EUROPEAN PLASMA RESEARCH ACCELERATOR WITH EXCELLENCE IN APPLICATIONS

ESFRI

ROADMAP 2021





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EuPRAXIA laser requirements and current conceptual design issues Leonida Antonio GIZZI (CNR, Pisa, Italy) with Paul CRUMP, (FBH, Germany) Luca LABATE, (CNR, Pisa, Italy) Guido TUC (CNR, Firenze, Italy)





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http://eupraxia-project.eu







- EuPRAXIA laser requirements
- Overall layout
- Thermal management options
- Modelling
- Pump lasers
- Summary





The EuPRAXIA Project



With the inclusion in ESFRI and the approval of the Preparatory Phase Project, EuPRAXIA must rapidly move from the conceptual design to a <u>viable</u> technical design of the laser driver.



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- The EuPRAXIA project aims at the construction of an **innovative compact electron accelerator** using laser- and electron-beam-driven plasma wakefield acceleration;
- EuPRAXIA foresees the implementation of a **laser wakefield accelerator** (LWFA) at the 1-5 GeV target energy and a repetition rate of 20-100 Hz, requiring the most advanced and robust ultrashort pulse laser technologies available to date;
- The **Design Study project** was carried out initially by 16 laboratories and universities from 5 EU member states within the European Union's Horizon 2020 programme;
- A **Conceptual Design Study** has addressed the development of a ultrashort pulse laser system (pulse durations in the range of tens of fs) and energies up to 100 joules, yielding a PW scale peak power, targeting a repetition rate of up to 100 Hz, a performance never achieved so far
- EuPRAXIA was included in the ESFRI Roadmap (2021) and a Preparatory Phase project is ongoing.





The EuPRAXIA project: main specs



| Quantity | Baseline Value | | |
|----------------------|--|----------------------------|---|
| | Laser systems | | |
| Wavelength | 800 nm | | |
| Energy on target | 5–100 J | | |
| Pulse duration | ≥20–60 fs | | Betatron source |
| Repetition rate | $20-100\mathrm{Hz}$ | Photon energy | $0.6{-}110\mathrm{keV}$ |
| High-energy electron | ı beam from beam-driven plasma accelerator (PWFA) | Source size | $1.4-2.4\mu{ m m}$ |
| Energy | $1.0-5.0\mathrm{GeV}$ | Photons per pulse | $2	imes 10^8$ – $4	imes 10^{10}$ |
| Charge | 30–40 pC | Peak X-ray brightness | 2×10^{21} -1 $\times 10^{26}$ photons/(mm ² mrad ² s[01%BW]) |
| Bunch duration | ~13 fs | | Inverse Compton source |
| Energy spread | 0.4 – 1.1% | Photon energy | $\geq 100 \mathrm{MeV}$ |
| Normalised emittance | 0.7–1.2 mm mrad | Pulse duration | $\sim 30 \mathrm{fs}$ |
| High-energy electro | n beam from laser-driven plasma accelerator (LWFA) | Divergence | <1 mrad |
| Energy | 5.0-6.0 GeV | Low-energy positron source | |
| Charge | 23–30 pC | Positron energy | 0.5–10 MeV (tunable) |
| Bunch duration | 3–11 fs | Beam duration | 20–90 ps |
| Energy spread | 0.1 - 0.9 % | Positrons per shot | $\geq 1 \times 10^6$ |
| Normalised emittance | 0.1–1.4 mm mrad | | High-energy positron source |
| | Free-electron laser | Positron energy | $\geq 1.0 \text{GeV} (\text{tunable})$ |
| Radiation wavelength | 0.19–35.9 nm | Beam duration | ≤10 fs |
| Pulse duration | 0.4–15 fs | Positrons per shot | $\sim 1 \times 10^{7}$ |
| Saturation length | 16–126 m | | |
| Photons per pulse | $1.9 	imes 10^9 - 7.2 	imes 10^{11}$ | | |
| Brightness | 2×10^{28} - 4.8×10^{32} photons/[mm ² mrad ² s(01%BW)] | | |







- In the EuPRAXIA project, several alternative technological approaches were considered and downselected, to provide the required laser driver performances.
- We based the design on **Chirped Pulse Amplification (CPA) in Ti:Sapphire**, pumped by all-solid state green lasers (i.e. diode pumped, frequency doubled Yb or Nd lasers)
- **Thermal management** related to the handling of high pump average power was the most complex aspect in the design, requiring out-of-the-box thinking and original solutions
- **Optimization of energy extraction** was also an issue, aimed to reduce pump energy requirements and waste heat production.

