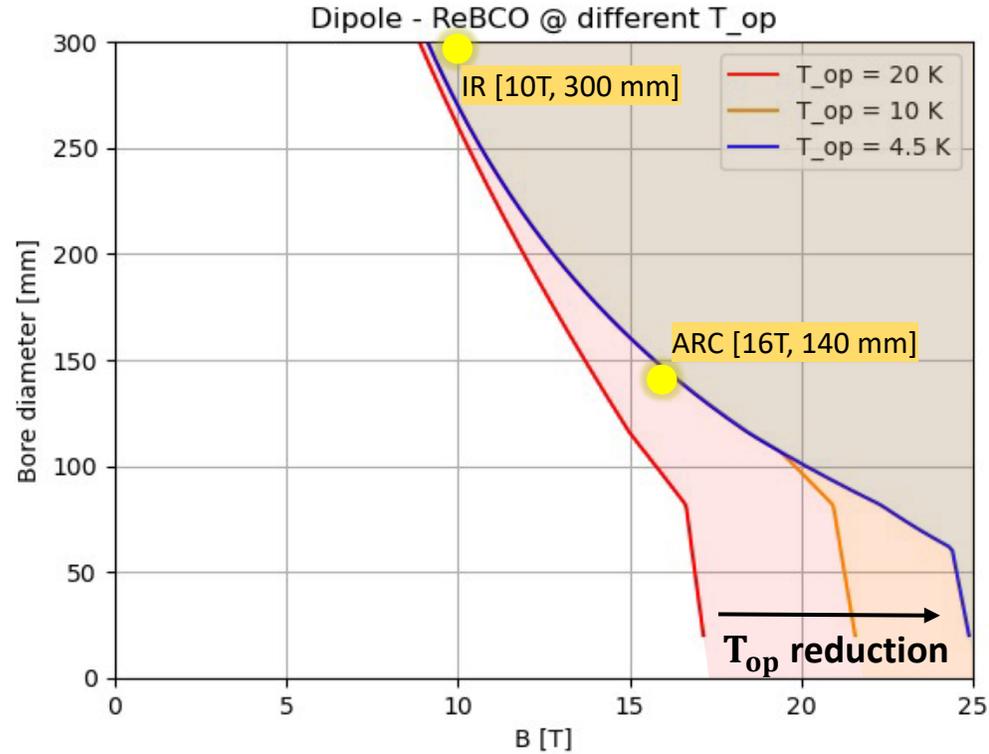


Nb₃Sn falls short of required performance because of **operating margin** and peak stress (at affordable cost !)



HTS falls short of required performance with classical insulated coils. Assuming MI or NI magnets, the **protection** limit becomes comparable with the other limits.

