

Modeling of JPA

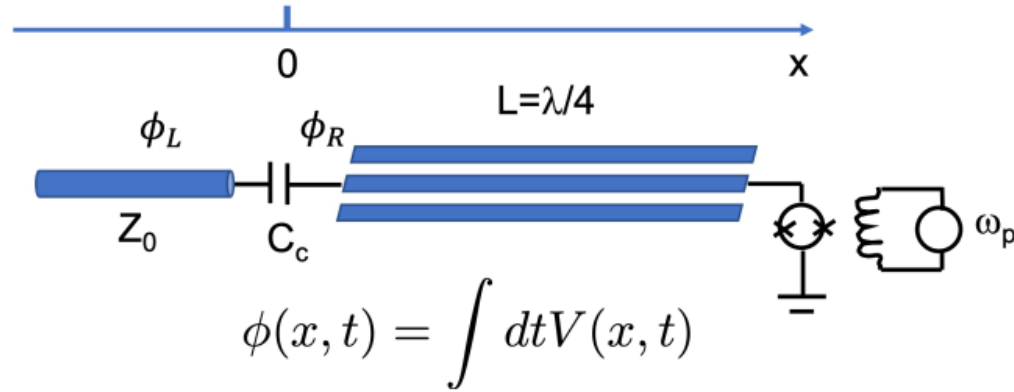
S. Pagano

Dip. Fisica Univ. Salerno

INFN G.C. Salerno

Aim: modelling of a JPA without simplifications of the nonlinear components

Model by Claudio Gatti



The Lagrangian density of the circuit in figure 1 is obtained by the sum of the capacitive energies minus the inductive energies:

$$\begin{aligned} \mathcal{L} = & \left(\frac{1}{2} C_L \dot{\phi}_L^2 - \frac{1}{2L_L} \phi_L^2 \right) \sigma(-x) + \left(\frac{1}{2} C_R \dot{\phi}_R^2 - \frac{1}{2L_R} \phi_R^2 \right) [\sigma(x) - \sigma(x - L)] \\ & + \left(\frac{1}{2} C_c (\dot{\phi}_L - \dot{\phi}_R) \right) \delta(x) + \left[\frac{C_J}{2} \dot{\phi}_J^2 + E_J(\phi_{ext}) \cos \left(2\pi \frac{\phi_J}{\phi_0} \right) \right] \delta(x - L) \end{aligned} \quad (1)$$

where $\phi_{L,R}(x)$ is the flux variable defined as $\phi(x) = \int^t dt' V(t')$ in the left (right) transmission line and $C_{L,R}$ and $L_{L,R}$ are their capacitances and inductances per unit length, and $\phi_J = \phi_R(x = L)$. $\sigma(x)$ is the Heaviside (step) function. The (symmetric) SQUID Josephson energy is:

$$E_J(\phi_{ext}) = 2E_{0J} \cos \left(\pi \frac{\phi_{ext}}{\phi_0} \right) \quad (2)$$

where E_{0J} is the Josephson energy of the single junction.

Wave equations for ϕ_L and ϕ_R

$$\begin{aligned} \sigma(-x) \left[C_L \ddot{\phi}_L - \frac{1}{L_L} \phi_L'' \right] + \delta(x) \left[C_c (\ddot{\phi}_L - \ddot{\phi}_R) + \frac{1}{L_L} \phi_L' \right] &= 0(4) \\ [\sigma(x) - \sigma(x-L)] \left[C_R \ddot{\phi}_R - \frac{1}{L_R} \phi_R'' \right] + \delta(x) \left[-C_c (\ddot{\phi}_L - \ddot{\phi}_R) - \frac{1}{L_R} \phi_R' \right] + \\ \delta(x-L) \left[C_J \ddot{\phi}_R + \frac{1}{L_R} \phi_R' + \frac{2\pi}{\phi_0} E_J(\phi_{ext}) \sin \left(2\pi \frac{\phi_R}{\phi_0} \right) \right] &= 0 \end{aligned}$$