Three laser systems envisaged, to drive three stages:

- Laser Plasma Injector at 150 MeV (LPI 150MeV)
- Laser Plasma Injector/Accelerator at 1 GeV (LPI 1GeV)
- Laser Plasma Accelerator at 5 GeV (LPA 5GeV)

For each system, two levels of performances considered: P0: low energy, 20 Hz rep rate P1: high energy, 100 Hz rep rate





GENERAL ARCHITECTURE





Modularity of amplification stages:

| LPI 150 MeV | \Rightarrow | Laser1 |
|-------------|---------------|--------------------------|
| LPI 1 GeV | \Rightarrow | Laser1 + Laser2 |
| LPA 5 GeV | \Rightarrow | Laser1 + Laser2 + Laser3 |

- adjustments on pulse duration/bandwidth
- Synchronization: common master oscillator
- Pulse duration/wavelength tailoring : separate front end
- Scalability: possibility to upgrade from P0 to P1 performance levels without a major changes







High repetition rate (100 Hz) will speed up R&D of pending issues for Ti:Sa laser TDR









Main challenges: large optics, mechanical stability, cooling of gratings, beam quality control ...











Different technologies under evaluation to address main issues with higher repetition rate. Strategy includes **reduction** of the thermal load at high average power, **cooling** of residual heat and **control** of thermal effects on compression quality.







Beam Pointing Stability



Eupraxia requirements for beam pointing stability are extremely demanding. Both passive and active control will be required. Prior to the implementation of control strategies, tools are being developed to measure pointing stability performances at EuPRAXIA facilities and labs.





AMPLIFICATION CHAIN: REQUIREMENTS



| LASER 1 - Injector 150 MeV | | | | | |
|--|----------------------|-----|------|--|--|
| Parameter | Label | P0 | P1 | | |
| Wavelength (nm) | $\lambda_{1 (nm)}$ | 800 | 800 | | |
| Maximum energy on target (J) | E _{target} | 5 | 7 | | |
| Maximum output energy (J) | E _{out} | 8.8 | 12.5 | | |
| Energy tuning resolution (% of targeted value) | dE | 7 | 5 | | |
| Total output energy (incl. Diagnostic beams) | E _{tot} | 7 | 10 | | |
| Pulse length (FWHM) (fs) | τ1 | 30 | 20 | | |
| Repetition rate (Hz) | f ₁ | 20 | 100 | | |
| Requirement on energy stability (RMS) % | σ _{<e></e>} | 1 | 0.6 | | |

| LASER 2 - Injector 1 GeV | | | | |
|--|----------------------|------|------|--|
| Parameter | Label | PO | P1 | |
| Wavelength (nm) | λ _{2 (nm)} | 800 | 800 | |
| Maximum energy on target (J) | E _{target} | 15 | 30 | |
| Maximum output energy (J) | E _{out} | 18.8 | 37.5 | |
| Energy tuning resolution (% of targeted value) | dE | 7 | 5 | |
| Shortest pulse length (FWHM) (fs) | τ2 | 30 | 20 | |
| Repetition rate (Hz) | f ₂ | 20 | 100 | |
| Requirement on energy stability (RMS) % | σ _{<e></e>} | 1 | 0.6 | |

| LASER 3 - Driver 5 GeV | | | |
|--|---------------------|------|-----|
| Parameter | Label | PO | P1 |
| Wavelength (nm) | $\lambda_{2 (nm)}$ | 800 | 800 |
| Maximum energy on target (J) * | E_{target} | 50 | 100 |
| Maximum output energy (J) | E _{out} | 62.5 | 125 |
| Energy tuning resolution (% of targeted value) | dE | 7 | 5 |
| Shortest pulse length (FWHM) (fs) | τ ₂ | 60 | 50 |
| Repetition rate (Hz) | f ₂ | 20 | 100 |
| Requirement on energy stability (RMS) % | σ< _{E>} | 1 | 0.6 |

Maximum output energy: (Energy on Target)/(Compressor Efficiency) Compressor efficiency assumed **80%** Seed energy: 1.5 J



