

## Ferrites analysis for the AC-Dipole magnet

Corrado Comino<br>Summer Internship Final Presentation<br>$$
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## Mu2e Experiment

The first part of mu2e experiment needs a low noise pulsed proton beam: AC - Dipole magnet is made to satisfy this requirement.

AC-Dipole




## AC-Dipole magnet

- AC- Dipole magnet is made by a row of bricks of ferrite (ferromagnetic material)
- Coil: single turn of copper tube
- Periodic magnetic field induced by the current through the tube
- AC-Dipole magnet steers the beam periodically to a
 collimator (a small opening)


## AC-Dipole magnet



Cross section


Top view

## Magnetic Permeability

The magnetic permeability is the measure of the ability of a material to support the formation of a magnetic field within itself.

$$
\boldsymbol{B}=\mu \boldsymbol{H}
$$

While at low frequencies this is a linear relationship, at high frequencies there is a phase delay between $B$ and $H$. Writing as a phasors:

$$
\boldsymbol{B}=B_{0} e^{j \omega t} \quad \boldsymbol{H}=H_{0} e^{j(\omega t-\delta)}
$$

The phase displacement is the responsible of losses. The imaginary part of the magnetic permeability takes account of this phenomenon:

$$
\mu=\mu^{\prime}-\mathrm{j} \mu^{\prime \prime}
$$

## CMD10

- CMD10: high resistivity and low losses ferrite
- Different batches have different behaviour of ferrites
- Factory data don't fit the measures (fornitors use a small ring to evaluate $\mu$ )
- $\mu \propto B, f$

CMD10 has the highest saturation flux density of our nickel-zinc ferrites, along with medium permeability and high resistivity. Its' formulation also exhibits a high Curie temperature, permitting continuous operation at elevated temperatures. It is ideal for broadband RF and transmission line transformers, solid state amplifier power splitters, pulsed power, and kicker magnets operating in or out of vacuum up to $200^{\circ} \mathrm{C}$

Typical Properties
Initial Permeability vs. Temperature

| Initial Permeability | 625 |
| :--- | :--- |
| Maximum Permeability | 3000 |
| Saturation Flux Density | 4300 Gauss |
| Remanent Flux Density | 2900 Gauss |
| Coercive Force | 0.36 Oersted |
| Curie Temperature | $250^{\circ} \mathrm{C}$ |
| dc Volume Resistivity | $10^{10}$ ohm-cm |
| Bulk Density | $5.20 \mathrm{~g} / \mathrm{cc}$ |



Unless otherwise specified, all tests were performed at $10 \mathrm{KHz}, 22^{\circ} \mathrm{C}$
Bs tested at $1 \mathrm{KHz}, 20$ Oersted $\cdot \mathrm{Br}$, Hc at $1 \mathrm{KHz}, 5$ Oersted

Permeability vs. Flux Density



Complex Permeability vs. Frequency


## Ferrites Parameters



Mostly interested in losses

- Low excitation quality factor $Q$

$$
\mathrm{Q}=\frac{\text { stored energy }}{\text { energy loss }}
$$

- Quality Factor at 1000

Gauss

## Work steps

- Measure ferrites
- Model the magnetic permeability $\mu$ of bricks
- Define acceptability
boundaries for brick's power loss and magnetic field



## Measurement Circuit

- Dipole Mode vs Toroidal Mode
- Toroidal Mode (no gap
 measure) to obtain measures to model
- Dipole Mode to verify the model $\mu$


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## Measurement Circuit

- Capacitors to obtain resonance with ferrites
- Measures taken in resonant condition
- $I_{\text {meas }}$ current inducing the magnetic field
- $\mathrm{V}_{\text {meas }}$ voltage at the ferrite terminals
- $\mathrm{l}_{\text {loss }}$ current producing power loss



