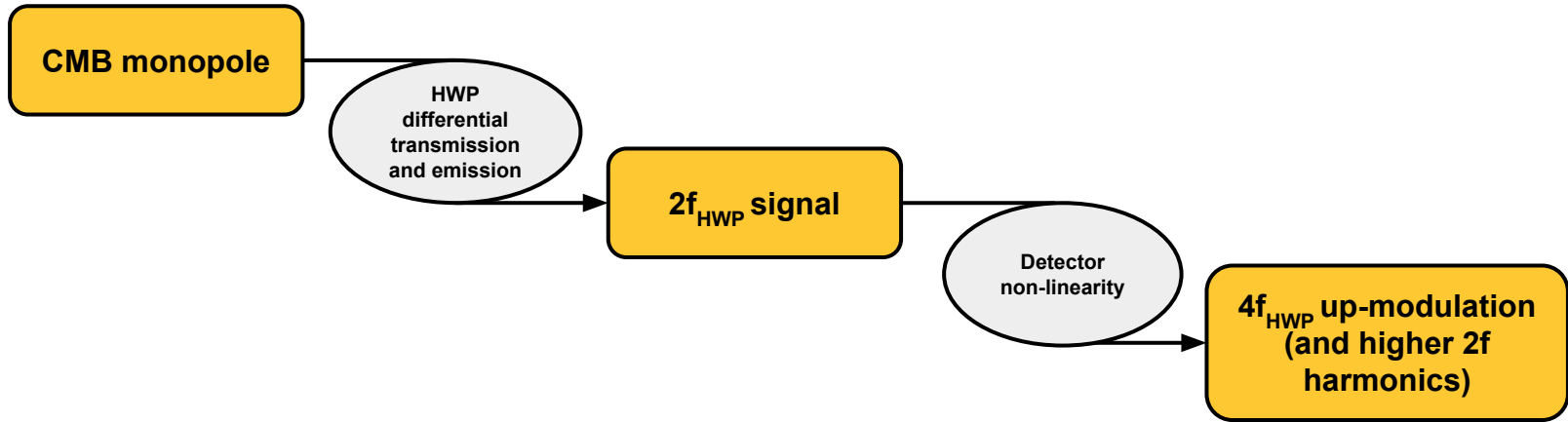


# **HWP differential optical load and non-linearity**

23/05/2023 Workshop LiteBIRD-Italia 2023 @ INFN-LNF

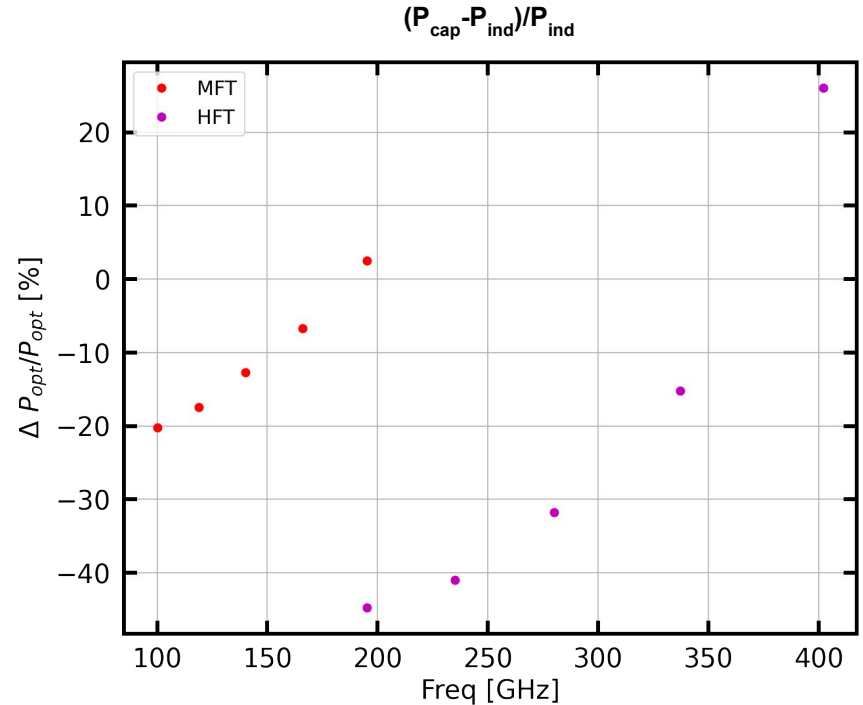
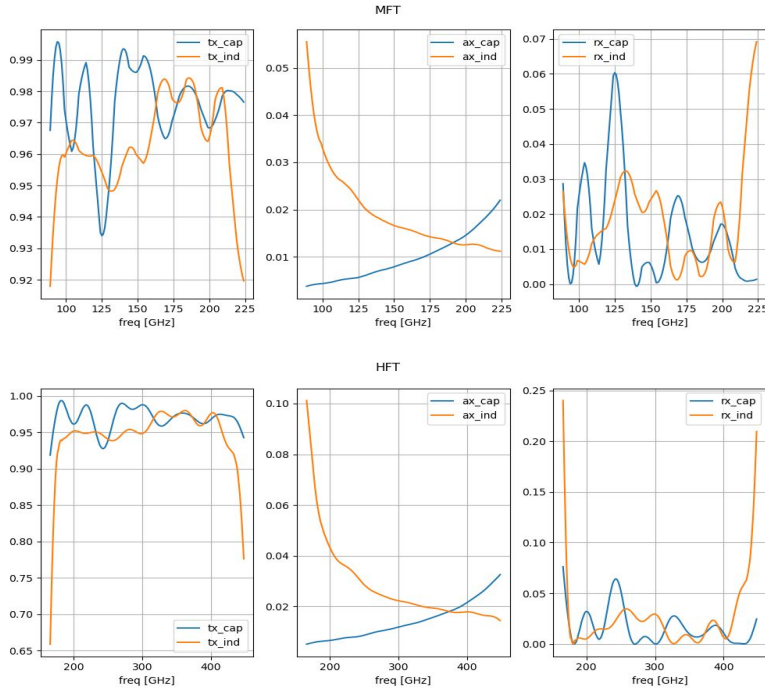
Silvia Micheli