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Foreseen I/O energy and pump requirements



Three main modules: LASER1, LASER2, LASER3 LASER1: stand-alone for LPI 150 MeV LASER2: output stage for LPI 1 GeV, second stage for LPA 5GeV LASER3: high energy stage for LPA 5GeV Two levels of performance : P0 and P1





THERMAL MANAGEMENT



Expanding knowledge base for water cooled with "through" propagation: some examples



Water cooled Ti:Sa amplifier ("Active Mirror" configuration) under development at ELI-HU (After V. Cvhykov et al., Opt. Lett, **41**, 3017, 2016)

Fluid (D₂O) cooled 3 kW Nd:YAG laser, 20 kW CW pump power, D₂O (After X. Fu et al., Opt. Express, 22, 18421 (2014)





Fluid (Siloxane) cooled Nd:YLF laser, 5 kW CW pump power (After Z. Ye et al., Opt. Express, 24, 1758 (2016)





AMPLIFICATION MODULES: CONCEPTUAL LAYOUT



Two possible solutions envisaged, determined by thermal management considerations

Common features:

- gas cooling found to be insufficient at the given power density
- face cooling of gain elements by water flow (longitudinal cooling)
- gain volume split in some sub-elements to increase cooling surface
- multi-step pumping for parasitic laser management



1 – Multipass amplification scheme in transmission

Double side, double pass pumping

Crystal split in 2 elements, face cooled by water flow, to increase cooling surface Multipass amplification (4 to 6 depending on stages)

Absorption layer on crystal sides for parasitic lasing suppression





AMPLIFICATION MODULES: CONCEPTUAL LAYOUT



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Common features:

- face cooling of gain elements by water flow (longitudinal coling)
- gain volume split in some sub-elements to increase cooling surface
- multi-step pumping for parasitic laser management





- Multi-pass pumping scheme to ensure effective pump absorption
- Overall pump energy equally divided among the 4 elements
- Overall gain length split in 4 elements, water cooled on the back side
- Multiple reflections required to obtain efficient energy extraction
- Absorption layer on crystal sides for parasitic lasing suppression







Which geometry is better?



<u>Pro's</u>

- Simpler scheme (up to 2 sub-crystals, single pump path)
- Broader cooling surface available
- Less sensitive to mechanical vibrations
- Less sensitive to parasitic reflections (contrast issues)

<u>Con's</u>

- Aberrations from fluid turbulences
- Very critical design of the fluid ducts



- No aberration from cooling fluid
- Modularity

<u>Con's</u>

- Less cooling capability
- More complex set-up (up to 3 units required , pump splitting)
- More sensitive to mechanical vibrations
- Possible issues from parasitic reflections (pulse contrast)

Both schemes equally studied in the preliminary design: equivalent perfomances from simulations Critical aspects (i.e. optical aberrations from cooling fluid) beyond numerical simulations capabilities Dedicated experimental development (i.e. realization and testing of small scale pilot devices) is required to address this design choice





EXAMPLE OF LAYOUT FOR TRANSMISSION AMPLIFIERS





Pumping path (single pump source, split in 2 pulses)

6 passes configuration, bow-tie geometryAngle between passes \sim n x 1.2° (n=1,2,3)Footprint length: \sim 4 mt (Laser 1)

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~ 5 mt (Laser 2)
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~ 8 mt (Laser 3)
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(to avoid beam superimposition)

Each pump pulses passes twice through the crystals Pumping from both sides to reduce peak fluence and parasitic lasing

Extraction During Puming (EDP) implementation

The pump pulse must be split before of the injection; one of the pulses goes through a delay line to implement the EDP

Off-plane angular multiplexing of the pump beams to have more pump "gates" available



PUMP TIMING AND EDP ENERGY RIPARTITION





Pump pulse absorption time ~10 ns t_r: pulse round trip time between passes

E^[^]PR

(12 ns, 15 ns, 18 ns respectively for Laser 1, Laser2 and Laser3

The delay line of the second pump pulse has to to provide the proper delay between the two pulses.





