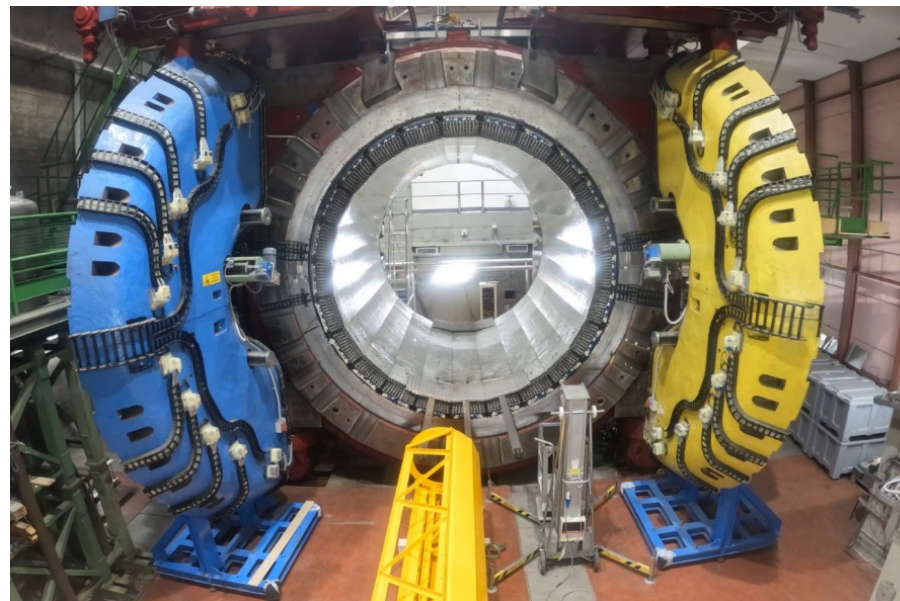

Studies for the optimization of the ECAL working point and FEE



Antonio Di Domenico, Viola Di Silvestre,
Paolo Gauzzi, Daniele Truncali
Dipartimento di Fisica, Sapienza Università di Roma
and INFN-Roma, Italy

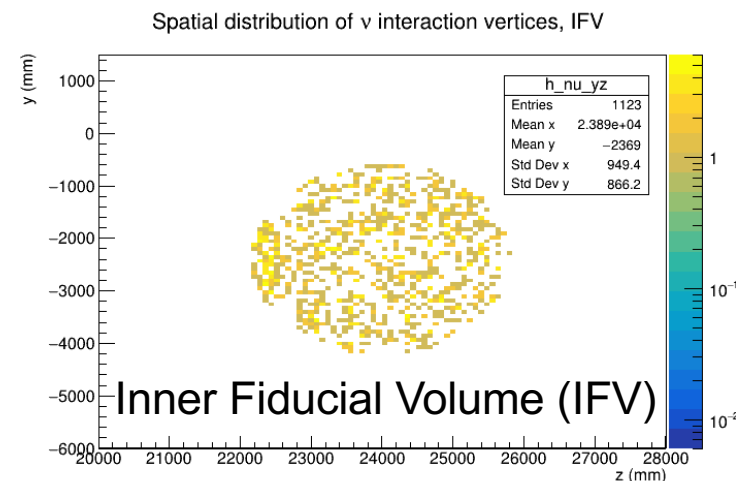
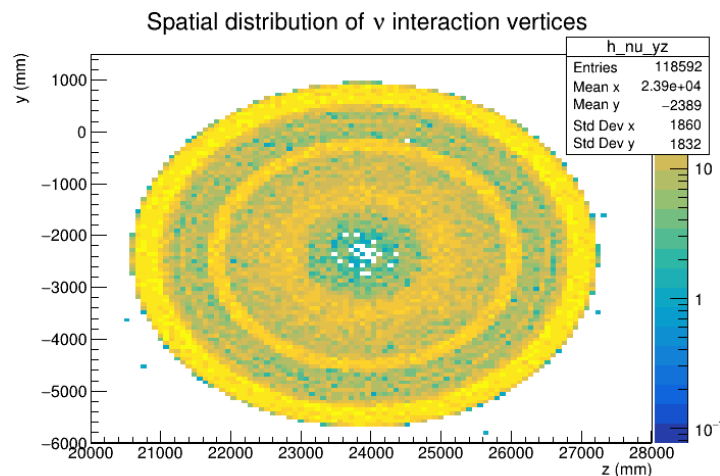
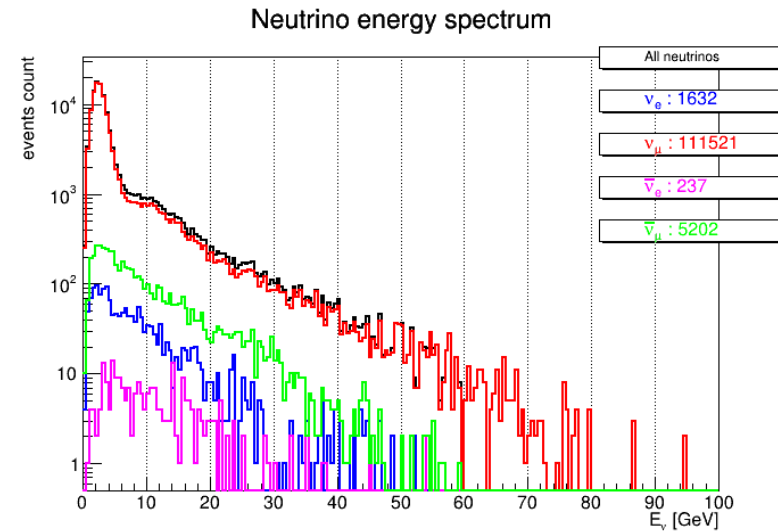


Alessandro Balla
INFN-LNF

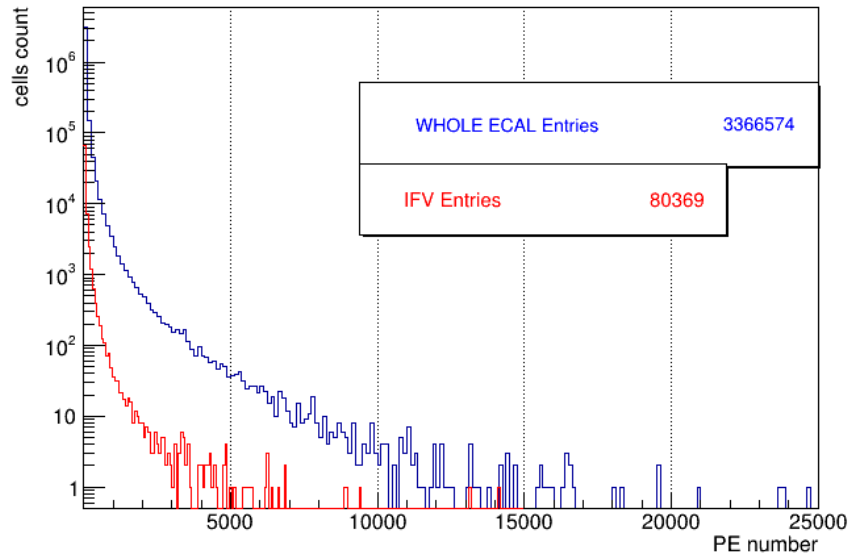


DUNE-ITALIA Meeting – Lecce 6 Novembre 2023

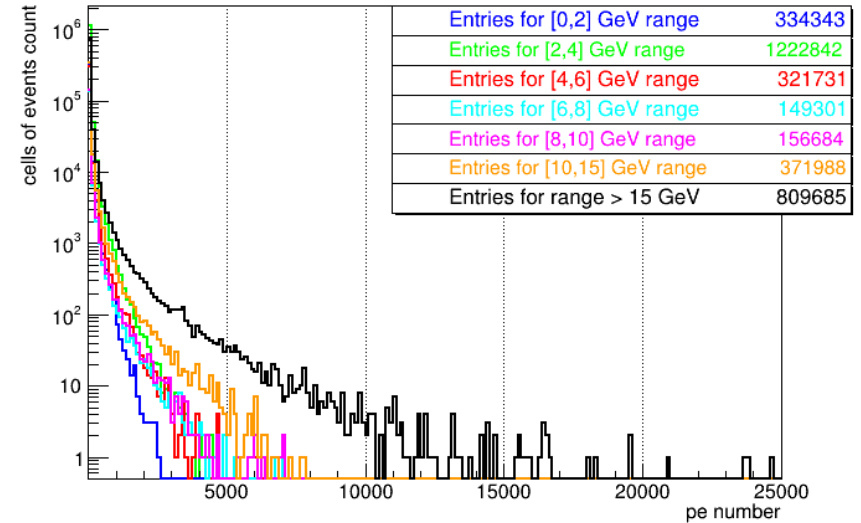
- Analyzed sample: sand-events.*.digi.root and sand-events.*.edep.root **(thanks to Matteo Tenti)**
(as for SAND docDB note 13262)
- 100 files
- Total evts = 118592
- Total p.o.t = 1.011×10^{17}
- p.o.t./spill = 7.5×10^{13} at 1.2 MW beam power
- corresponding to ~ 30 minutes of data taking in FHC mode
- Inner Fiducial Volume (IFV) defined at a distance of 20 cm from ECAL internal surface



PE distribution



PE distribution at E_ν fixed



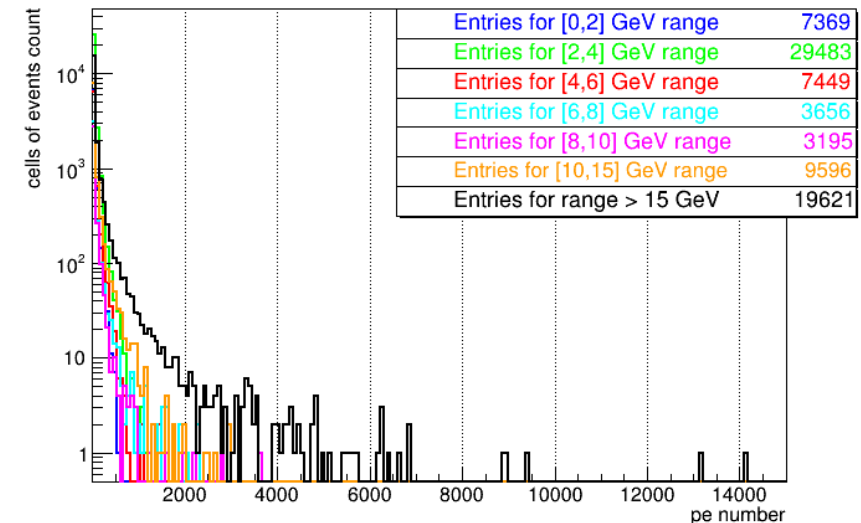
E_ν range = [0,10] GeV

Events number 101,696

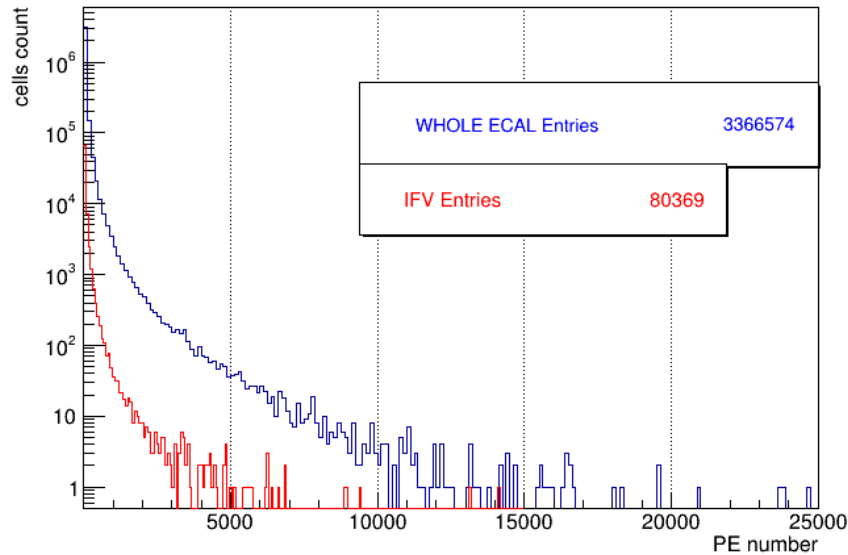
Events cells number 2,184,901

Fraction of events with at least one cell above PE threshold	[%]
1000 PE threshold	2.58
2000 PE threshold	0.49
3000 PE threshold	0.13
4000 PE threshold	$3.64 \cdot 10^{-2}$
Fraction of hit cells above PE threshold	[%]
1000 PE threshold	0.19
2000 PE threshold	$3.03 \cdot 10^{-2}$
3000 PE threshold	$7.19 \cdot 10^{-3}$
4000 PE threshold	$2.11 \cdot 10^{-3}$