HTS dipole A-B Plots

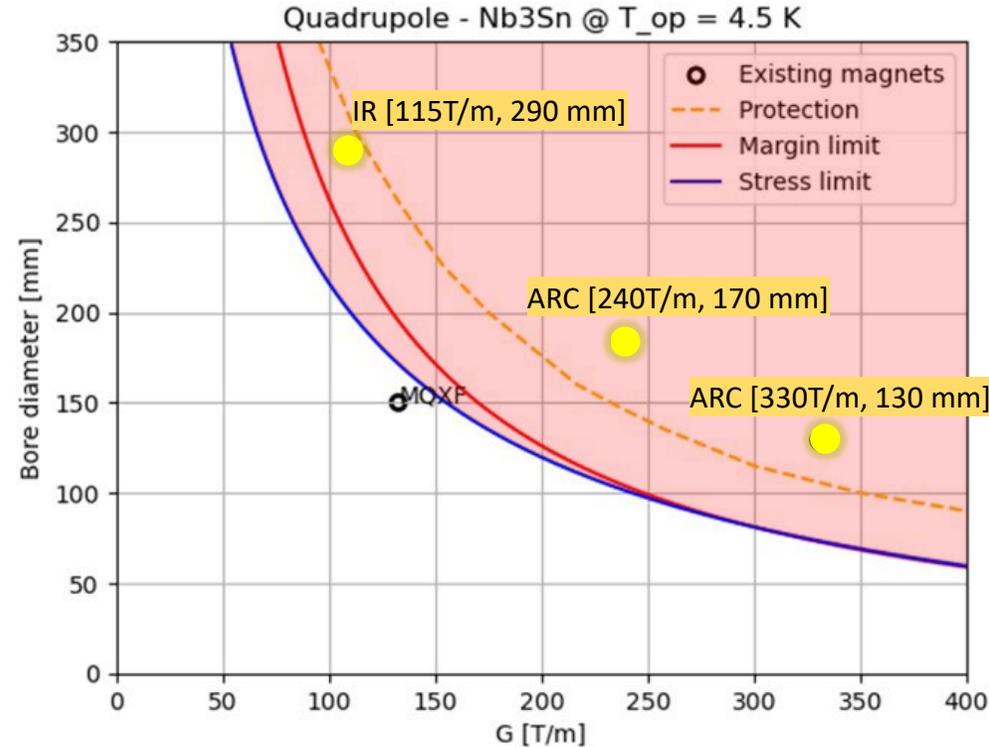


A reduction of operating temperature will result in wider design A-B range

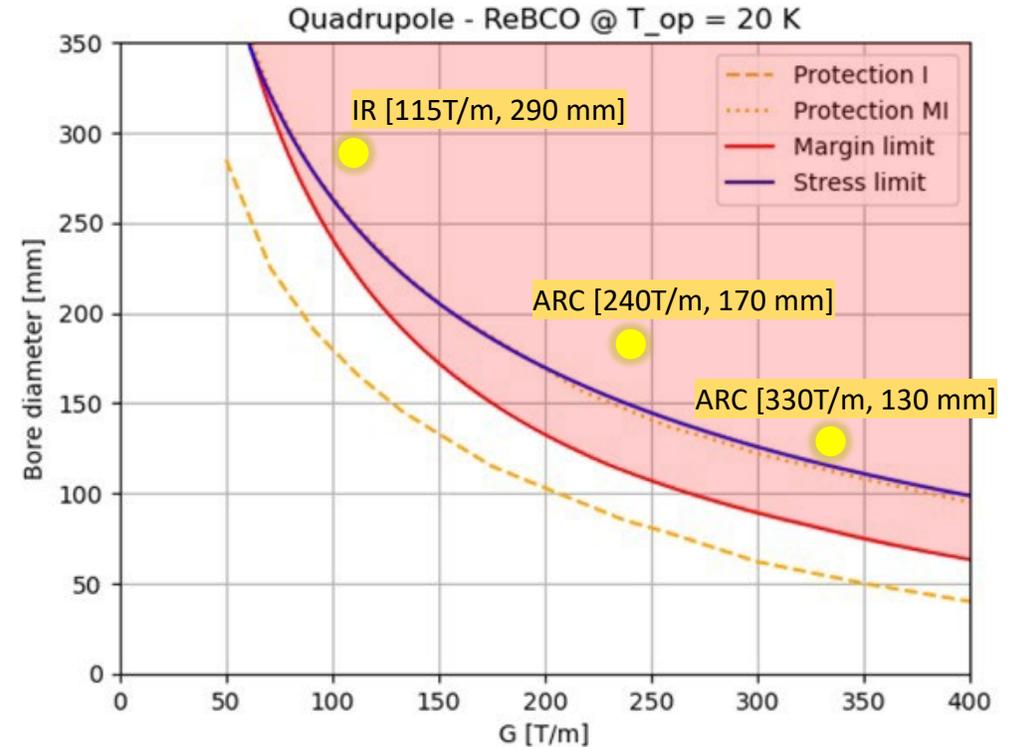
The curves shown in the plots are the limit curves, i.e., for each aperture value the strictest limit is taken, excluding the limit for insulated magnets.

A reduction of HTS cost will result in wider design A-B range

Quadrupole A-B Plots

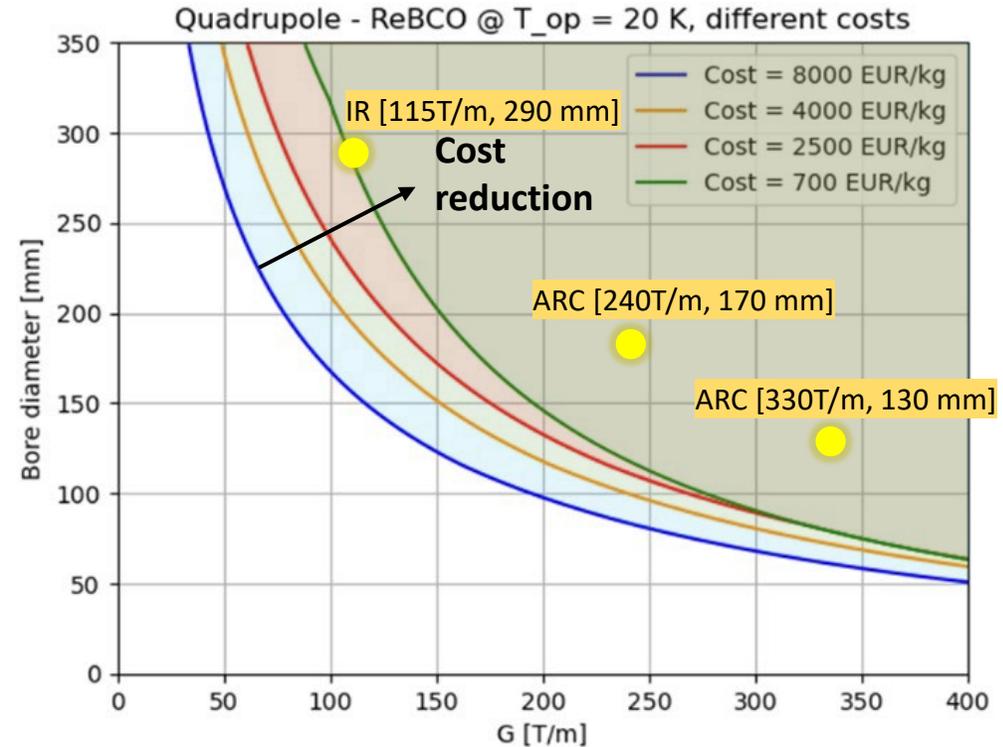
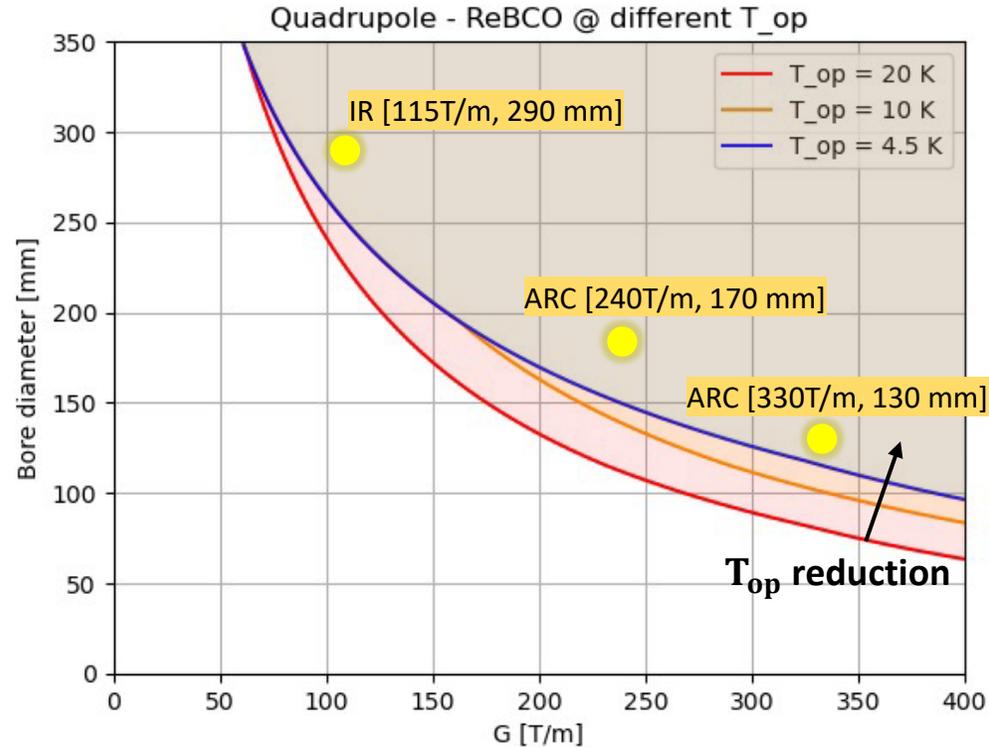