EXAMPLE OF LAYOUT FOR REFLECTION AMPLIFIERS



∮ Ÿ ●─→ X



Amplification path

Pumping path (single pump source)





3 disks, 2 double passes configuration Half angle between passes ~ 1.2°-2.4 ° Footprint length: ~ 3 mt (Laser 1) ~ 5 mt (Laser 2) ~ 8 mt (Laser 3) (to avoid beam superimposition) Footprint width < 1.5 m

Straightforward extension to 4 disks

Pump pulse energy is distributed among the disks by beamsplitters (or waveplates+polarizers) Each pump pulse passes twice through the crystals

EDP implementation

The arrival of the pump pulse is synchronized with the arrival of the amplified pulse by means of fixed delay lines (equal path length). Energy repartition between the passes is achieved by fine tuning of the delay

Off-plane pump injection to avoid beam path occlusions One injection "gate" for each pump source



PUMP TIMING AND EDP ENERGY RIPARTITION



Seed pulse (at t=0) Seed pulse Disk 1 Pump pulse Stored energy 6t_r 0 Disk 2 f_2 f₁ 5tr t tr 0 Disk 3 • f₂ t₁ 2t_r 4t_r 0

t_r: pulse round trip time between passes (12 ns, 15 ns, 18 ns respectively for Laser 1, Laser2 and Laser3

FUPR

The delay lines of the pump between the disk ensures **synchronization of pump arrival** with the seed pulse. Fraction f_1 of pump pulse energy is available for 1° pass amplification, fraction f_2 for the 2° pass. The ratio f_1/f_2 can be adjusted by finely tuning the delay between the pump and the seed pulse



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NUMERICAL SIMULATION OF AMPLIFICATION MODULES



The amplification stages were numerically simulated (MIRO - CEA) The code allows for the simulation of amplification of ultrashort pulses, accounting for GVD, nonlinear effects, spectral narrowing effects and so on

The different amplification stages were extensively analyzed in the different architectures (transmission vs reflection scheme)

Simulations for the two architectures implemented:

- same overall gain length, number of passes
- same doping level
- same overall pump energy
- same beam cross section

We obtained:

- Very similar energy extraction performance for the two schemes
- Very similar sensitivity of output energy vs seed, pump energy

Results are summarized in the following slides



VS.









| Crystal clear aperture \varnothing (cm) | 6 cm | Crystal thickness (cm, overall) | 1.2 |
|---|-------|---------------------------------|-----|
| Doping level (%Wt.) | 0.075 | Absorption coefficient (cm-1) | 1.2 |

Performance level P0

| Pump energy (J) | 19.2 | Pump beam diameter (cm, FWHM) | 5.0 |
|---|---------------|---|---------------------------|
| Pump fluence at crystal surfaces (J/cm ²) | 0.76 | Absorbed pump energy (%) | 94% |
| Seed pulse energy (J) | 1.5 | Seed beam diameter (cm, FWHM) | 4.7 |
| Output energy | 8.9 | Extraction efficiency | 38.7% |
| Output beam diameter (cm FWHM) | 4.5 | Output beam peak fluence (J/cm2) | 0.55 |
| EDP scheme | 65% 1st pass, | Max G _T | \sim 15 (before the 4th |
| | 35% 4th pass | | pass) |
| S_{pump} ($\Delta E_{out}/\Delta E_{pump}$) | 0.53 | $S_{seed} (\Delta E_{out} / \Delta E_{seed})$ | 2.4 |

Performance level P1

| Pump energy (J) | 25.7 | Pump beam diameter (cm, FWHM) | 5.0 |
|---|-------------------------------|---|----------------------------|
| Pump fluence at crystal surfaces (J/cm2) | 1.01 | Absorbed pump energy (%) | 94% |
| Seed pulse energy (J) | 1.5 | Seed beam diameter (cm, FWHM) | 4.7 |
| Output energy (J) | 12.7 | Extraction efficiency | 43.6% |
| Output beam diameter (cm FWHM) | 4.6 | Output beam peak fluence (J/cm ²) | 0.765 |
| EDP scheme | 65% 1st pass, 35% 4th pass | Max G _T | ~ 30 (before the 4th pass) |
| S_{pump} ($\Delta E_{out}/\Delta E_{pump}$) | 0.58 | $S_{seed} (\Delta E_{out} / \Delta E_{seed})$ | 2.67 |



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6 passes amplification scheme



AMPLIFICATION MODULES: AMP 2



| Crystal clear aperture \varnothing (cm) | 10 | Crystal thickness (cm, overall) | 2.0 |
|---|------|---------------------------------|------|
| Doping level (%Wt.) | 0.05 | Absorption coefficient (cm-1) | 0.79 |