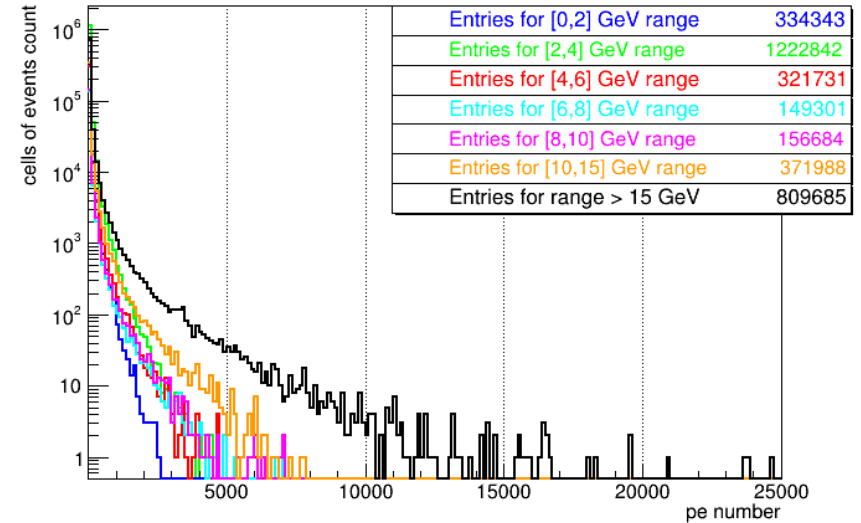
PE distribution at E_ν fixed, IFV



PE distribution



PE distribution at E_ν fixed



E_ν range = [0,10] GeV

Events number 101,696
Events cells number 2,184,901

PE distribution at E_ν fixed, IFV

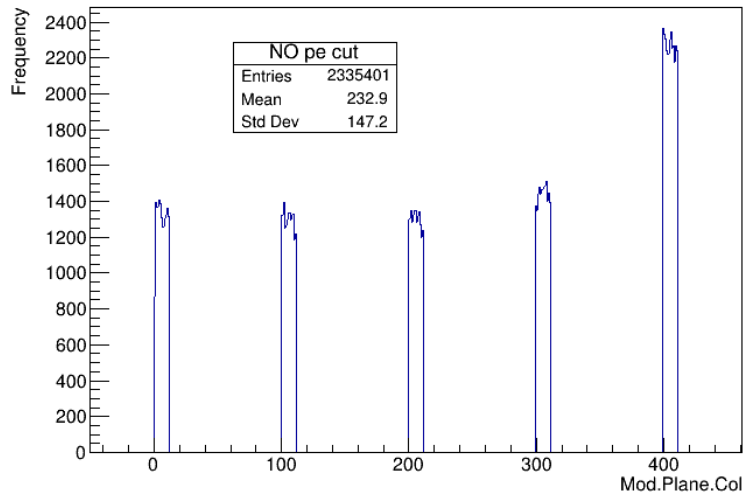


Fraction of events with at least one cell above PE threshold	[%]
1000 PE threshold	2.58
2000 PE threshold	0.49
3000 PE threshold	0.13
4000 PE threshold	$3.64 \cdot 10^{-2}$
Fraction of hit cells above PE threshold	[%]
1000 PE threshold	0.19
2000 PE threshold	$3.03 \cdot 10^{-2}$
3000 PE threshold	$7.19 \cdot 10^{-3}$
4000 PE threshold	$2.11 \cdot 10^{-3}$

- Neutrino energy range of interest for oscillation analyses is [0,10] GeV
- In this range the MAXIMUM Np.e. that has to be treated by FEE can be safely set between 1000 and 2000
=> see next slides for the choice of the FEE dynamic range

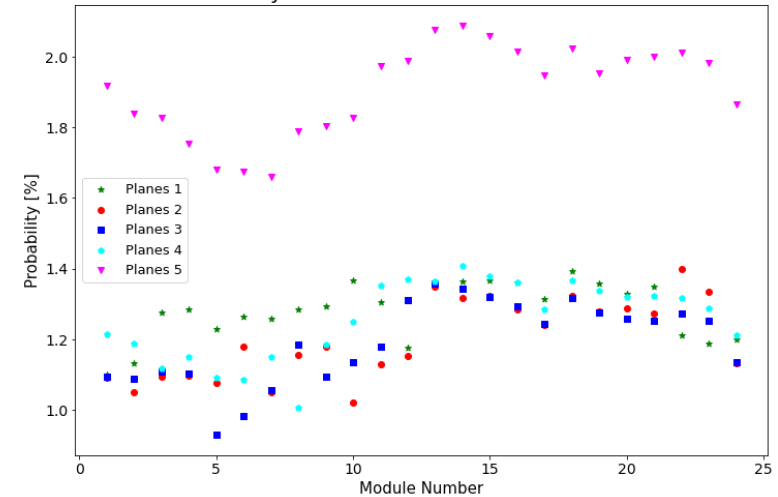
Cell occupancy plots and hit probability

Occupancy plot 1st Barrel MODULE



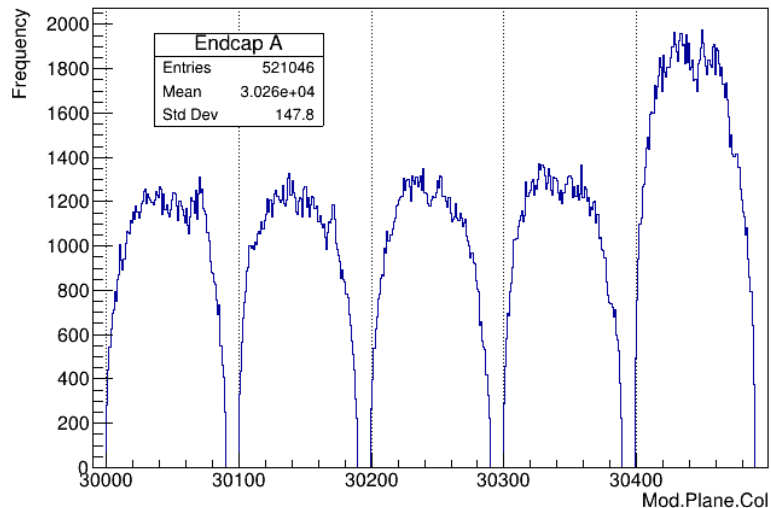
Barrel

Probability of hit a SINGLE PLANE barrel module



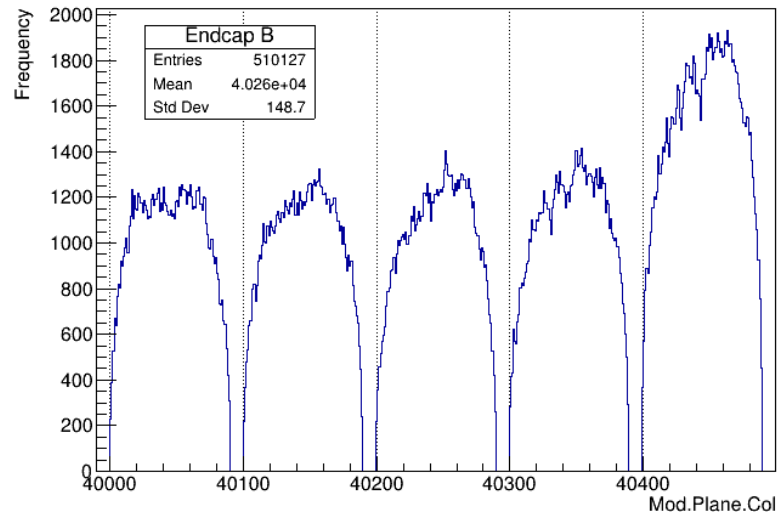
Ecap A

Occupancy plot Endcap A



Ecap B

Occupancy plot Endcap B



Average probability that a cell is fired/hit in a neutrino interaction event:

$$P_{\text{barrel}} = 1.37\%$$

$$P_{\text{ecapA}} = 0.88\%$$

$$P_{\text{ecapB}} = 0.86\%$$

$$P_{\text{cell}} = 1.16\%$$

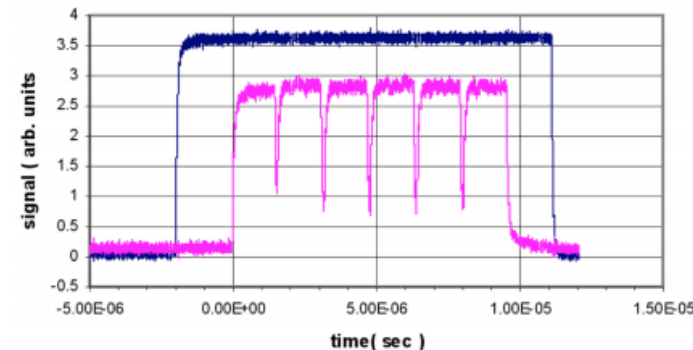
Beam power 1.2 MW

7.5×10^{13} protons extracted every 1.2 s at 120 GeV

1.1×10^{21} pot/year

Spill time structure

- 9.6 μs per spill
- 6 batches, 84 bunches/batch
- 2 empty bunches
- 1 bunch: Gaus($\sigma = 1.5$ ns)
- Δt bunches = 19 ns



Event rates expected in SAND

~ **84 interactions/spill**

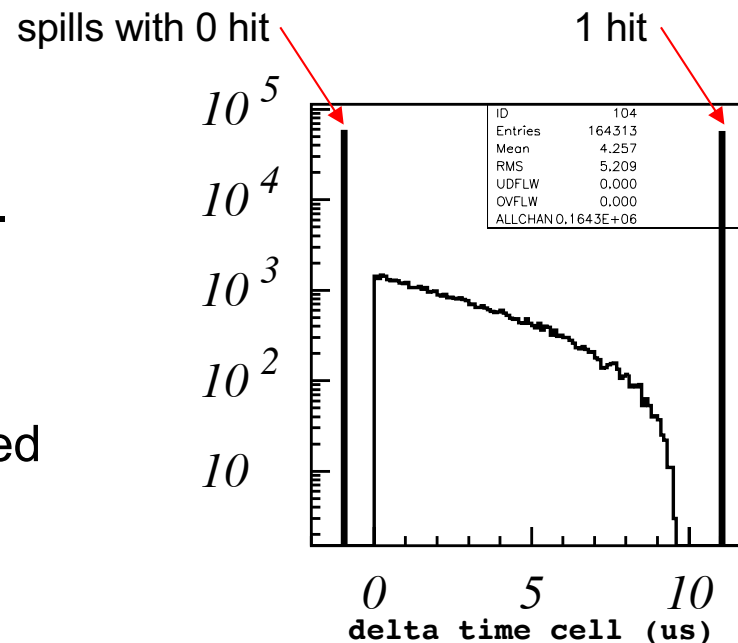
$\lesssim 1$ interaction/spill in the SAND fiducial volume

(negligible rock muons and cavern background assumed)

Pile-up probability

The beam time structure is reconstructed to simulate the time of the neutrino interaction event and calculate the pile-up probability that, given a PMT signal, a second signal arrives within a fixed time window (TW) after the first signal.

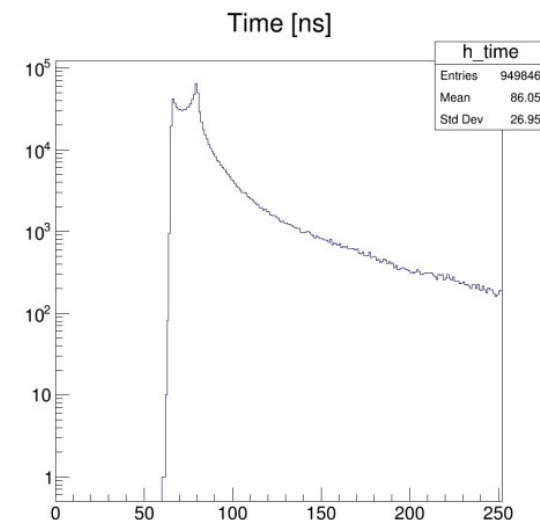
The times of N interactions per spill (in average $N=84$) are extracted uniformly between 0 and $9.6 \mu\text{s}$. The time difference between two consecutive interactions is calculated for all spills, following an exponential distribution with $\tau_{\text{spill}} \simeq 114 \text{ ns}$. From this, the distribution of time differences for a single cell with a probability to be hit of $P_{\text{cell}} = 1.16\%$ is evaluated, and then the pile-up probabilities for different time windows are also evaluated, $\text{TW} = 50, 100, 150, 200 \text{ ns}$.



before smearing

after smearing

$P_{\text{CELL}} [\%]$	1.16	1.5	2.0	1.16	1.5	2.0
Time window [ns]						
50	0.67	0.90	1.28	0.64	0.86	1.36
100	1.33	1.81	2.52	1.32	1.71	2.56
150	1.95	2.71	3.72	1.91	2.60	3.78
200	2.59	3.58	4.87	2.52	3.48	4.93

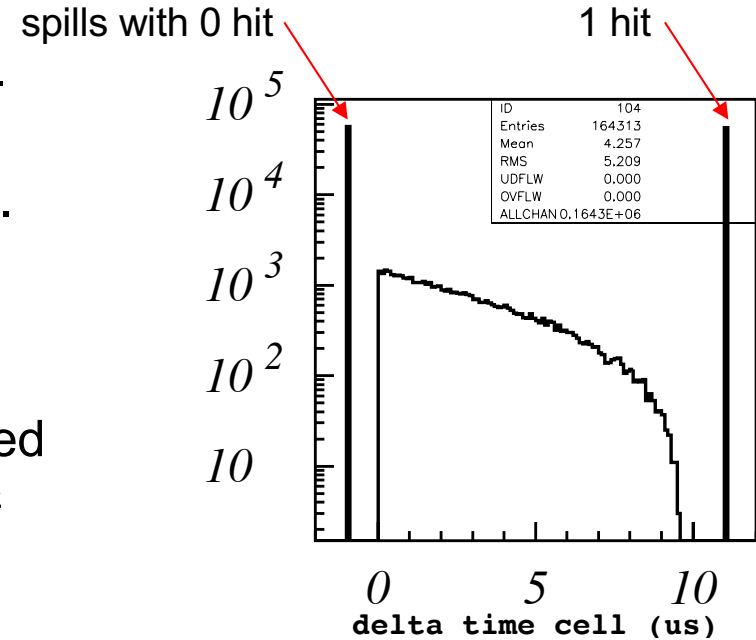


Time propagation/smearing of hits in a single neutrino interaction event.

