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# SAMARA

Superconducting Alternative Materials  
for Accelerating cavities and  
haloscope Resonators for Axions



# Role in the project and Status

## WP2 – SRF in extreme conditions

WP2: SRF in extreme conditions

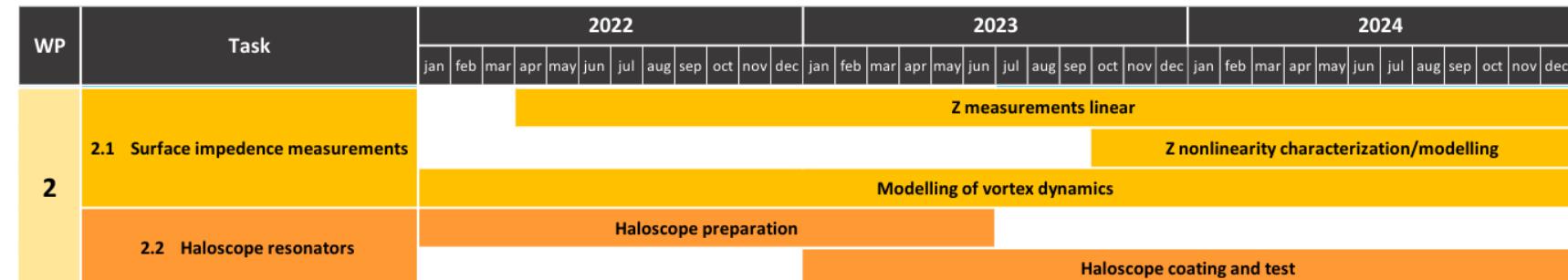
Task 2.1 Surface impedance measurements	
Sample coatings: NbTi and Nb <sub>3</sub> Sn	LNL
Dielectric-loaded resonators measurements	RM3
Patterned coplanar waveguide resonator measurements	TO
Multi-harmonic susceptibility	LNF
Physical Modelling	RM3, TO
Nonlinearity studies	TO, RM3
Task 2.2 Haloscope resonators	
Haloscope design and production	LNF
Haloscope deposition	LNL
Haloscope measurement	LNF

## Proposed Milestones 2022

First surface impedance measurements on  
NbTi and Nb<sub>3</sub>Sn films on insulating substrates

- ΔZ measurements on 2 NbTi samples
- T range 4-15 K
- H range <1.2 T (⊥ and // )

## GANTT



## Budget 2022

- ✓ - 500 l LHe acquired ( $\approx$  1<sup>st</sup> year budget)
- acquired additional 1.5 k€

# Outline

- The measurand: surface impedance in the mixed state
- The experimental technique
- Measurements & preliminary results

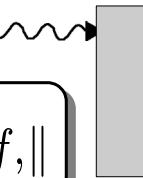
# Surface impedance

# Surface impedance - introduction

- Electrodynamic response at high frequency: surface impedance

At the surface:

$$\mathbf{E}_{rf,\parallel} = Z_s \hat{\mathbf{n}} \times \mathbf{H}_{rf,\parallel}$$



$$Z_s = R_s + iX_s$$

losses + screening

- $Z_s$ : “performance” of microwave cavities

$$Q = \frac{2\pi\nu_0 W}{P_{diss}}$$

quality factor

$$\frac{1}{Q} = \frac{R_s}{G}$$

dissipation

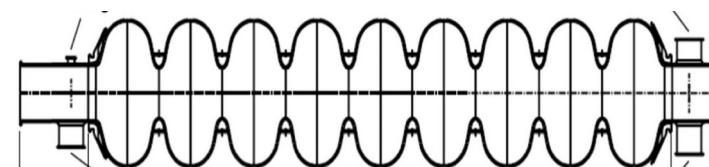
W: stored energy  
 $P_{diss}$ : dissipated power  
G: geometrical factors  
(computed | calibrated)



NbTi haloscope

Alesini et al.  
Phys. Rev. D 99  
101101(R) (2019)

$R_s(H) \Rightarrow Q \Rightarrow$  Axion signal  
(linear regime)



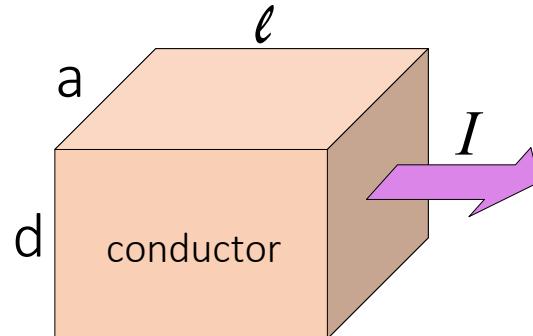
9-cell TESLA-type accelerating cavity  
H. Padamsee,  
Supercond. Sci. Technol. 30,  
053003 (2017)

$R_s(H_{rf}) \Rightarrow Q \Rightarrow E_{acc}$   
(non linear regime)

- $Z_s$ : probe for basic properties  $\rightarrow$  input to theory and material engineering

# Surface impedance

d.c. regime, normal conductor



Ohm laws

$$P_{diss} = RI^2 = \rho \frac{l}{ad} I^2$$

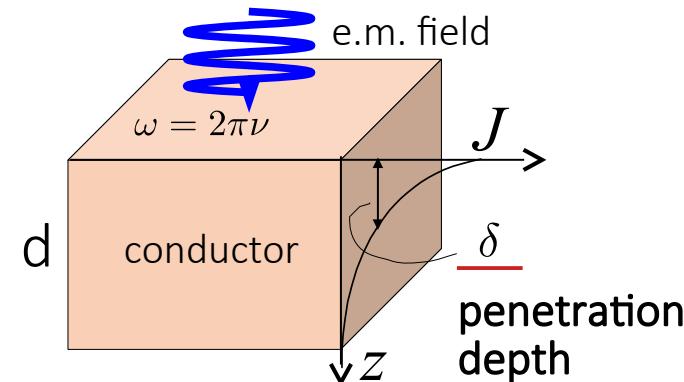
$$\frac{P_{diss}}{\square} = \rho \frac{l}{ad} I^2 \frac{1}{al}$$

$$\frac{P_{diss}}{\square} = R_s J_s^2$$

$$R_s = \frac{\rho}{d} \quad \text{sheet resistance}$$

$$J_s = \frac{I}{a} \quad \text{surface current density}$$

high frequency  $\nu$ , normal conductor



-  $J(z)$  attenuated along **skin depth**:

$$\delta = \sqrt{\frac{2\rho}{\omega\mu_0}} , \quad \rho \quad \text{real}$$

- surface resistance:

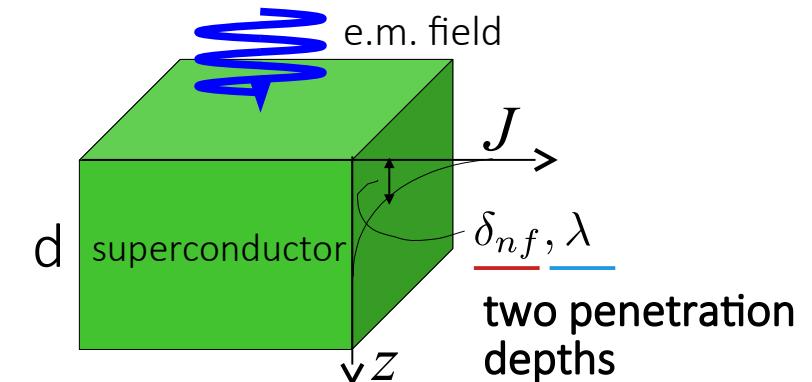
$$R_s = \frac{\rho}{\delta} \quad \text{dissipation}$$

- surface impedance:

$$Z_s = \sqrt{i\omega\mu_0\rho} = R_s + iX_s$$

(bulk limit:  $\delta \ll d$  )

high frequency, superconductor,  $H=0$



- complex  $\rho$ , two fluid model:

$$\tilde{\rho}^{-1} = \sigma_{2f} = \sigma_{nf} - i \frac{1}{\omega\mu_0\lambda^2} , \quad \delta_{nf} = \sqrt{\frac{2\rho_{nf}}{\omega\mu_0}}$$

**normal fluid skin depth**

- (bulk) surface impedance:

$$Z_s = \sqrt{i\omega\mu_0\tilde{\rho}}$$

**London penetration depth**

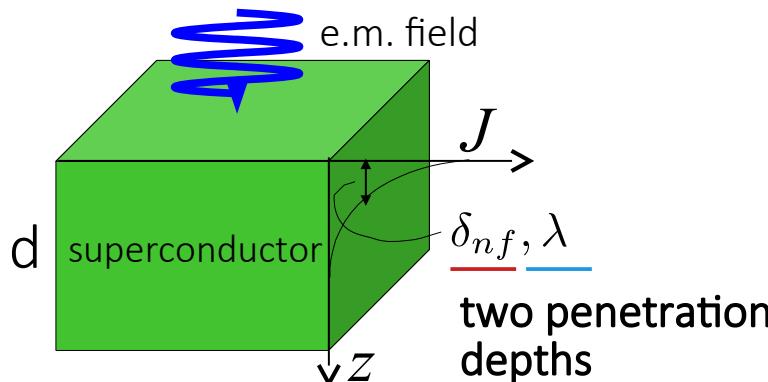
(bulk limit:  $(\delta_{nf}, \lambda) \ll d$  )

- actual surface resistance for SRF:

$$R_s = \text{Re}(Z_s)_{(BCS)} + R_{res} + R_{fl}$$

# Surface impedance in superconductors

high frequency, superconductor,  $H=0$



$$\delta_{nf} = \sqrt{\frac{2\rho_{nf}}{\omega\mu_0}}$$

normal fluid skin depth

$$\lambda$$

London penetration depth

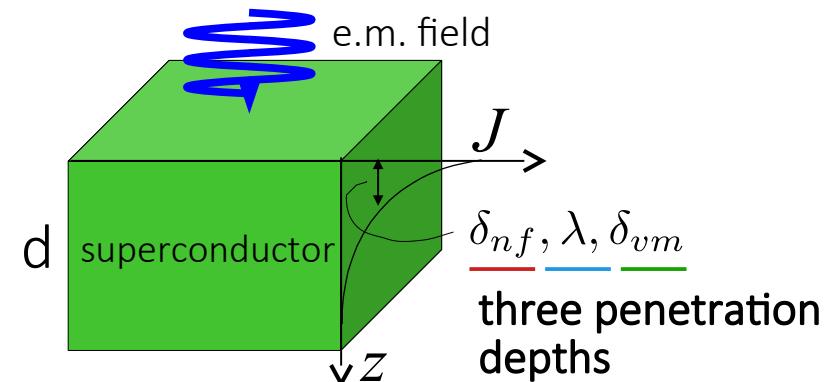
- (bulk) surface impedance:

$$Z_s = \sqrt{i\omega\mu_0\tilde{\rho}}$$

(bulk limit:  $(\delta_{nf}, \lambda) \ll d$ )

Coffey and Clem, Phys. Rev. Lett. 67 386 (1991)

high frequency, superconductor, mixed state



- complex  $\rho$ : two fluid  $\sigma_{2f}$  + **vortex motion**  $\rho_{vm}$

$$\tilde{\rho} = \frac{\rho_{vm} + i\omega\mu_0\lambda^2}{1 + i\sigma_n\omega\mu_0\lambda^2}$$

