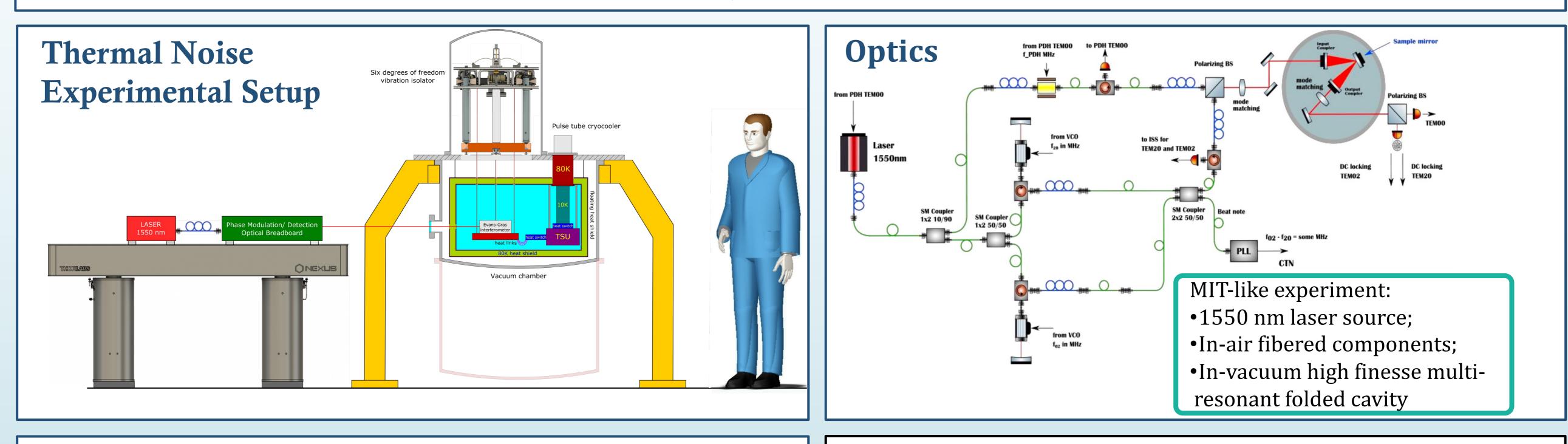
#### Vibration attenuation system for a cryogenic Nikhef **Coating Thermal Noise measurement**

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#### Motivation & goals

- Major improvements in GW instrumentation science are expected from the Thermal Noise (TN) reduction in the mid-frequency range of the detectors, achievable also by cooling down the mirrors to cryogenic temperature. In order to select the coating material that are intended to be used in the 3<sup>rd</sup> generation of detectors, the TN of new coatings should be directly measured using an interferometric method in a cryogenic environment.
- Reduction of local control noise in cryogenic 3<sup>rd</sup> gen. detectors requires new sensors and actuators compatible with low temperature environment. A low noise fast turn around cryogenic test bench would be essential.
- Liquid free low noise cryogenics is more and more required in many fields of fundamental physics. R&D on new low noise technology is of wide interest.



## Cryogenics

- Dual stage cryocooler (CC) to cool the heat-shields (80 K and 4 K) and to charge a **Thermal Storage Unit (TSU)**.
- Ultra-pure Aluminum low stiffness wires heat links.
- CC off during the measurement to avoid vibrations, **TSU used as a heat** sink.

-IFM TSU optics TSU  $[\mathbf{K}]$  $1.5 \leftarrow M_2 \rightarrow 2$  $\leftarrow$  CD<sub>1</sub>  $\rightarrow$  $\leftarrow M_1 \rightarrow 0.5$ Example simulation results 0.5 hour quiet condition to make measurement.

# **Mechanics**

• Vibrations and thermal isolation: the optical bench is suspended by means of three titanium wires.

A cryogenic optical bench with  $\sim 10^{-13} \text{ m}/\sqrt{\text{Hz}}$  residual motion above 30 Hz.