The solution is the sum of an outgoing and an incoming wave

$\phi(x, t) = \phi^{in}(t - x/v_p) + \phi^{out}(t + x/v_p)$ and $v_p = 1/\sqrt{LC}$. The other equations give the boundary conditions:

$$-\frac{1}{L_L} \phi_L' = C_c (\ddot{\phi}_L - \ddot{\phi}_R) \quad (x = 0)$$

$$\phi' = \frac{1}{v_p} (\dot{\phi}^{out} - \dot{\phi}^{in}) \quad \text{in and out fields.} \quad -\frac{1}{L_R} \phi_R' = C_c (\ddot{\phi}_L - \ddot{\phi}_R) \quad (x = 0)$$

$$\dot{\phi} = \dot{\phi}^{in} + \dot{\phi}^{out} \quad C_J \ddot{\phi}_R + \frac{1}{L_R} \phi_R' + \frac{2\pi}{\phi_0} E_J(\phi_{ext}) \sin \left(2\pi \frac{\phi_R}{\phi_0} \right) = 0 \quad (x = L)$$

$$2\ddot{\phi}_R^{in} + \frac{1}{C_c Z_0} \dot{\phi}_R^{in} = \ddot{\phi}_L^{in} + \frac{1}{C_c Z_0} \dot{\phi}_R^{out} \quad (x = 0)$$

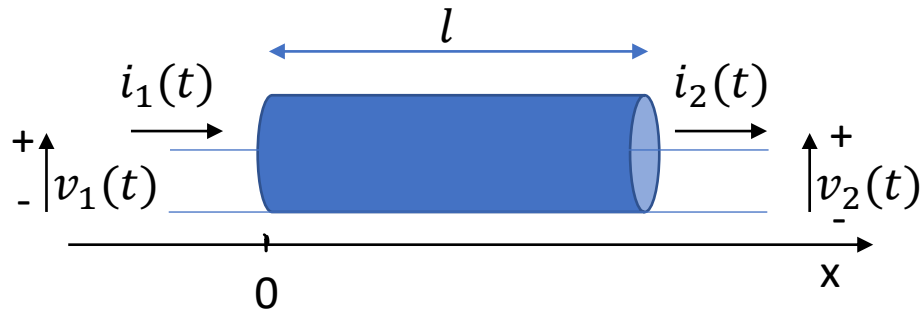
$$C_J \ddot{\phi}_J + \frac{1}{Z_0} \dot{\phi}_J + \frac{2\pi}{\phi_0} E_J(\phi_{ext}) \sin \left(2\pi \frac{\phi_J}{\phi_0} \right) = \frac{2}{Z_0} \dot{\phi}_R^{in} \quad (x = L) \quad \phi_R^{in}(t, x = L) = \phi_R^{in}(t - L/v_p, x = 0)$$

$$\begin{aligned} \phi_R^{out}(t, x = L) &= \phi_R^{out}(t + L/v_p, x = 0) = \phi_J(t) - \phi_R^{in}(t, x = L) \\ &= \phi_J(t) - \phi_R^{in}(t - L/v_p, x = 0) \end{aligned}$$

$$\phi_L^{out} = \phi_R^{out} - \phi_R^{in} + \phi_L^{in} \quad (x = 0)$$

Transient Analysis of Lossless Transmission Lines

Manuscript received July 7, 1967; revised September 8, 1967.



$$\tau = \sqrt{LC} \text{ } l \text{ line delay}$$

$$Z_0 = \sqrt{\frac{L}{C}} \text{ line impedance}$$

$$\Delta e = +Z_0 \Delta i \quad \Delta e = -Z_0 \Delta i$$

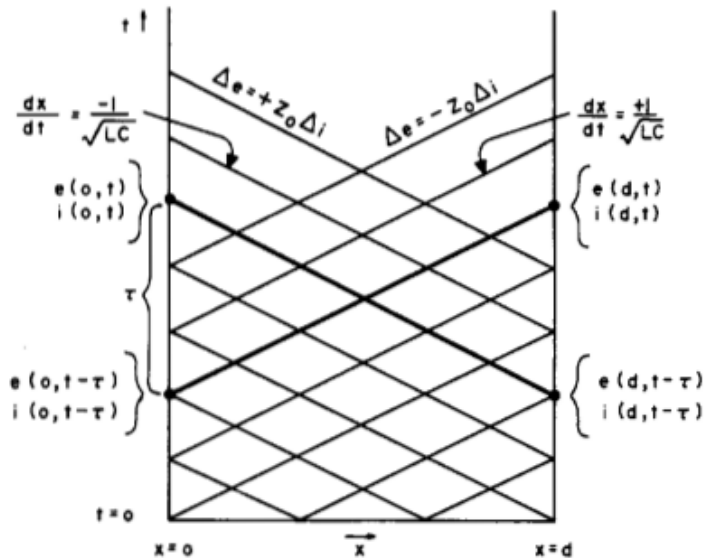


Fig. 1. Characteristic curves for a uniform transmission line.