- We calculate how much Popt variation is expected in each band due to HWP differential emissivity and transmission
- We simulate how the TES non-linearity up-modulates the 2f<sub>HWP</sub> signal resulting in a  $l \rightarrow 4f_{\text{HWP}}$  leakage
- We implement a simplified model to measure and remove the non-linearity

- Nominal power values → worse value in each band for a conservative estimation (inductive axis, except for 195 GHz and 402 GHz bands)
- Band-averaged estimation
- MHFT optical power variation wrt nominal values, due to HWP **differential transmittance and emissivity**

from Giampaolo Pisano data



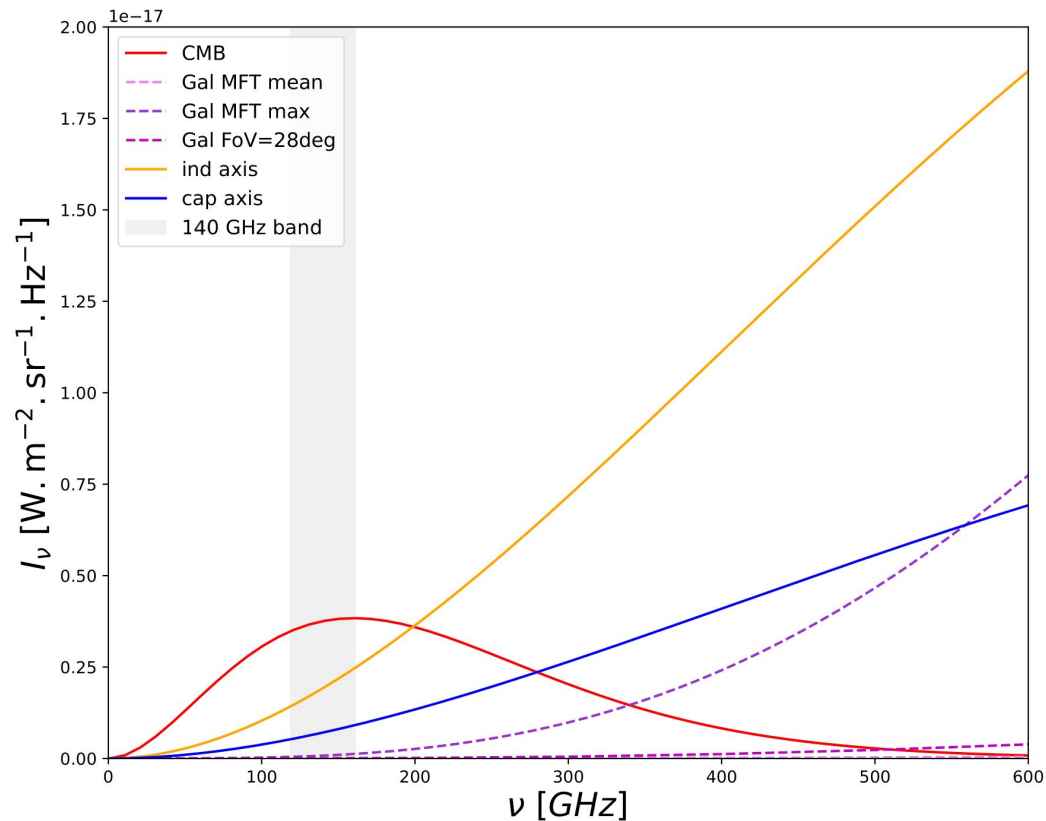
# Example: HWP differential emission @140 GHz compared with galactic emission

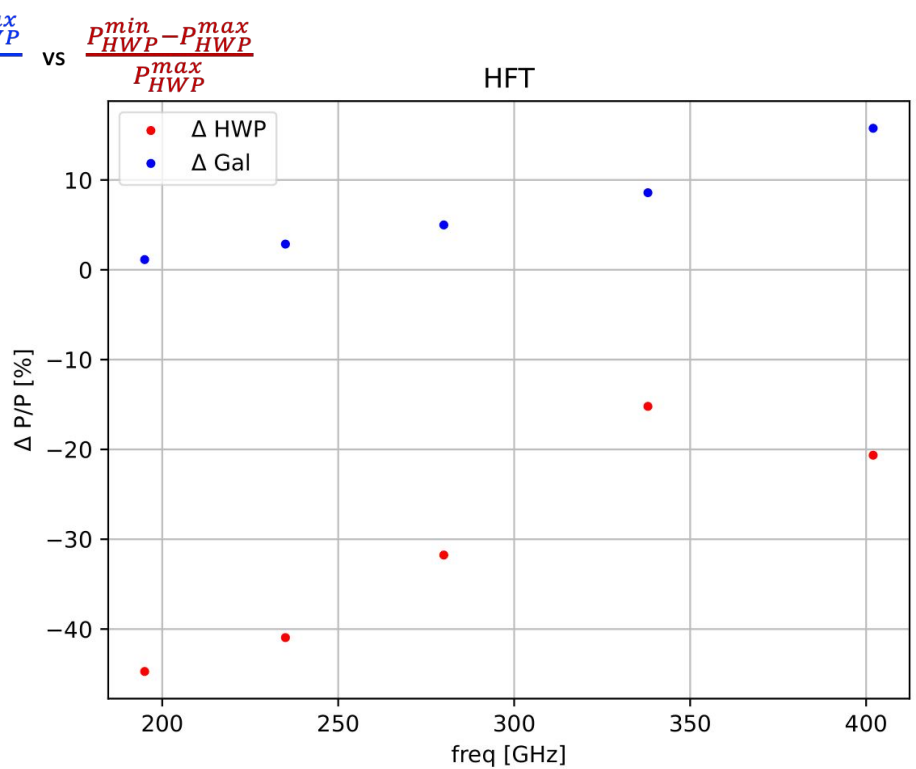
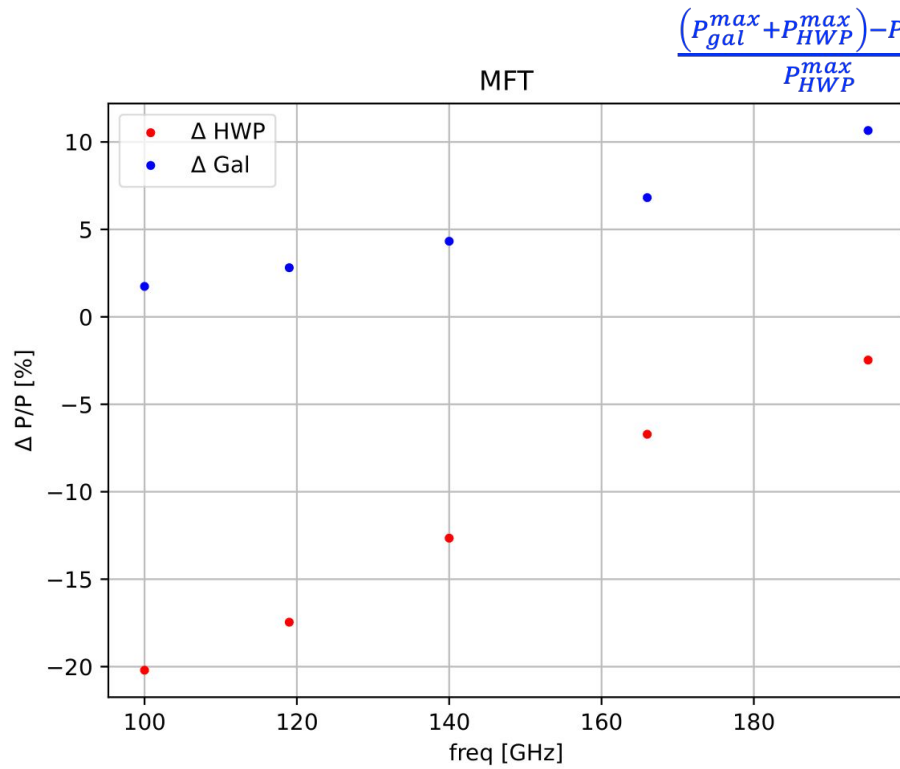
$$I_{\nu}^{ind} = BB(\nu, 20K) \cdot \epsilon_{140}^{ind}$$

