

# Coating Brownian Thermal Noise

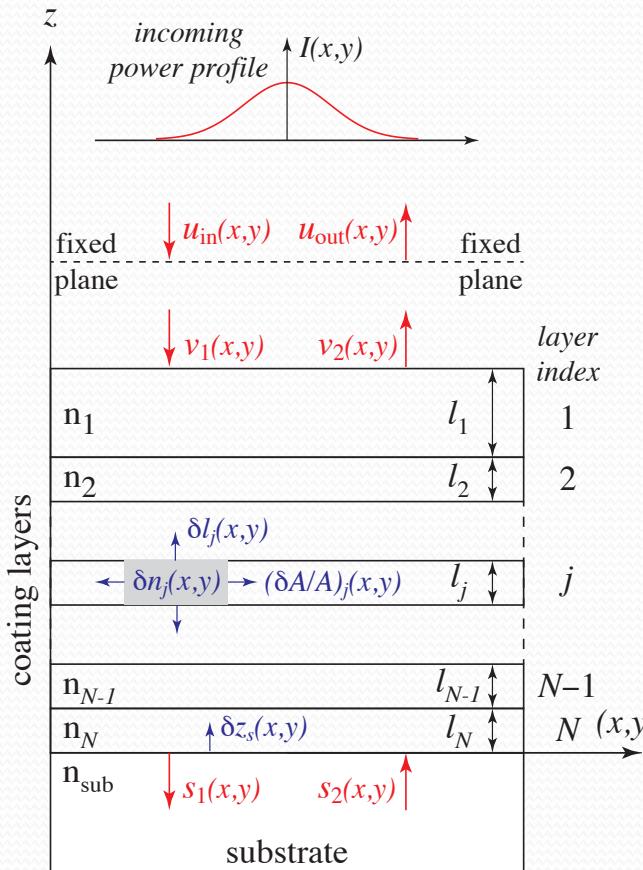
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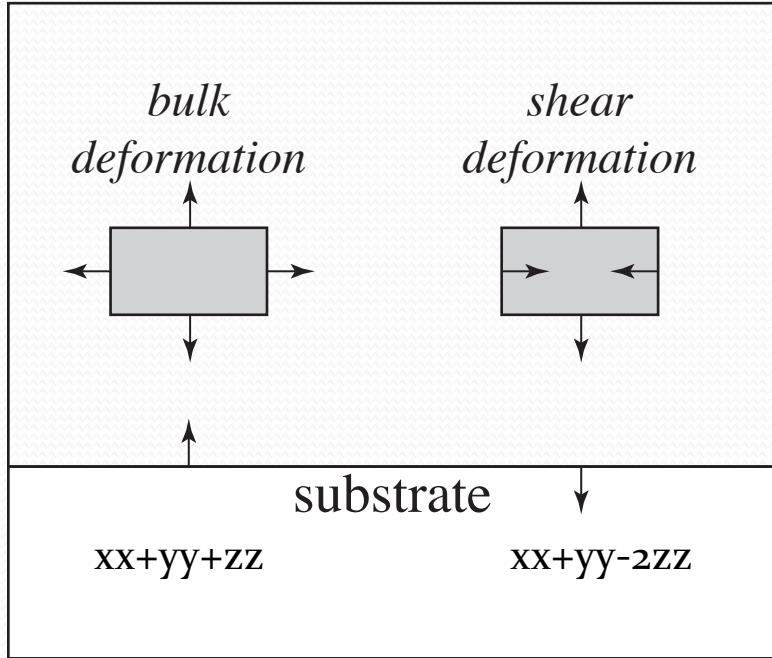
# Coating Brownian Noise Components



1. Thickness fluctuations of the coating layers
2. Height fluctuation of coating-substrate interface
3. Refractive index fluctuations of the coating layers

# Fluctuations induced by Bulk and Shear Losses

coating layers



$\phi_\Theta$

$\phi_\Sigma$

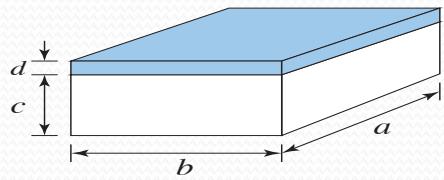
We assign a separate loss angle for bulk and shear energy.