F. H. BRANIN, JR.
Systems Development Div. Lab.
IBM Corporation
Kingston, N. Y.

$$v = v(x, t) \quad i = i(x, t)$$

$$\begin{aligned} L \frac{\partial i}{\partial t} + \frac{\partial v}{\partial x} &= 0 \\ C \frac{\partial v}{\partial t} + \frac{\partial i}{\partial x} &= 0 \end{aligned} \quad \longrightarrow \quad \begin{aligned} i_{tt} - \frac{1}{LC} i_{xx} &= 0 \\ v_{tt} - \frac{1}{LC} v_{xx} &= 0 \end{aligned}$$

The method of characteristics for solving these equations is based on a transformation in the $x-t$ plane which accomplishes the conversion of (1) and (2) into a pair of ordinary differential equations. Each of these two ordinary differential equations holds true along a different family of characteristic curves in the $x-t$ plane, one family corresponding to the forward or incident wave and the other to the backward or reflected wave. These two families of characteristic curves are, in effect, the basis for a new coordinate system instead of the canonical coordinates $x=\text{constant}$ and $t=\text{constant}$.

$$dx/dt = 1/\sqrt{LC} \quad \text{and} \quad dx/dt = -1/\sqrt{LC}$$

$$\sqrt{\frac{L}{C}} di + \left(Ri + \sqrt{\frac{L}{C}} Ge \right) dx + de = 0 \quad (3)$$

which holds true only along the *forward* characteristics, defined as $dx/dt = 1/\sqrt{LC}$, and

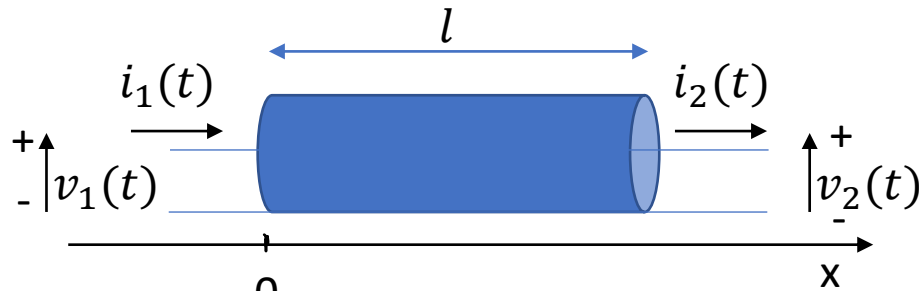
$$-\sqrt{\frac{L}{C}} di + \left(Ri - \sqrt{\frac{L}{C}} Ge \right) dx + de = 0 \quad (4)$$

which holds true only along the *backward* characteristics, defined as $dx/dt = -1/\sqrt{LC}$.

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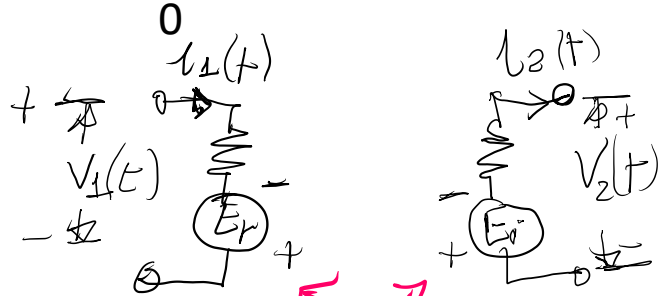
F. H. BRANIN, JR.
Systems Development Div. Lab.
IBM Corporation
Kingston, N. Y.