$$I_{\nu}^{cap} = BB(\nu, 20K) \cdot \epsilon_{140}^{cap}$$

$$\epsilon_{140}^{cap} = 0.007$$

$$\epsilon_{140}^{ind} = 0.019$$





- Differential emissivity causes a loss of power wrt the nominal power in each band
- In most bands  $\% \Delta P_{HWP} > \% \Delta P_{GAL}$
- **Signal from the sky is modulated by a  $2f_{HWP}$  signal with amplitude  $\Delta P_{HWP}$**

## Input signal simulation

nside = 1024 ; smoothing fwhm=0.5 deg, 24 h obs

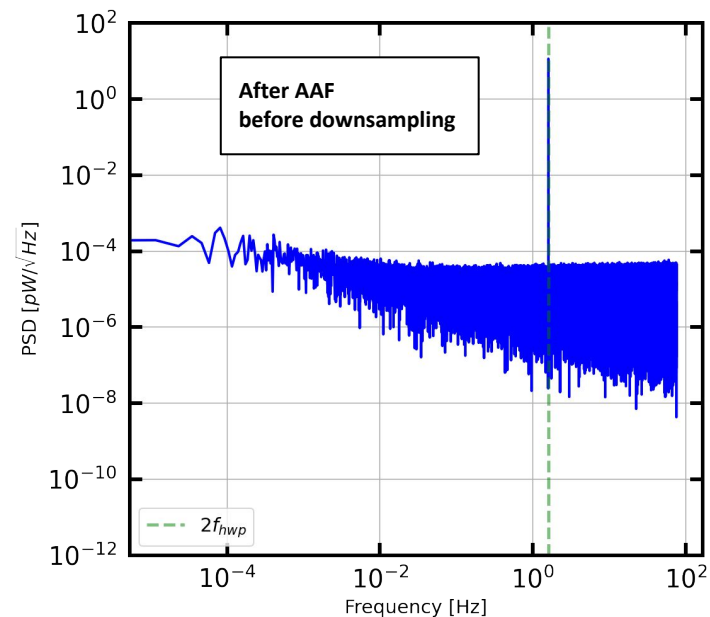
CMBpol @140 GHz +  $2f_{\text{HWP}}$  + 1/f noise; no fg

Anti-aliasing filter has been applied:

sample\_rate = 152 Hz

duration = 3600\*24 s

q = 8 (downsampling factor to be applied later)



## Input signal simulation

nside = 1024 ; smoothing fwhm=0.5 deg, 24 h obs

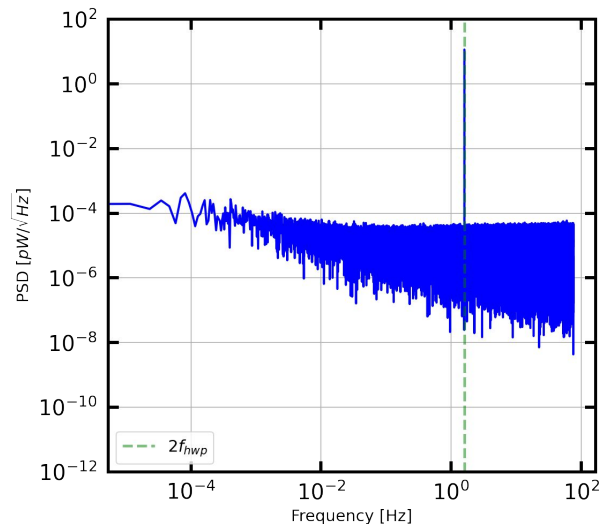
CMBpol @140 GHz +  $2f_{\text{HWP}}$  + 1/f noise; no fg