- Nb₃Sn is limited by peak stress and operating margin



- HTS is mainly limited by cost production and protection. Working @20K the margin curve is also a limiting factor.

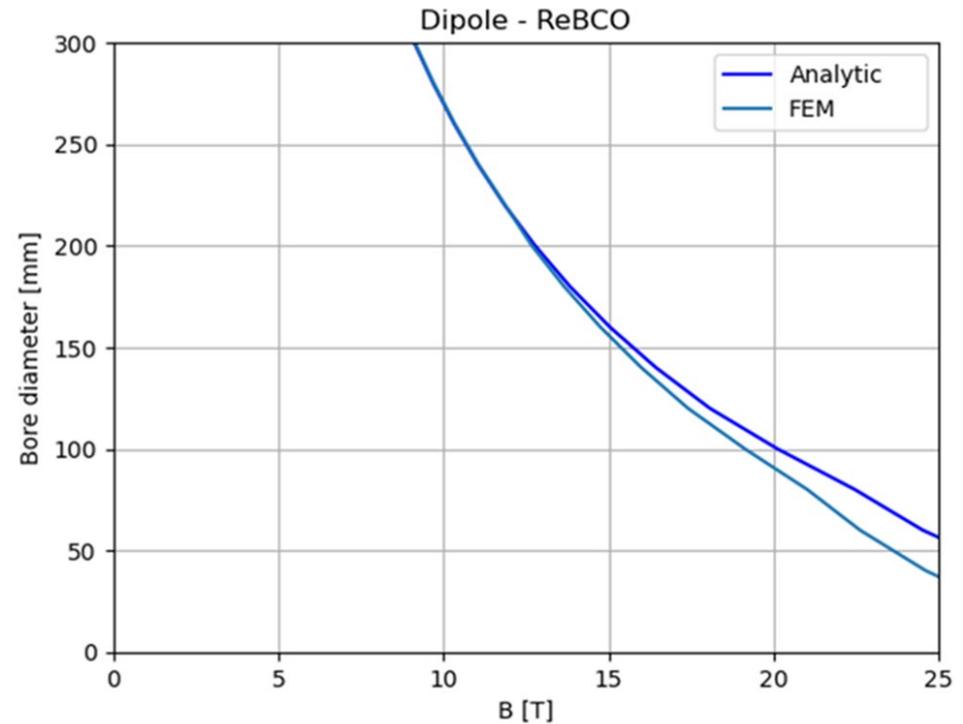
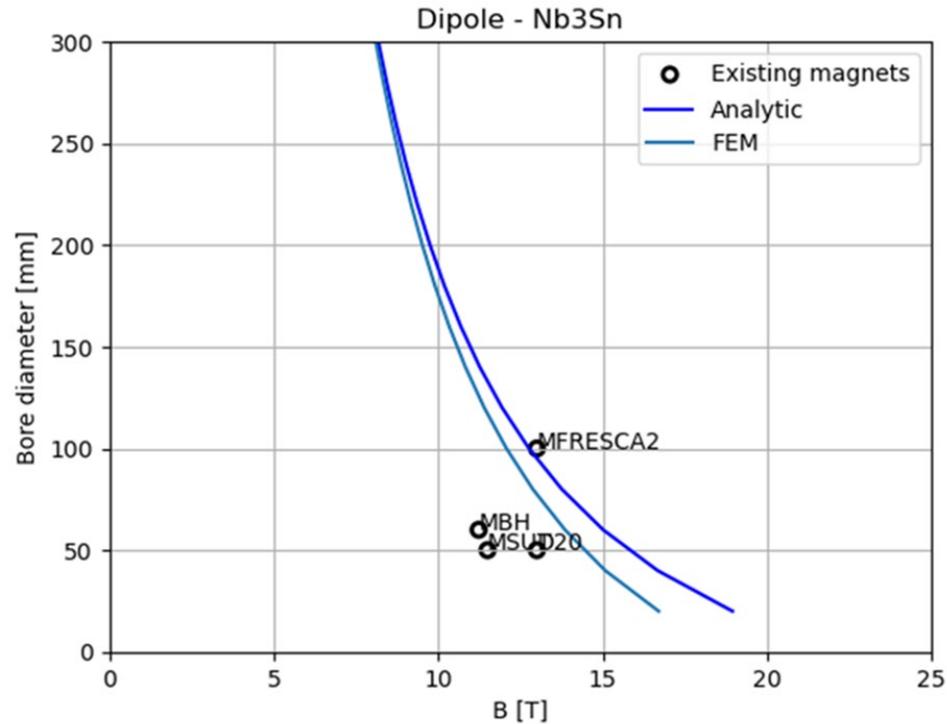
HTS quadrupole A-B Plots