Pile-up probability

The beam time structure is reconstructed to simulate the time of the neutrino interaction event and calculate the pile-up probability that, given a PMT signal, a second signal arrives within a fixed time window (TW) after the first signal.

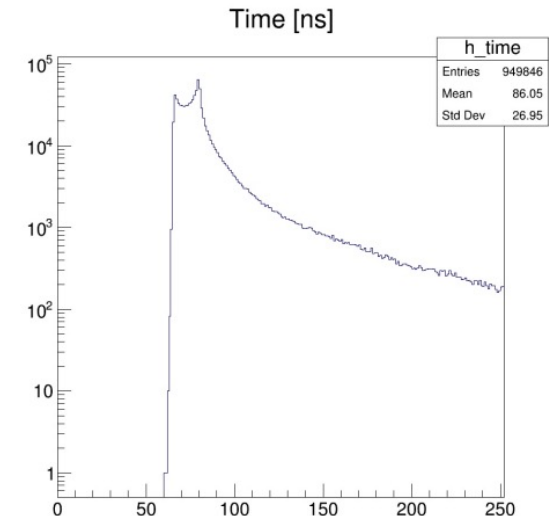
The times of N interactions per spill (in average $N=84$) are extracted uniformly between 0 and $9.6 \mu\text{s}$. The time difference between two consecutive interactions is calculated for all spills, following an exponential distribution with $\tau_{\text{spill}} \simeq 114 \text{ ns}$. From this, the distribution of time differences for a single cell with a probability to be hit of $P_{\text{cell}} = 1.16\%$ is evaluated, and then the pile-up probabilities for different time windows are also evaluated, $\text{TW} = 50, 100, 150, 200 \text{ ns}$.



before smearing

after smearing

$P_{\text{CELL}} [\%]$	1.16	1.5	2.0	1.16	1.5	2.0
Time window [ns]						
50	0.67	0.90	1.28	0.64	0.86	1.36
100	1.33	1.81	2.52	1.32	1.71	2.56
150	1.95	2.71	3.72	1.91	2.60	3.78
200	2.59	3.58	4.87	2.52	3.48	4.93



Time propagation/smearing of hits in a single neutrino interaction event.

PMT signal and discriminator threshold in KLOE

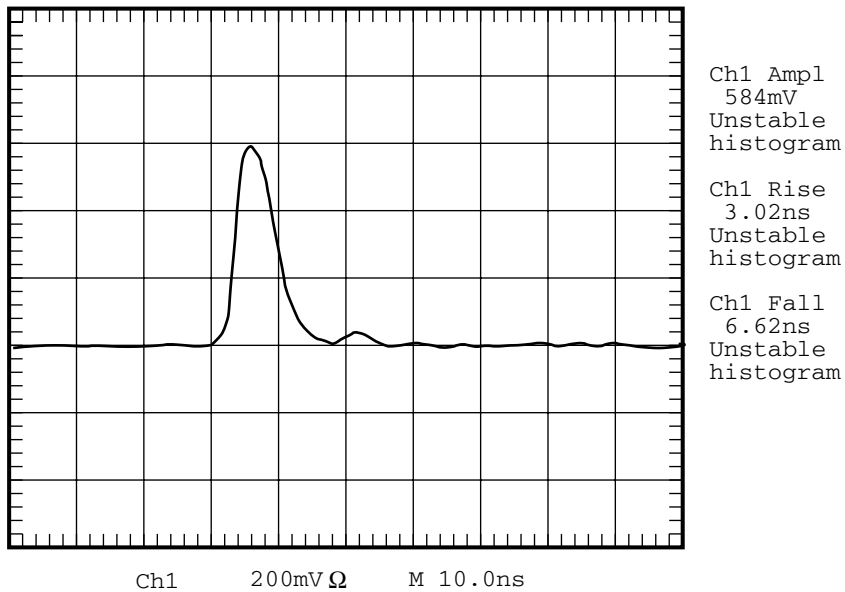


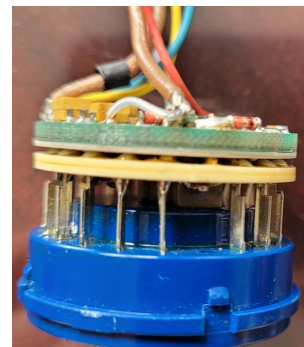
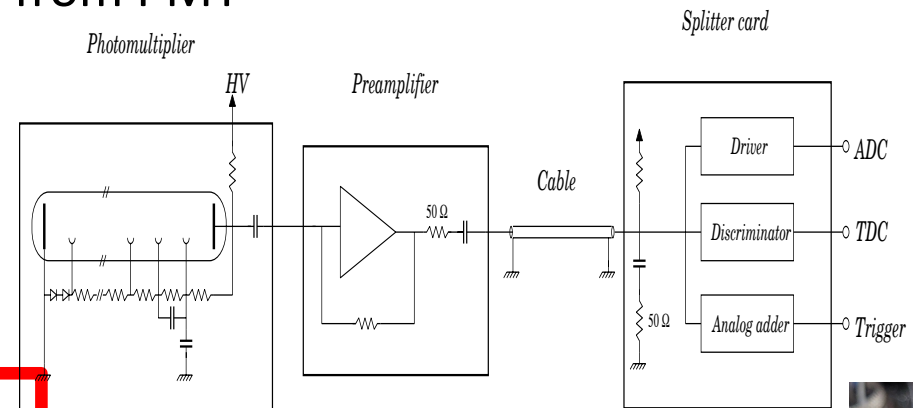
Figure 4: Typical signal from the PM base.

Constraints:

- minimum discriminator threshold 4-5 mV
- maximum HV for PMs divider is 2300 V
typical HV 1700-1800 => $G \sim 1-3 \times 10^6$
- preamplifier linear (within 0.2%) for signals up to 4.7 V (gain preamp ~ 2.5)
=> 1.74 V at discriminator level after 12-15 m long cables and termination

Constant fraction discriminators.

Effective thresholds are in the range 4–5 mV: They correspond to signals originated by 3–4 photoelectrons or a 3–4 MeV photon at 2 m from PMT



thanks to A. Balla and P. Ciambone

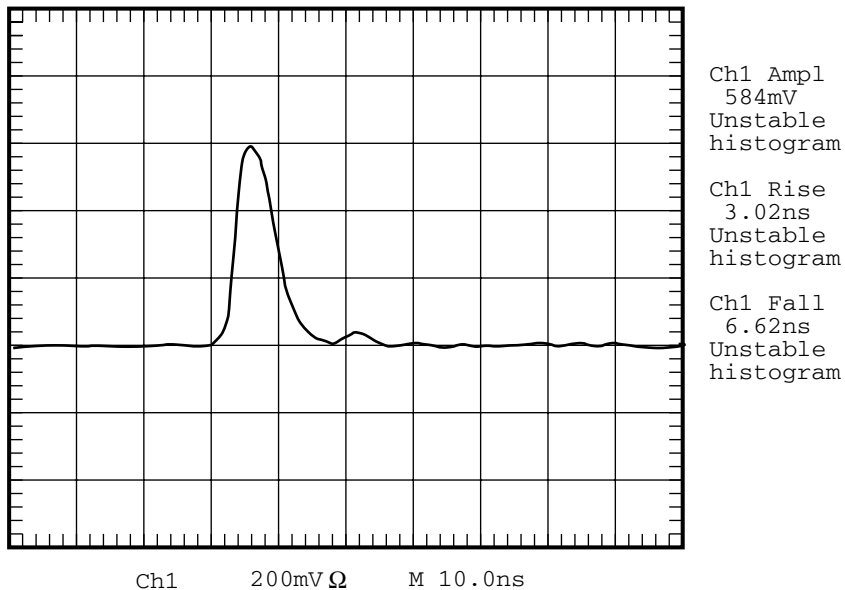


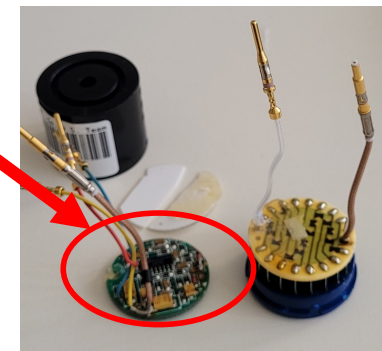
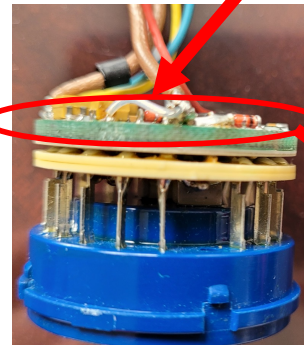
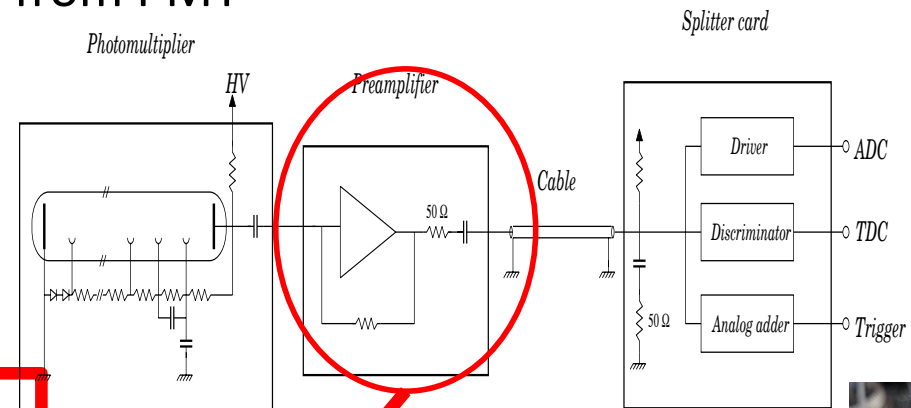
Figure 4: Typical signal from the PM base.

Constraints:

- minimum discriminator threshold 4-5 mV
- maximum HV for PMs divider is 2300 V
typical HV 1700-1800 $\Rightarrow G \sim 1-3 \times 10^6$
- preamplifier linear (within 0.2%) for signals up to 4.7 V (gain preamp ~ 2.5)
 $\Rightarrow 1.74$ V at discriminator level after 12-15 m long cables and termination

Constant fraction discriminators.

Effective thresholds are in the range 4–5 mV: They correspond to signals originated by 3–4 photoelectrons or a 3–4 MeV photon at 2 m from PMT

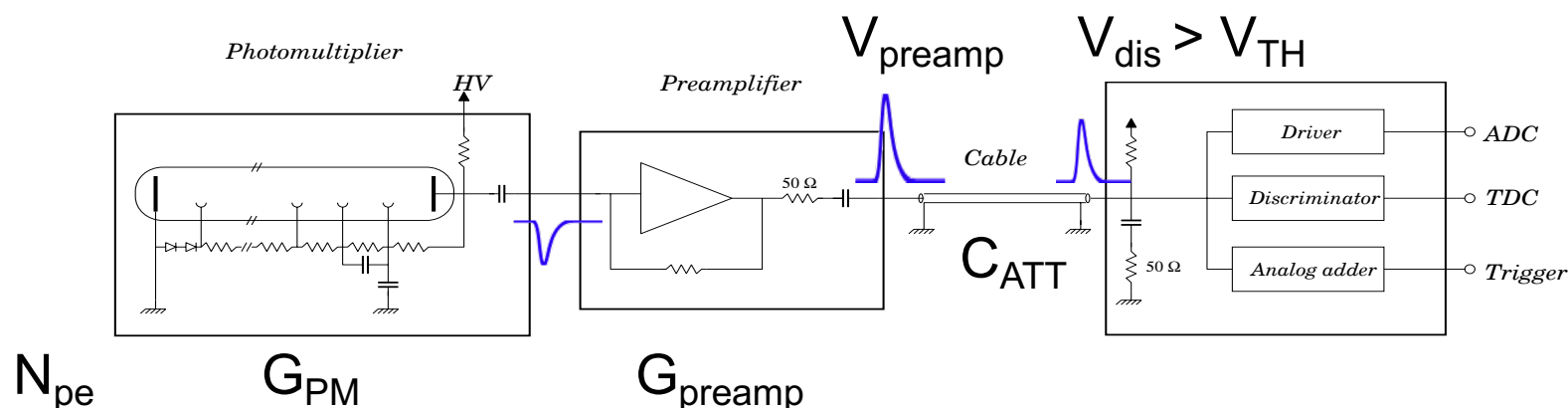


thanks to A. Balla and P. Ciambone

Choice of the dynamic range - I

The dynamic range in terms of N_{pe} can be evaluated using the following constraints for the FEE after the PMT:

- Minimum discriminator/digitizer threshold $V_{TH} = 5$ mV
- Preamp linearity (within 0.2%) range = $[0, 4.7]$ V $\Rightarrow V_{preamp}(\max) = 4.7$ V
- preamp transimpedance gain $G = 250$ V/A $\Rightarrow I_{peak}(\max) = 19$ mA \Rightarrow max signal charge $Q(\max) = 133$ pC; from $Q = e N_{pe} G_{PM} \Rightarrow (N_{pe} G_{PM})(\max) = 83 \cdot 10^7$
- $G_{TOT} = G_{PM} G_{preamp}$ with $G_{preamp} \approx 2.5$
- 12m long cable attenuation: $C_{ATT} = 0.74$
- MAX single pulse amplitude at the discriminator/digitizer input is:
 $V_{dis}(\max) = V_{preamp}(\max) \cdot 0.5 \cdot C_{ATT} = 1.74$ V
- signal ampl = $V_{dis}(\max) / N_{pe}(\max)$
- $N_{pe}(\min) = V_{TH} / (\text{signal ampl}) \Rightarrow N_{pe}(\max) / N_{pe}(\min) = V_{dis}(\max) / V_{TH}$