Anti-aliasing filter has been applied:

sample\_rate = 152 Hz

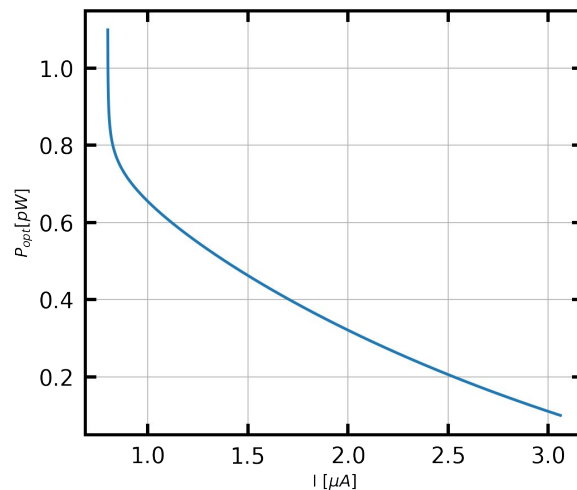
duration = 3600\*24 s

q = 8 (downsampling factor to be applied later)



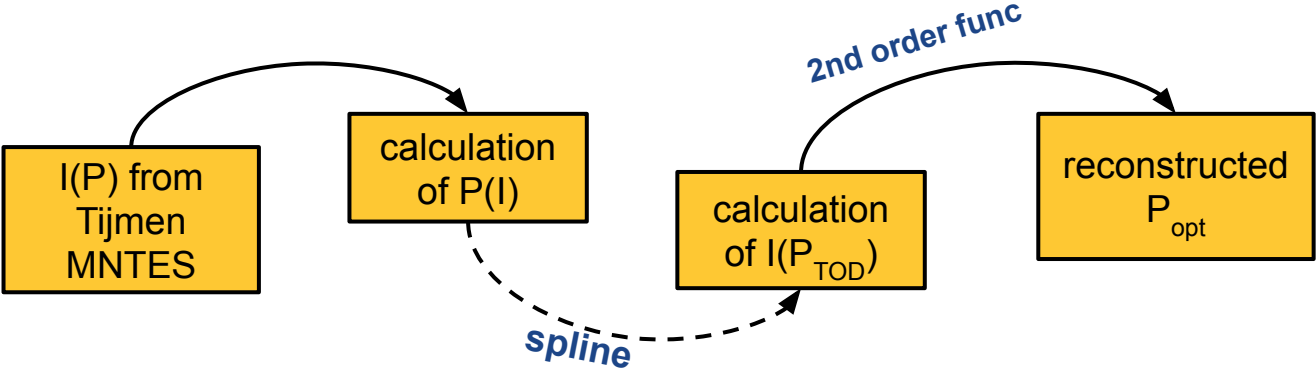
## Modeling I(P) from Tijmen code (MNTES)

```
'Voltage bias': 8e-07,  
'T_c': 0.18,  
'transition_width': 0.002,  
'R_normal': 1.0,  
'T_bath': 0.1,  
'z_series': (0.1+0j),  
'n_index': 3.6,  
'tau_intrinsic': 0.033,  
'V_bias': 8e-07}
```



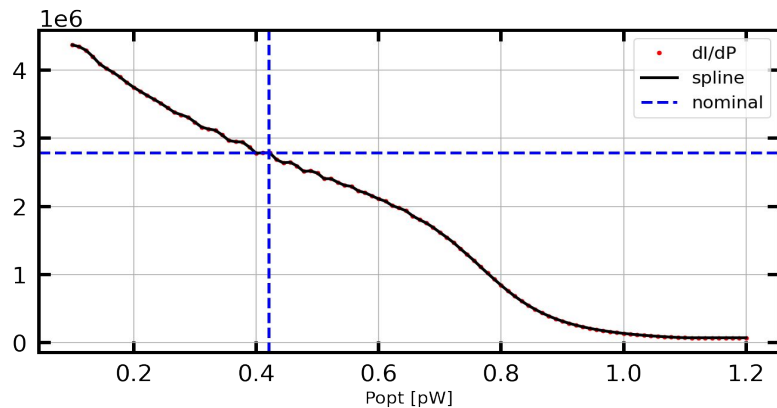
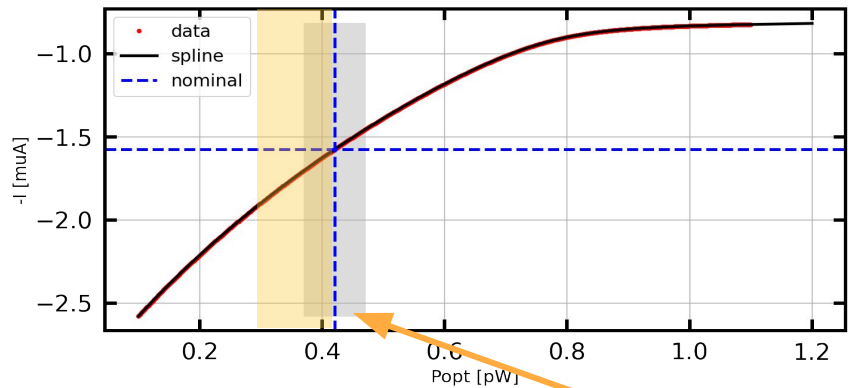
# Scheme of the implementation