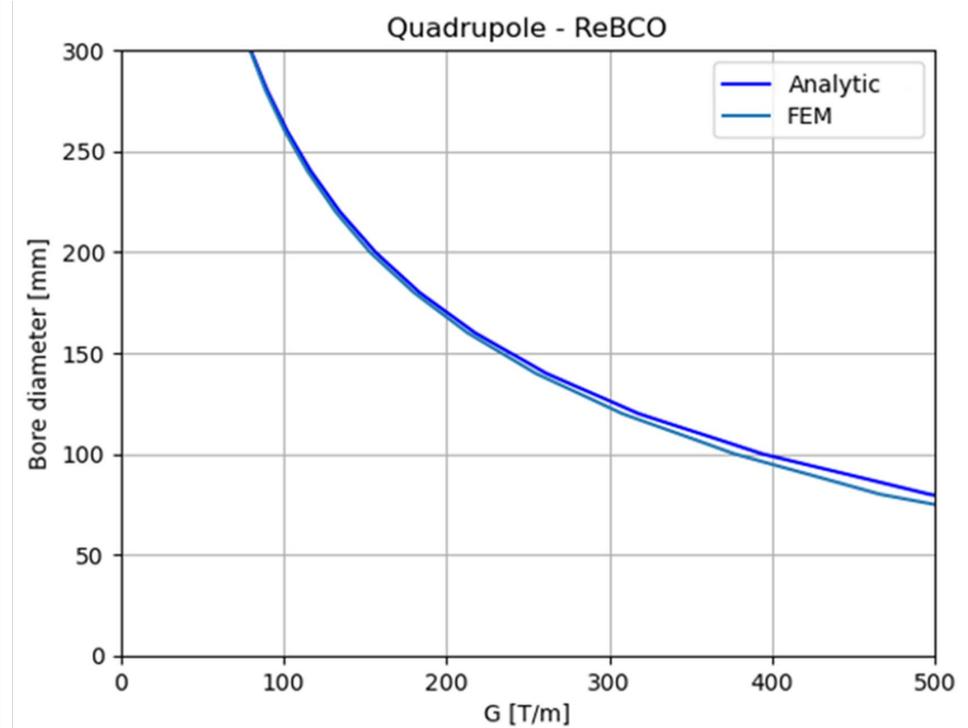
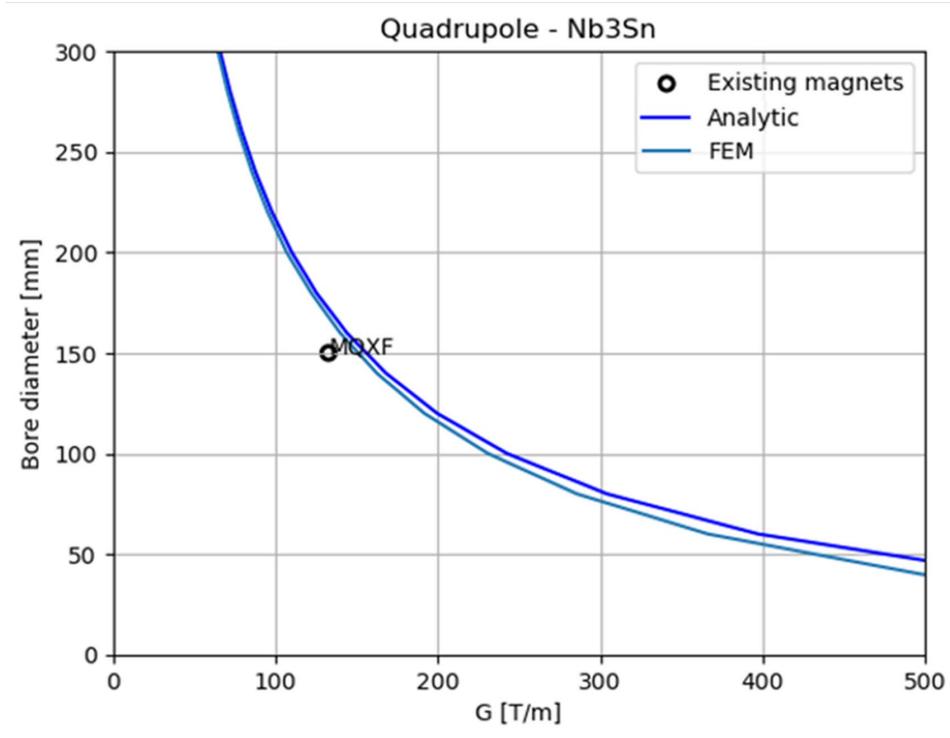
A reduction of operating temperature will result in wider design A-B range

The curves shown in the plots are the limit curves, i.e., for each aperture value the strictest limit is taken, excluding the limit for insulated magnets.