$$U = \frac{1}{2} K \Theta^2 + \mu \Sigma^2$$

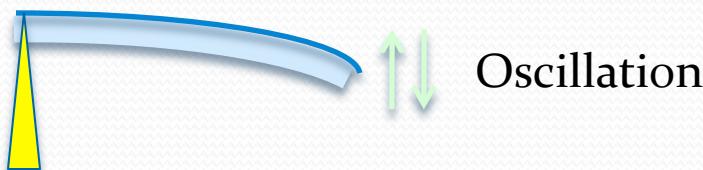
$$W_{diss}(\text{per\_cycle}) = \phi_\Theta \frac{1}{2} K \Theta^2 + \phi_\Sigma \mu \Sigma^2$$

- Bulk Noise:
  - $\text{xx+yy+zz}$  Coating thickness and interface
- Shear Noise:
  - $\text{xz+zx}$  and  $\text{yz+zy}$  No influence
  - $\text{xx-yy}$  and  $\text{xy+yx}$  Coating-Substrate Interface
  - $\text{xx+yy-2zz}$  Coating thickness and Interface

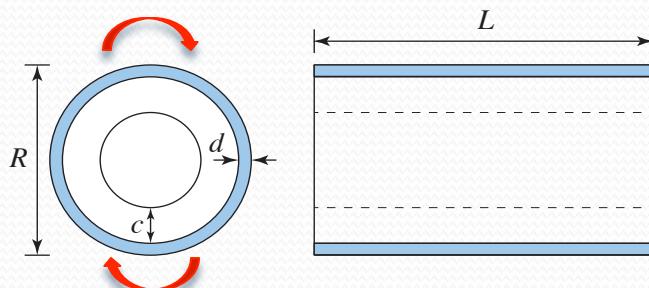
# Ringdown Measurement of Loss angles



$$\phi = \frac{d}{c} \frac{Y_c}{Y_s} \frac{(1 - \sigma_s^2)}{(1 - \sigma_c)^2} [\phi_B(1 - 2\sigma_c) + 2\phi_s \frac{1 - \sigma_c + \sigma_c^2}{1 + \sigma_c}] + \phi_{sub}$$

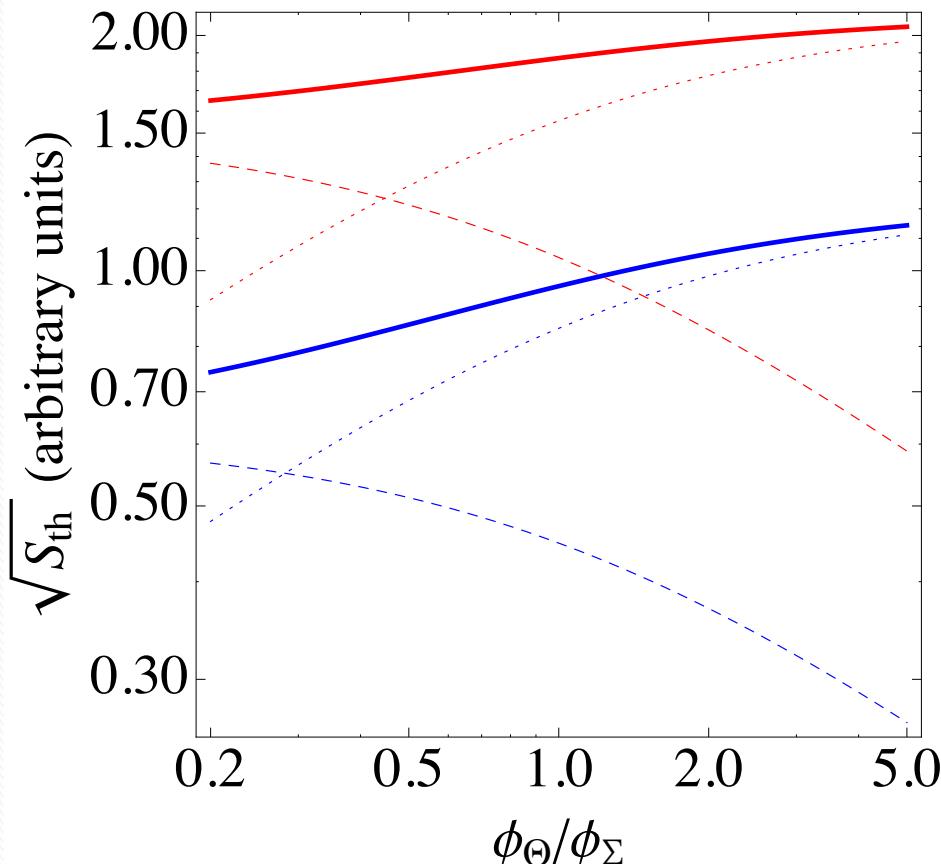


$$\phi = \frac{1}{Q}$$



$$\phi = \phi_{sub} + \frac{d}{c} \frac{Y_c}{Y_s} \frac{(1 + \sigma_s)}{(1 + \sigma_c)} \phi_s$$