Performance level P0

| Pump energy (J) | 37.2 | Pump beam diameter (cm, FWHM) | 9.0 |
|--|---------------|---|---------------------|
| Pump fluence at crystal surfaces (J/cm ²) | 0.425 | Absorbed pump energy (%) | 96% |
| Seed pulse energy (J) | 6.25 | Seed beam diameter (cm, FWHM) | 8.0 |
| Output energy (J) | 19.1 | Extraction efficiency | 35.0% |
| Output beam diameter (cm FWHM) | 8.0 | Output beam peak fluence (J/cm ²) | 0.38 |
| EDP scheme | 60% 1st pass, | Max G _T | ~ 6 (before the 3rd |
| | 40% 3rd pass | | pass) |
| $S_{pump} \left(\Delta E_{out} / \Delta E_{pump} \right)$ | 0.45 | $S_{seed} (\Delta E_{out} / \Delta E_{seed})$ | 1.8 |

Performance level P1

| Pump energy (J) | 65.2 | Pump beam diameter (cm, FWHM) | 9.0 |
|---|---------------|---|---------------------------|
| Pump fluence at crystal surfaces (J/cm ²) | 0.75 | Absorbed pump energy (%) | 96% |
| Seed pulse energy (J) | 8.75 | Seed beam diameter (cm, FWHM) | 8.0 |
| Output energy (J) | 37.5 | Extraction efficiency | 44.1% |
| Output beam diameter (cm FWHM) | 8.3 | Output beam peak fluence (J/cm ²) | 0.72 |
| EDP scheme | 60% 1st pass, | Max G _T | \sim 14 (before the 3rd |
| | 40% 3rd pass | | pass) |
| S_{pump} ($\Delta E_{out}/\Delta E_{pump}$) | 0.53 | $S_{seed} (\Delta E_{out} / \Delta E_{seed})$ | 1.49 |



6 passes amplification scheme





| Crystal clear aperture \varnothing (cm) | 16 cm | Crystal thickness (cm, overall) | 3.2 |
|---|-------|---------------------------------|------|
| Doping level (%Wt.) | 0.03 | Absorption coefficient (cm-1) | 0.47 |

Performance level P0 (6 passes)

| Pump energy (J) | 105 | Pump beam diameter (cm, FWHM) | 14.0 |
|---|---------------|---|---------------------------|
| Pump fluence at crystal surfaces (J/cm ²) | 0.51 | Absorbed pump energy (%) | 96% |
| Seed pulse energy (J) | 18.8 | Seed beam diameter (cm, FWHM) | 12.8 |
| Output energy (J) | 62.4 | Extraction efficiency | 41.5% |
| Output beam diameter (cm FWHM) | 12.8 | Output beam peak fluence (J/cm ²) | 0.49 |
| EDP scheme | 65% 1st pass, | Max G _T | \sim 18 (before the 1st |
| | 35% 3rd pass | | pass) |
| $S_{pump} (\Delta E_{out} / \Delta E_{pump})$ | 0.53 | S_{seed} ($\Delta E_{out}/\Delta E_{seed}$) | 1.64 |

Performance level P1 (4 passes)

| Pump energy (J) | 197 | Pump beam diameter (cm, FWHM) | 14.0 |
|---|---------------|---|-----------------------|
| Pump fluence at crystal surfaces (J/cm ²) | 0.95 | Absorbed pump energy | 96% |
| Seed pulse energy (J) | 37.5 | Seed beam diameter (cm, FWHM) | 12.8 |
| Output energy (J) | 126.0 | Extraction efficiency | 44.9% |
| Output beam diameter (cm FWHM) | 13.0 | Output beam peak fluence (J/cm ²) | 1.08 |
| EDP scheme | 65% 1st pass, | Max G _T | \sim 20 (before the |
| | 35% 3rd pass | | 3rd pass) |
| S_{pump} ($\Delta E_{out}/\Delta E_{pump}$) | 0.54 | $S_{seed} (\Delta E_{out} / \Delta E_{seed})$ | 1.4 |







Input/output spectrum (AMP3, P1)



Output energy vs. number of passes (AMP3, P1, transmission / reflection schemes)



Input/output beam profile (AMP3, P1)



