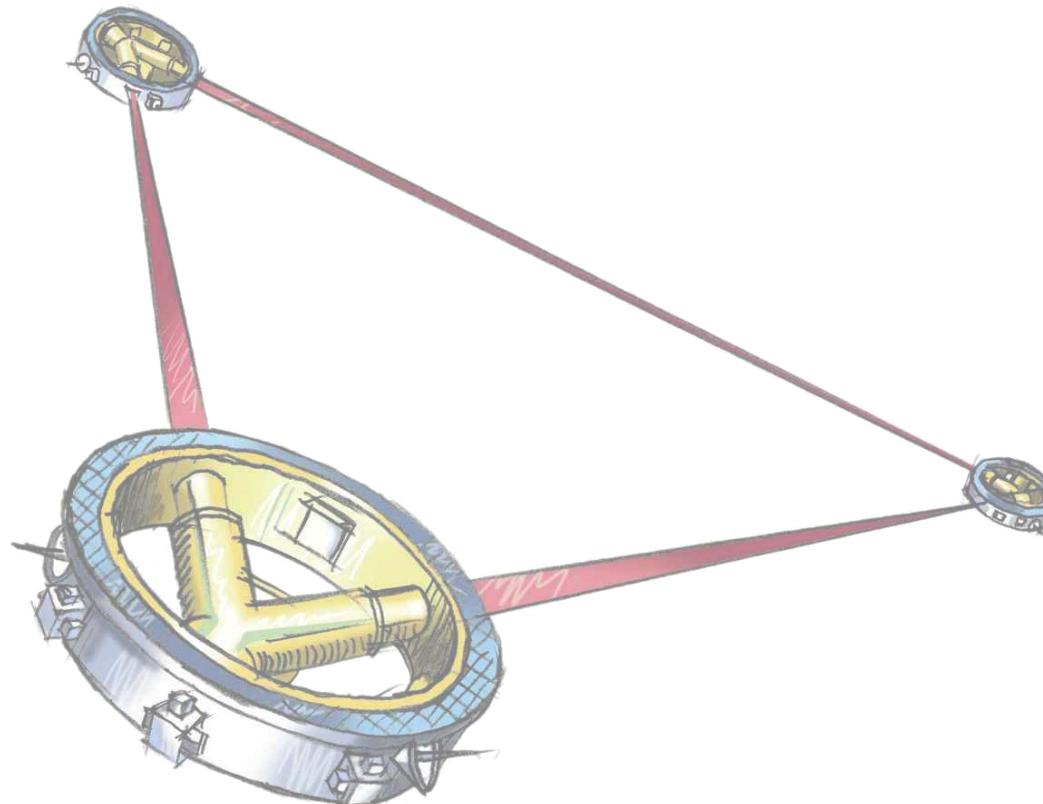


Laser systems for LISA and its precursor mission LISA Pathfinder

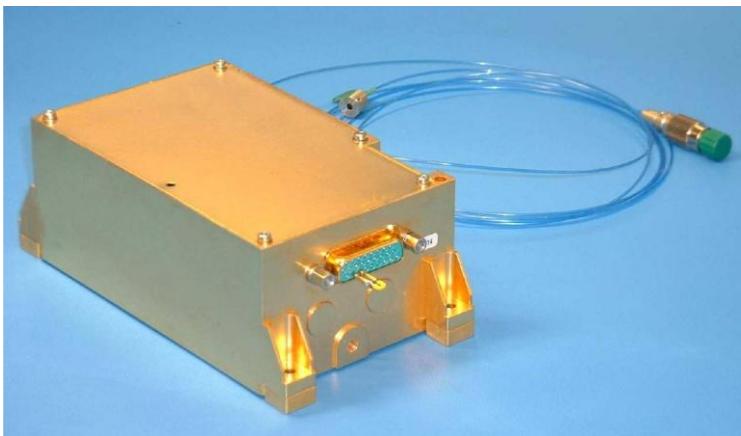
Michael Tröbs

Max-Planck-Institut für Gravitationsphysik und Universität Hannover

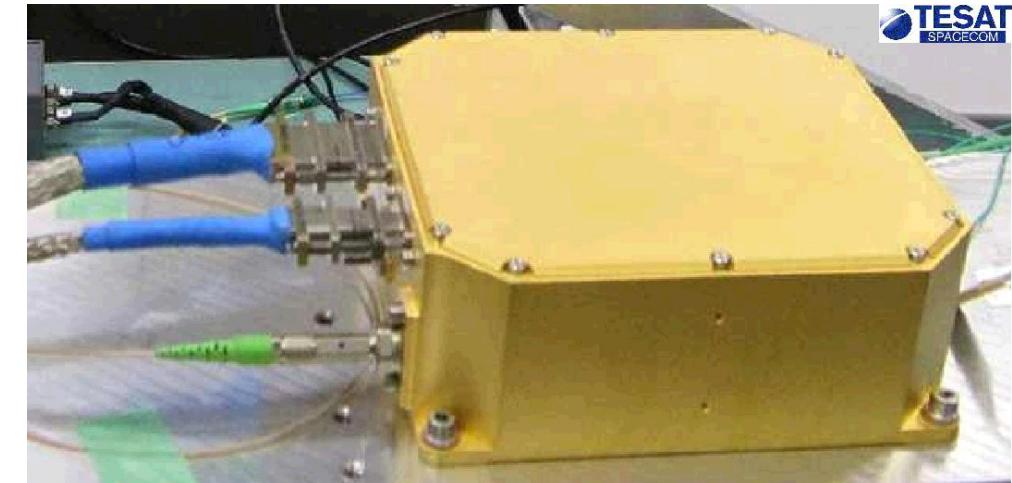


Lasers for LISA Pathfinder

breadboard model



flight model

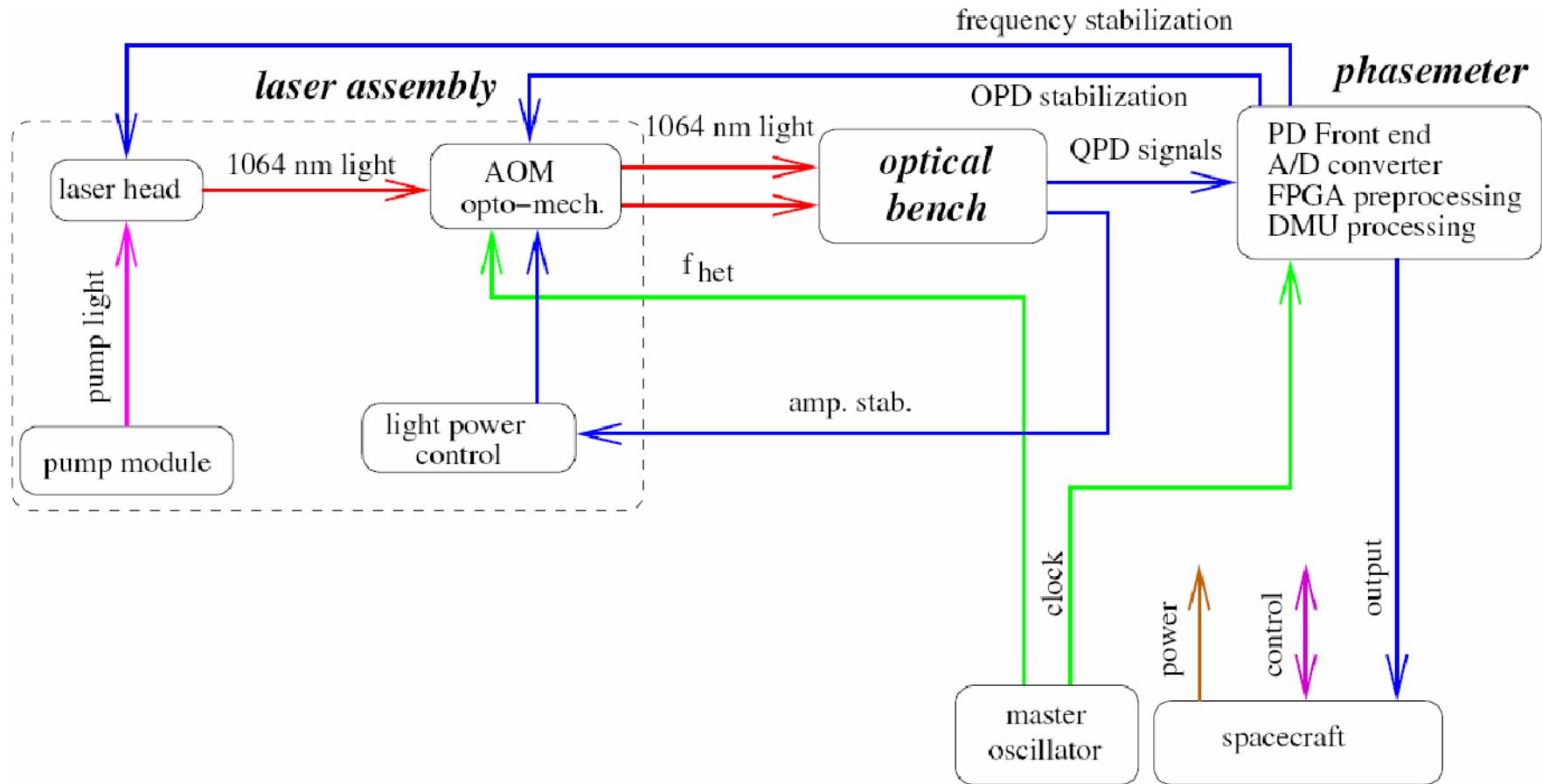


engineering model



- Lasers manufactured by Tesat Spacecom
- Flight model has space heritage already: TerraSar, NFire

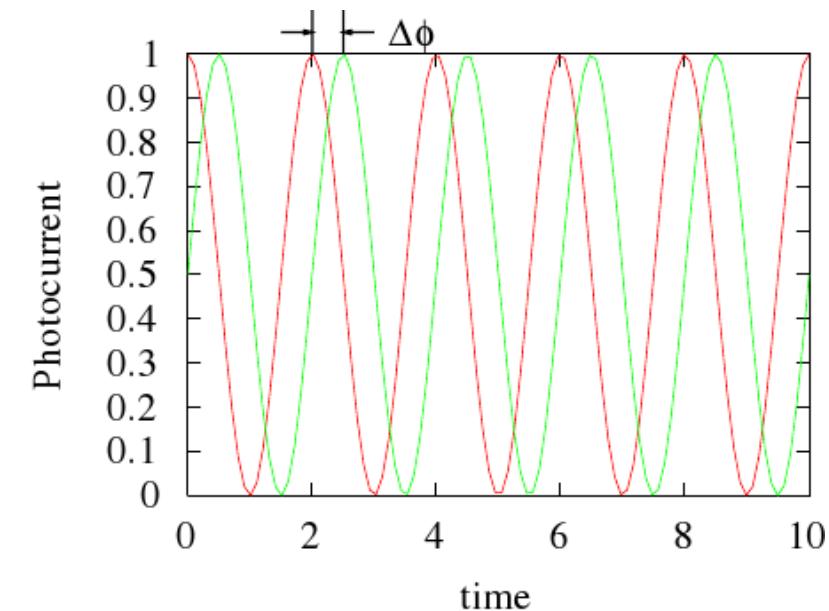
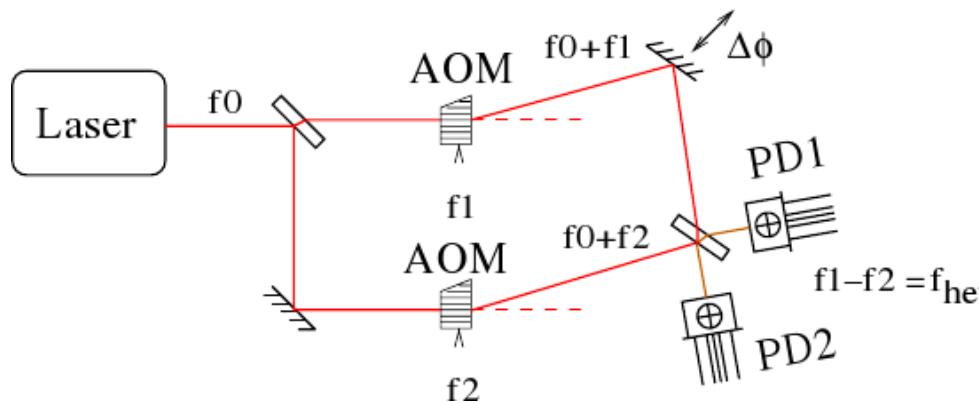
LISA Pathfinder optical metrology system