Simulations: TOAST/litebird\_sim



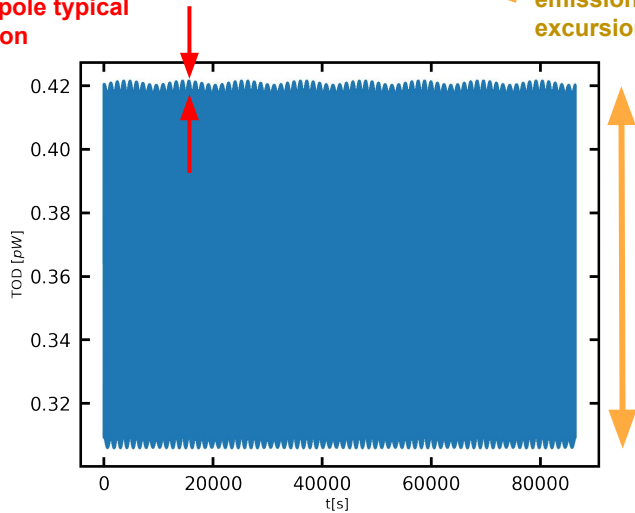


# (1) - Modeling I(P) from Tijmen code (MNTES)

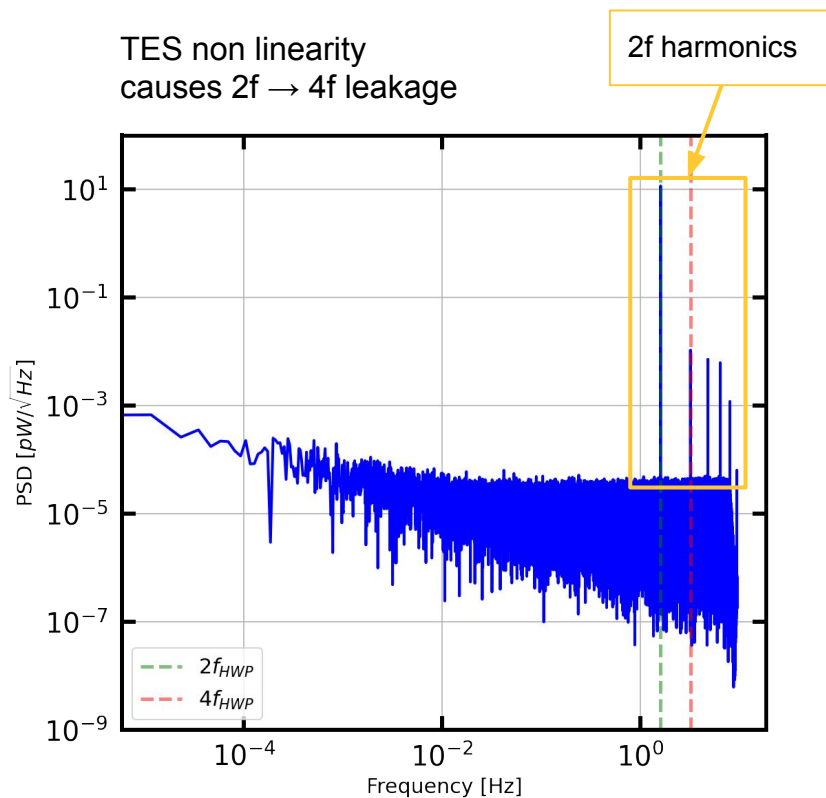
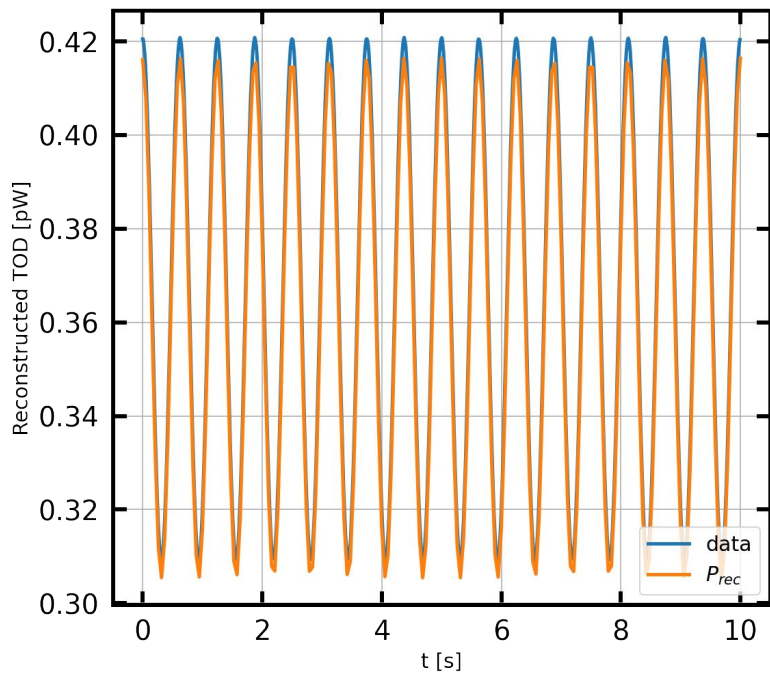


**CMB dipole typical excursion**

**HWP differential emission typical excursion**

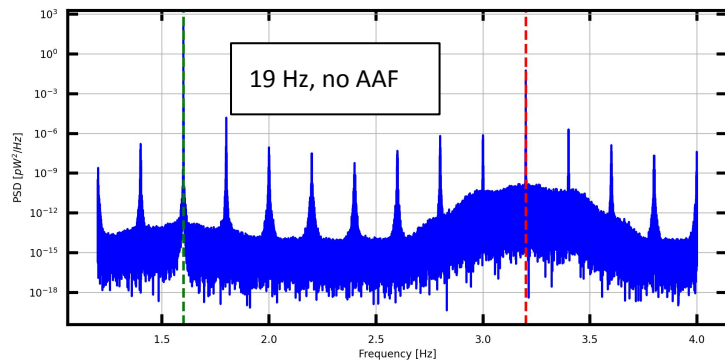
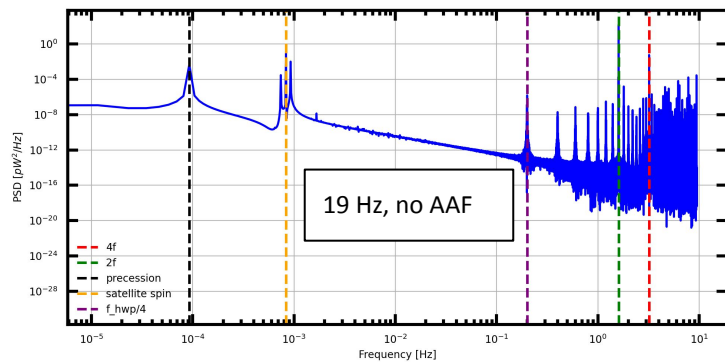