Choice of the dynamic range - I

The dynamic range in terms of N_{pe} can be evaluated using the following constraints for the FEE after the PMT:

- Minimum discriminator/digitizer threshold $V_{TH} = 5$ mV
- Preamp linearly (within 0.2%) range = $[0, 4.7]$ V $\Rightarrow V_{preamp}(\text{max}) = 4.7$ V
- preamp transimpedance gain $G = 250$ V/A $\Rightarrow I_{peak}(\text{max}) = 19$ mA \Rightarrow max signal charge $Q(\text{max}) = 133$ pC; from $Q = e N_{pe} G_{PM} \Rightarrow (N_{pe} G_{PM})(\text{max}) = 83 \cdot 10^7$
- $G_{TOT} = G_{PM} G_{preamp}$ with $G_{preamp} \approx 2.5$
- 12m long cable attenuation: $C_{ATT} = 0.74$
- MAX single pulse amplitude at the discriminator/digitizer input is:
 $V_{dis}(\text{max}) = V_{preamp}(\text{max}) \cdot 0.5 \cdot C_{ATT} = 1.74$ V
- signal ampl = $V_{dis}(\text{max})/N_{pe}(\text{max})$
- $N_{pe}(\text{min}) = V_{TH}/(\text{signal ampl}) \Rightarrow N_{pe}(\text{max})/N_{pe}(\text{min}) = V_{dis}(\text{max})/V_{TH}$

G_{PM} ($\times 10^5$)	G_{tot} ($\times 10^6$)	$N_{pe}(\text{max})$	signal amplitude (mV/pe)	$N_{pe}(\text{min})$ $V_{TH} = 5$ mV	MeV at module center
4.2	1.04	~ 2000	0.87	~ 6	6.0
5.5	1.38	~ 1500	1.16	~ 4	4.0
8.3	2.1	~ 1000	1.74	~ 3	3.0
10	2.5	~ 800	2.18	~ 2	2.0

Choice of the dynamic range - I

The dynamic range in terms of N_{pe} can be evaluated using the following constraints for the FEE after the PMT:

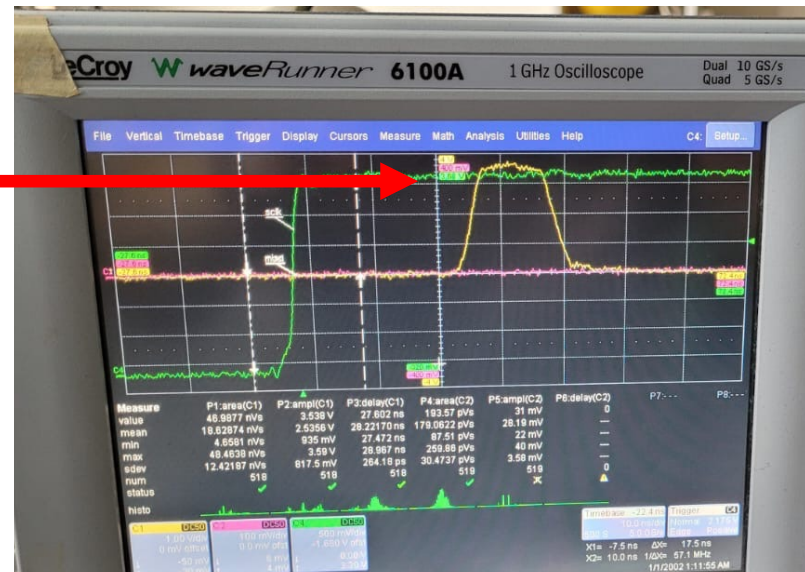
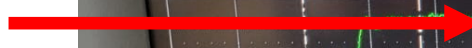
- Minimum discriminator/digitizer threshold $V_{TH} = 5$ mV
- Preamp linearly (within 0.2%) range = $[0, 4.7]$ V $\Rightarrow V_{preamp}(\text{max}) = 4.7$ V
- preamp transimpedance gain $G = 250$ V/A $\Rightarrow I_{peak}(\text{max}) = 19$ mA \Rightarrow max signal charge $Q(\text{max}) = 133$ pC; from $Q = e N_{pe} G_{PM} \Rightarrow (N_{pe} G_{PM})(\text{max}) = 83 \cdot 10^7$
- $G_{TOT} = G_{PM} G_{preamp}$ with $G_{preamp} \approx 2.5$
- 12m long cable attenuation: $C_{ATT} = 0.74$
- MAX single pulse amplitude at the discriminator/digitizer input is:
 $V_{dis}(\text{max}) = V_{preamp}(\text{max}) \cdot 0.5 \cdot C_{ATT} = 1.74$ V
- signal ampl = $V_{dis}(\text{max})/N_{pe}(\text{max})$
- $N_{pe}(\text{min}) = V_{TH}/(\text{signal ampl}) \Rightarrow N_{pe}(\text{max})/N_{pe}(\text{min}) = V_{dis}(\text{max})/V_{TH}$

G_{PM} ($\times 10^5$)	G_{tot} ($\times 10^6$)	$N_{pe}(\text{max})$	signal amplitude (mV/pe)	$N_{pe}(\text{min})$ $V_{TH} = 5$ mV	MeV at module center
4.2	1.04	~ 2000	0.87	~ 6	6.0
5.5	1.38	~ 1500	1.16	~ 4	4.0
8.3	2.1	~ 1000	1.74	~ 3	3.0
10	2.5	~ 800	2.18	~ 2	2.0

Test of preamp saturation

with preamplifier

saturation over 3.2 V



In this specific case (negligible cable length) we expect:

$$V_{\text{dis}}(\text{max}) = V_{\text{preamp}}(\text{max}) \cdot 0.5 = 2.35 \text{ V}$$

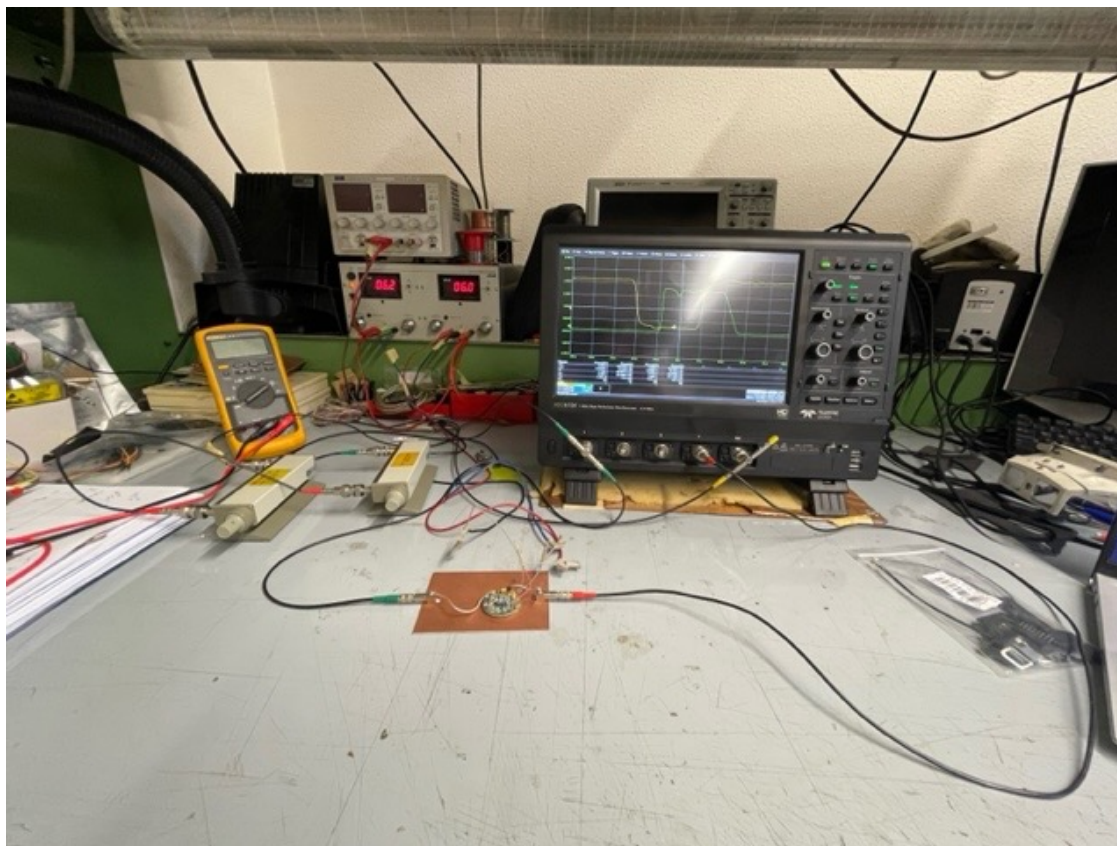
Assuming to increase $V_{\text{preamp}}(\text{max})$ by 15% while keeping linearity at an acceptable level, e.g. 1% (to be tested), we get:

$$V_{\text{preamp}}(\text{max}) = 5.4 \text{ V}$$

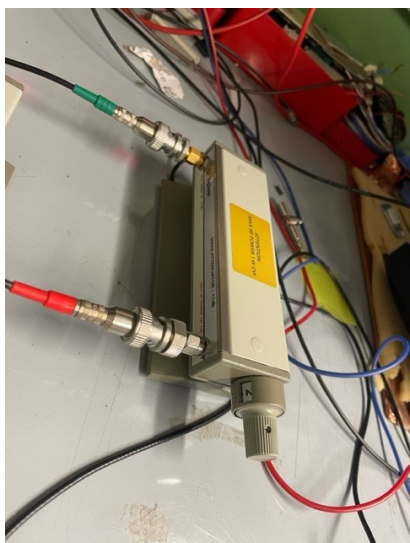
$$V_{\text{dis}}(\text{max}) = V_{\text{preamp}}(\text{max}) \cdot 0.5 = 2.7 \text{ V}$$

Preamp linearity test and saturation threshold

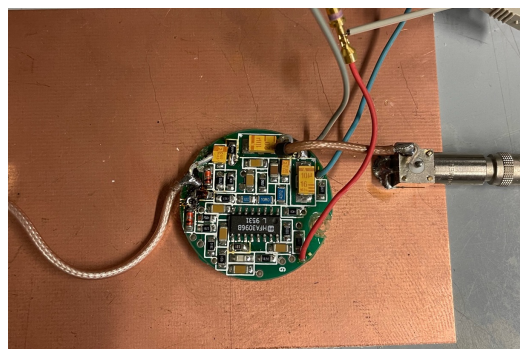
Test set-up



Signal amplitude varied with calibrated attenuators

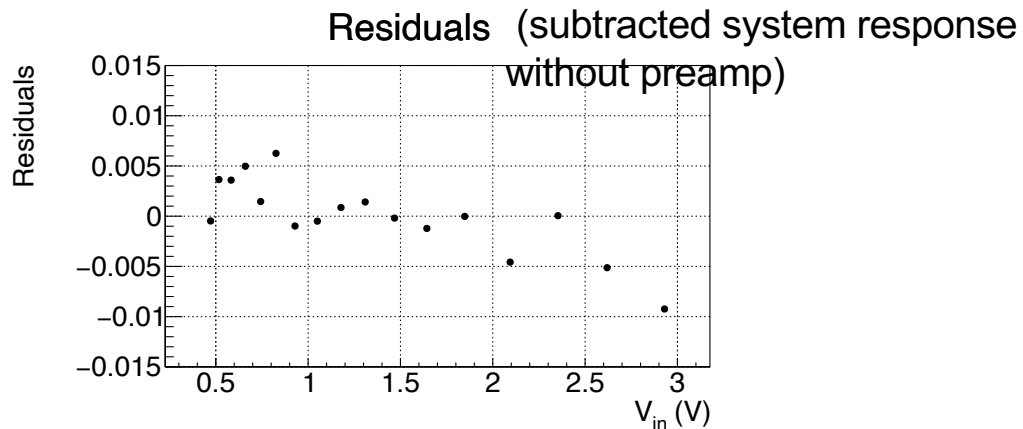
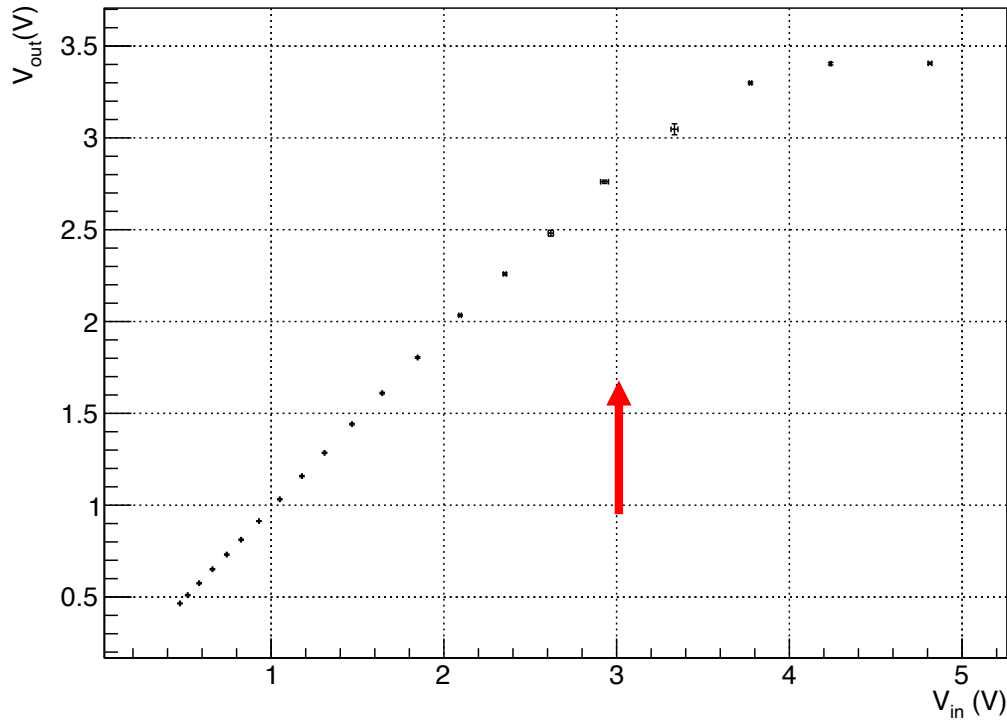