- Laser delivers light to laser modulator (LM)
- LM produces light at two frequencies to operate optical bench
- Frequency, power, optical pathlength difference stabilization active

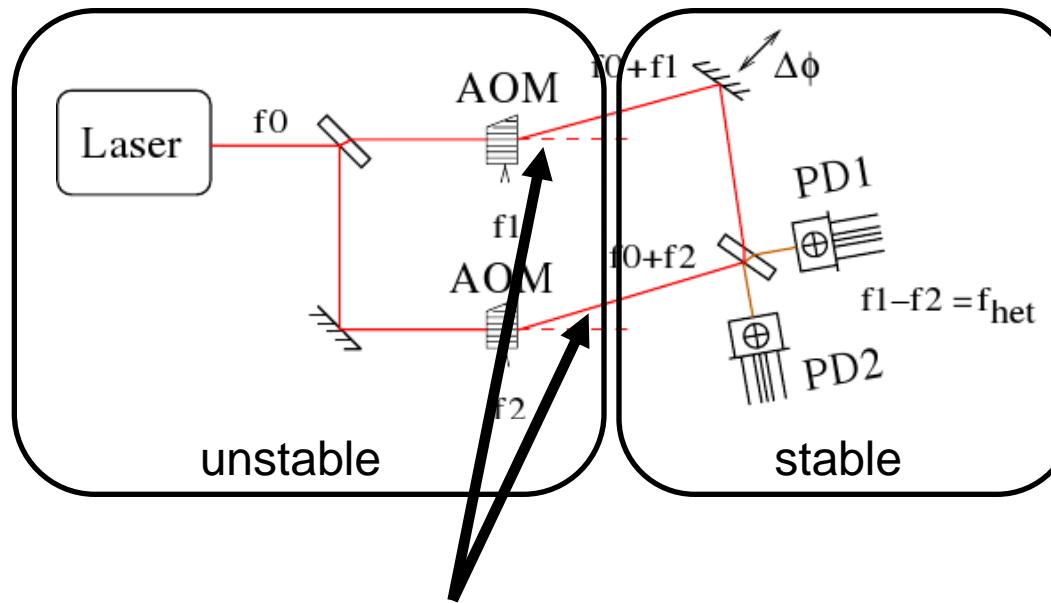
LISA Pathfinder interferometry concept

- Locking to dark fringe not possible due to large motion of test masses – no actuators available with pm accuracy
- Use heterodyne interferometer



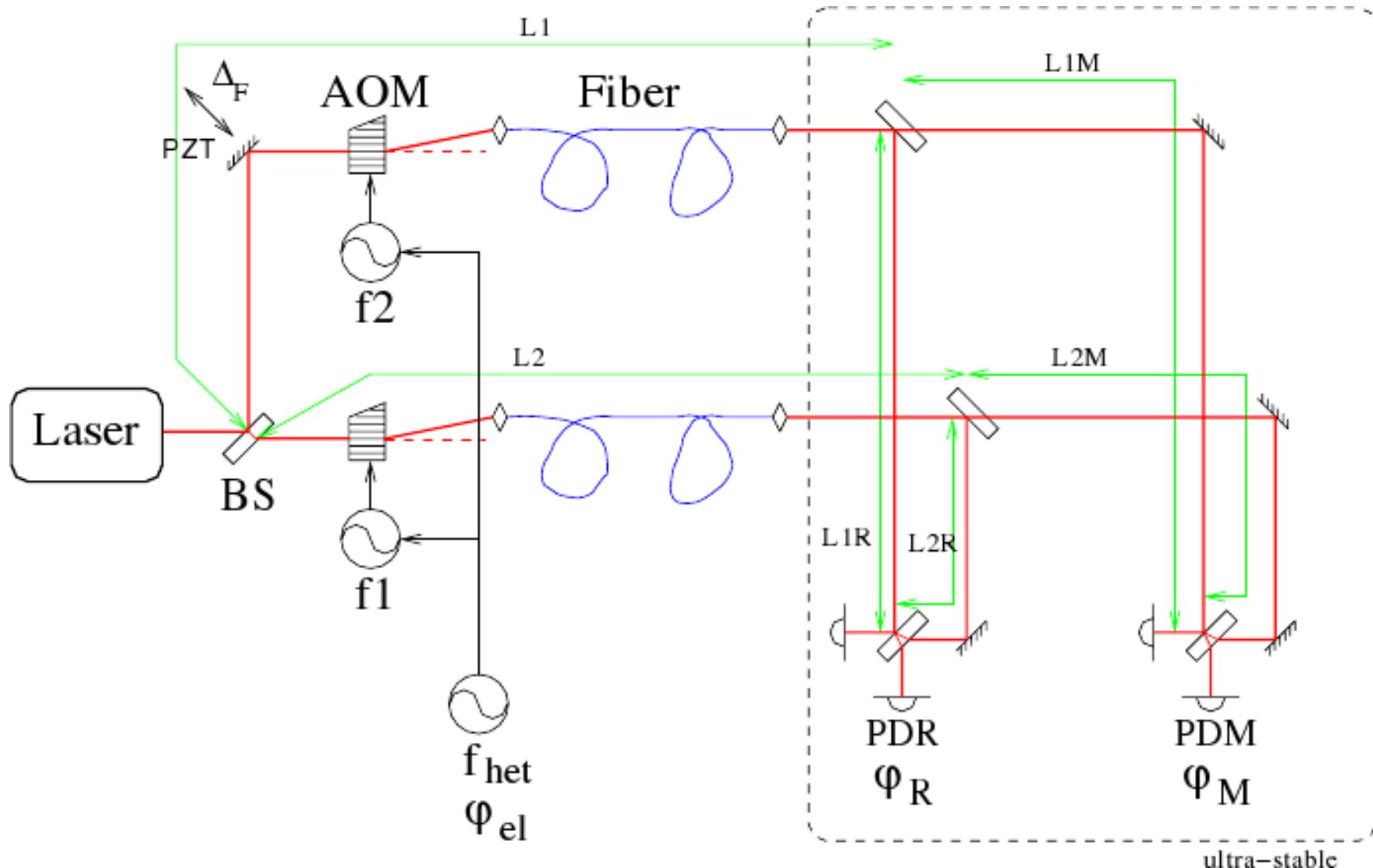
Heinzel et al. CQG vol. 20 pp. S153 (2003)

LISA Pathfinder interferometry concept



- Fibres used behind AOMs
 - as spatial mode cleaner
 - to separate AOMs from the optical bench and test masses
- reference interferometer required

LISA Pathfinder Interferometry concept



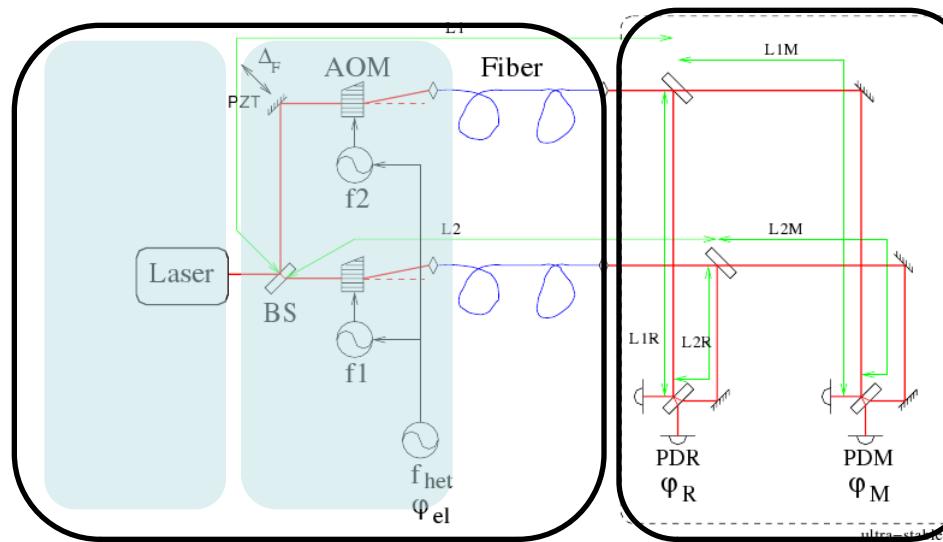
Wand et al. CQG vol. 23 pp. S159 (2006)