- additional penetration depth:

$$\delta_{vm} = \sqrt{\frac{2\rho_{vm}}{\omega\mu_0}}$$

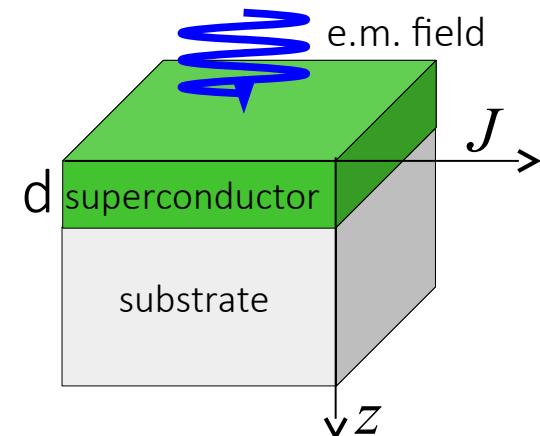
Vortex motion penetration depth

- overall complex penetration depth:

$$\tilde{\lambda}^2 = \frac{\lambda^2 - \frac{i}{2}\delta_{vm}^2}{1 + 2i\frac{\lambda^2}{\delta_{nf}^2}}$$

complex interplay  
 $|\tilde{\lambda}| > \lambda$

finite thickness effects



- $d \sim (\delta_{nf}, \lambda, |\delta_{vm}|)$   
→ rf fields reach the substrate  
→ **effective**  $Z_s$  depends on both SC and substrate

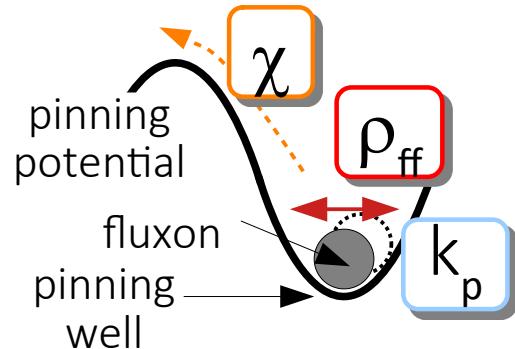
Pompeo et al, IEEE Trans. App. Supercond. 5 8003405 (2019)  
Pompeo et al, I2MTC 2017 Conf. Proceedings

- thin film approx:

$d \ll (\delta_{nf}, \lambda, |\delta_{vm}|)$   
insulating substrate

$$Z_s = \frac{\tilde{\rho}}{d}$$

# High frequency vortex motion response



$$\mathbf{J} \times \Phi_0 - \eta \dot{\mathbf{u}} - k_p \mathbf{u} + \mathbf{F}_{thermal} = m \ddot{\mathbf{u}}$$

$$\rightarrow \mathbf{E}_{rf} = \mathbf{B} \times \dot{\mathbf{u}} \Rightarrow \rho_{vm}$$

Many models,  
one equation

Pompeo, Silva, PRB 78 , 094503 (2008)

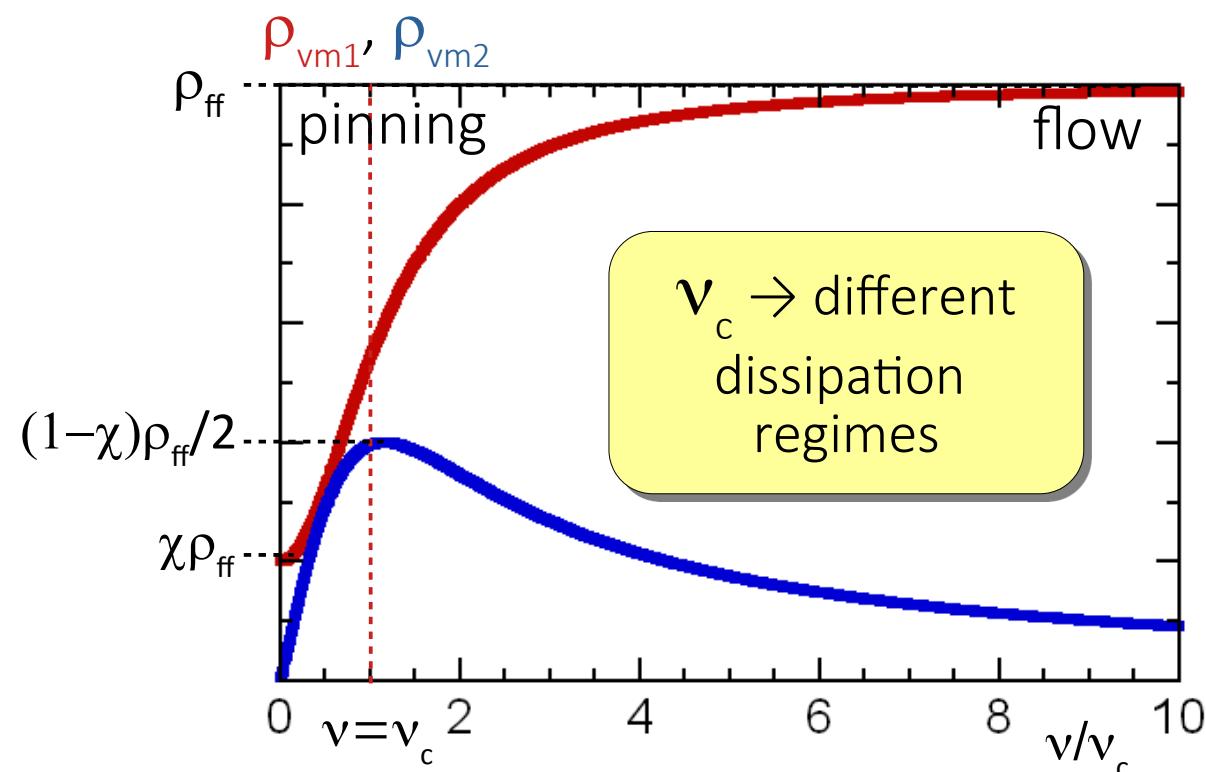
Gittleman, Rosenblum PRL 16 734 (1966)