Signal at a modified test input: preamp gain ~ 1

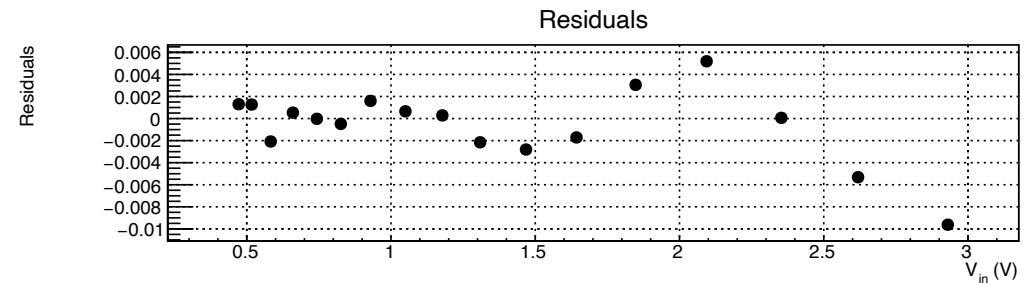
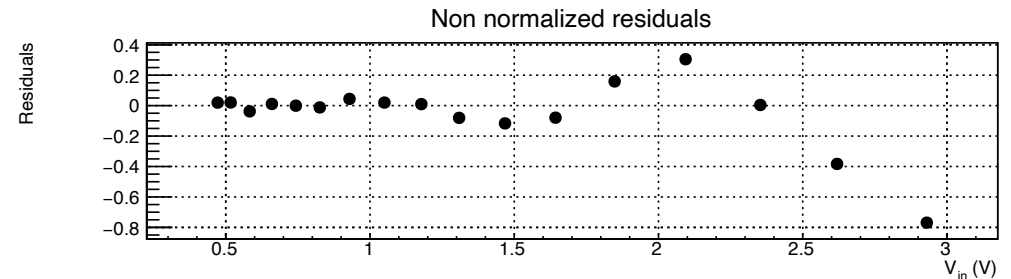
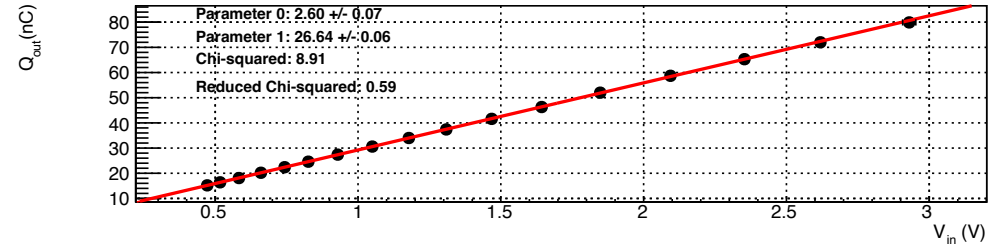


Preamp linearity test and saturation threshold

Linearity test



Linear fit



Choice of the dynamic range - II

Assuming:

- to increase $V_{\text{preamp}}(\text{max})$ by 15% $\Rightarrow V_{\text{preamp}}(\text{max}) = 5.4 \text{ V}$
- $(N_{\text{pe}} G_{\text{PM}})(\text{max}) = 95 \cdot 10^7$
- $V_{\text{dis}}(\text{max}) = V_{\text{preamp}}(\text{max}) \cdot 0.5 \cdot C_{\text{ATT}} = 2.0 \text{ V}$
- to have a very low noise environment as in KLOE \Rightarrow lowering (halving) the minimum discriminator/digitizer threshold to $V_{\text{TH}} = 2.5 \text{ mV}$

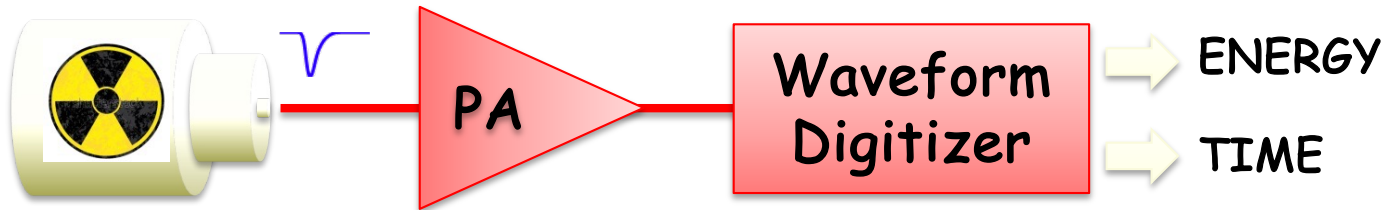
G_{PM} ($\times 10^5$)	G_{tot} ($\times 10^6$)	$N_{\text{pe}}(\text{max})$	signal amplitude (mV/pe)	$N_{\text{pe}}(\text{min})$ $V_{\text{TH}} = 2.5 \text{ mV}$	MeV at module center
4.8	1.2	~ 2000	1.0	~ 3	3.0
6.4	1.6	~ 1500	1.3	~ 2	2.0
9.5	2.4	~ 1000	2.0	~ 1	1.0

- Different dynamic ranges can be implemented changing $G_{\text{PM}} \Rightarrow$ the final choice should be a compromise between an affordable level of events with energy saturated cells, depending on $N_{\text{pe}}(\text{max})$, and an acceptable neutron detection efficiency, depending on $N_{\text{pe}}(\text{min})$.

Constraints on signal dynamic range
see previous slides

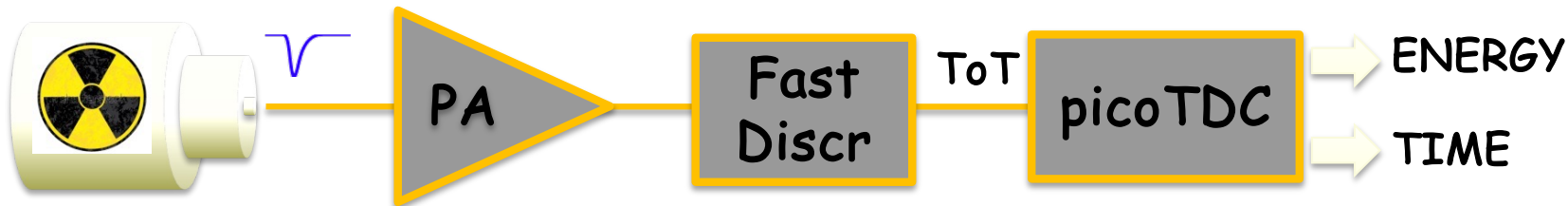
Two possible read-out schemes:

Detector



High Flexibility
 $F_{\text{sampl}} \sim 1 \text{ GS/s} \Rightarrow \text{High Cost}$
or
 $F_{\text{sampl}} \sim 125\text{-}250 \text{ MS/s}$
+ signal shaper
 $\Rightarrow \text{medium Cost}$

Detector



No Flexibility
 $\Rightarrow \text{medium cost}$
energy by ToT
with 2 or more
thresholds not to
worsen energy resol.

CAEN:

possible ready-to-use solution maintaining KLOE energy and time performance

Choice of FEE for SAND/ECAL

Digitizer solution:

$$V_{\text{signal}}(\text{max}) = 2 \text{ V}$$

$$V_{\text{signal}}(\text{min}) = O(0.1) \text{ mV}$$

=> no problems to set V_{TH} and $V_{\text{signal}}(\text{max})$ to match $V_{\text{dis}}(\text{max})$

Best choice, high cost:

1 GS/s digitizer => 1 ns: 4-5 time measurements on the rising edge of the 14 ns base signal to preserve time resolution

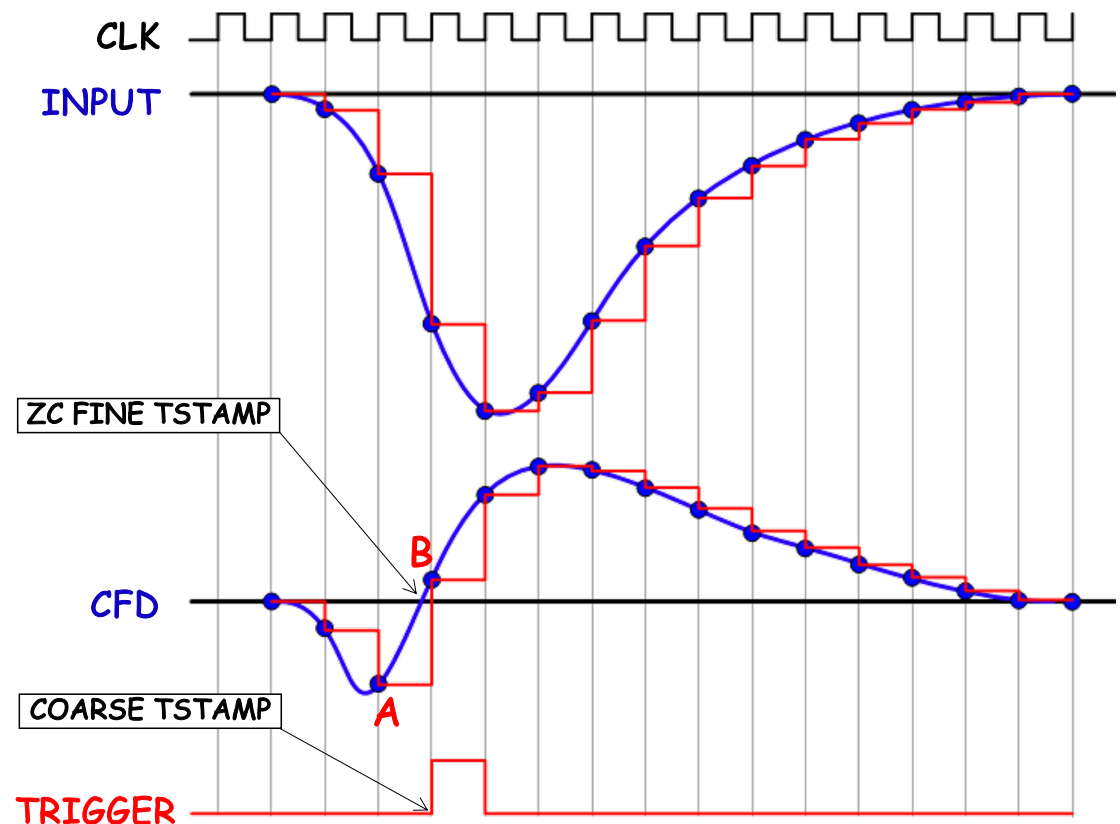
Alternative lower cost choice:

Using a lower cost digitizer, 125 or 250 MS/s => 8 or 4 ns, requires a shaper to stretch the signal.

In principle this solution does not worsen the time resolution, but requires to keep the pile-up under control, as confirmed by MC (or to detect it from the signal shape).

A 500 MS/s digitizer (14 bit) => 2 ns might not need to stretch the signal (use of ad-hoc correction algorithms and calibration for measuring the time) => under test at CAEN.