reference
interferometer

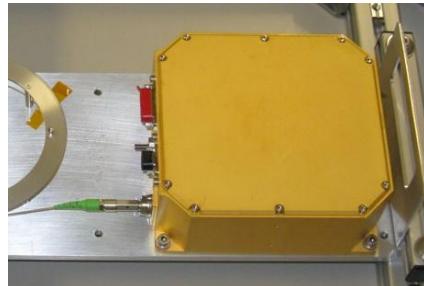
measurement
interferometer

LISA Pathfinder hardware implementation

unstable



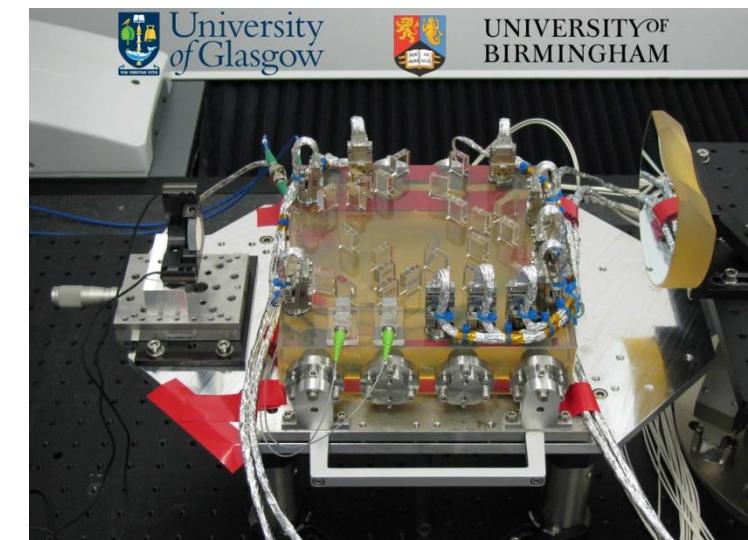
stable



Laser



Laser modulator



Optical bench

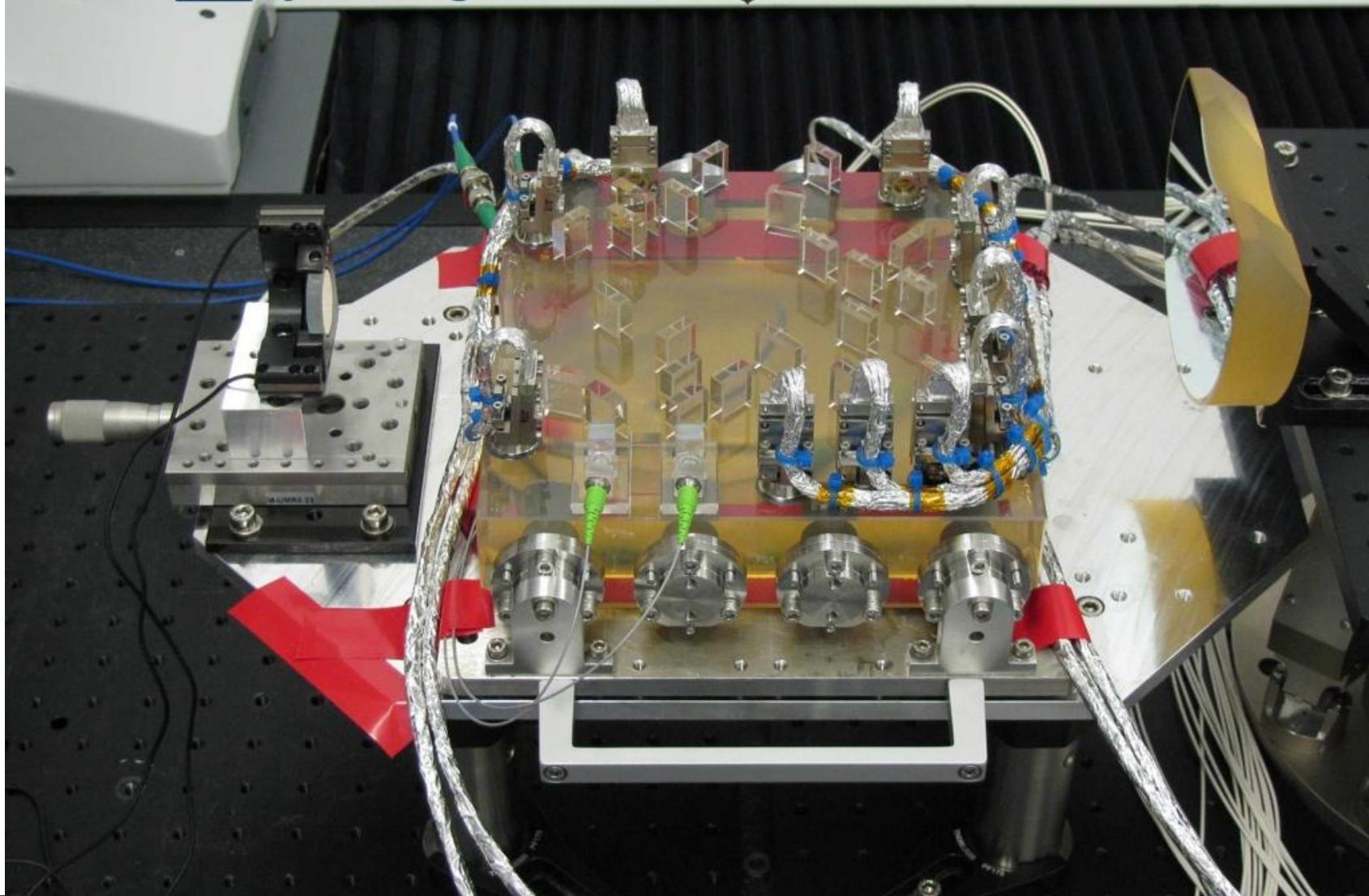
LISA Pathfinder optical bench PFM



University
of Glasgow



UNIVERSITY OF
BIRMINGHAM



LISA Pathfinder optical bench PFM

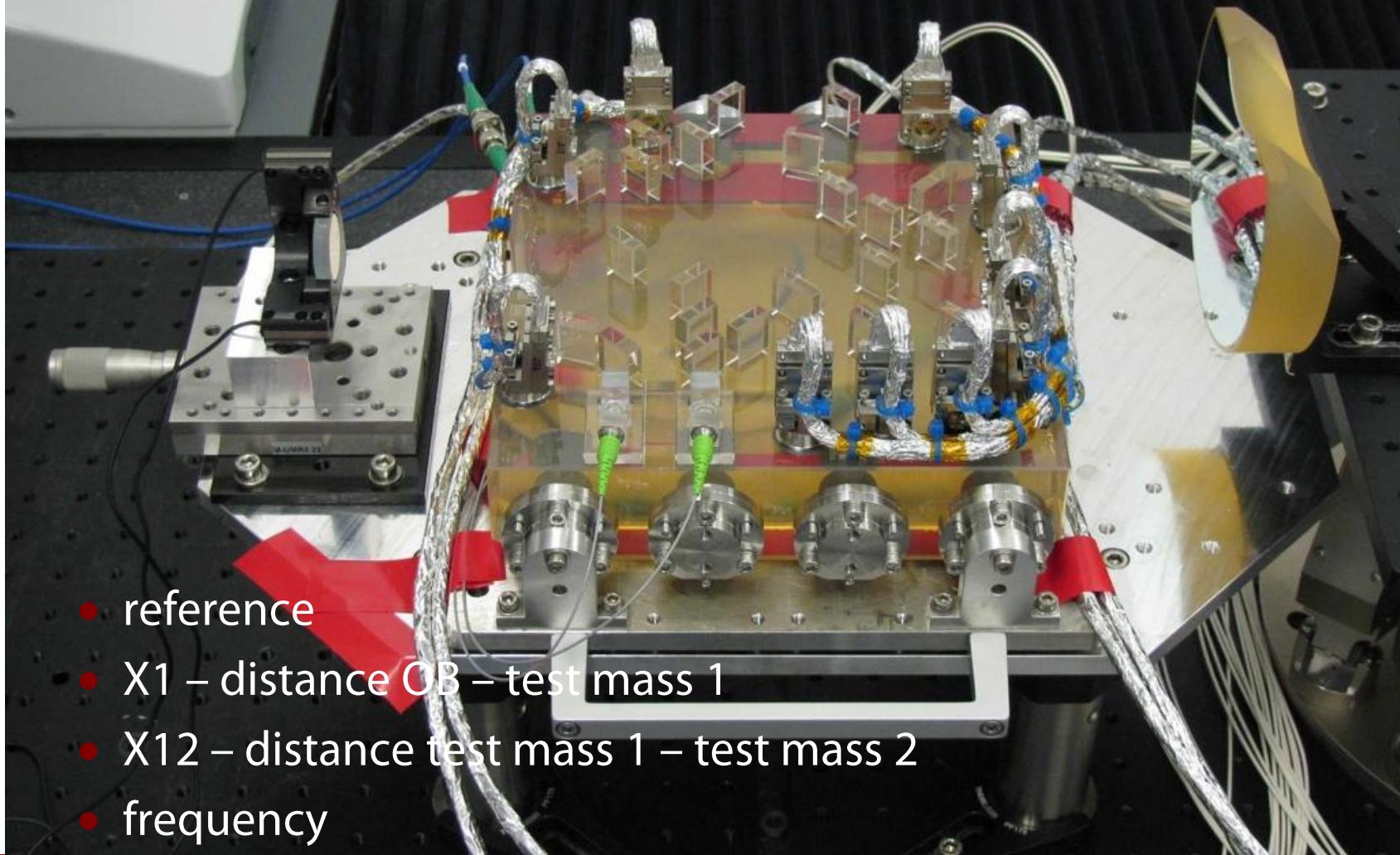


University
of Glasgow



UNIVERSITY OF
BIRMINGHAM

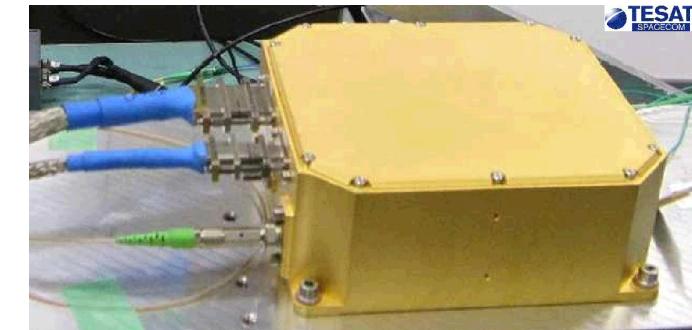
- Contains four interferometers



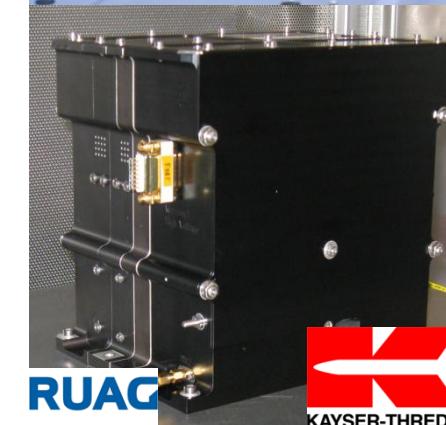
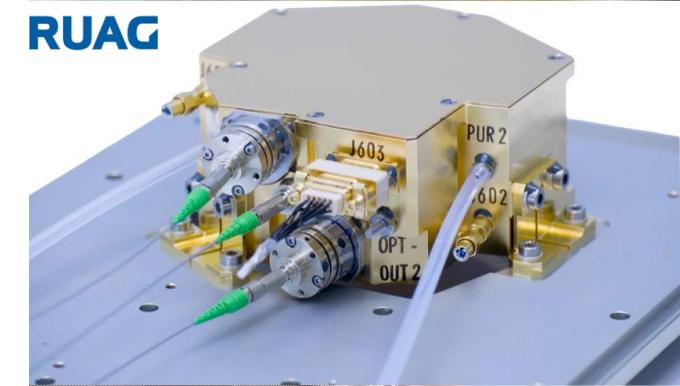
- reference
- X1 – distance OB – test mass 1
- X12 – distance test mass 1 – test mass 2
- frequency

Laser system for LISA Pathfinder

- Consists of
 - Reference laser unit
 - 40 mW @ 1064 nm
 - Actuators: slow power, slow and fast frequency
 - Laser modulator unit
 - Beam splitter
 - Two AOMs
 - Two optical pathlength actuators
 - Laser control unit
 - Power supply
 - actuates frequency, power, OPD