No creep Coffey, Clem PRL 67 386 (1991) Sinusoidal potential

Brandt PRL 67 2219 (1991) Thermally relaxing pinning

Placais et al PRB 54 13083 (1996) Two-modes

$$\rho_{vm} = \rho_{vm1} + i\rho_{vm2} = \rho_{ff} \frac{\chi + i\nu/\nu_c}{1 + i\nu/\nu_c}$$



flux flow resistivity  $\rho_{ff}$   
(viscosity  $\eta$ )

$$\rho_{ff} = \alpha \rho_n \frac{B}{B_{c2}}$$

characteristic freq.  $\nu_c$   
pinning freq.  $\nu_p$

$$\nu_c \xrightarrow{\chi \rightarrow 0} \nu_p$$

pinning constant  $k_p$

$$k_p = 2\pi \nu_p \eta$$

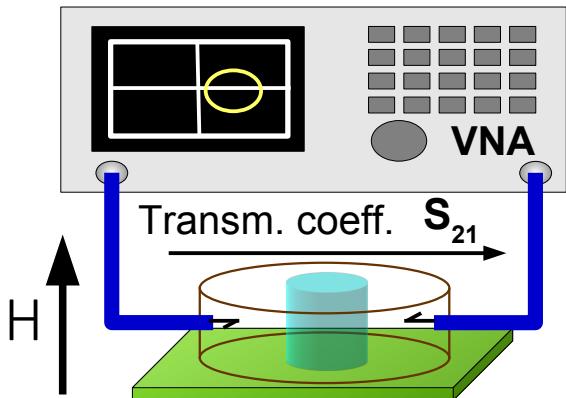
creep factor  $\chi$

$$\text{related to pinning barriers heights } U_0 \\ 0 \leq \chi \leq 1$$

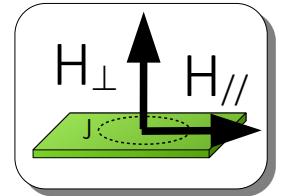
# Experimental technique

# Measurement technique

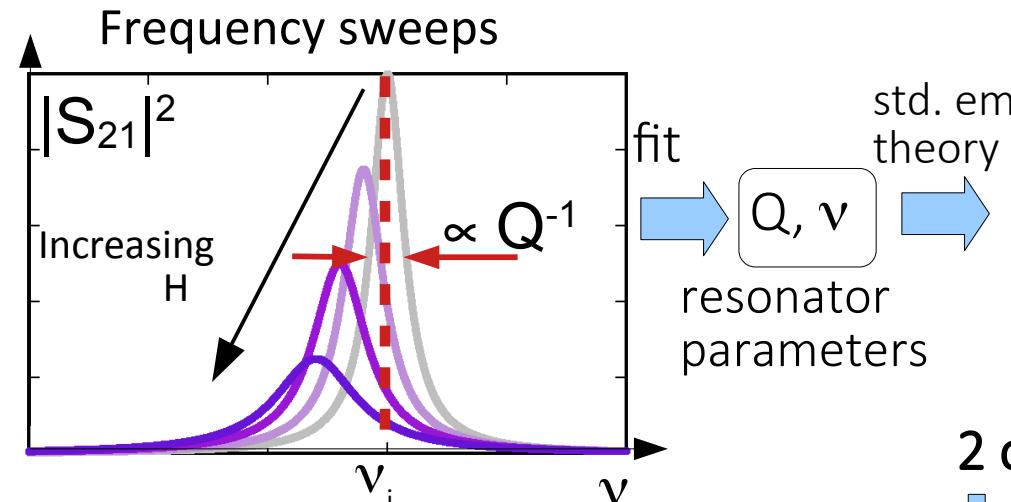
Dielectric-loaded resonator (surface perturbation method).



- dual frequency operation:  
 $\nu_1=16.5 \text{ GHz}$ ,  
 $\nu_2=26.7 \text{ GHz}$



- Rotatable H
- $0 < \mu_0 H < 1.2 \text{ T}$



H-induced variations:

$$\Delta R_s(H) = G \left( \frac{1}{Q(H)} - \frac{1}{Q(0)} \right)$$

$$\Delta X_s(H) = -2G \frac{\nu(H) - \nu(0)}{\nu(0)}$$

2 observables vs many parameters

↳ Multifrequency (rarely performed)