## (2) - $I(P)$ is calculated in the $P$ range using (1) spline



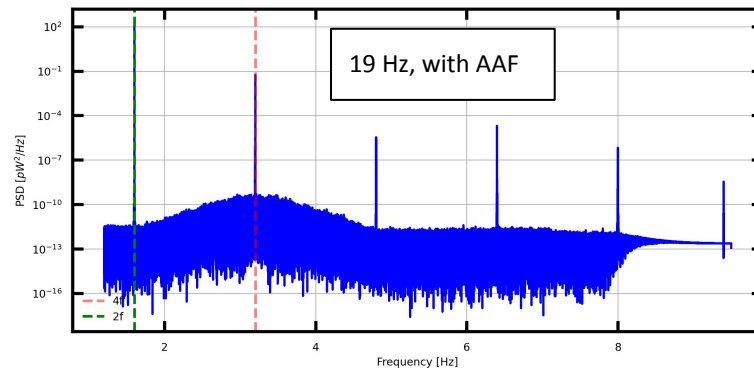
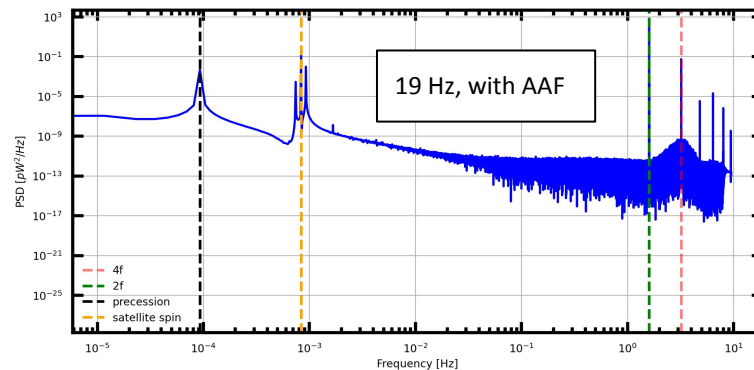
# IMPORTANT NOTE FOR SIMULATIONS

If we simulate at 19 Hz we see a lot of aliased signal!

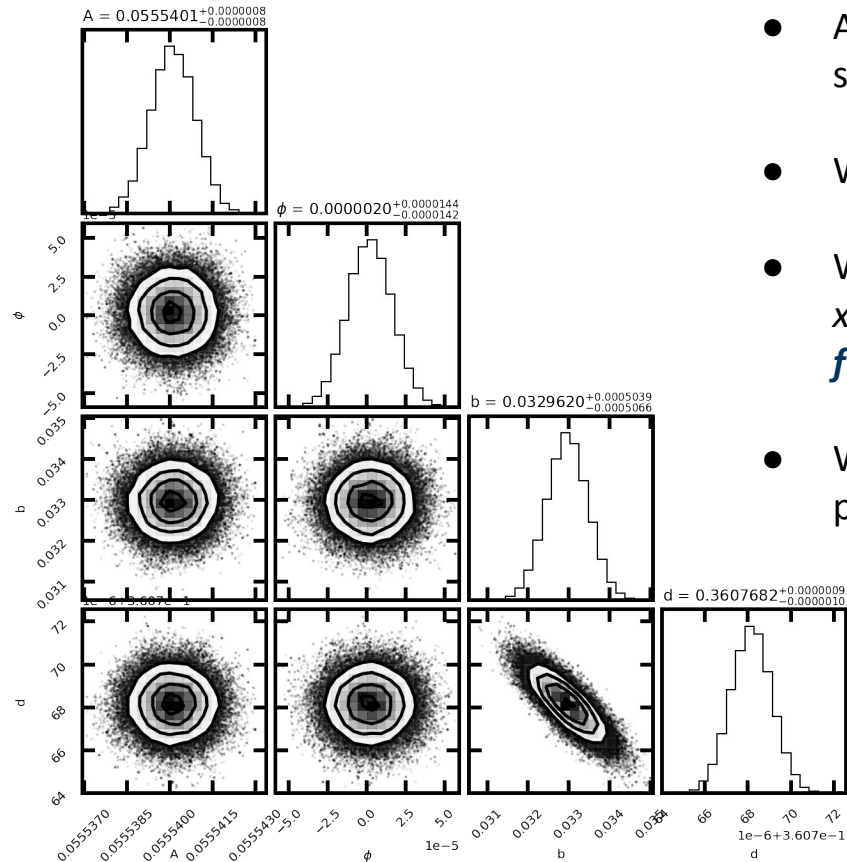


Correct procedure (as in the on-board computer):

- simulation at 152 Hz ( $20\text{MHz}/2^{17}$ )
- anti-aliasing filter
- downsampling by a factor 8



# Fitting NL parameters



- At this step we did not include the dipole in the simulation to simplify the analysis
- We simulate a 24 h observation
- We parametrize the HWP signal + NL through 4 parameters as:  
 $x = A \cos(2\omega t + \phi)$   
 $f = x + bx^2 + d$  (quadratic approximation of the NL)
- We run a MCMC to find the best fit of the reconstructed power

$\sigma_A = 8 \cdot 10^{-7} \text{ pW}$   
 $\sigma_\phi = 0.05 \text{ arcmin}$   
 $\sigma_b = 5 \cdot 10^{-4} \text{ pW}^{-1}$   
 $\sigma_d = 9 \cdot 10^{-7} \text{ pW}$

very low uncertainty !