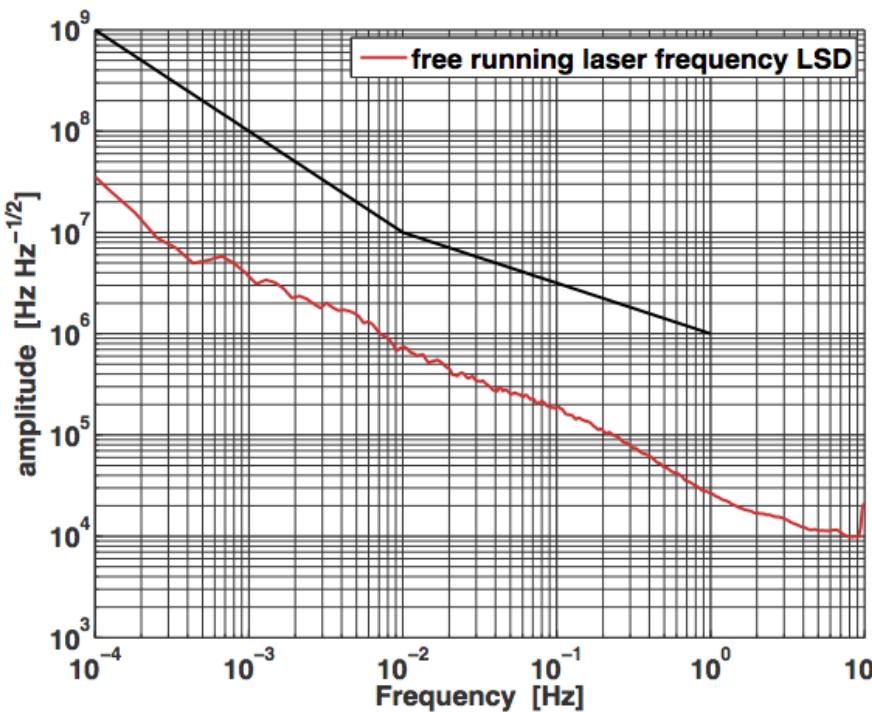
RUAG



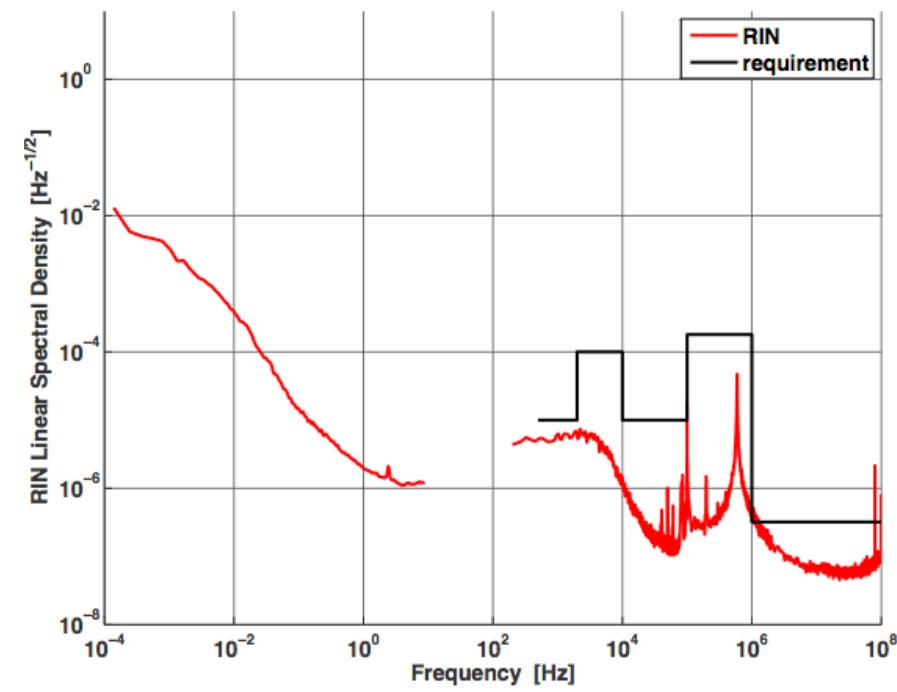
TESAT
SPACECOM

Reference laser unit FM free-running noise

- Nominal 40 mW output power
- 30 kHz/ $\sqrt{\text{Hz}}$ @ 1 Hz freq. noise



Frequency noise



Relative power noise

Laser frequency stabilization

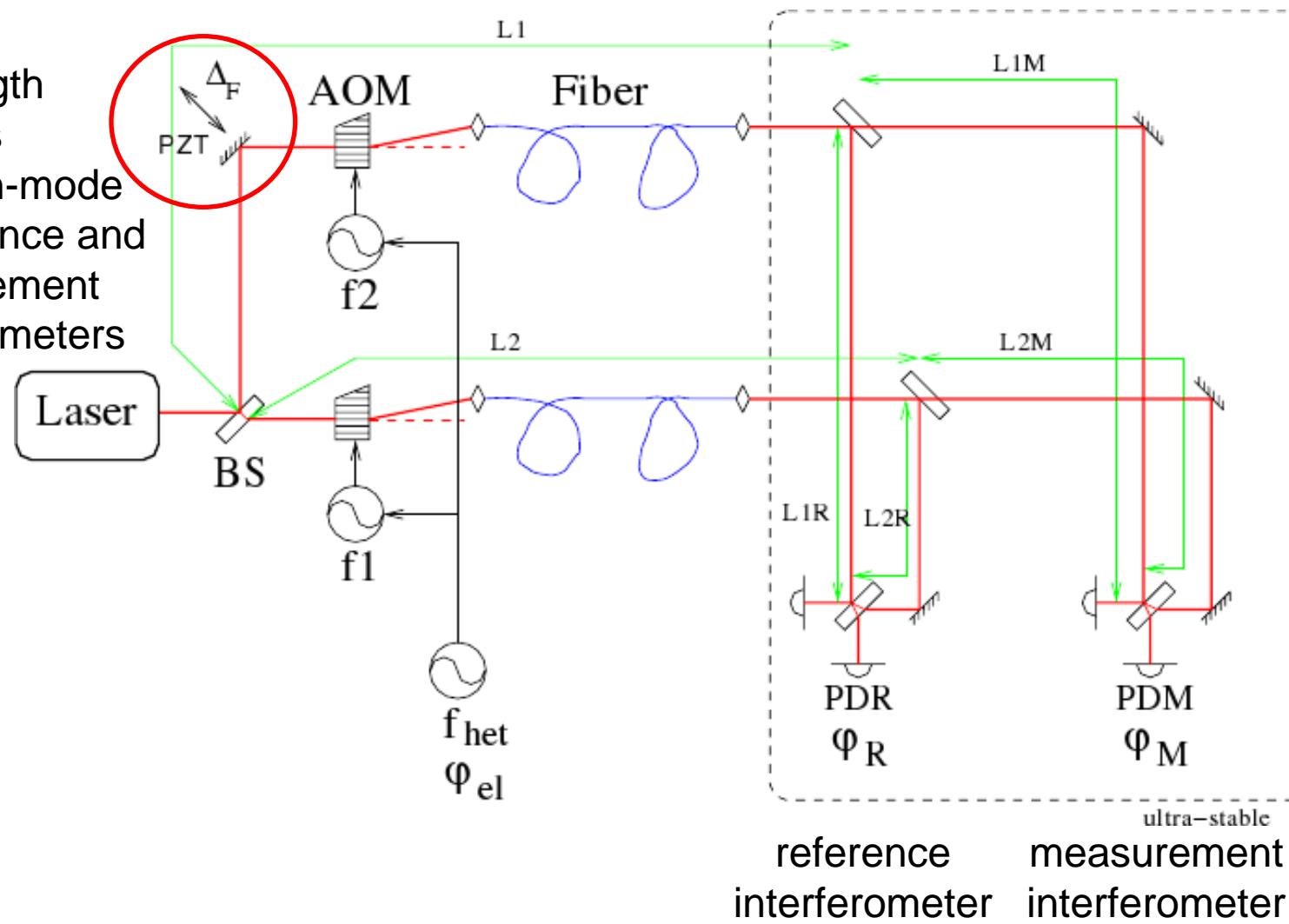
- Pathlength differences up to 1 cm in interferometers
- $28 \text{ kHz}/\sqrt{\text{Hz}}$ frequency noise required to keep impact on length measurement below $1 \text{ pm}/\sqrt{\text{Hz}}$
- Two nested digital loops (100 Hz sampling frequency) running in data management unit (DMU)
- Inner loop acting on fast frequency actuator (PZT on laser crystal)
- Outer loop acting on slow frequency actuator (temperature of laser crystal)

Laser power stabilisation

- Two reasons for laser power stabilisation
 - Limit radiation pressure noise at test masses in measurement band
 - Limit power noise at heterodyne frequency
- Two control loops
 - inner fast analog loop acting on RF power applied to individual AOM
 - Outer slow loop acting on laser power

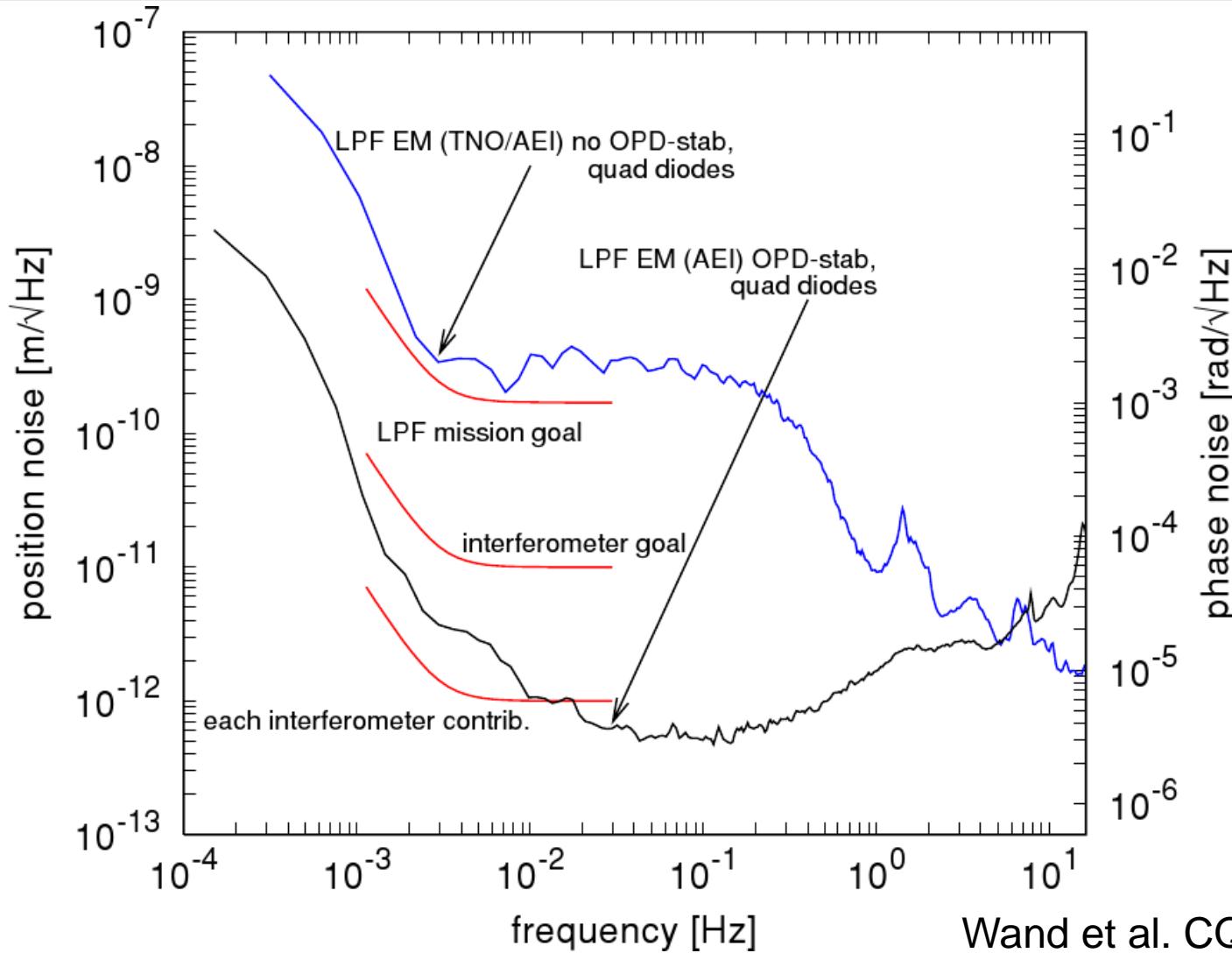
Optical pathlength difference stabilisation