Digital CFD with interpolation



Preliminary tests with FERS by CAEN

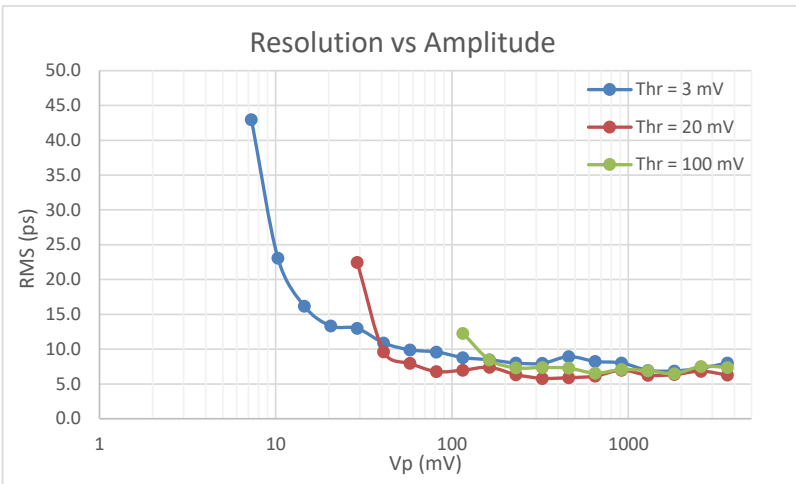


Fig. 2.2: Timing Resolution vs Pulse Amplitude

FERS A5203 (pico TDC)

fast input signal:
FWHM = 1.6 ns,
Rise = 1.1 ns,
Fall = 1 ns

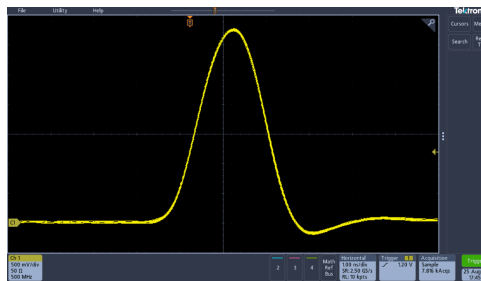


Fig. 2.1: Fast pulse from Agilent 81110A (width=1.5 ns, rise=fall=0.8 ns)

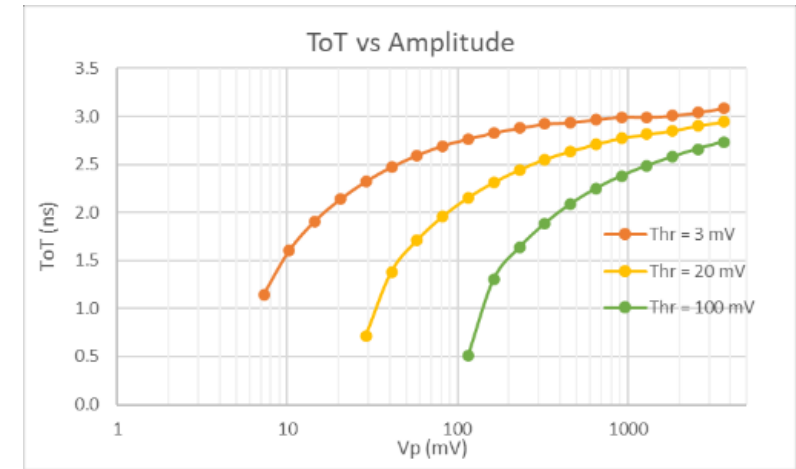


Fig. 2.3: ToT vs Amplitude

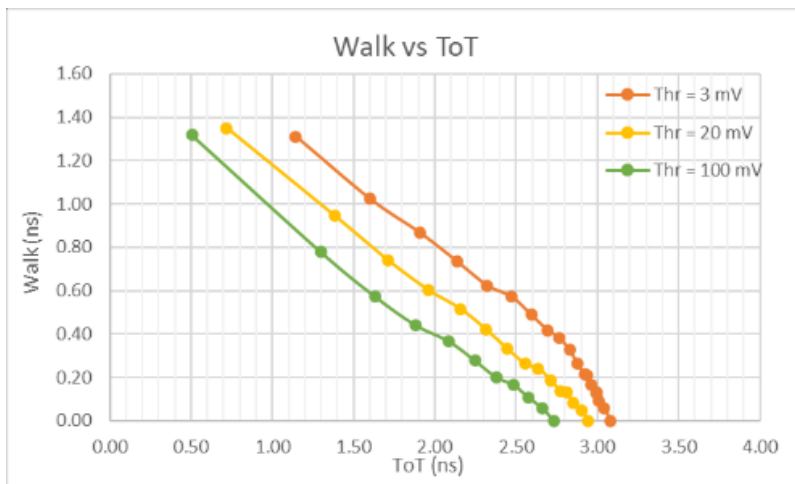


Fig. 2.5: Walk vs ToT

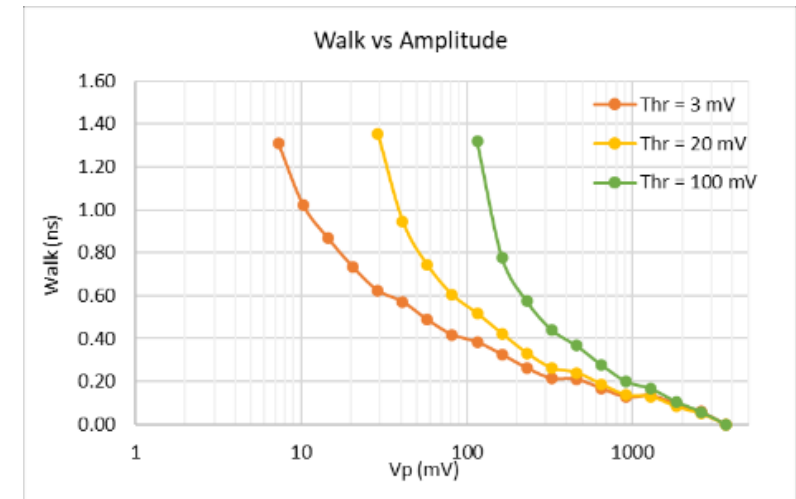


Fig. 2.4: Walk vs Amplitude

Studies for the optimization of the working point of the SAND calorimeter read-out electronics have been performed.

The MC simulation of the ECAL digitized response has been used to study the dynamic range and pile-up of the signals.

A test of the linearity of the PMT preamplifier has been performed; $V_{\text{preamp}}(\text{max})$ can be extended, e.g. from 4.7 to 5.4 V, still keeping the deviation from linearity $< 1\%$.

The preamplifiers of PMT bases are well compatible with the proposed FEE solutions, given that the maximum amplitude of signals accepted before digitization is around 2 V, i.e.

$$V_{\text{signal}}(\text{max}) = 2 \text{ V.}$$

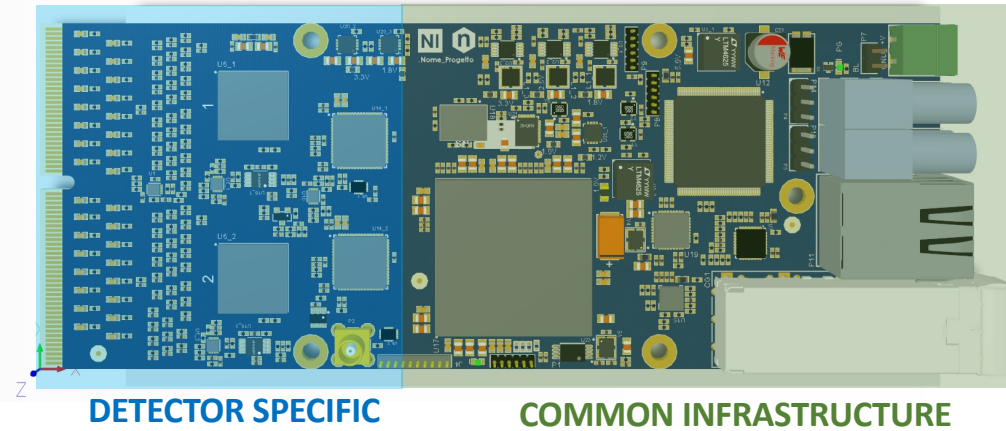
Keeping the preamplifiers has the advantage (i) to simplify the ECAL dismounting and test phases, and (ii) to keep the PMTs working point at a lower gain and HV level, beneficial for their lifetime.

In the long term, it would be necessary to design and build anew spare bases (with new components), to cope with possible long-term degradation of electronic components.

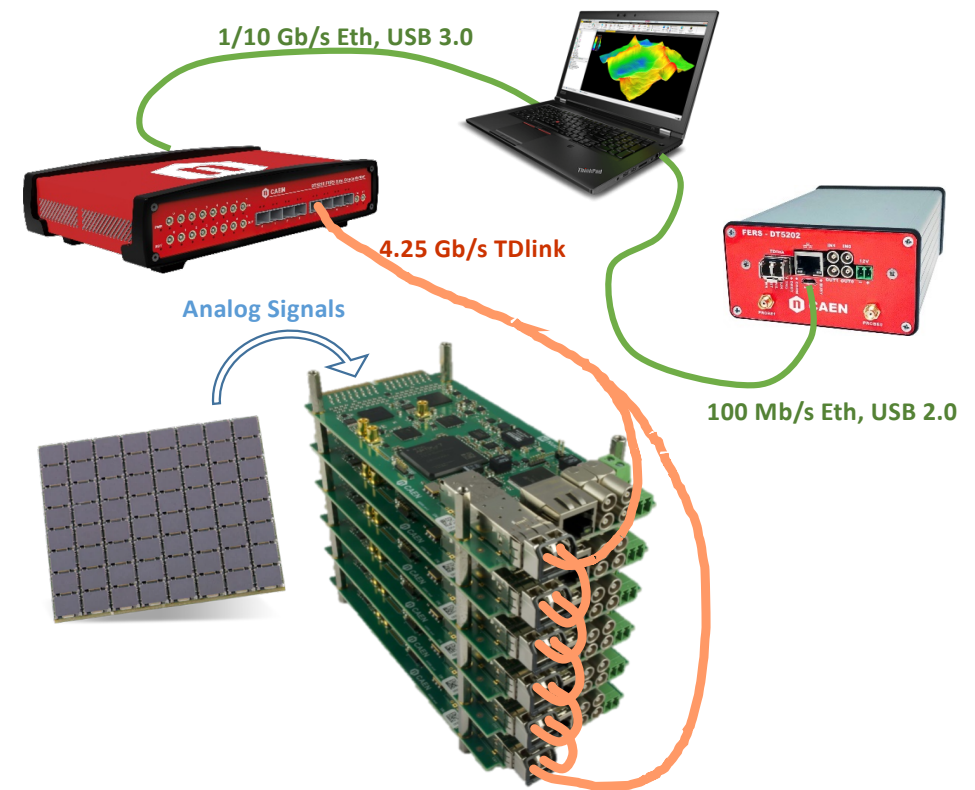
Possible solutions for the FEE that could constitute a good compromise between cost and performance are being investigated in collaboration with CAEN. These solutions have the advantage to be ready-to-use, preliminary results are encouraging, more detailed tests tailored on our case are needed and are in progress.

Spare

FERS: a scalable readout system



- **FERS:** Front End ASIC + ADC/TDC + Scalable Readout Infrastructure
- Easy integration of new ASICs
- **Scalability:** from single stand alone version for evaluation, to 10k/100k channels with same electronics
- **TDL:** daisy chainable optical link protocol with **data+sync**
- **Readout Tree:**
 - 1 link = 16 FERS units
 - 1 Concentrator = 8 links = 128 FERS = 8k/16k channels
 - Multiple Concentrators for unlimited readout...



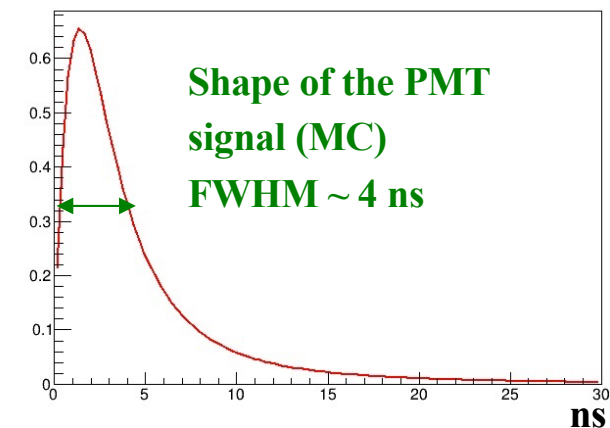
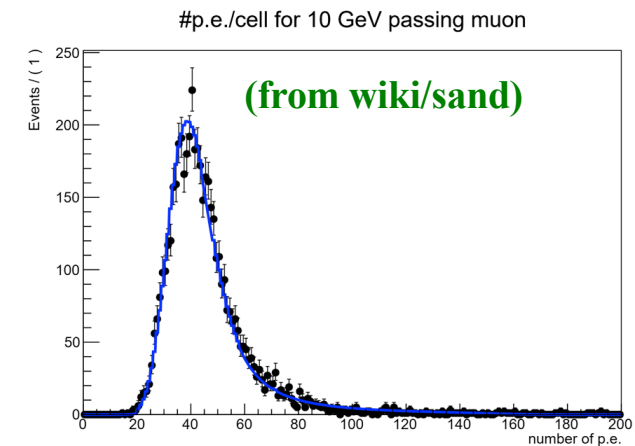
picoTDC (FERS A5203) + ToT solution

Digitization of ECAL similar to KLOE MC:

- Deposited energy in the cells propagated to PMTs with double exp. attenuation curve

$$f(x) = Ae^{-\frac{x}{\lambda_1}} + (1 - A)e^{-\frac{x}{\lambda_2}}$$

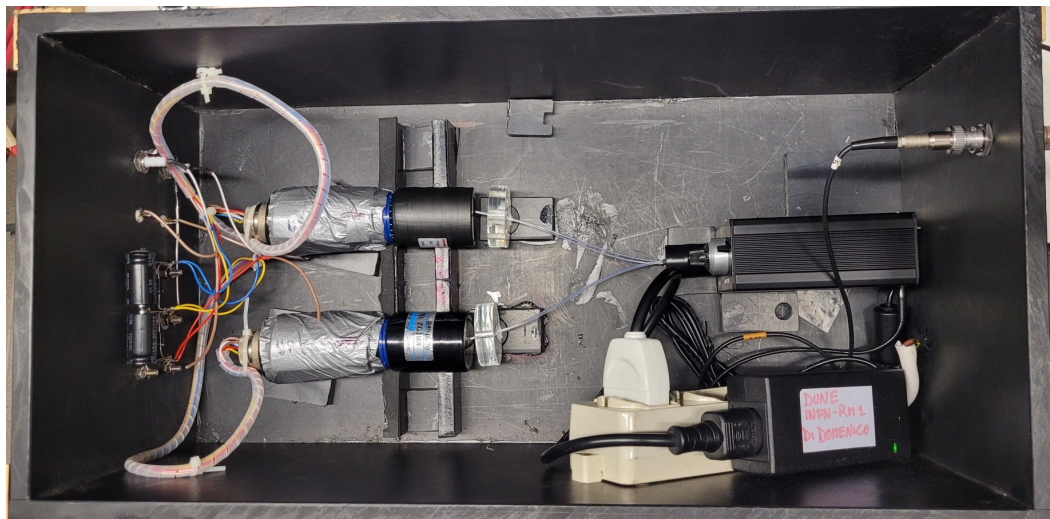
- Converted into p.e. number \Rightarrow 18.5 p.e./MeV of deposited energy (MIP at the module center \sim 40 p.e.)
- Light yield \sim 1 p.e./MeV of total energy of the particle
- Threshold = 2.5 p.e.
- Constant fraction discriminator at 15% of the signal
- Multihit TDC simulation (30 ns integration time + 50 ns dead time)