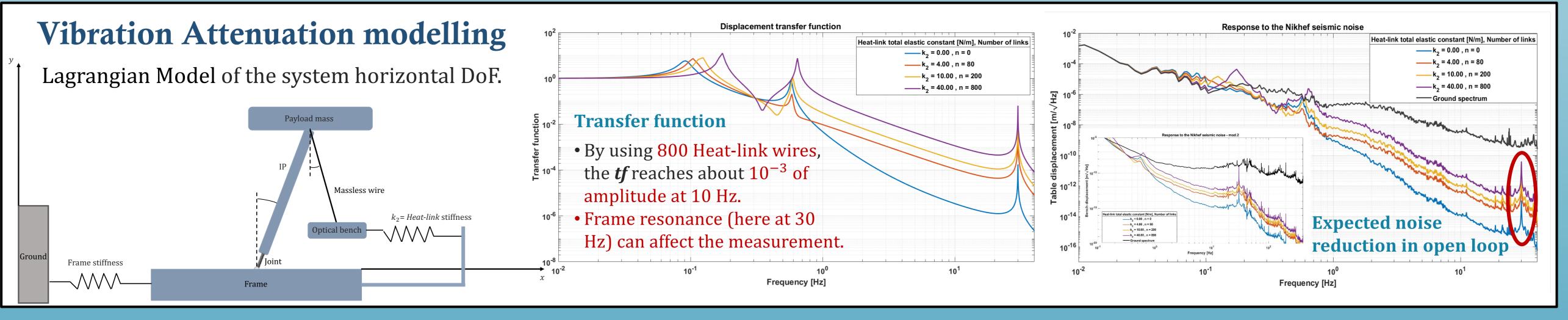
- Vertical & Tilt vibration isolation: each wire is connected to a pair of blade springs in Geometric Anti Spring (GAS) configuration located on the top platform. All three rigid body modes below **0.3 Hz**.
- Horizontal isolation: Three inverted pendulum (IP) legs support the top platform. Translational modes at ~0.1 Hz and the yaw mode at 0.5 Hz.

#### **Sensors and Actuators**

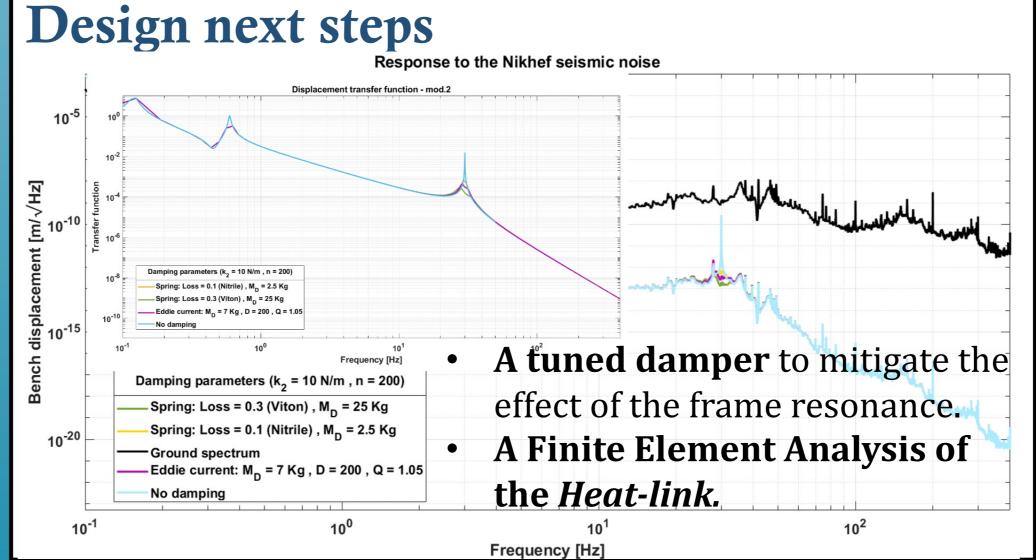
- Three horizontal and three vertical LVDT displacement sensors at the top platform level.
- Tri-axial seismometer "Trillium 120" at the center of the top platform inside a vacuum pod.
- Three Maxwell-pair actuators collocated to the horizontal LVDTs.
- Three voice-coil actuators collocated to the vertical LVDTs.

## **Control strategy**

- NO sensors and actuators inside the cryostat.
- Horizontal DoFs controlled by a super-sensor LVDT+Seismometer.
- Yaw DoF controlled only by LVDTs.
- Vertical, Pitch and Roll controlled by sensor corrected LVDTs.



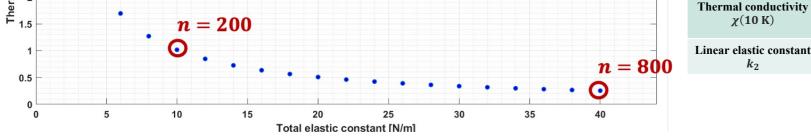
#### **Heat-links Stiffness and Thermal Resistance** ness and modal shapes (FEM Two competing requirements from modal FEM [ZH∕∕ш] • Thermal resistance should be minimized. Fin-plan • Stiff heat-links can spoil the measurement. n = 40 $\odot$ Attenuation of $\sim 10^{-4}$ at 10 Hz by using $\sim 200$ *Heat-links* with the cryostat temperature n = 80 within 1 K even with 1 W heat load. $\frac{20000 \frac{W}{m * K}}{(KAGRA)}$



#### Conclusion

Using **200** *heat-links* seems the best compromise up to now:

•Vibration attenuation @ 10 Hz: ~3000 • $R_T = \frac{l}{\gamma sn} \approx 1 \frac{K}{W} @ 10 K$ • $\Delta T_{bench-battery} \sim 1$  K even by applying 1 W of power.



es 2.5



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