Pathlength changes
common-mode
in reference and
measurement
interferometers



Common-mode noise suppression only works down to nm/ $\sqrt{\text{Hz}}$

Optical pathlength difference stabilisation

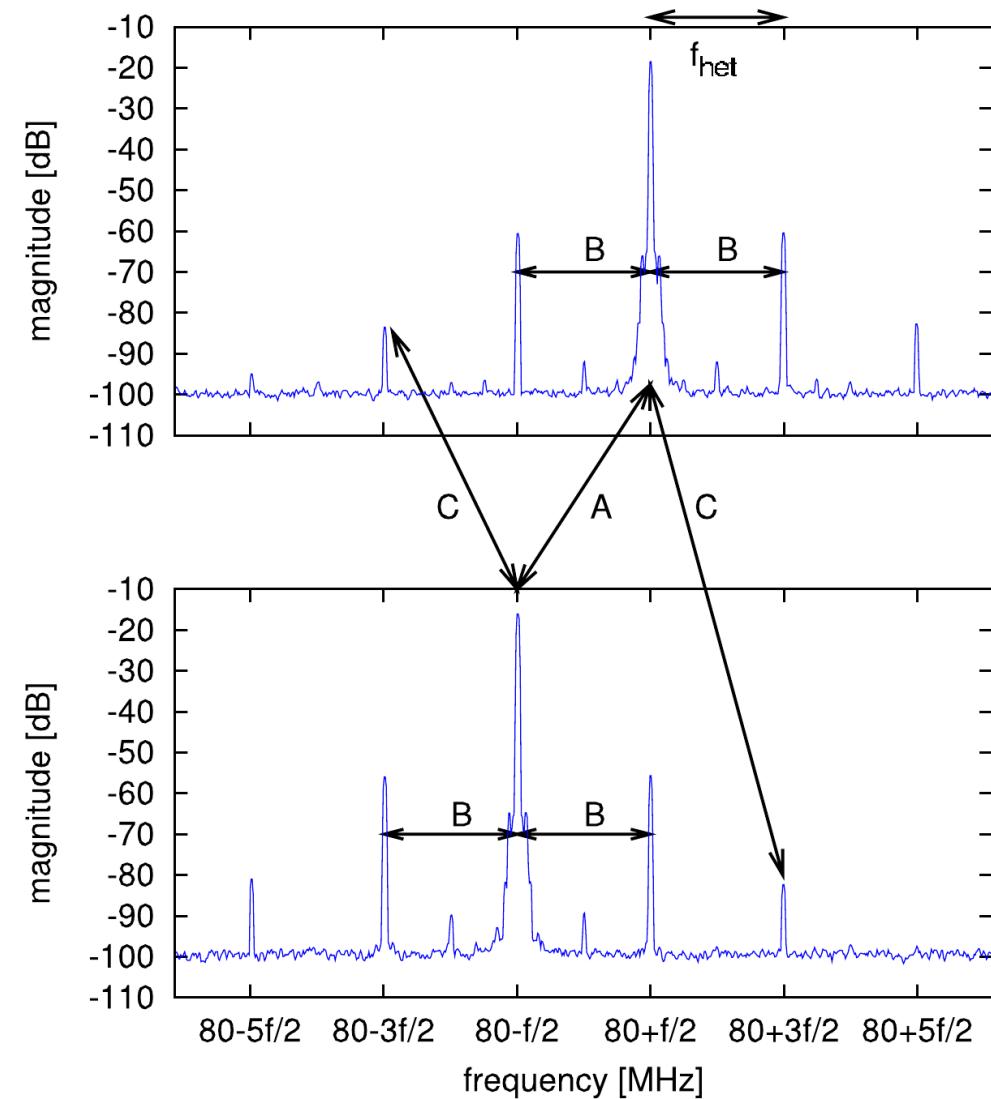


Wand et al. CQG
vol. 23 pp. S159 (2006)

- Noise mitigation works, $\text{nm}/\sqrt{\text{Hz}}$ without stabilisation, $\text{pm}/\sqrt{\text{Hz}}$ with stab.

Optical pathlength difference stabilisation

- AOM driving signals show parasitic sidebands spaced at the heterodyne frequency caused by electro-magnetic coupling between AOM drivers
- A denotes the nominal heterodyne signal
- B,C denote parasitic heterodyne signals
- parasitic phase depends on sum and difference of measurement and reference phase
- both phases are dominated by external disturbances
- mitigation of noise effect: keep reference phase constant
- achieved by PZT actuators in laser modulator unit



Wand et al. CQG vol. 23 pp. S159 (2006) 16

LISA laser



- Breadboard demonstrated
 - 1.2 W out-of-fiber
 - $30 \text{ Hz}/\sqrt{\text{Hz}}$ frequency noise
 - $2 \times 10^{-4}/\sqrt{\text{Hz}}$ relative power noise

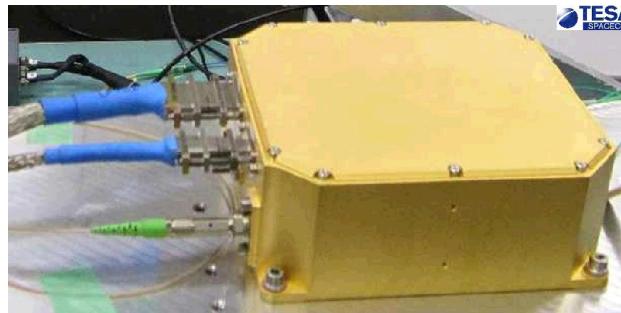


- ESA has issued ITT for engineering model
 - 2 W @ 1064 nm
 - actuators for stabilization
- Concept
 - Master oscillator power amplifier
 - EOM in-between for clock-noise transfer, ranging

LISA laser system components

- Seed laser

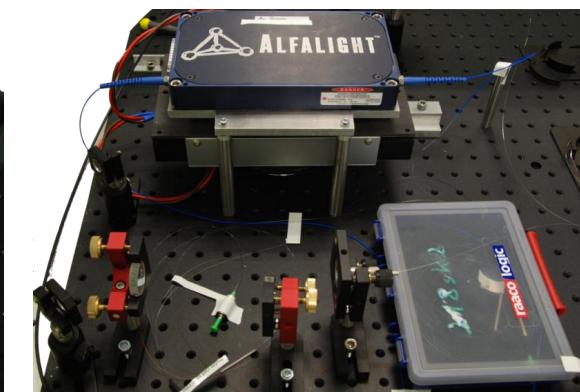
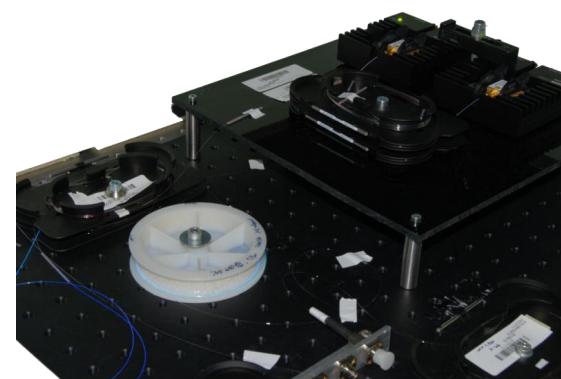
- NPRO



- EOM (clock-noise transfer, ranging)