# Effect of Uncertainties in Loss Angles



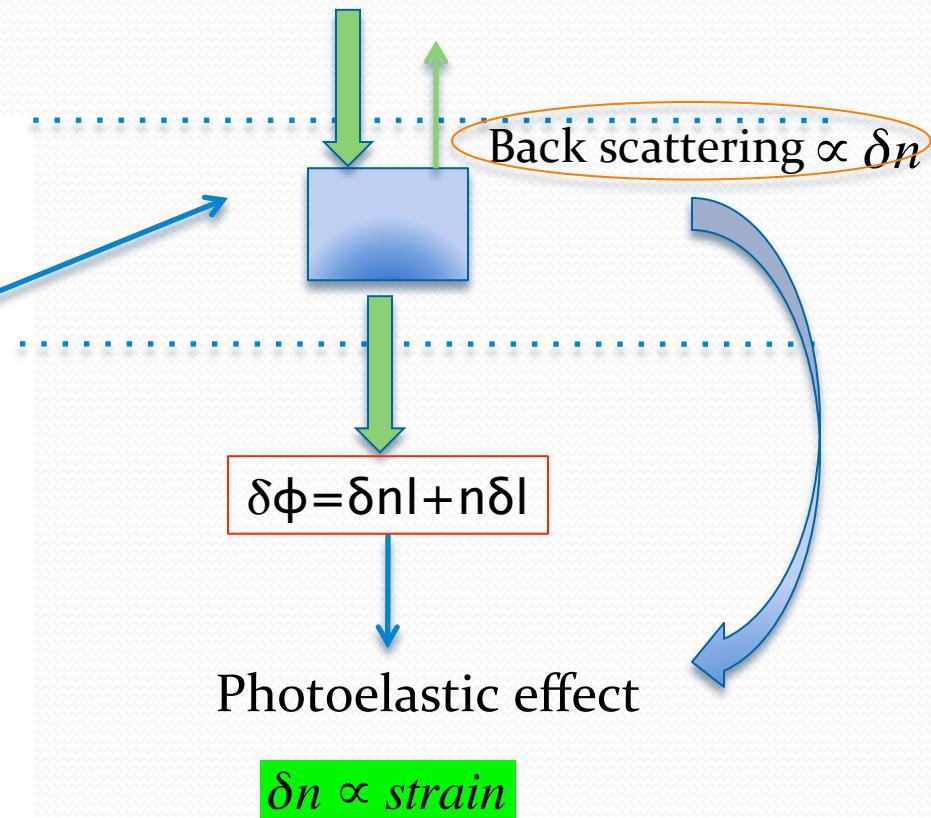
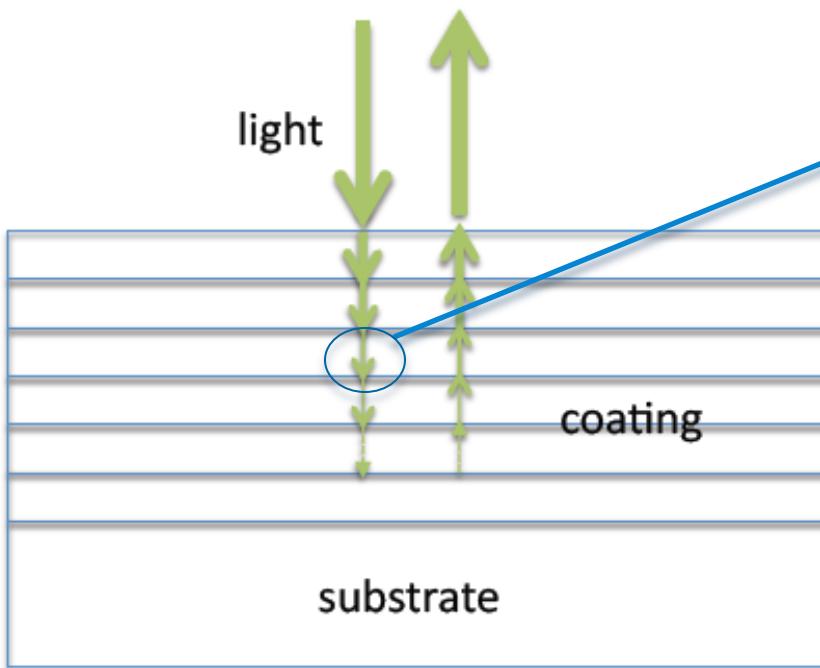
Baseline Parameters used for Coating