$$\Delta Z_s(H) \rightarrow \rho_{vm}$$

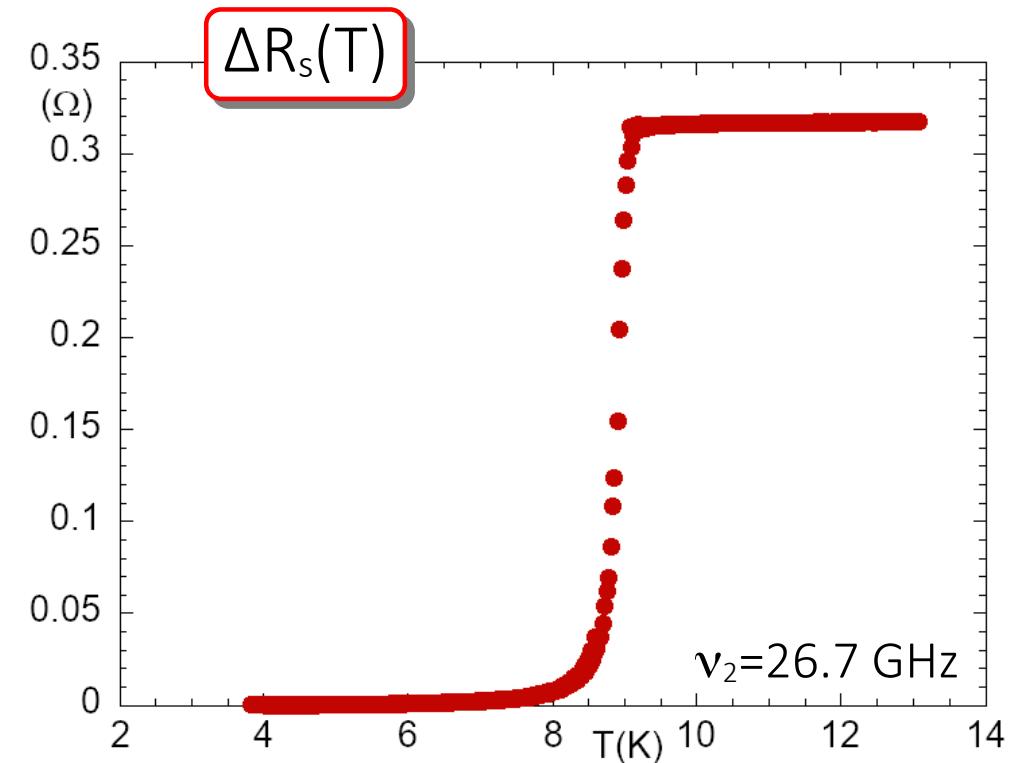
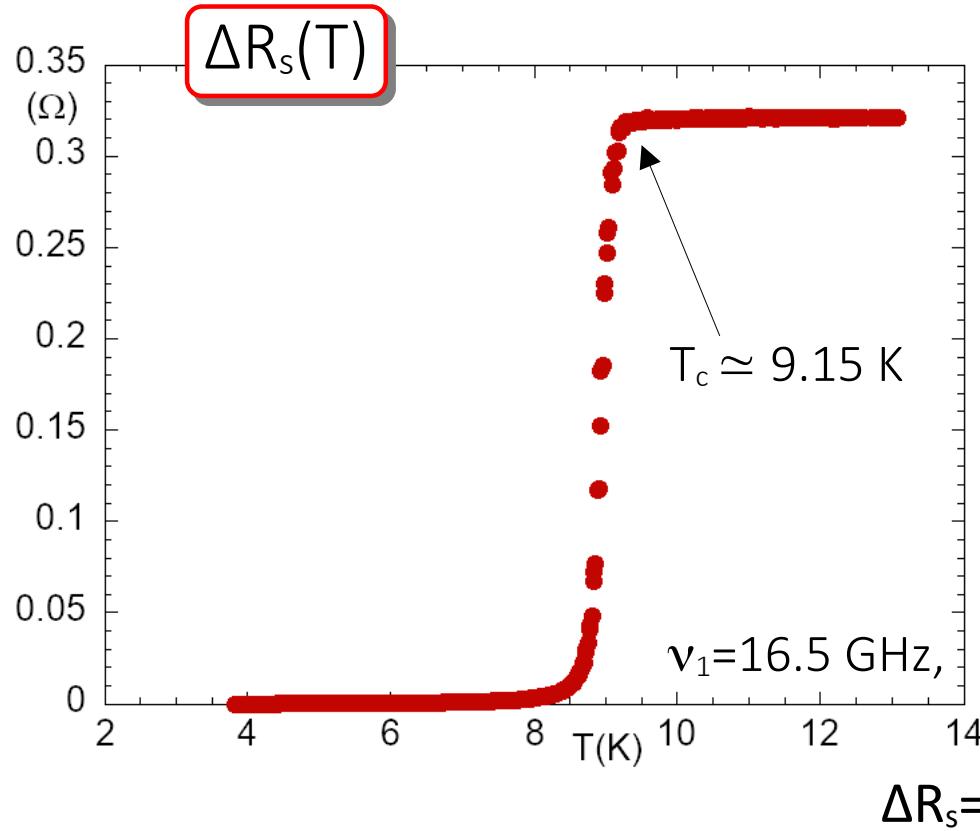
Various limits:

- thin film on insulator  $Z_s \propto \rho$
- bulk  $Z_s \propto \sqrt{\rho}$
- film on metal & thick film  $Z_s(\rho)$

# Measurements and preliminary analysis

# Superconducting transition

- Nb<sub>60</sub>Ti<sub>40</sub> films on dielectric ( $d \simeq 1.7 \pm 0.2 \mu\text{m}$  thick) - sample 1



$$\Delta R_s = R_s(T) - R_s(T_{\min})$$

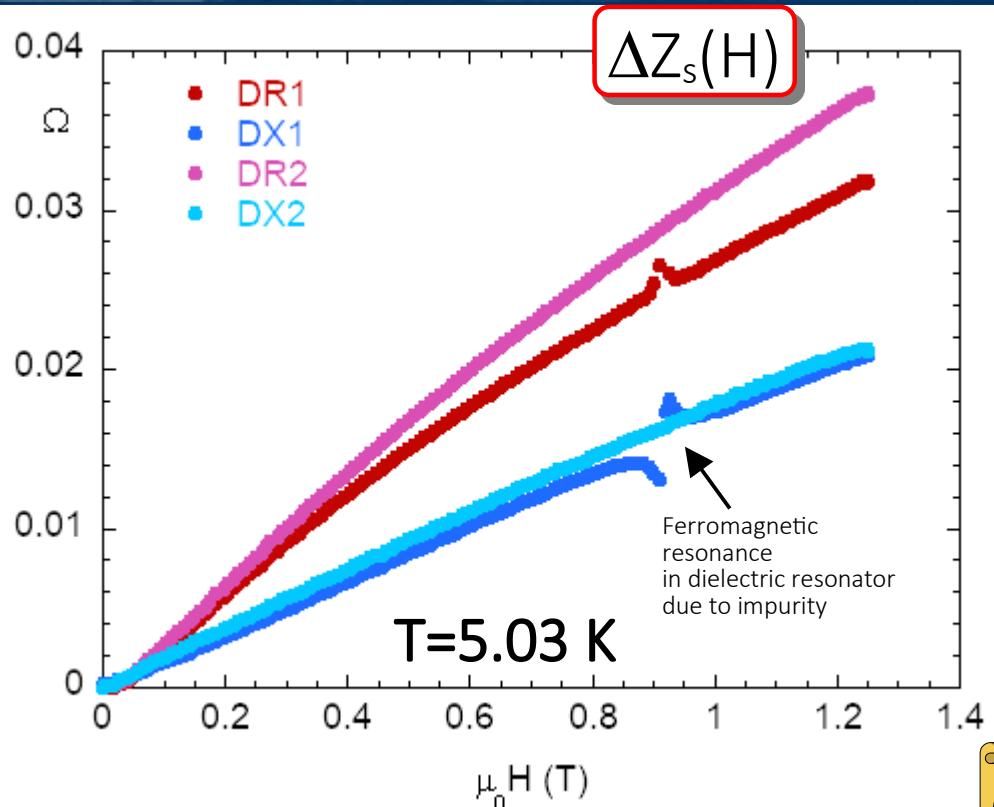
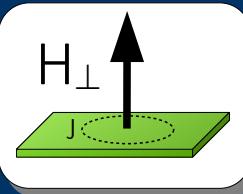
- Normal state resistivity:

$$\rho_n = R_s(T > T_c) \cdot d \simeq 5.4 \cdot 10^{-6} \Omega \cdot m$$

wrt  $(4 \div 7) \cdot 10^{-6} \Omega \cdot m$

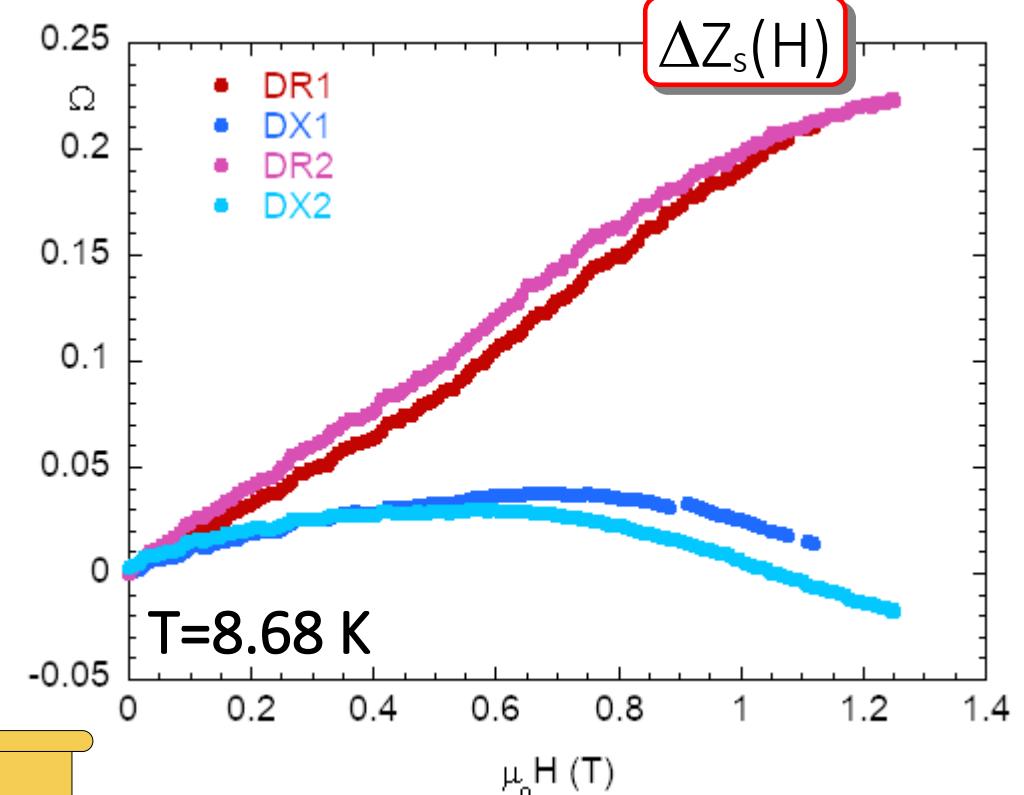
Benvenuti et al, Fifth Workshop RF Supercond. 1991

# $\Delta Z(H)$ at selected $T$



All  $T$  :  $\Delta R$  &  $\Delta X$  increase with  $H$   
 $\rightarrow$  vortex motion