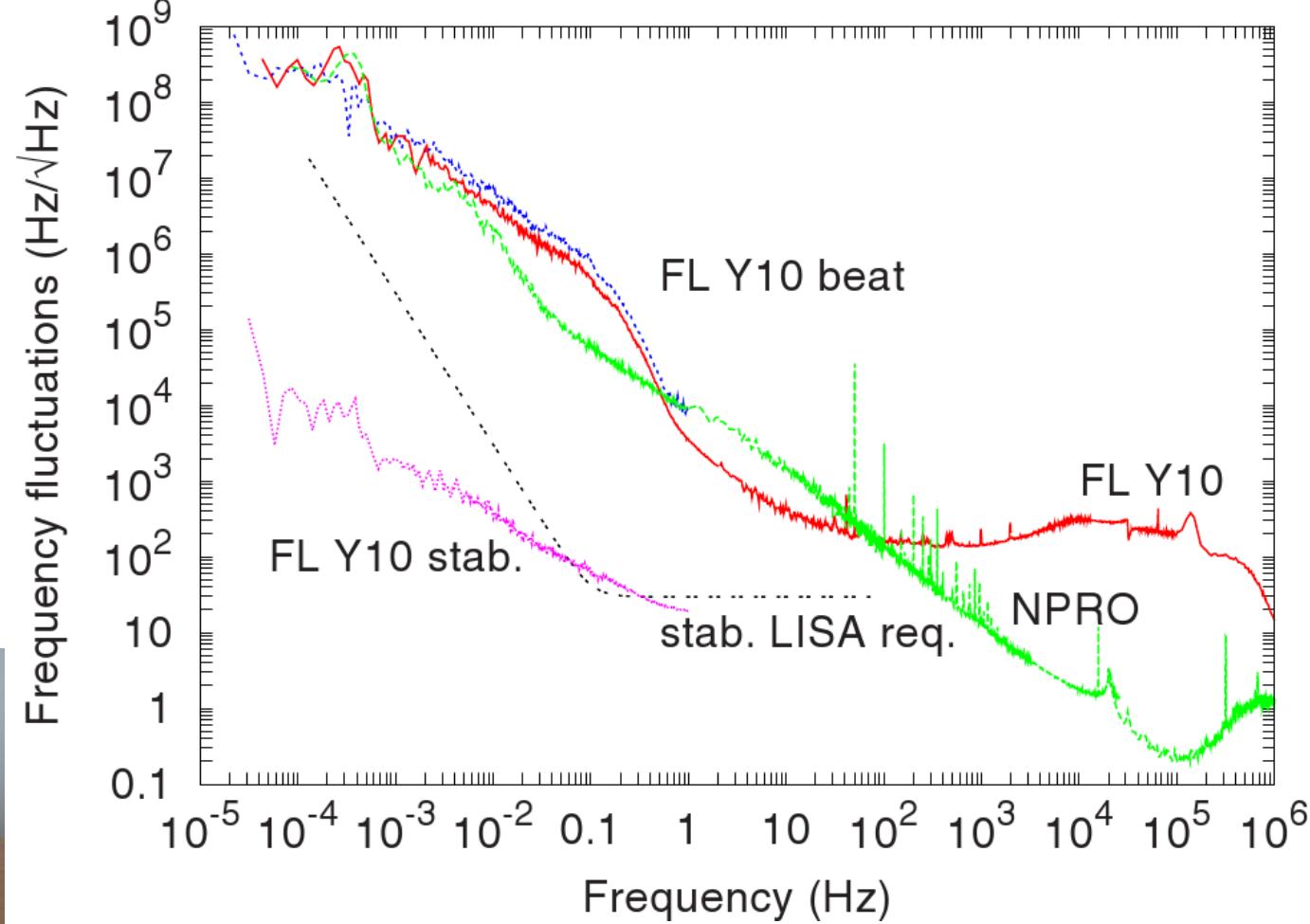


- fiber amplifier
 - core-pumped
 - cladding pumped



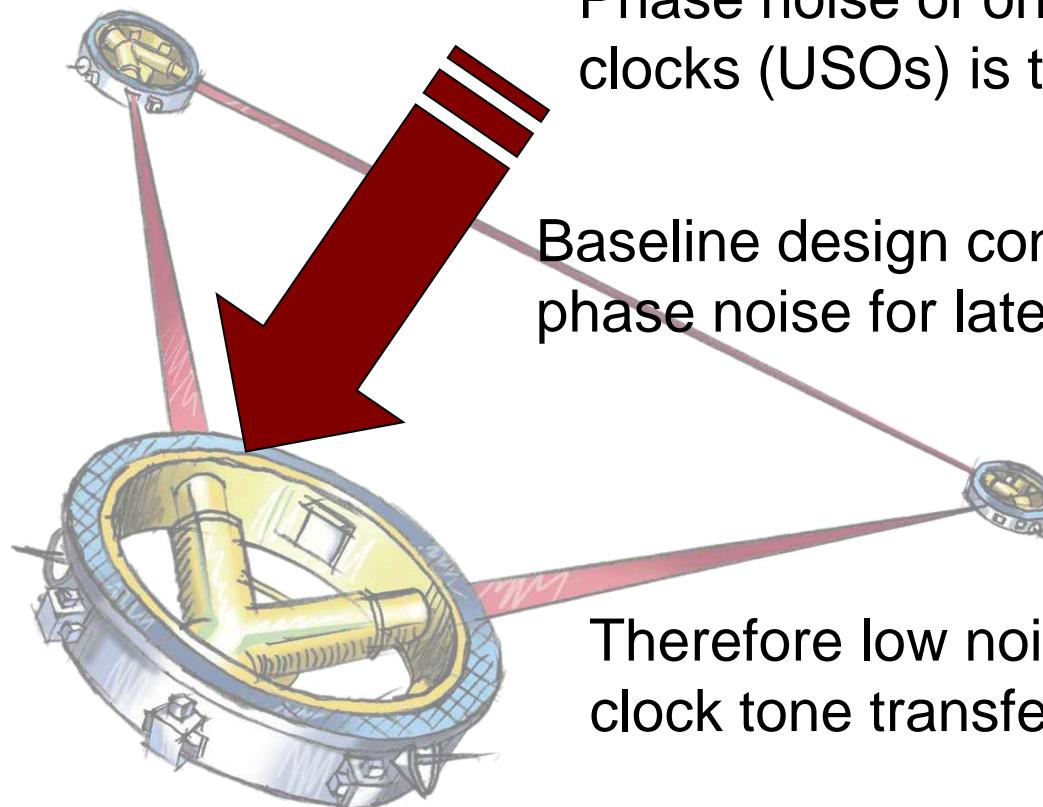
Seed lasers for LISA

- Frequency noise of commercial fiber laser (Boostik by Koheras, labelled FL Y10) comparable to NRPO below 100 Hz



Tröbs et al. JOSAB 26 pp. 1137 (2009)

Ultra Stable Oscillator (USO) phase noise

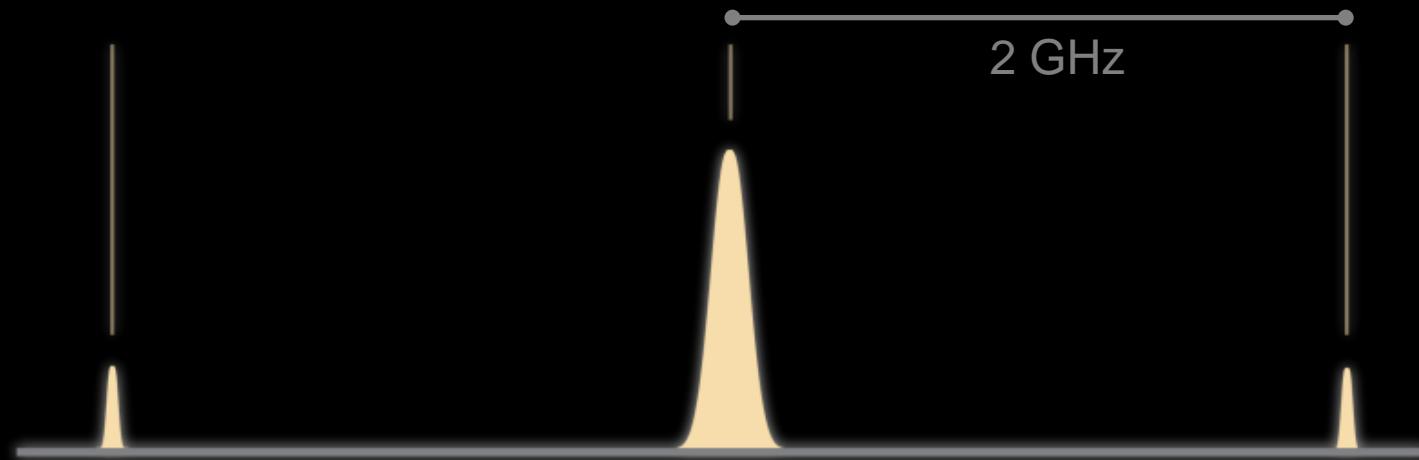
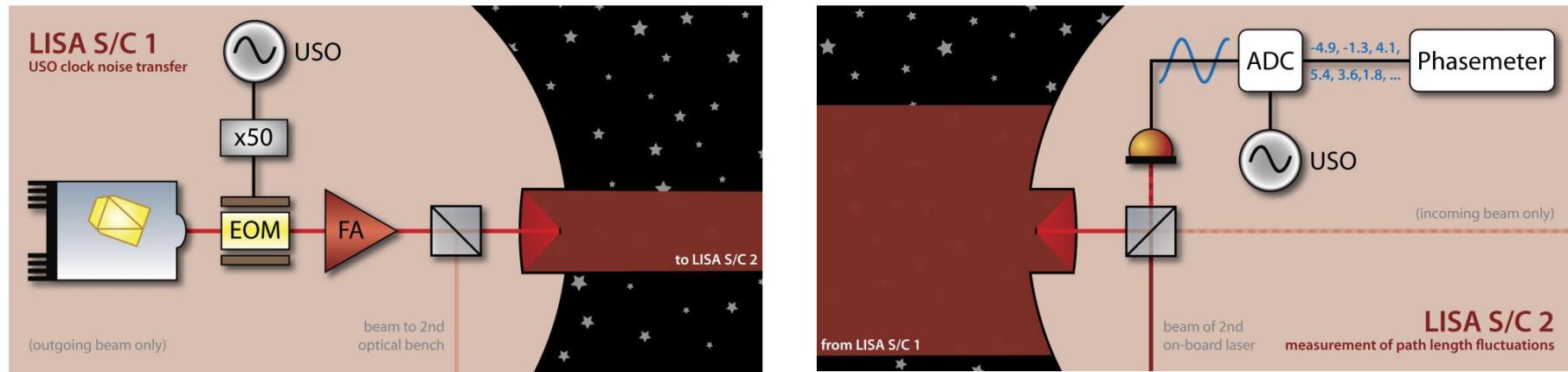


Phase noise of on-board
clocks (USOs) is too high!

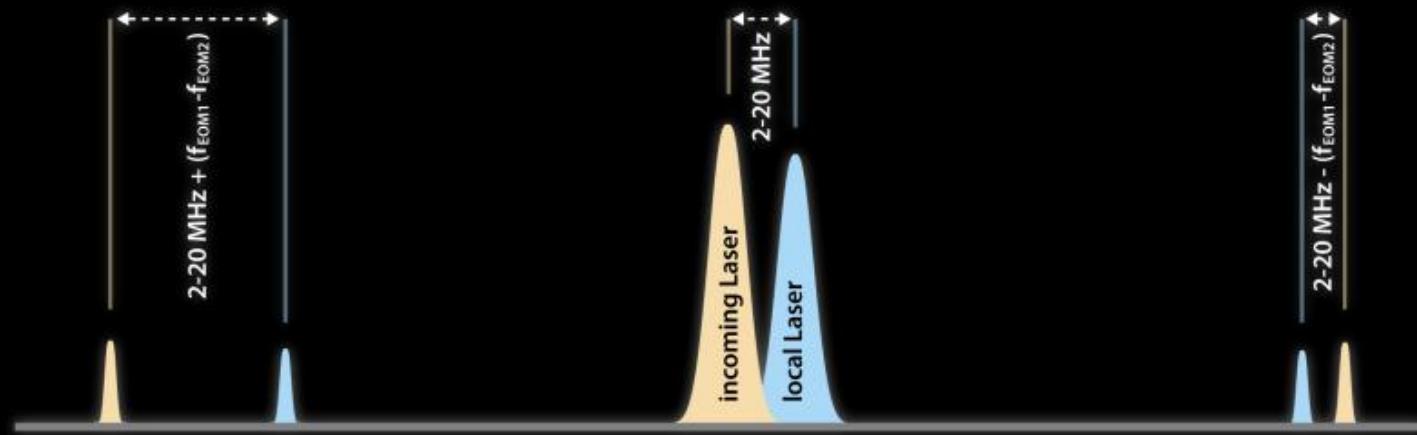
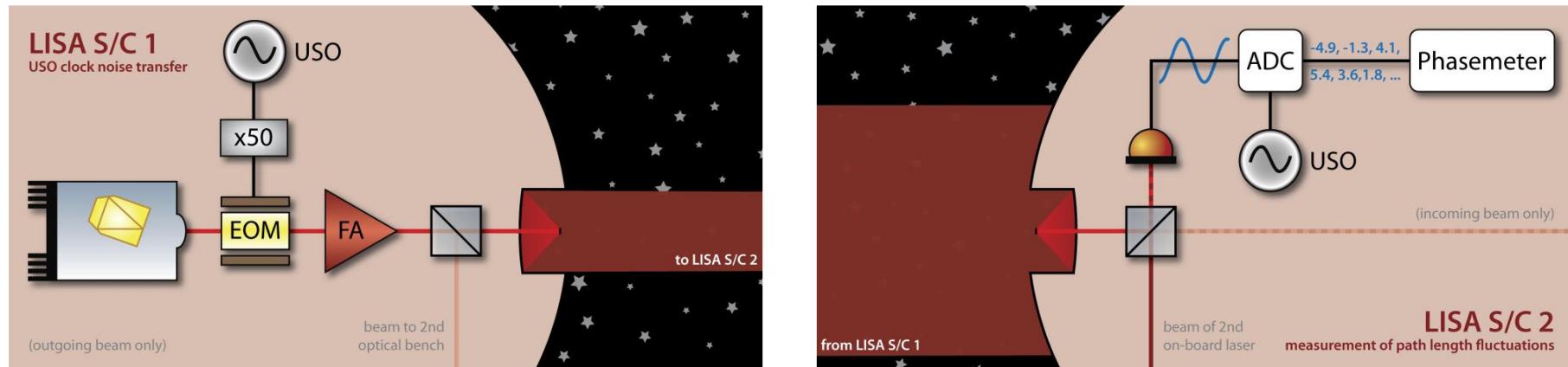
Baseline design concept: measure
phase noise for later cancellation.