A reduction of HTS cost will result in wider design A-B range



- We implemented a FEM model for a sector **dipole** in ANSYS.
- We implemented a **Python** code able to work with **Ansys** software to run FEM simulations with the same inputs as the analytical study.
- In the comparison, the FEM curves are always more restricting than the analytical ones since they take the maximum pressure on the midplane instead of an average over the coil width.



- We implemented a FEM model for a sector **quadrupole** in ANSYS.
- We implemented a **Python** code able to work with **Ansys** software to run FEM simulations with the same inputs as the analytical study.
- In the comparison, the FEM curves are always more restricting than the analytical ones since they take the maximum pressure on the midplane instead of an average over the coil width.

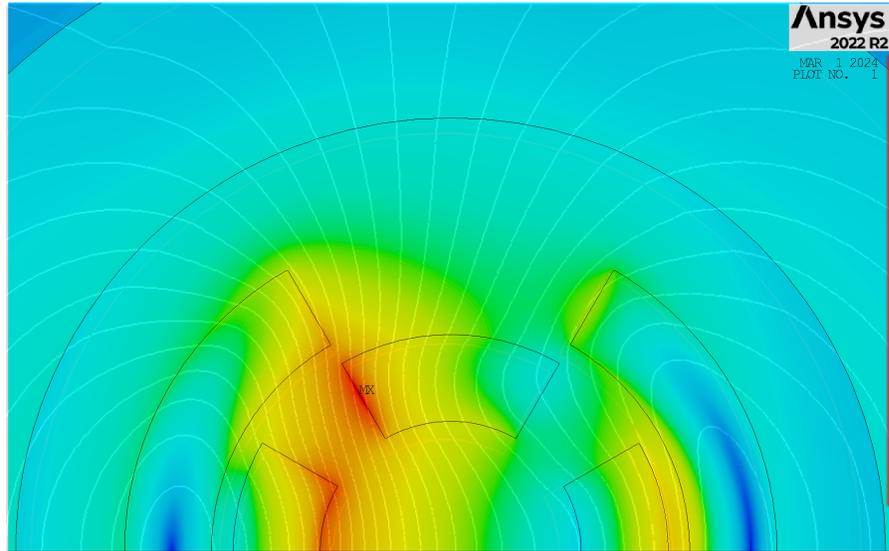
Arc:

- Combined function magnets: B1, **B1+B2** and **B1+B3**
- $B \approx 8...16$ T; $G \approx 320$ T/m; $G' \approx 7100$ T/m²
- Aperture ≈ 160 mm

Final focus:

- Combined function magnets: B1, B2, **B1+B2**, **B1+B3**
- $B \approx 4...16$ T; $G \approx 100...300$ T/m; $G' \approx 12000$ T/m²
- Aperture $\approx 120...300$ mm

Preliminary results obtained with ANSYS in a sector coil approximation



Quad into dipole:

(ReBCO @20 K)

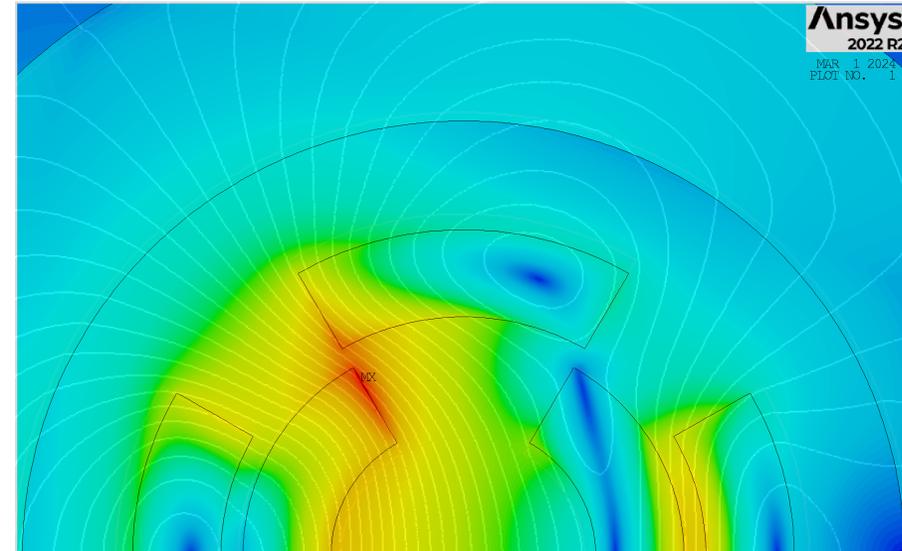
$$J = 3.5 \cdot 10^8 \text{ A/m}^2$$

$$B \sim 11.7 \text{ T}$$

$$G \sim 143.3 \text{ T/m}$$

$$r_{\text{aperture}} = 70 \text{ mm}$$

$$w_{\text{coil}} = 80 \text{ mm}$$



Dipole into quad:

(ReBCO @20 K)