# Correction of the NL:

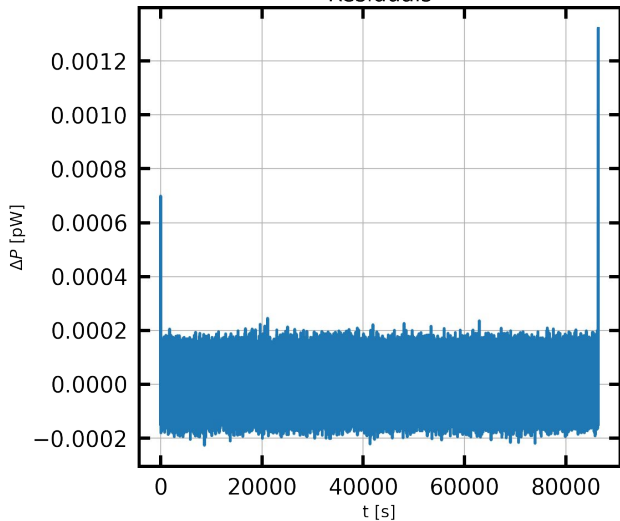
## (3) - P is reconstructed using a quadratic model function

$$x_{rec} = \frac{-1 + \sqrt{1 - 4\tilde{b}(\tilde{d} - P_{rec})}}{2\tilde{b}}$$

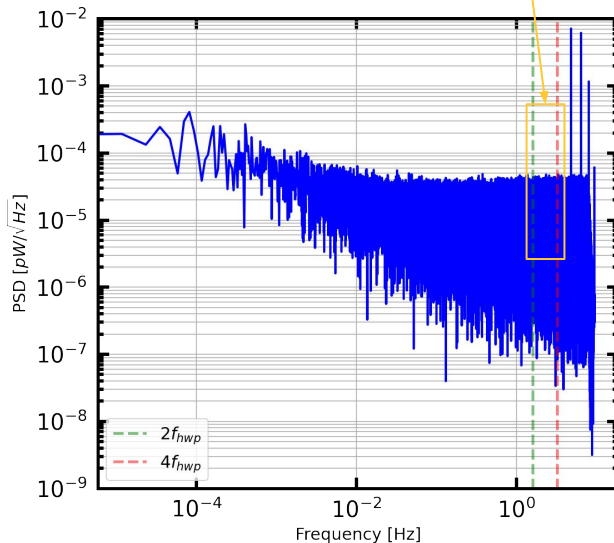
$$\tilde{x} = \tilde{A} \cos(2\omega t + \tilde{\phi})$$

$$\tilde{x} - x_{rec}$$

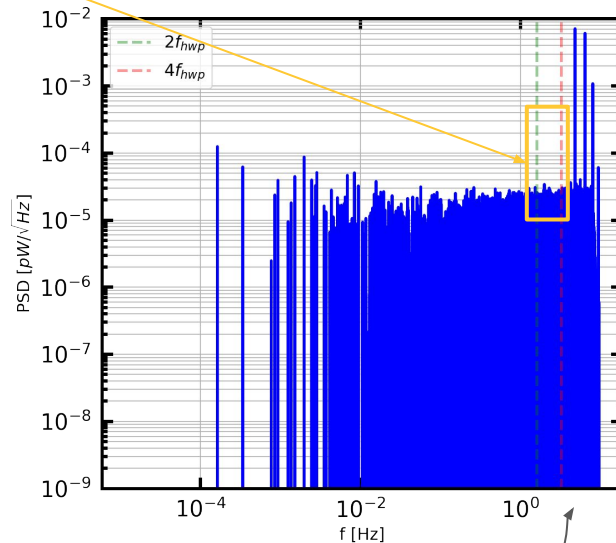
Residuals



2f and 4f harmonics  
have been removed



1/f noise spectrum  
has been subtracted

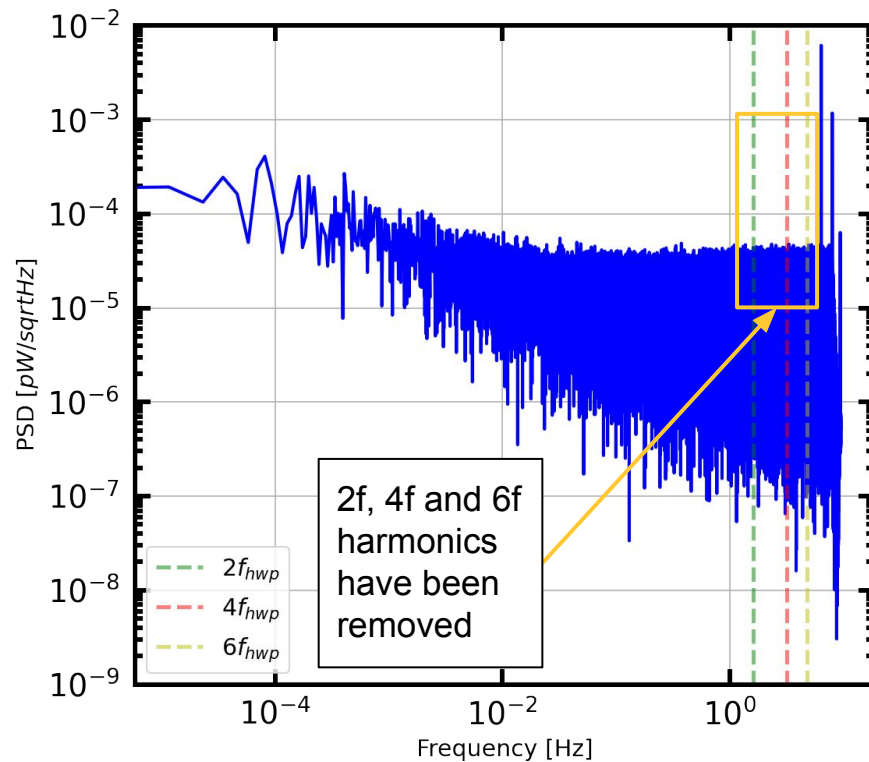
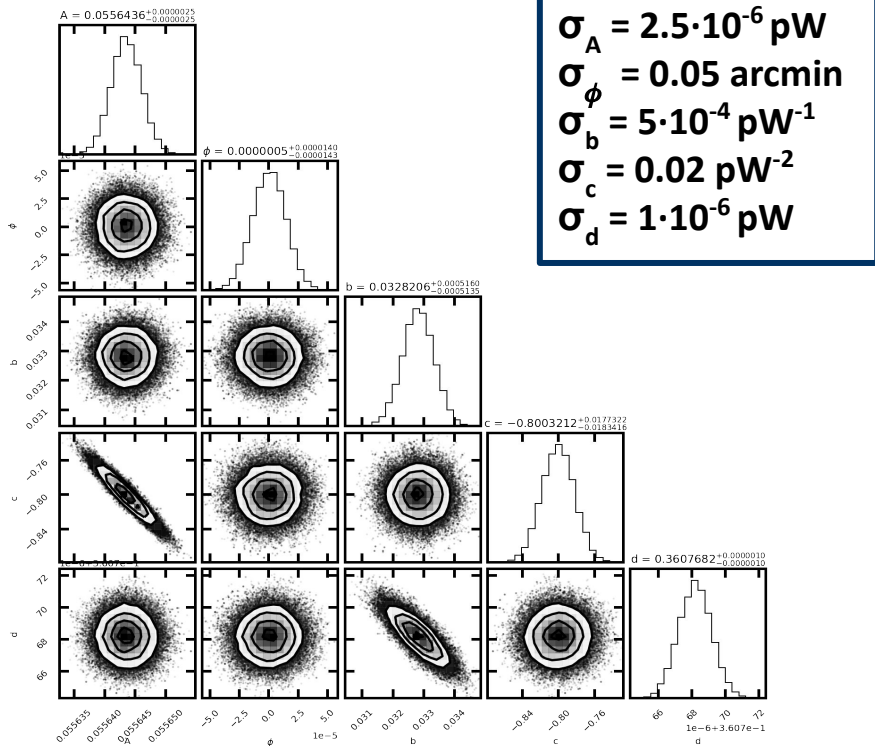