Therefore low noise in
clock tone transfer chain required

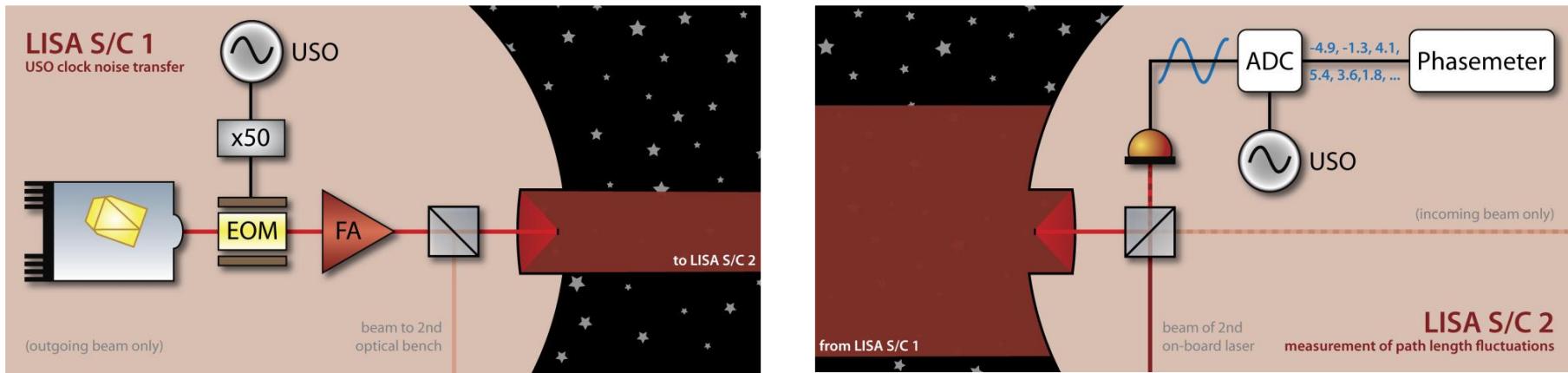
USO clock tone transfer chain



USO phase noise measurement



Requirements



Phase read-out:

$$\Delta\phi_{1\text{pm}} < \frac{1 \text{ cycle}}{1064 \text{ nm}} \cdot \frac{1 \text{ pm}}{\sqrt{\text{Hz}}} \approx 1 \frac{\mu\text{cycles}}{\sqrt{\text{Hz}}} \approx 6 \frac{\mu\text{rad}}{\sqrt{\text{Hz}}}$$

Ancillary Modulation Error:

$$\Delta\phi_{\text{AME}} < \Delta\phi_{1\text{pm}} \cdot \frac{f_{\text{USO}}}{f_{\text{het}}} \cdot \frac{f_{\text{mod}}}{f_{\text{USO}}} \approx 6 \cdot \frac{2 \text{ GHz}}{20 \text{ MHz}} \frac{\mu\text{rad}}{\sqrt{\text{Hz}}}$$

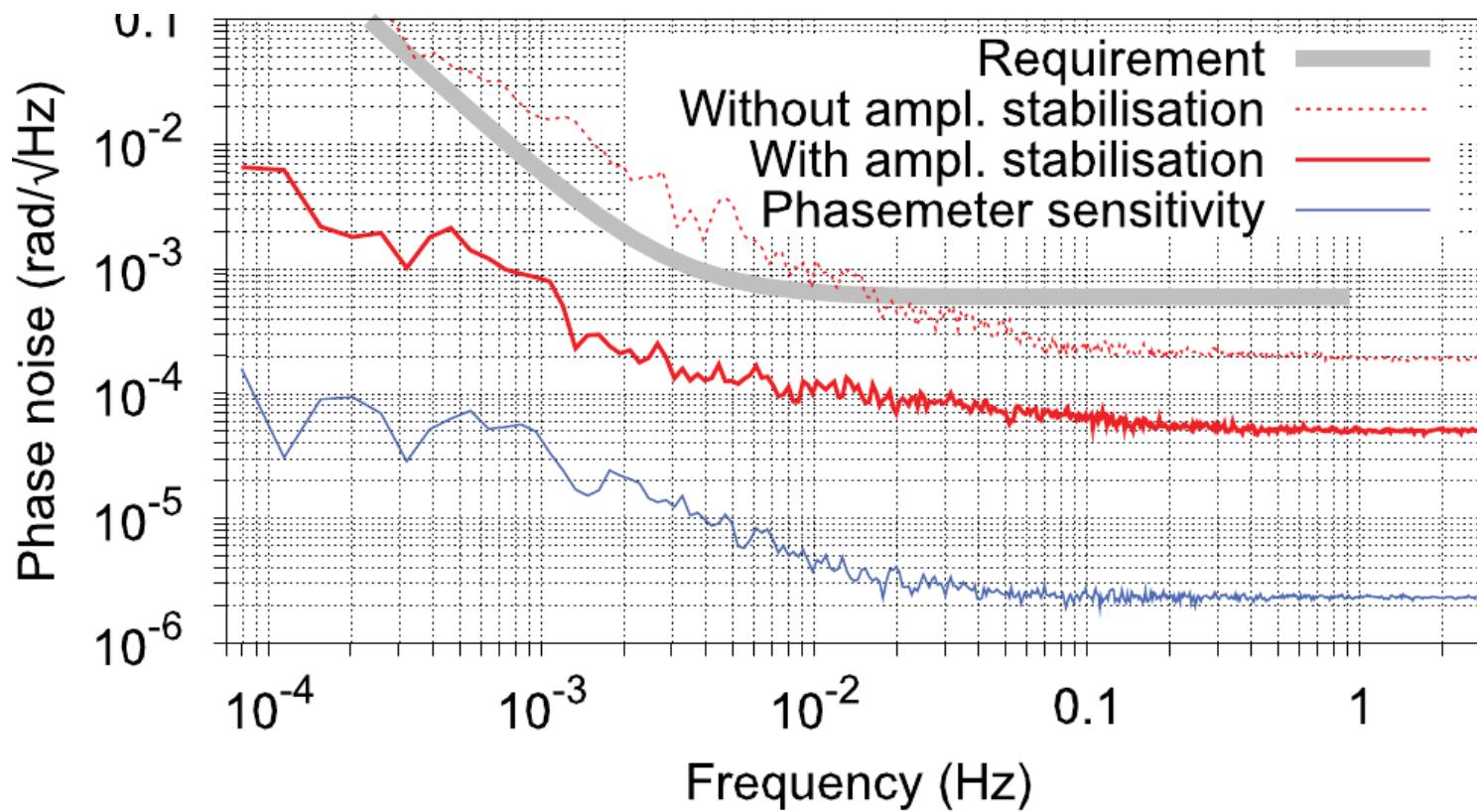
LISA frequency band:

$$\Delta\phi_{\text{AME}'}(f) = 0.6 \cdot \sqrt{1 + \left(\frac{2.8 \cdot 10^{-3} \text{ Hz}}{f}\right)^4} \frac{\text{mrad}}{\sqrt{\text{Hz}}}$$



EOM phase fidelity

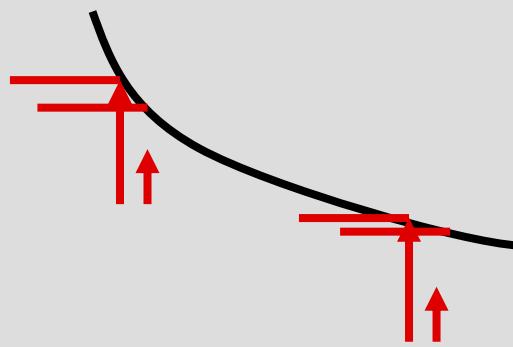
- Phase fidelity of waveguide EOM fulfills LISA requirements
- Space-qualified version available



Barke et al. Appl Phys B (2010) 98: 33–39

Potential sources of differential phase noise in amplifiers

- nonlinear dispersion and laser frequency changes



- first measurements show tiny effect
- should be negligible in LISA

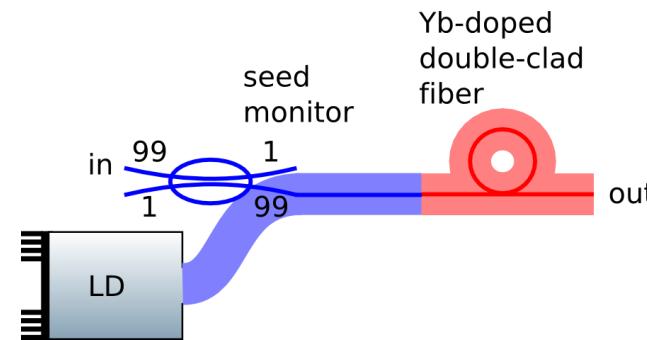
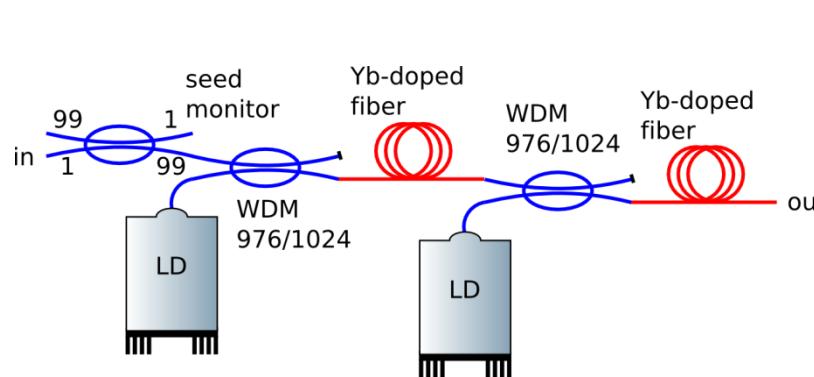
- amplifier length changes due to