$$v = v(x, t) \quad i = i(x, t)$$

$$\tau = \sqrt{LC} l \text{ line delay}$$

$$Z_0 = \sqrt{\frac{L}{C}} \text{ line impedance}$$



$$v(l, t) = -Z_0 i(l, t) + [v(0, t - \tau) + Z_0 i(0, t - \tau)]$$

$$v(0, t) = +Z_0 i(0, t) + [v(l, t - \tau) - Z_0 i(l, t - \tau)]$$

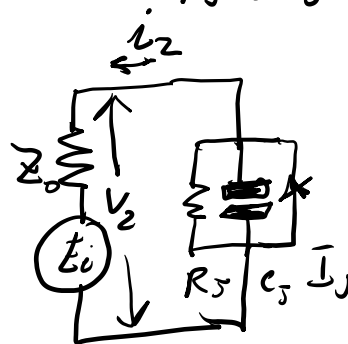
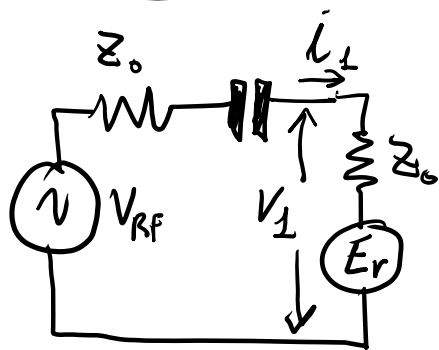
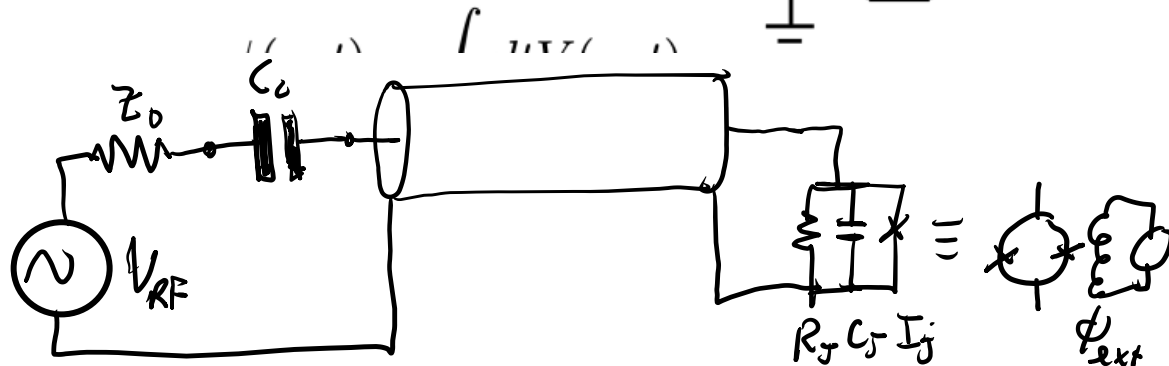
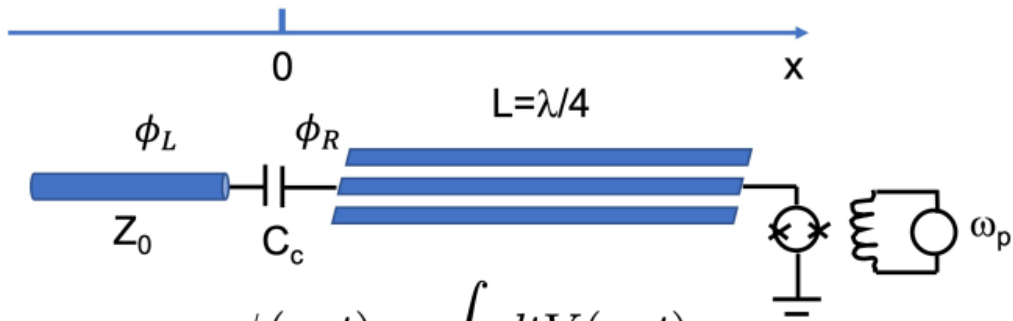
$$v_2(t) = -Z_0 i_2(t) + [v_1(t - \tau) + Z_0 i_1(t - \tau)]$$

$$v_1(t) = +Z_0 i_1(t) + [v_2(t - \tau) - Z_0 i_2(t - \tau)]$$

$$\begin{cases} v_2(t) = -Z_0 i_2(t) - E_i(t - \tau) \\ v_1(t) = +Z_0 i_1(t) - E_r(t - \tau) \end{cases}$$

$$E_i(t) = -[2v_1(t) + E_r(t - \tau)]$$

$$E_r(t) = -[2v_2(t) + E_i(t - \tau)]$$



In our case we have:

$$\begin{aligned}\dot{v}_1 &= -\frac{1}{2 C_c Z_0} v_1 + \frac{1}{2} \dot{v}_{rf}(t) - \frac{1}{2} \dot{E}_r(t - \tau) - \frac{1}{2 C_c Z_0} E_r(t - \tau) \\ \dot{v}_2 &= -\left(\frac{1}{C_j Z_0} + \frac{1}{C_j R_j}\right) v_2 - \frac{2 I_j}{C_j} \cos\left(2\pi \frac{\phi_{ext}}{\phi_0}\right) \sin \varphi - \frac{1}{C_j Z_0} E_i(t - \tau) \\ \dot{\varphi} &= \frac{2 e}{\hbar} v_2\end{aligned}$$

where

$$\dot{v}_{rf}(t) = v_{rf} \omega \cos \omega t$$

$$\phi_{ext}(t) = \phi_{ext} \cos \omega_p t$$

$$Z_0 = 50 \Omega$$

$$\tau = \frac{T}{4} = \frac{\pi}{2 \omega}$$

We start with E_i and E_r set to zero

The values of E_i and E_r are updated during the integration according to:

$$E_i(t) = -[2v_1(t) + E_r(t - \tau)]$$

$$E_r(t) = -[2v_2(t) + E_i(t - \tau)]$$

Next step is to integrate the system and do some checks with published data