in principle a 3rd order model  
function should remove the 6f  
harmonic peak, and so on

In fact, if we apply the same procedure with a **third order model function** we eventually obtain:

$$x = A \cos(2\omega t + \phi)$$

$$f = x + bx^2 + cx^3 + d$$

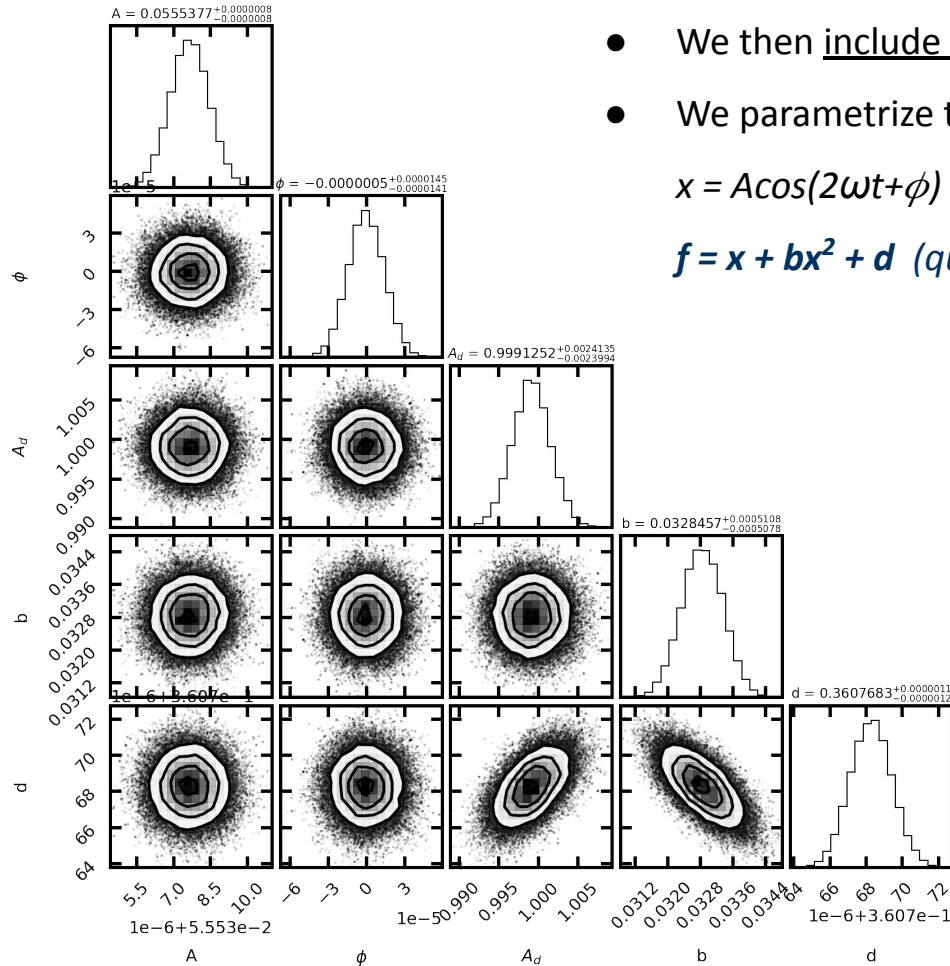


# Fitting NL parameters with the dipole

- We then include the dipole in the simulation
- We parametrize the HWP signal + dipole + NL through 5 parameters as:

$$x = A \cos(2\omega t + \phi) + A_d \text{dip}(t)$$

$$f = x + bx^2 + d \quad (\text{quadratic approximation of the NL})$$



$$\sigma_A = 8 \cdot 10^{-7} \text{ pW}$$

$$\sigma_\phi = 0.05 \text{ arcmin}$$

$$\sigma_{A_d} = 2 \cdot 10^{-3}$$

$$\sigma_b = 5 \cdot 10^{-4} \text{ pW}^{-1}$$

$$\sigma_d = 9 \cdot 10^{-7} \text{ pW}$$

# Summary

- We estimate the power variation due to HWP differential emissivity and transmission (up to 44%)
- We include the  $2f_{\text{HWP}}$  signal in the simulated input signal
- We apply the Tijmen model for TES non-linearity (MNTES) to this total signal
- We fit a quadratic approximation of the MNTES on the  $2f_{\text{HWP}}$  signal
  - to be assessed if the procedure is affected by other  $4f_{\text{HWP}}$  effects
  - $\sigma_{\phi} = 0.05$  arcmin
- We correct the  $I \rightarrow 4f_{\text{HWP}}$  leakage due to detector non-linearity
  - $4f_{\text{HWP}}$  residual < white noise level
- On going: maps in presence of detector non-linearity