Low  $T$  : downward curvature  
 $\rightarrow$  possible bulk regime

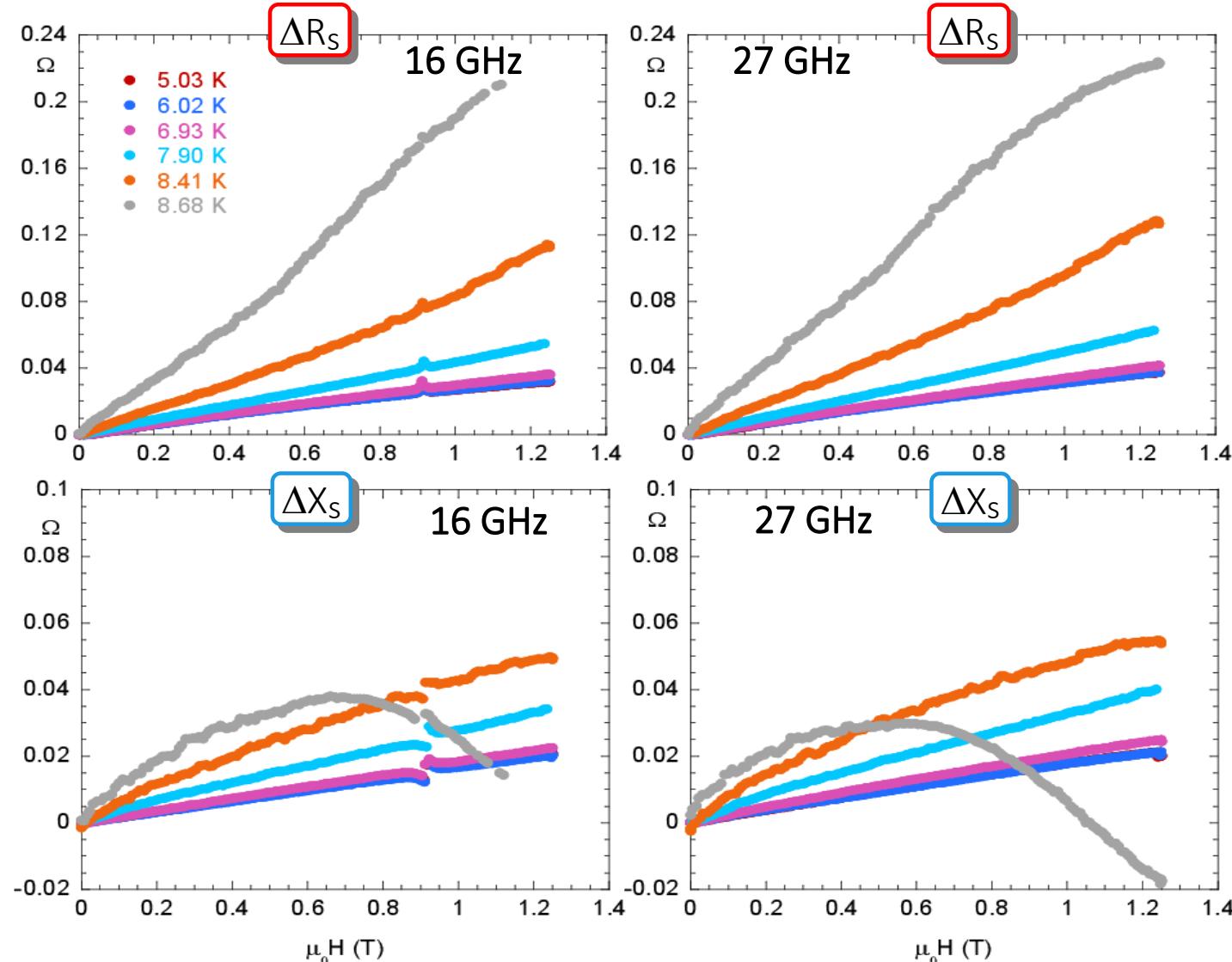
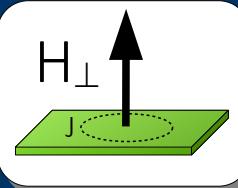


Near  $T_c$  :  $\Delta X < 0$   
 $\rightarrow$  e.m. thin film & 2-fluids contribution

Change in effective regime

by nearing  $H_{c2}(T) \rightarrow$  thin film regime  
 $\rightarrow$  choice of coating thickness in function of  $(H, T, v)$

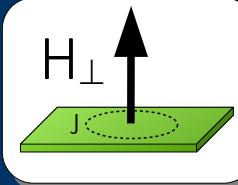
# $\Delta Z(H)$ – temperature evolution



- $\Delta R(H)$  curvature changes with  $T$   
 $\rightarrow$  complex electrodynamics  
 (thermal creep, two fluid,  
 B-dep. vortex parameters)

Focus on low  $T$

# Extraction of vortex parameters



## Fit model

- complex resistivity:

$$\tilde{\rho} = \rho_{ff} \frac{1 + i \frac{\nu_p}{\nu}}{1 + \left(\frac{\nu_p}{\nu}\right)^2} + i \omega \mu_0 \lambda^2(T)$$

$$\rho_{ff} = \alpha \rho_n \frac{B}{B_{c2}(T)} \quad \lambda(T) = \lambda_0 / (1 - (T/T_c)^4)$$

→ two field independent fit parameters:  $\alpha, \nu_p$

Parameters set from other measurements:  $\rho_n, T_c$

Parameters taken from literature:  $B_{c2}(0 \text{ K})$

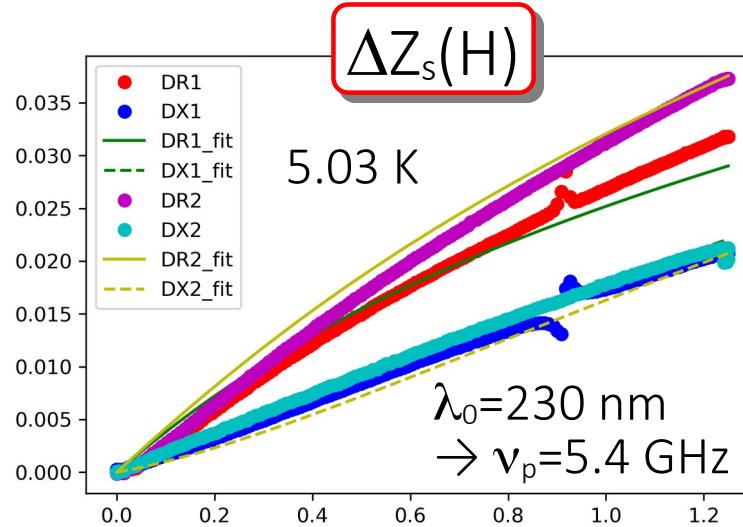
$$\lambda_0 \in [230, 300] \text{ nm}$$

Giordano et al, IEEE Trans. Magn. v. MAG-11 437 (1976)

Benvenuti et al, Fifth Workshop RF Supercond. 1991

- expression for the **effective** surface impedance  $Z_s$

## model sensitivity on $\lambda_0$

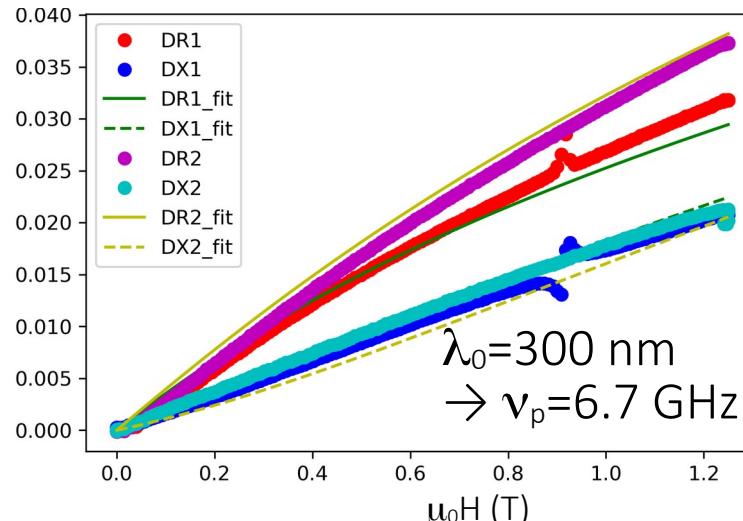


• Robust result  
 $\nu_p \sim 6 \text{ GHz}$

- NbTi coated: ✗
- $\nu_p \sim 44 \text{ GHz}$   
 $\text{@ } 4.2 \text{ K, 0-5 T}$