| Materials                        | $Ti_2O_5$            | $SiO_2$            |
|----------------------------------|----------------------|--------------------|
| Refractive index                 | 2.07                 | 1.45               |
| Poisson Ratio                    | 0.23                 | 0.17               |
| Young's Modulus (Pa)             | $1.4 \times 10^{11}$ | $7 \times 10^{10}$ |
| Loss Angle ( $\phi_B = \phi_S$ ) | $2 \times 10^{-4}$   | $4 \times 10^{-5}$ |

G. M.Harry et al., Class. Quantum Grav. 19, 897 (2002)

Red: Tantala. Blue:Silica. Bulk in dotted lines and shear in dashed lines

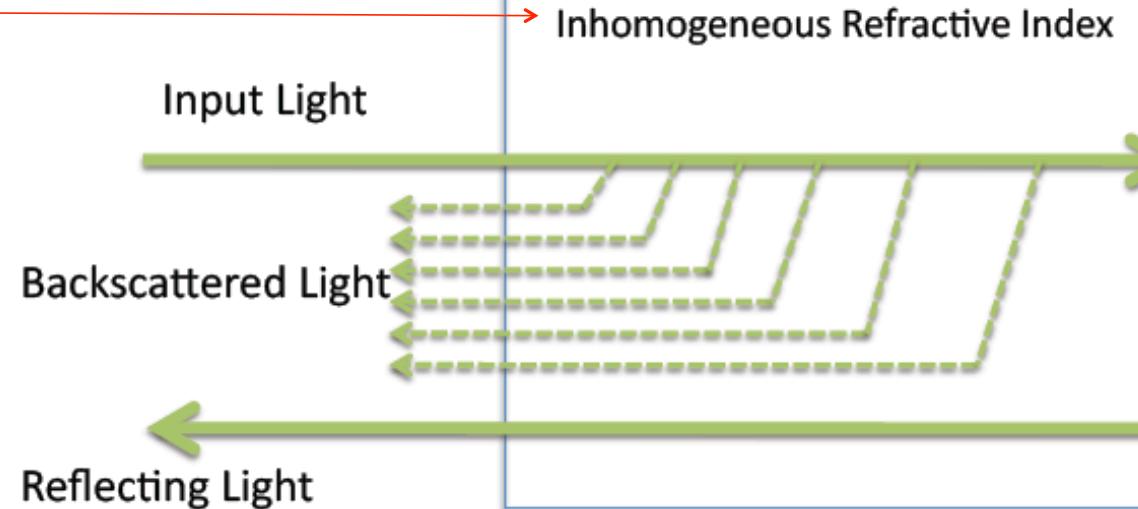
# Thermal Noise Considering Light Penetration