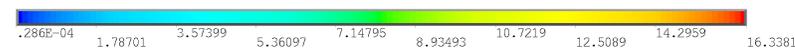
$$J = 3.5 \cdot 10^8 \text{ A/m}^2$$

$$B \sim 12.4 \text{ T}$$

$$G \sim 90.4 \text{ T/m}$$

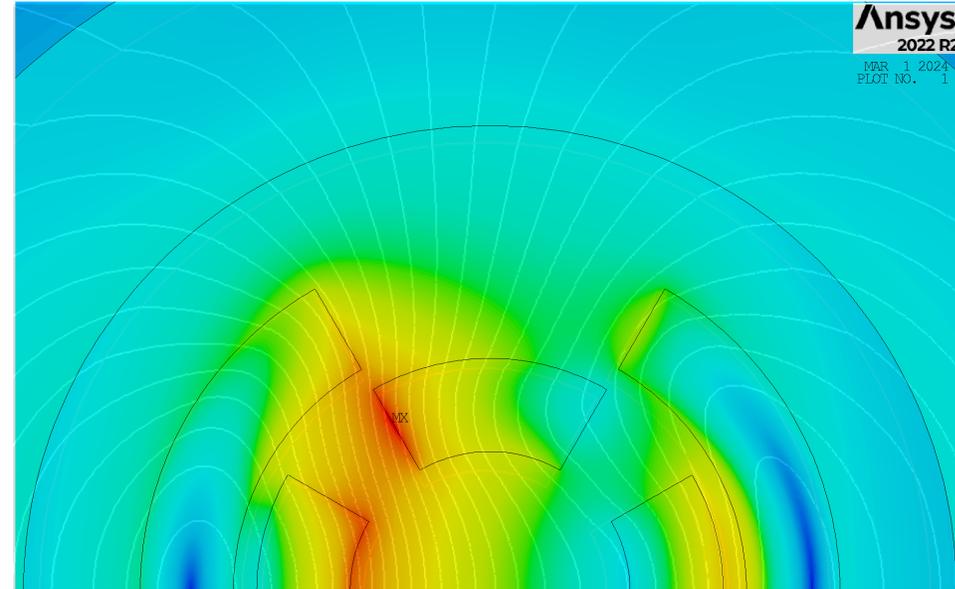
$$r_{\text{aperture}} = 70 \text{ mm}$$

$$w_{\text{coil}} = 80 \text{ mm}$$



Quadrupole inside dipole is more efficient, in agreement with *US-MAP* [ref]