Di Gioacchino et al.  
IEEE Trans. Appl. Supercond.  
29 3500605 (2019)

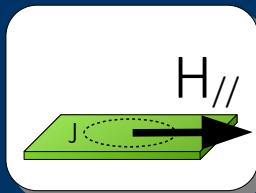
(different H orientation)



- Nb3Sn bulk: ✓
- $\nu_p \sim 7 \text{ GHz}$ ,  
 $\text{@ } 6 \text{ K, 2 T}$

Alimenti et al.  
Supercond. Sci. Technol.  
34 014003 (2021)

# $\Delta Z(H)$ – temperature evolution - $H \parallel ab$

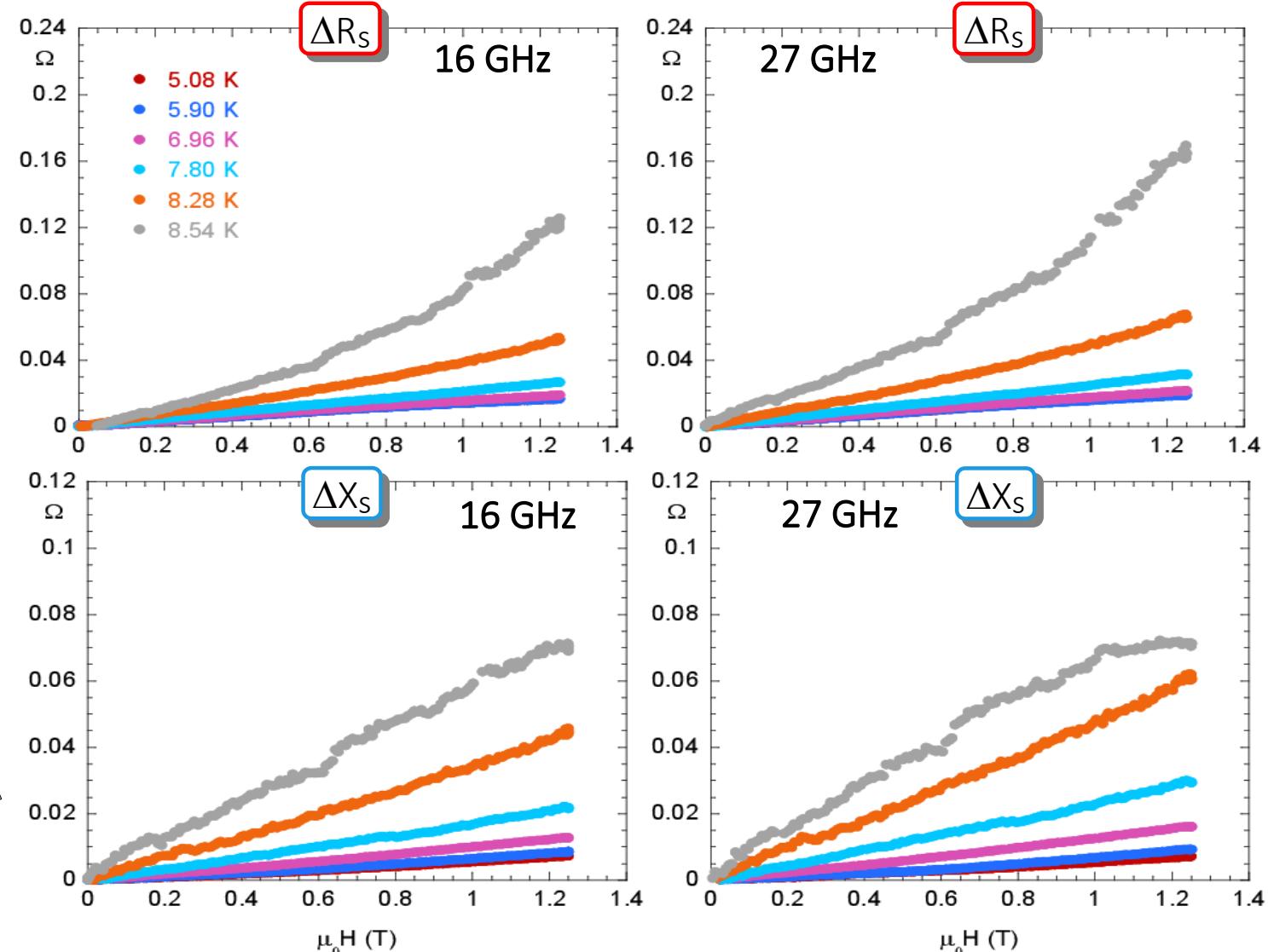


Need for measurements at different  $H$  orientations:  
- haloscopes:  $H \parallel J$

Di Gioacchino et al. IEEE Trans. Supercond. 29 3500605 (2019)  
Alesini et al. Phys. Rev. D 99 101101(R) (2019)  
Alimenti et al Instruments 6 1 (2022)

- typical dielectric resonator setup:  
 $H \perp J$   
→ use of rotatable magnet

Preliminary result:  
 $v_p \approx 5-10$  GHz



# Summary

Preliminary results on NbTi films on insulator at fields < 1.2 T

- Identification of regimes/models for  $Z_s$
- Determination of
  - pinning frequency:  $v_p \sim 6 \text{ GHz}$  at 5 K
  - change in regimes (bulk vs thin film)  $\rightarrow$  coating thickness

Thanks!