$$\Delta n = -\frac{1}{2} n^3 p_{ij} a_j$$

Photoelastic Effect

Strain Fluctuation

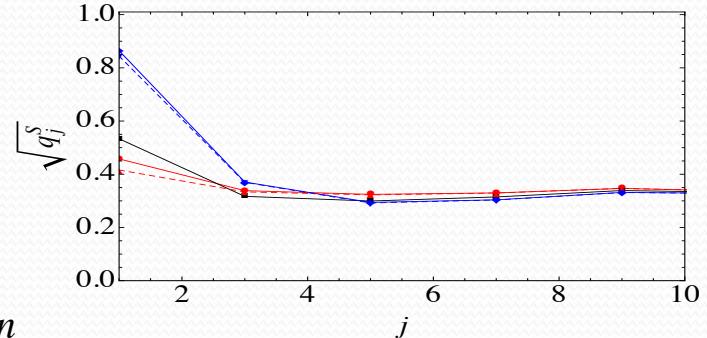
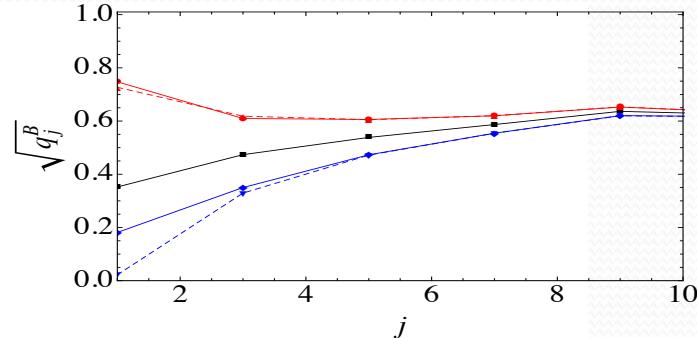


$$\delta\phi_j = k_0 \left[ (n_j + \beta_j) \delta l_j + \left( \frac{1-r_j^2}{2r_j} \beta_j \delta l_j^c - \frac{1+r_{j-1}^2}{2r_{j-1}} \beta_{j-1} \delta l_{j-1}^c \right) \right], \quad \boxed{\delta r_j = k_0 t_j^2 \beta_j \delta l_j^s}$$

$$\begin{aligned} \delta l_j^c &= \int_{\text{layer } j} \frac{\cos(2k_0 n_j z')}{\sin(2k_0 n_j z')} u_{zz}(z') dz' \\ \beta_j &= \frac{\partial n}{\partial u_{zz}} = -\frac{n_j^3}{2} p_{12}^{(j)} \end{aligned}$$

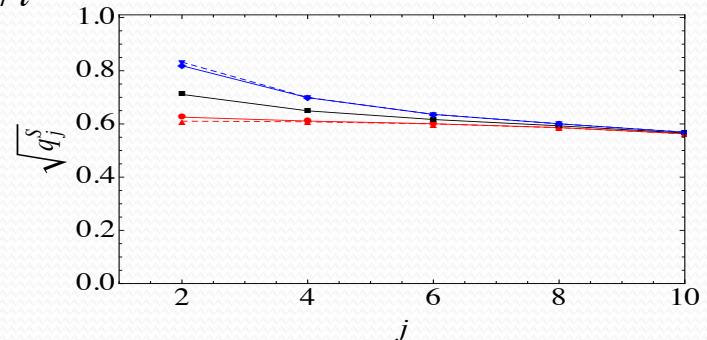
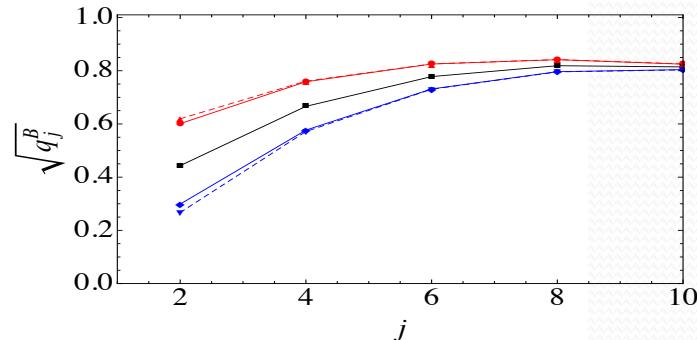
# Coating Brownian Noise: Full Calculation

Silica



$$\beta = \frac{\delta n}{\delta l / l}$$

Tantal  
a



Bulk

Shear

Red for  $\beta=1$ , blue for  $\beta=-1$ , dashed for ignoring back-scattering terms

$$S = \sum_j (q_j^B \phi_B^j + q_j^S \phi_S^j) S_j$$

$$S_j \equiv \frac{4k_B T \lambda_j (1 - \sigma_j - 2\sigma_j^2)}{3\pi f Y_j (1 - \sigma_j)^2 A_{eff}}$$

# Conclusion

- Different components of Coating Brownian Noise
  - Coating-substrate bending is important
  - Back-scattering of light is important when considering light penetration
- Bulk & shear loss angle and their measurement
- Reduce Bending effect: Stiffer Substrate
  - Sapphire? (Reduce noise by factor of 3)
- Optimized coating design based on bulk and shear loss angle measurements