## Measures



## Measures

|  | Measurement on the 1.2 cm gap ferrite CMD10 e 5005 ,Toroidal Mode, 8 AWG wire, Two Turn. September 5, 2019. |  |  |  |  | (Vc*Il/2)/loss |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | meas | 1/(2*freq) | meas | $\mathrm{Vc} / 2$ | meas |  |  |  |
|  | freq | sec | Vc | OneTurn V | Il | Q | L (H) |  |
|  |  |  |  |  |  |  | (2*pi*freq* $I$ |  |
| CMD10 | [ Hz ] |  | [pk-volts] | [pk-volts] | [pk-amps] | [pk-volts] |  |  |
| "50V" | $2.532 \mathrm{E}+05$ | $1.974 \mathrm{E}-06$ | 24.2 | 12.1 | 0.70100 | 45.56 | $2.166 \mathrm{E}-05$ |  |
| "100V" | $2.494 \mathrm{E}+05$ | $2.005 \mathrm{E}-06$ | 49.9 | 25.0 | 1.44000 | 28.86 | $2.213 \mathrm{E}-05$ |  |
| "200V" | $2.469 \mathrm{E}+05$ | $2.025 \mathrm{E}-06$ | 101.0 | 50.5 | 2.80000 | 20.26 | $2.326 \mathrm{E}-05$ |  |
| "500V" | $2.533 \mathrm{E}+05$ | $1.974 \mathrm{E}-06$ | 251.0 | 125.5 | 5.89000 | 8.69 | $2.679 \mathrm{E}-05$ |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| "50V" | $2.433 \mathrm{E}+05$ | $2.055 \mathrm{E}-06$ | 25.0 | 12.5 | 0.26500 | 14.35 | $6.163 \mathrm{E}-05$ |  |
| "100V" | $2.477 \mathrm{E}+05$ | $2.019 \mathrm{E}-06$ | 49.6 | 24.8 | 0.48950 | 9.45 | $6.514 \mathrm{E}-05$ |  |
| "200V" | $2.537 \mathrm{E}+05$ | $1.971 \mathrm{E}-06$ | 99.0 | 49.5 | 0.89500 | 6.82 | $6.942 \mathrm{E}-05$ |  |
| "300V" | $2.488 \mathrm{E}+05$ | $2.009 \mathrm{E}-06$ | 152.0 | 76.0 | 1.57000 | 6.41 | $6.196 \mathrm{E}-05$ |  |
| "500V" | $2.528 \mathrm{E}+05$ | $1.978 \mathrm{E}-06$ | 253.0 | 126.5 | 2.37000 | 4.34 | $6.725 \mathrm{E}-05$ |  |
|  |  |  |  |  |  |  |  |  |
|  | $\mathrm{Vc} / 1.571$ | meas | Vcav* (T/2)/N*area | $\left(\mathrm{Vc}\right.$ * $\mathrm{I}_{\text {- }}$ ) / 2 | Point-to-Point |  | B-Loop |  |
|  | V av | I R meas | delB | Loss | Loss | loss/m* $\mathrm{m}^{\star} \mathrm{m}$ | delb |  |
| CMD10 | [volts] | [pk amps] | [Gauss pk-pk] | [watts] | [watts] | [watts] | [Gauss_pk-pk] |  |
| "50V" | 15.374 | 0.025 | 30 | 0.3 | 0.18578341 | 71 | 30 |  |
| "100V" | 31.767 | 0.058 | 62 | 1.4 | 1.24471 | 477 | 62 |  |
| "200V" | 64.299 | 0.163 | 128 | 8.2 | 6.97767 | 2,676 | 128 |  |
| "500V" | 159.792 | 0.698 | 309 | 87.5 | 85.10816 | 32,638 | 309 |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| "50V" | 15.884 | 0.023 | 32 | 0.3 | 0.23043 | 88 | 32 |  |
| "100V" | 31.576 | 0.060 | 62 | 1.5 | 1.28470 | 493 | 62 |  |
| "200V" | 63.025 | 0.147 | 122 | 7.3 | 6.49149 | 2,489 | 122 |  |
| "300V" | 96.766 | 0.269 | 191 | 20.4 | 18.61279 | 7,138 | 191 |  |
| "500V" | 161.065 | 0.583 | 312 | 73.7 | 69.14820 | 26,518 | 312 |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  | Core Par | neters |  |  |  |  |
|  |  | N | core area | Path length | Core volume | Resonant |  |  |
|  |  | turns | [ $\mathrm{n}^{\star} \mathrm{m}$ ] | [m] | [ $\mathrm{m}^{\star} \mathrm{m}$ * m ] | Capacitance |  |  |
|  | " 1.2 cm " | 2 | $5.10 \mathrm{E}-03$ |  | 0.00261 |  |  |  |

## Model $\mu$



- COMSOL Multiphysics
- Design of ferrite bricks
- Simulation of magnetic field within the brick varying current through the coil


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## Model $\mu$

- Iterative method: modelling $\mu^{\prime}$ and $\mu^{\prime \prime}$ in order to fit measures
- Small measures steps to finely track the magnetic permeability behaviour
- Increasing $\mu^{\prime}$, magnetic flux increases
- Increasing $\mu^{\prime \prime}$, power loss increases

Slowly increasing B
Low excitation
( $B_{\max }$ 200G)
$\mu^{\prime}$ and $\mu^{\prime \prime}$ until 200G (almost constant)


Refine $\mu^{\prime}$ and $\mu^{\prime \prime}$ to
fit the measures

## Resulting Model

- The maximum magnetic field measured is 2700G (equal to 0.27 T )
- $\mu^{\prime}$ modelled with a linear function of B under $B_{\text {max }}$
- $\mu^{\prime \prime}$ modelled with a quadratic function of $B$ under $B_{\text {max }}$
- These models fit magnetic field and losses measures with less than $10 \%$ of error


CMD10_mu2_fun(B) (1)


## Using the model

- Fringe Effect evaluation
- Dipole Mode behaviour




# Thank you for your attention 

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