PMT system test at LNF

PMT system test with CAEN LED driver (wavelength ~ 400 nm) and scint. fiber splitter

two PMTs, one for reference

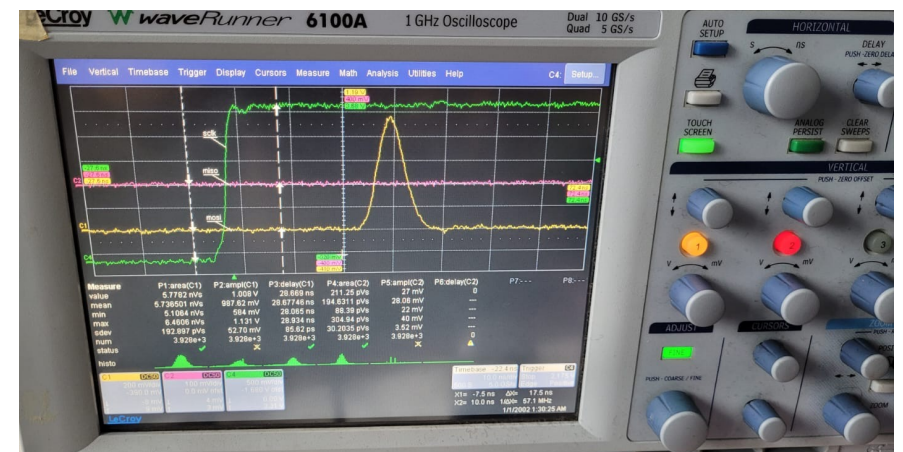


with preamplifiers a lower gain is needed, which is beneficial for PMT lifetime

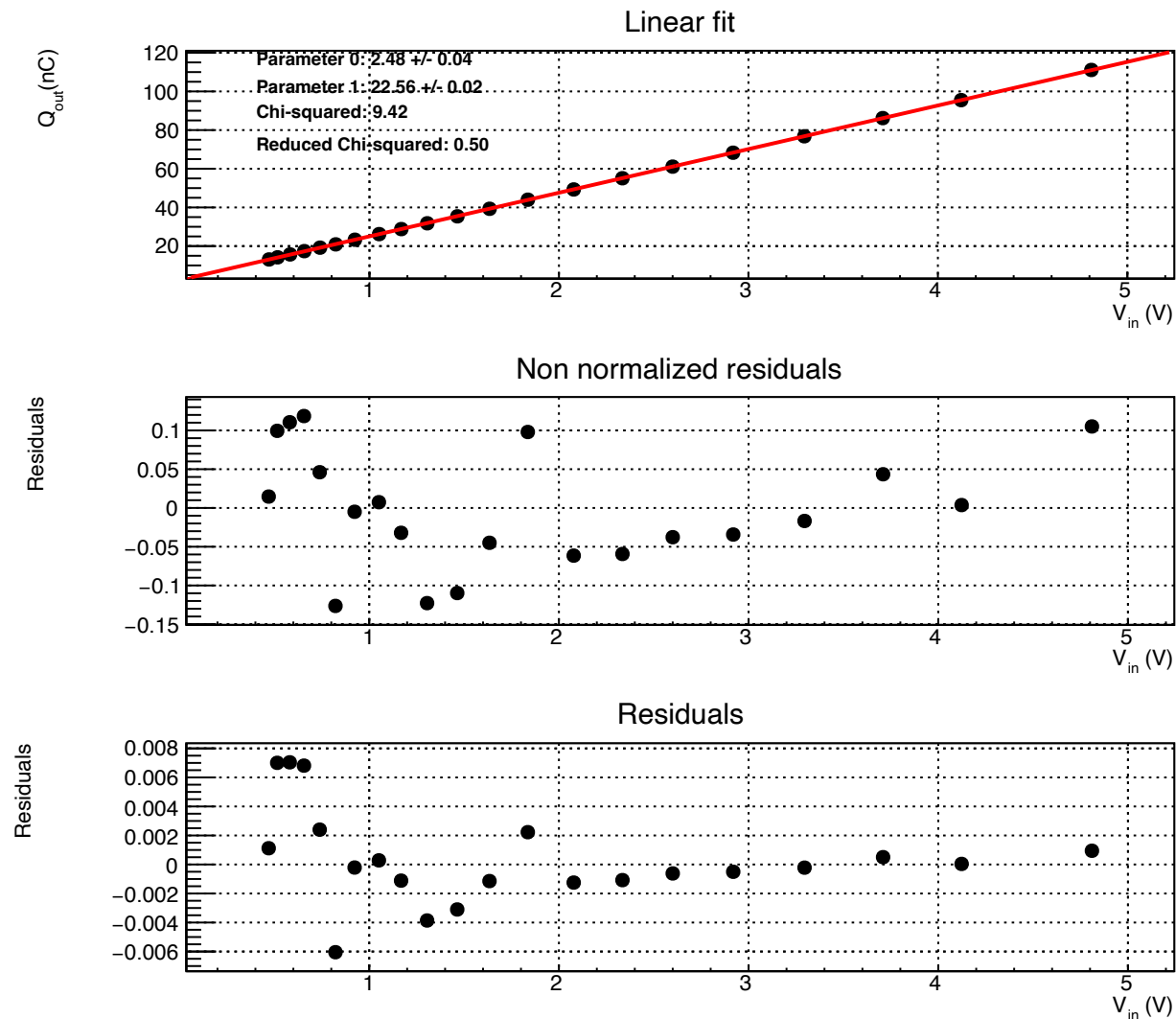
no preamplifier



with preamplifier



Linearity of the test system without preamp



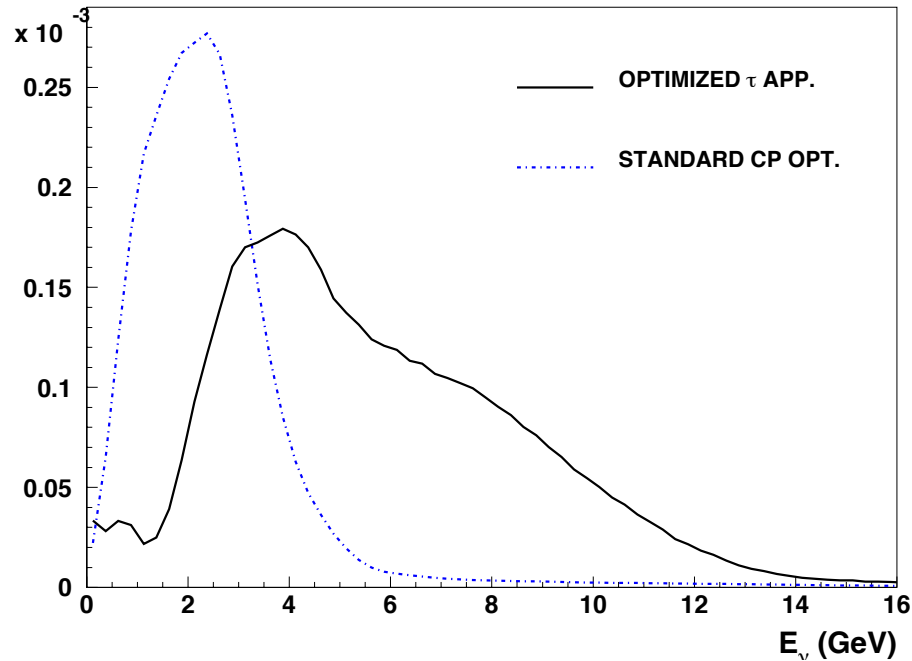


Figure 87: Comparison of LBNF ν_μ fluxes: (a) default 3 horn beam optimized for CP violation (dash-dotted); (b) ν_τ appearance optimized beam (solid).

From DUNE docDB note 13262
A proposal to enhance the DUNE near detector complex

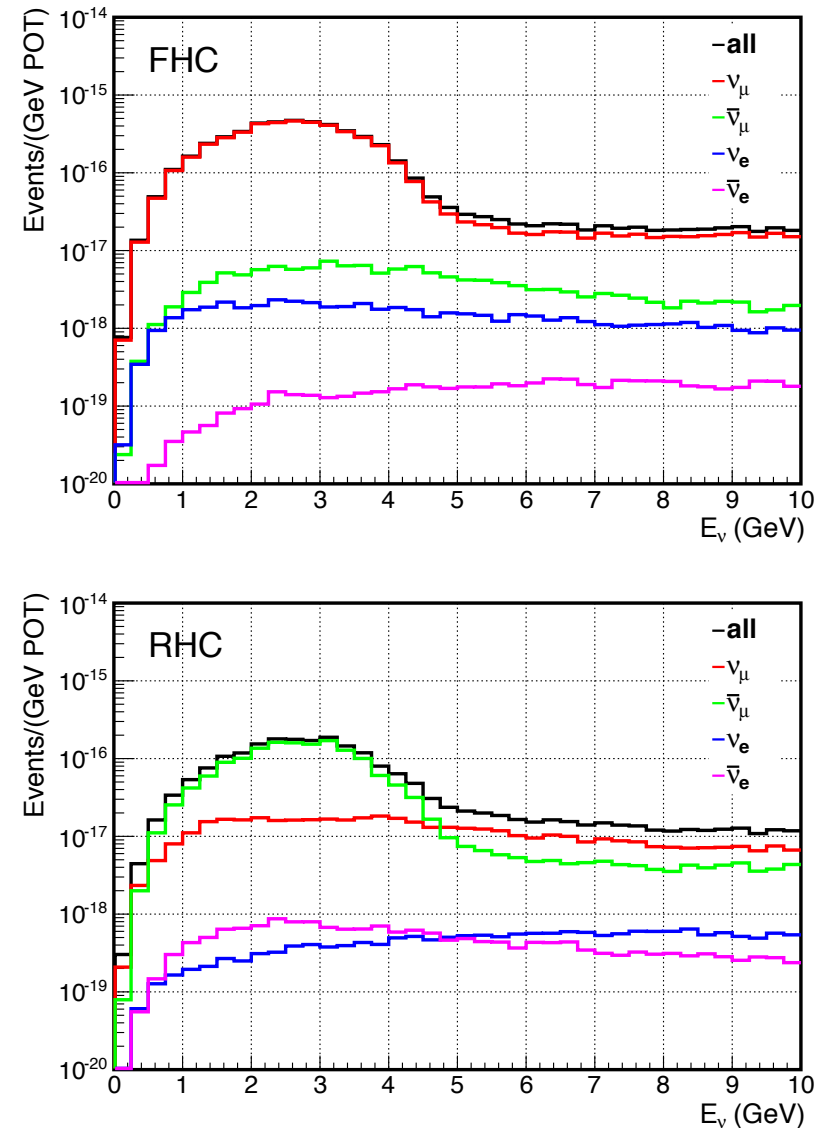
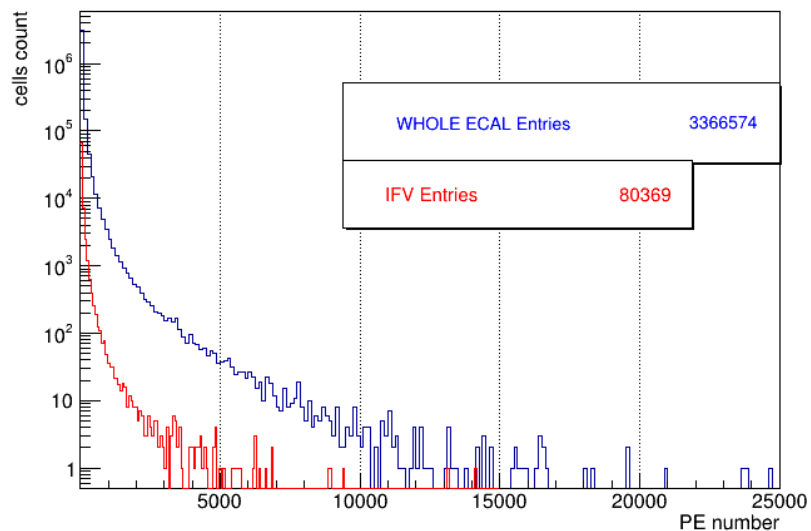
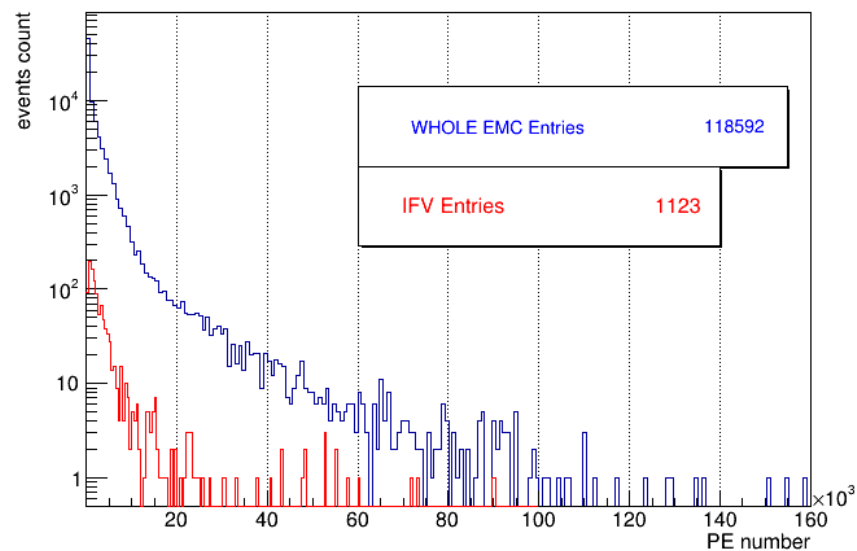


Figure 89: Energy spectra of CC interacting neutrinos in the internal LAr target, having a mass of 1.01 ton, and considering a 120 GeV proton beam in both FHC and RHC modes.