- changes in ambient temperature
- pump power changes
- seed power changes

$$\Delta\varphi = \frac{2\pi \cdot f_{\text{EOM}}}{c} \cdot \Delta L$$

- combined effect measured

Optical amplifiers under test



Core-pumped amplifier

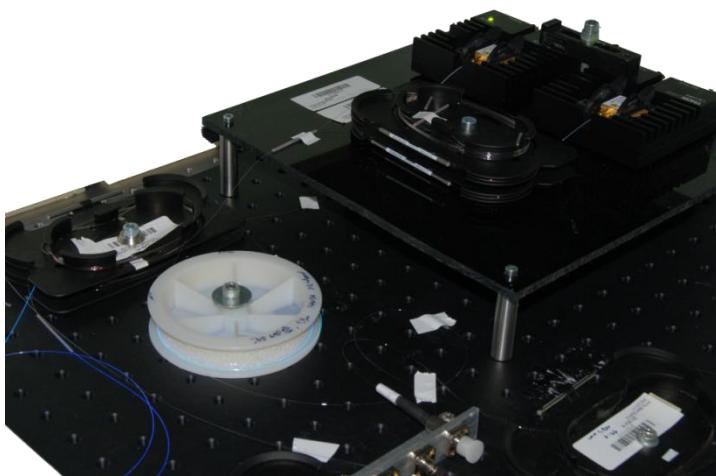
- Two identical stages
- Pumping directly the core of a single-mode fiber
- 2 x 0.4 m active fiber
- 1 W output power

Cladding-pumped amplifier

- Single stage
- Pumping in the multi-mode cladding
- 3 m active fiber
- 1 W output power

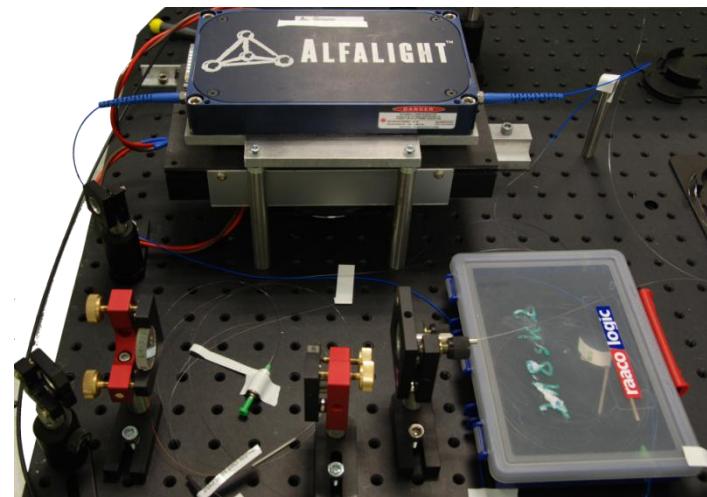
Amplifiers supplied by Laser Zentrum Hannover e. V.

Optical amplifiers under test



Core-pumped amplifier

- Two identical stages
- Pumping directly the core of a single-mode fiber
- 2 x 0.4 m active fiber
- 1 W output power

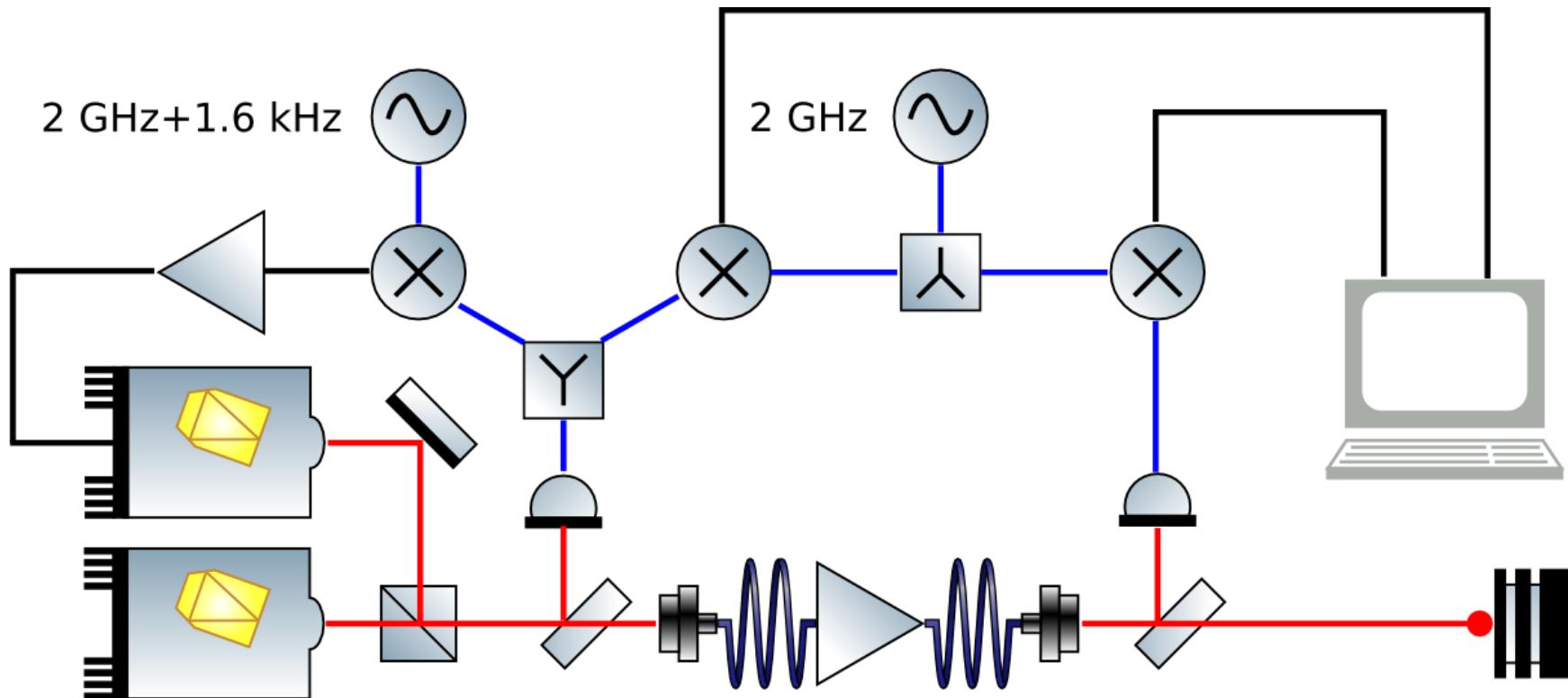


Cladding-pumped amplifier

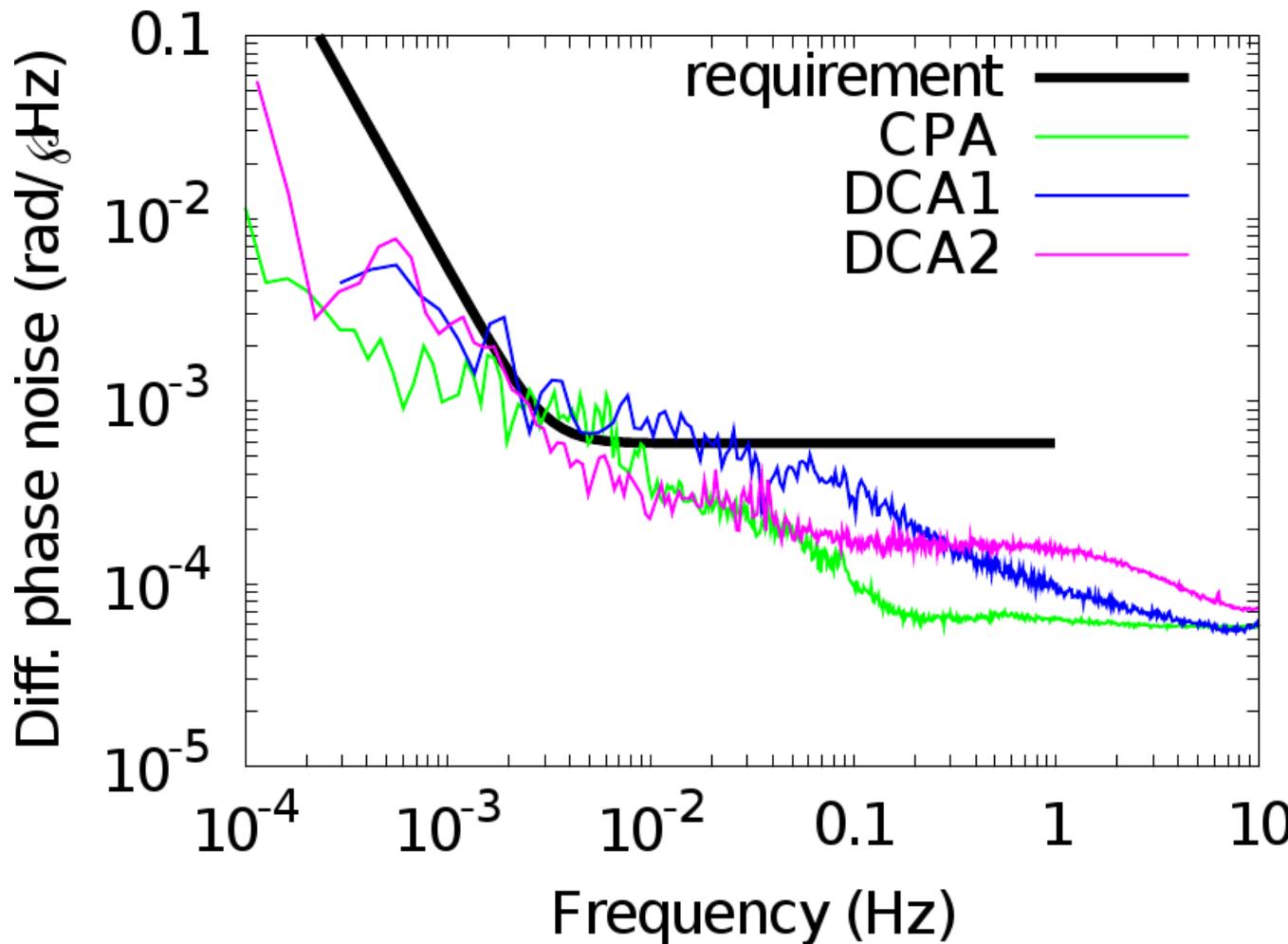
- Single stage
- Pumping in the multi-mode cladding
- 3 m active fiber
- 1 W output power

Amplifiers supplied by Laser Zentrum Hannover e. V.

Measurement setup



Differential phase noise of amplifiers

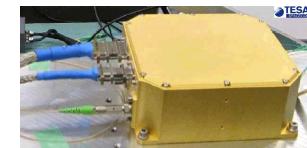


- 1 W output power
- Within LISA requirement
- 2 GHz sideband frequency

Tröbs et al. JPCS (2010) 208: 012042

Summary

- Laser system for LISA Pathfinder
 - laser unit, laser modulator unit, laser control unit
 - FMs finished and extensively tested
- Laser system for LISA
 - breadboard demonstrated pre-stabilisation
 - components for EM are available
 - phase fidelity of EOM and fiber amplifiers was verified



Thank you

- J Reiche, A Garcia & LTP team
- HSL team



LISA Pathfinder in acoustic test chamber at ESA