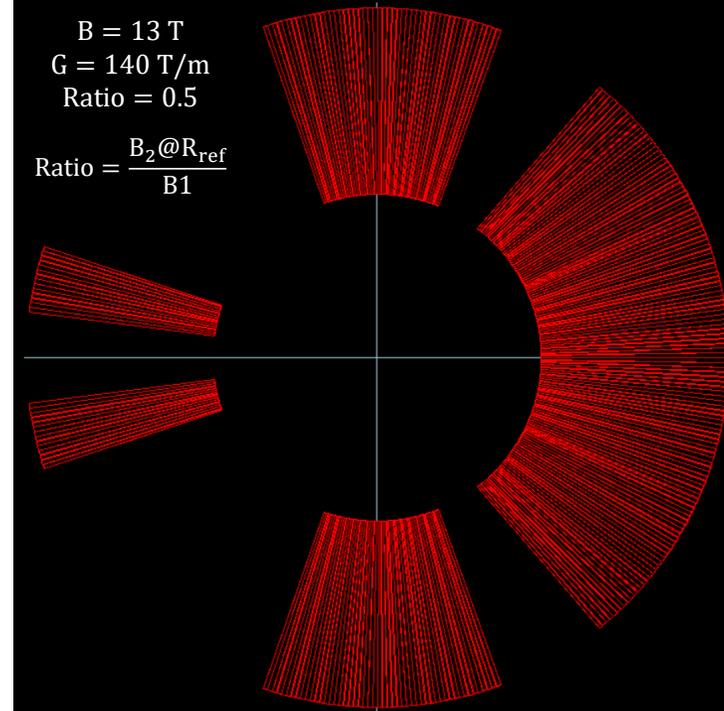
Nested: Quad into dipole



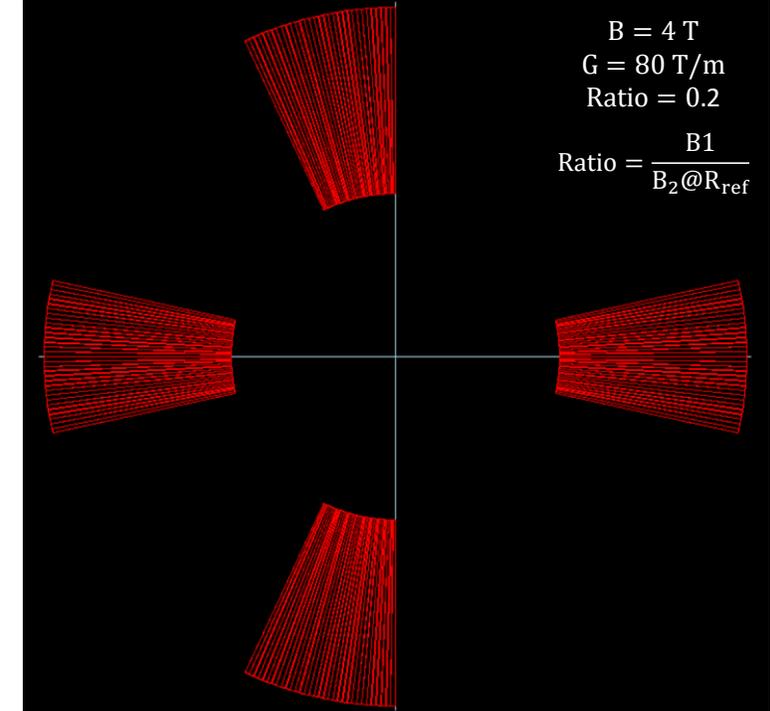
ANSYS
2022 R2
MAR 1 2024
PLOT NO. 1



Asymmetric Dipole



Asymmetric Quadrupole

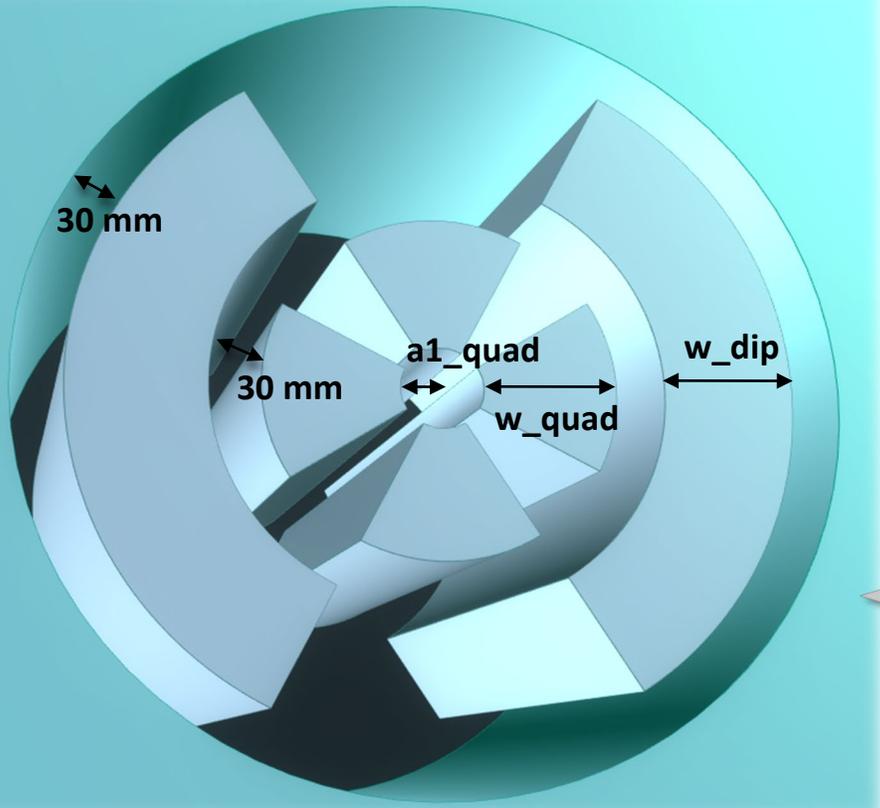


B and G are not independent and the feasibility of windability still to be studied

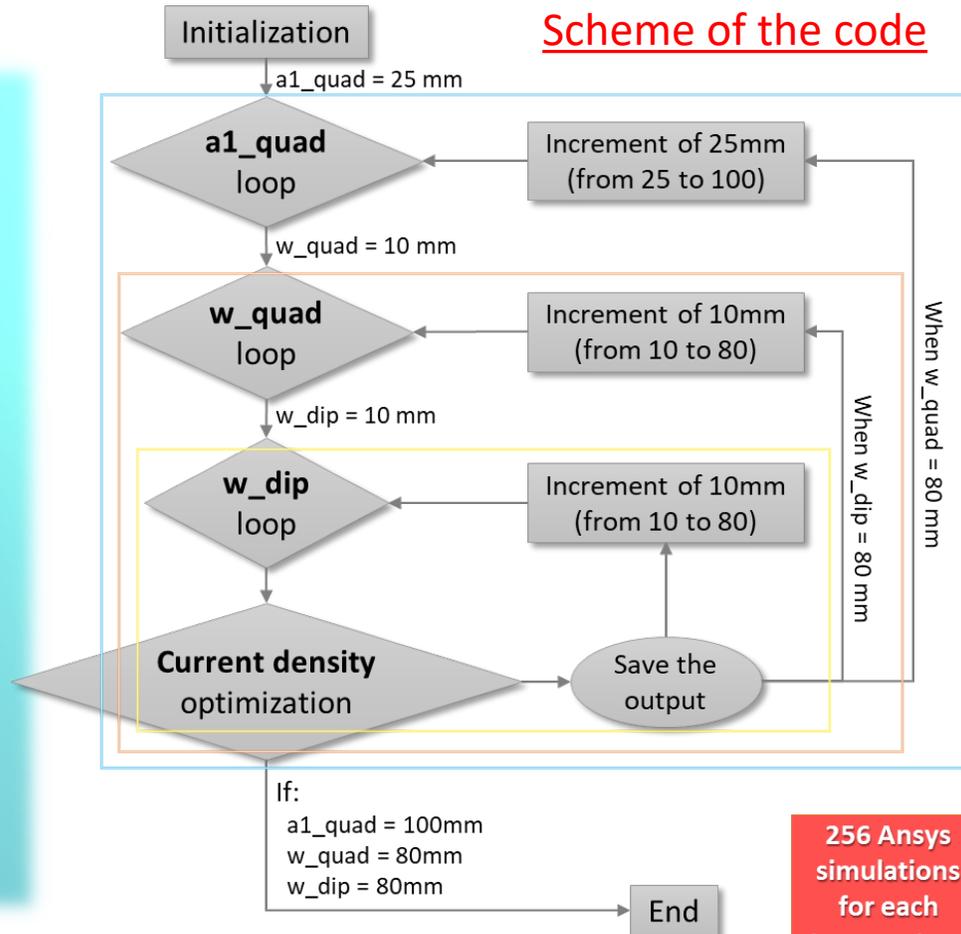
Quadrupole inside dipole is the primary choice for the combined functions of the muon collider

What's next? We would like to produce B-G plots in order to provide the allowed area for the combined function magnets