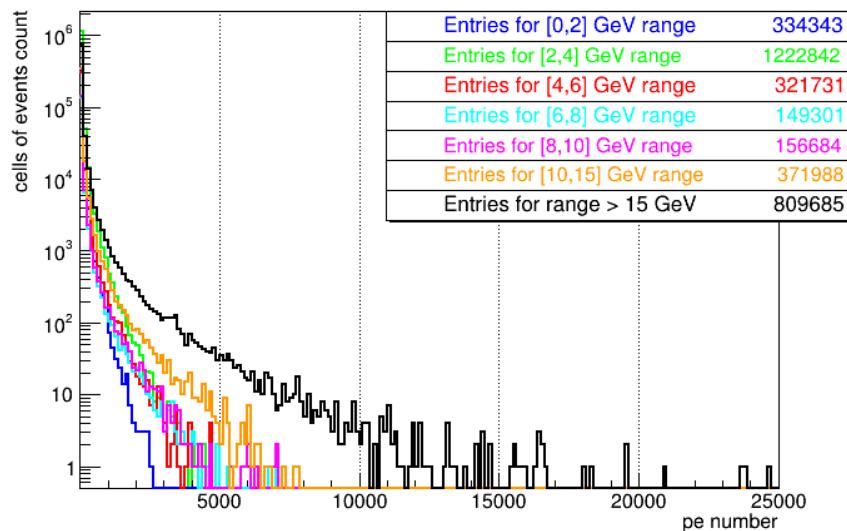
PE distribution



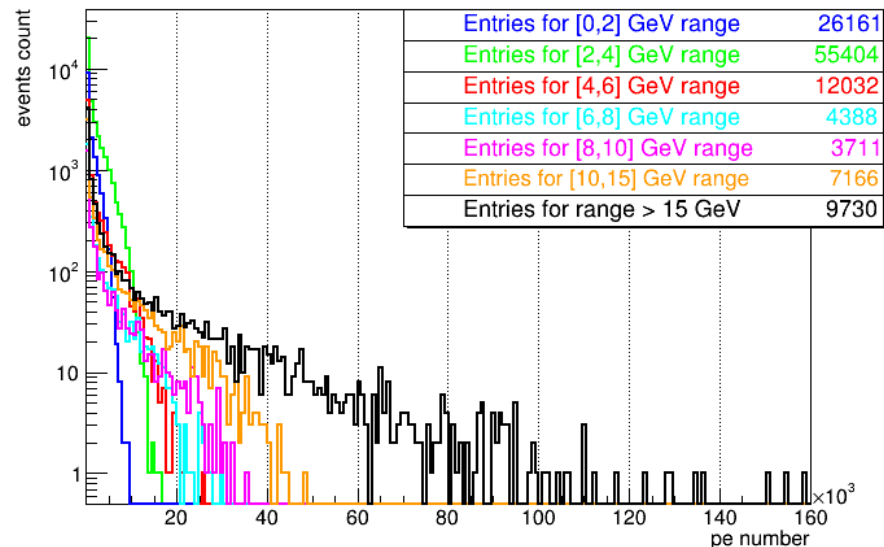
Total PE release



PE distribution at E_ν fixed

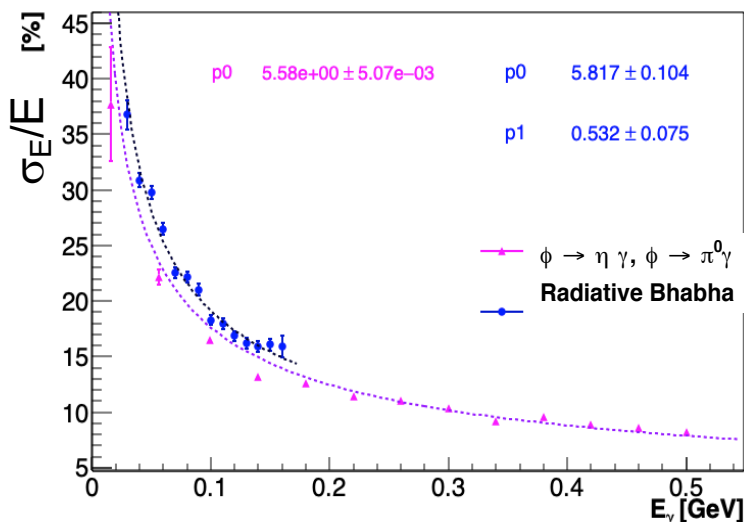


Total PE number distribution at E_ν fixed



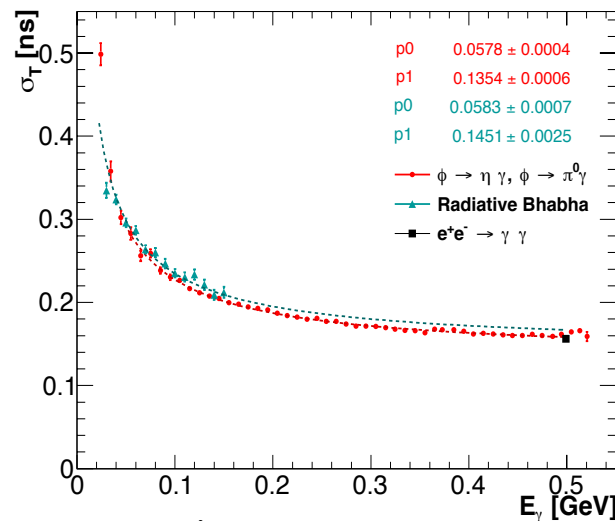
KLOE ECAL performance in KLOE-2 and with neutrons

Check e.m. calorimeter performance during KLOE-2 data taking (2015-2018): compatible with known performance.

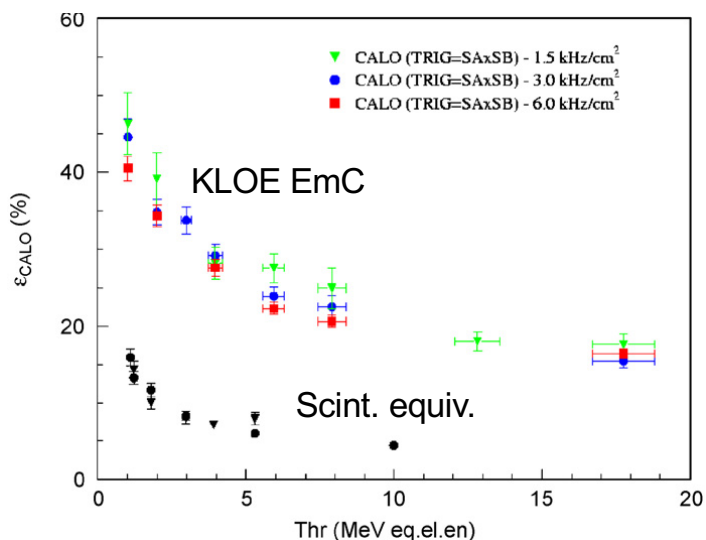


$$\sigma_E/E \cong 5.6\% / \sqrt{E(\text{GeV})}$$

$$\sigma_\tau \cong 58 \text{ ps} / \sqrt{E(\text{GeV})} \oplus 135 \text{ ps}$$



Thanks to E. Diociauti - LNF

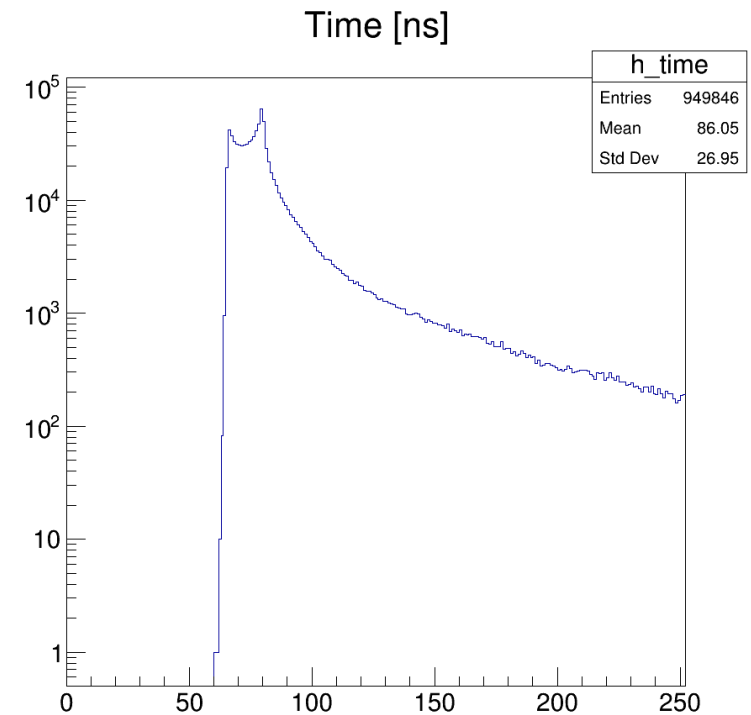
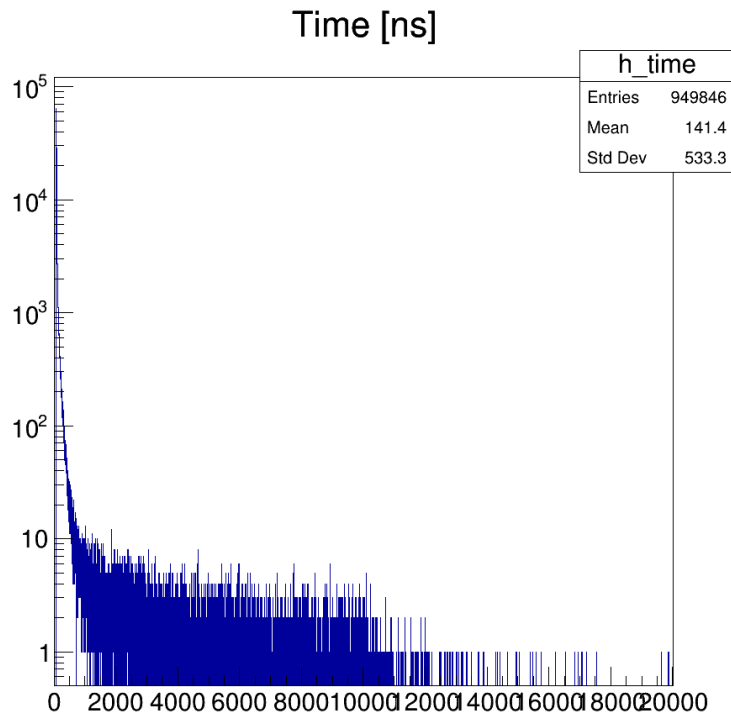
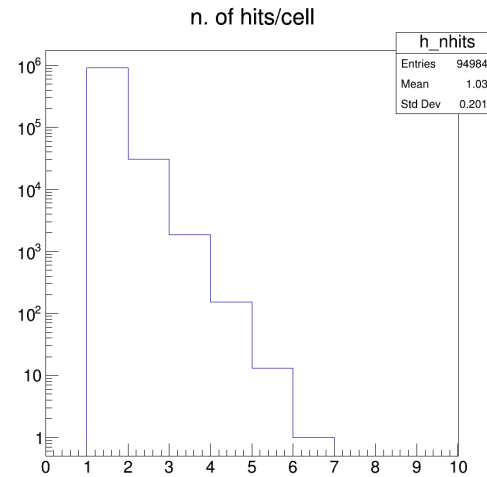


Measurement of the neutron response of the KLOE EmC

- M. Anelli et al., "Measurement and simulation of the neutron response and detection efficiency of a Pb-scintillating fiber calorimeter", NIM **A581** (2007) 368
- M. Anelli et al., "Measurement of the neutron detection efficiency of a 80% absorber-20% scintillating fibers calorimeter", NIM **A626** (2011) 67 (Gauzzi corresponding author)

Time simulation

- **TDC Multihit simulation:**
integration time 30 ns
(starting from first p.e. time)
50 ns dead time
- **Constant fraction simulation: 15%**
of the total p.e. number



Neutron detection efficiency

thresholds 250 eV in STT and 1.1 p.e. in ECAL

