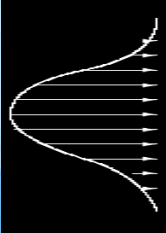


# Stress-optic noise?



GWADW  
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LIGO-G1100571

May 2011  
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# Outline

- Generalized Fluctuation-Dissipation Theorem
  - And the choice of TD variables
- Stress-Optic effect
  - and a simple example
- What we ought to do

# Fluctuation-Dissipation, general

- A 2<sup>nd</sup> set of conjugate TD variables: S & T

$$dF(T, \vec{\varepsilon}) = -SdT + \vec{\sigma}d\vec{\varepsilon}$$

- F-D theorem applicable:

- Thermal Impedance Z
- Drive the system with

$$\begin{pmatrix} \vec{F} \\ \vec{S} \end{pmatrix} = G_0 \begin{pmatrix} \vec{f}_x \\ \vec{f}_T \end{pmatrix} \cos(\omega t)$$

$$\text{where } e = \vec{f}_x + \vec{x} + \vec{f}_T + \vec{T}$$

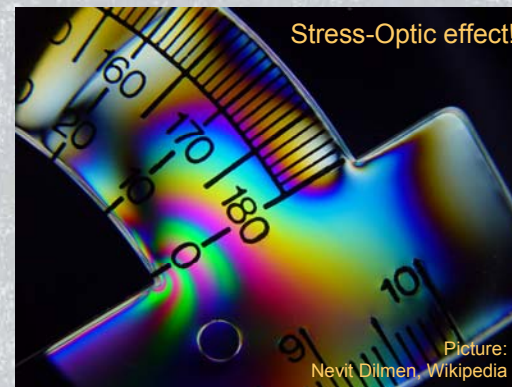


$$S_{ee}(f) = \frac{8k_B T}{\omega^2} \frac{P_{\text{diss}}}{G_0^2}$$



# Choice of your TD variables

- Hooke's law:  $\vec{\sigma} = \vec{H} \bullet (\vec{\varepsilon} - \vec{\alpha}T)$   $\vec{\sigma} = \vec{H} \bullet (\vec{\varepsilon}_\sigma)$
- Lin. expansion:  $\delta d = \varepsilon_1 \cdot d$   $\delta d = (\vec{\varepsilon}_\sigma + \vec{\alpha}T)_1$
- TD variables:  $T$  and  $\vec{\varepsilon}$   $T$  and  $\vec{\varepsilon}_\sigma$
- TE noise from: adiabatic heating (Fejer et. al.) explicit T dependence (Levin)
- Opt. thickness:  $\frac{\delta(nd)}{nd} = \delta\varepsilon_1 + \frac{\beta}{n} \delta T$   $\frac{\delta(nd)}{nd} = \delta\varepsilon_{\sigma 1} + \left(\frac{\beta}{n} + \alpha_1\right) \delta T$   
(one layer)
- So far missing in GW literature:



# Stress-Optic Effect

- $n$  depends on both  $T$  and  $\sigma$

– Typically measured:

$$\beta = \left. \frac{\partial n}{\partial T} \right|_{\sigma \text{ const}}$$

$$C_p = \left. -\frac{2}{n^3} \frac{\partial n}{\partial \sigma_p} \right|_{T \text{ const}} \quad C_s = \left. -\frac{2}{n^3} \frac{\partial n}{\partial \sigma_s} \right|_{T \text{ const}}$$

- $\sigma_p$  &  $\sigma_s$  are parallel and orthogonal strain

– Values for Silica:

$$\begin{matrix} C_p & = & 4.22 \\ C_s & = & 0.65 \end{matrix} \times 10^{-12} \frac{m^2}{N}$$

Stone, Journal of Lightwave Technology Vol 6 No 7 July 1988

- Convert to  $T$  &  $\varepsilon$  dependence using TD id's.
- Small effect for mirror coatings, but...

# Example: Propagation in bulk

- For simplicity:
  - Uniform, 3-D model, Silica
- Brownian noise:
  - without Stress-optic effect:

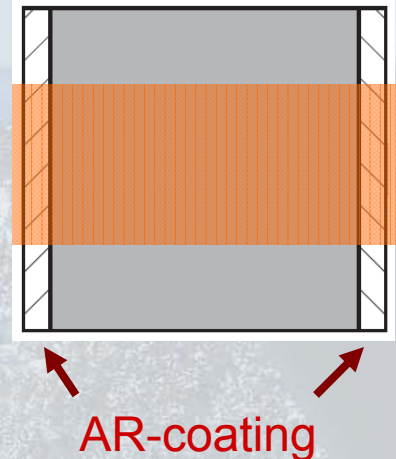
$$S_{xx}(f) = \frac{4k_B T}{\omega} \Phi \frac{L}{A} \frac{(n-1)^2}{E}$$

$$S_{xx}(f) = \frac{4k_B T}{\omega} \Phi \frac{L}{A} \times 2.81 \times 10^{-12} \frac{m^2}{N}$$

- including Stress-optic effect:

$$S_{xx}(f) = \frac{4k_B T}{\omega} \Phi \frac{L}{A} \times 0.81 \times 10^{-12} \frac{m^2}{N}$$

- Relevant e.g. for Khalili cavities...



Silica:

$$n = 1.45$$

$$E = 7.2 \times 10^{10} \text{ pa}$$

$$C_p = 4.22 \times 10^{-12} \frac{m^2}{N}$$
$$C_s = 0.65 \times 10^{-12} \frac{m^2}{N}$$

# What we ought to do

- More realistic calculations get complicated
- We ought to
  - Use an FEM model to calculate  $P_{\text{diss}}$
  - Calc. Brownian & Thermo-optic noise in one run
  - Optimize for mirror / coating geometries
- I advertised this before
  - No progress yet – man power needed



That's it...

Adirondack Park  
New York



# Example: Propagation through bulk

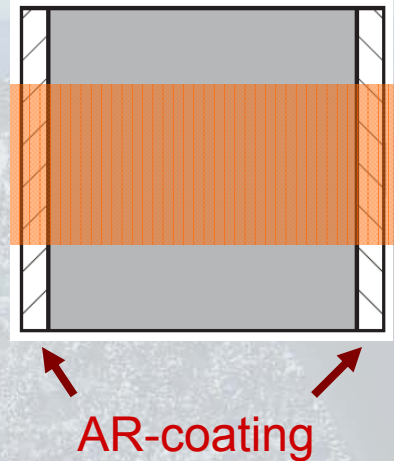
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- Brownian noise:
  - without Stress-optic effect:

$$S_{xx}(f) = \frac{4k_B T}{\omega} \Phi \frac{L}{A} \frac{(n-1)^2}{E}$$

$$S_{xx}(f) = \frac{4k_B T}{\omega} \Phi \frac{L}{A} \times 2.81 \times 10^{-12} \frac{m^2}{N}$$

- including Stress-optic effect:

$$S_{xx}(f) = \frac{4k_B T}{\omega} \Phi \frac{L}{A} \left[ (n-1)\delta_1^T - \frac{n^3}{2} C^T H \right] H^{-1} \left[ (n-1)\delta_1 - \frac{n^3}{2} HC \right]$$



Silica:

$$n = 1.45$$

$$E = 7.2 \times 10^{10} \text{ pa}$$

$$C_p = 4.22 \times 10^{-12} \frac{m^2}{N}$$

$$C_s = 0.65 \times 10^{-12} \frac{m^2}{N}$$