Output energy vs. pump pulse energy (AMP1, P0)









Water cooling of disk amplifiers: modelling physics

- Simulation software: COMSOL multiphysics (ver. 4.2 and 5.2)
- Finite Element Analysis approach
- Numerical solution of the Navier-Stokes equations for mass and energy transport
- Low Reynolds k-ε solution method
- Thermal coupling with boundary layer at the channel walls (heated Ti:Sa crystal)
- Time-averaged simulation (i.e. time-dependent turbulences not modelled)



Temperature of Ti:Sa surface at different inlet flow speed Water inlet temperature 15°C (288.15 K) Heat input 25 W/cm2, Channel heigth 5 mm Example:

- channel thickness 5 mm, flat channel walls
- inlet flow speed 6 m/sec,
- heat input 25 W/cm² (AMP3 at P1 performance level)
- heated length 160 mm (AMP3 pump beam \varnothing);
- temperature dependence of water properties
- water input temperature 15 °C
- mesh ~ 128000 elements



Effective film coefficient (heat exchange coefficient between water and heated wall for different flow speed and heat input levels



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THERMOMECHANICAL SIMULATIONS



Temperature distribution

Temperature distribution for AMP3 transmission disk (left, 1.6 cm thickness) and AMP3 reflection disk (right 1.3 cm thickness) at P1 pump level

Deformation distribution

Axial displacement distribution (mm) for AMP3 transmission disk (left, 1.6 cm thickness) and AMP3 reflection disk (right 0.8 cm thickness) at P1 pump level

Optical path difference (OPD)

OPD in microns resulting from thermal expansion and thermooptic effect. Parabolic fit and higher order aberrations also shown. Left: AMP3 transmission disk; right AMP3 reflection disk at P1 pump level





PUMP SOURCES TECHNOLOGIES



DiPOLE 100 (STCF)



Cryogenically operated Yb:YAG, diode pumped 100J @1030 nm , 10 Hz demonstrated Energy stabilty 1% RMS (few hours of operation) 60 J SHG @ 515 nm, 10 Hz expected

Possible upgrades include:

- IR Output energy 150 J
- SHG output > 100 J
- PRF 100 Hz @ 10 J

P-60 technology (Amplitude)



Nd:YAG Disk Amplifier Heads (DAH), liquid cooled. Current design: flashlamp pumping Scalable design (n. of DAH units): P20, P30...

Design specificatons (6 DAH): ~80 J @ 1064 nm, 10 Hz 60 J @ 532 nm, 10 Hz

Possible developments

- Diode pumping
- 50 Hz rep rate







P0 performance level

Issue: P0 operation regime has a pulse repetition rate of 20 Hz. The two available pump sources have a repetition rate of only 10 Hz.

To circumvent this problem (until higher rep rate devices are developed) we considered to use two (or two sets) of pump sources and shot them interleaved, so that repetition rate of the pump pulses arriving to the amplifiers id effectively doubled.

Issue: Pump energies higher than about 60 J (as needed by the AMP3 module) require more than a single pump source.

This calls for specific arrangements to multiplex the input from several pump units to the amplification crystals.

P1 performance level

Issue: P1 operation regime considers a pulse repetition rate of 100 Hz, along with higher energies than P0. Currently no solutions for pump sources are available to meet these requirements.
 Speculatively, we have considered the availability of a system similar to Amplitude P60 but operating at 50 Hz (conversion to diode laser pumping of the flashlamp pumped P60) with the same output energy of 60 J/pulse in the green.

Again, reaching 100 Hz requires the time interleaving of a pair of twin sources. This analysis did not include the DiPOLE 100 system, as no developments are currently planned toward a high energy, high rep rate system.





Diode laser developments



FBH brilliant high duty cycle pump: small-series prototype



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- Requirements on energy, pulse duration, stability etc set by the LPA working point
- Design based on CPA in Ti:Sapphire, dictated by requirements vs. time scale
- Thermal management issues addressed by means of liquid cooling
- Main developments required:
- Prototyping of Ti:Sa amplifiers: fluid cooling (choice between reflection/transmission amplifier): possibly by means of pilot devices
- Addressing 100 Hz pump lasers developments
- Thermal management of compressor gratings
- Stability (pointing & more) and active control
- Driver pulse temporal shaping and synchronization
- Construction
- Integration Issues









The end