Python-Ansys Interface



Graphical representation

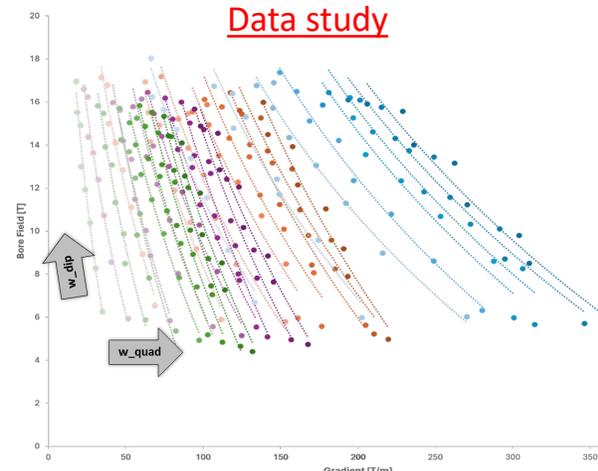


Scheme of the code

Data saving

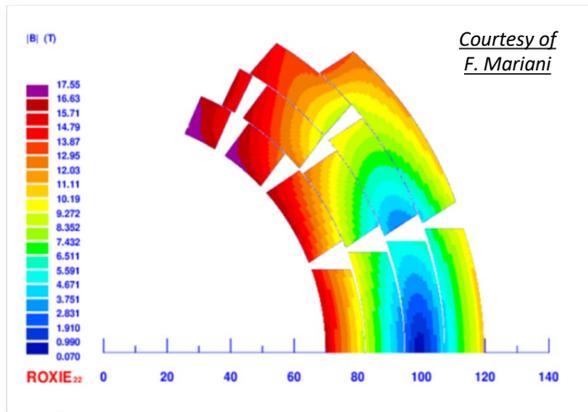
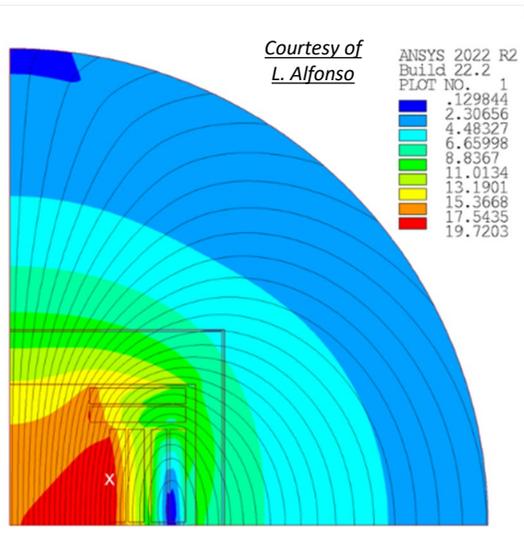
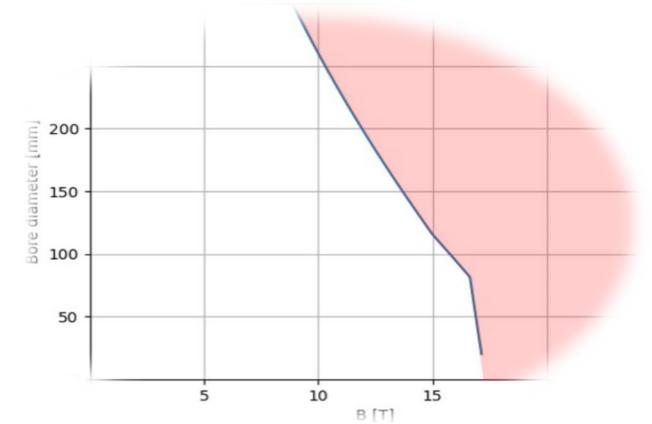
w_quad = 60 mm	w_quad = 70 mm	w_quad = 80 mm	w_quad = 90 mm
20 307812028.7 459617968.0 7.7125573 17.328216 13.04607 17.328216 143.1934 123.19532 3972855 523.3702699	30 274260517.6 335207299.3 9.6915878 18.103519 15.357962 18.103519 109.04388 -109.04388 5683768.2 621.6933235	40 301680569.3 301680569.3 11.220857 18.718351 16.56396 18.718351 97.822498 -97.822498 7603862.7 725.3943669	50 234737121 286900925.6 12.951131 20.036199 18.198751 20.036199 92.822428 -92.822428 10496129 834.472394

Data study

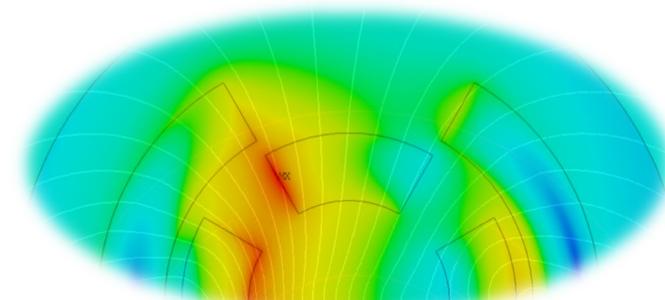


256 Ansys simulations for each temperature

- The allowed magnet aperture (A) - magnetic field (B) phase spaces are provided and discussed, representing the starting point to define possible beam optics which are also **acceptable** from a technological point of view.



- Thanks to the A-B plots, we were able to identify a target design, allowing us to begin studying specific designs. In particular, we are exploring a cos-theta design and a block coil design.



- To address the issue of neutrino flux in the straight sections, combined function magnets must be used in the Muon Collider. In this regard, we are working to identify realistic target designs from a technological point of view.



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Thank you for your attention

Daniel Novelli

Ph.D. in Accelerator Physics – XXXVIII cycle

24 October 2024

