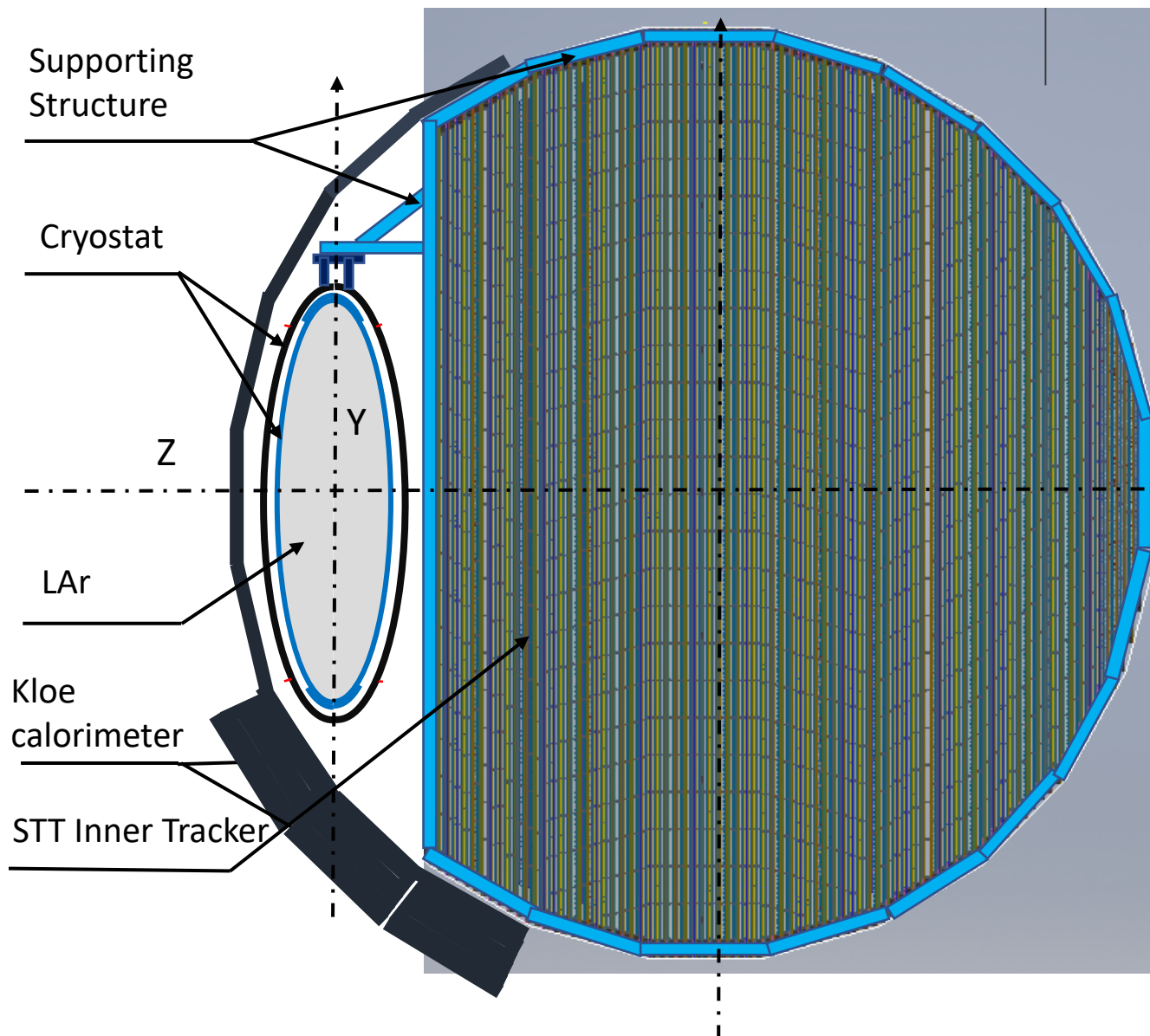


# GRAIN Inside SAND



GRAIN :  
Granular Argon for Interaction  
Of Neutrinos

LAr Cryostat  $V = 0,7 \text{ m}^3$  min

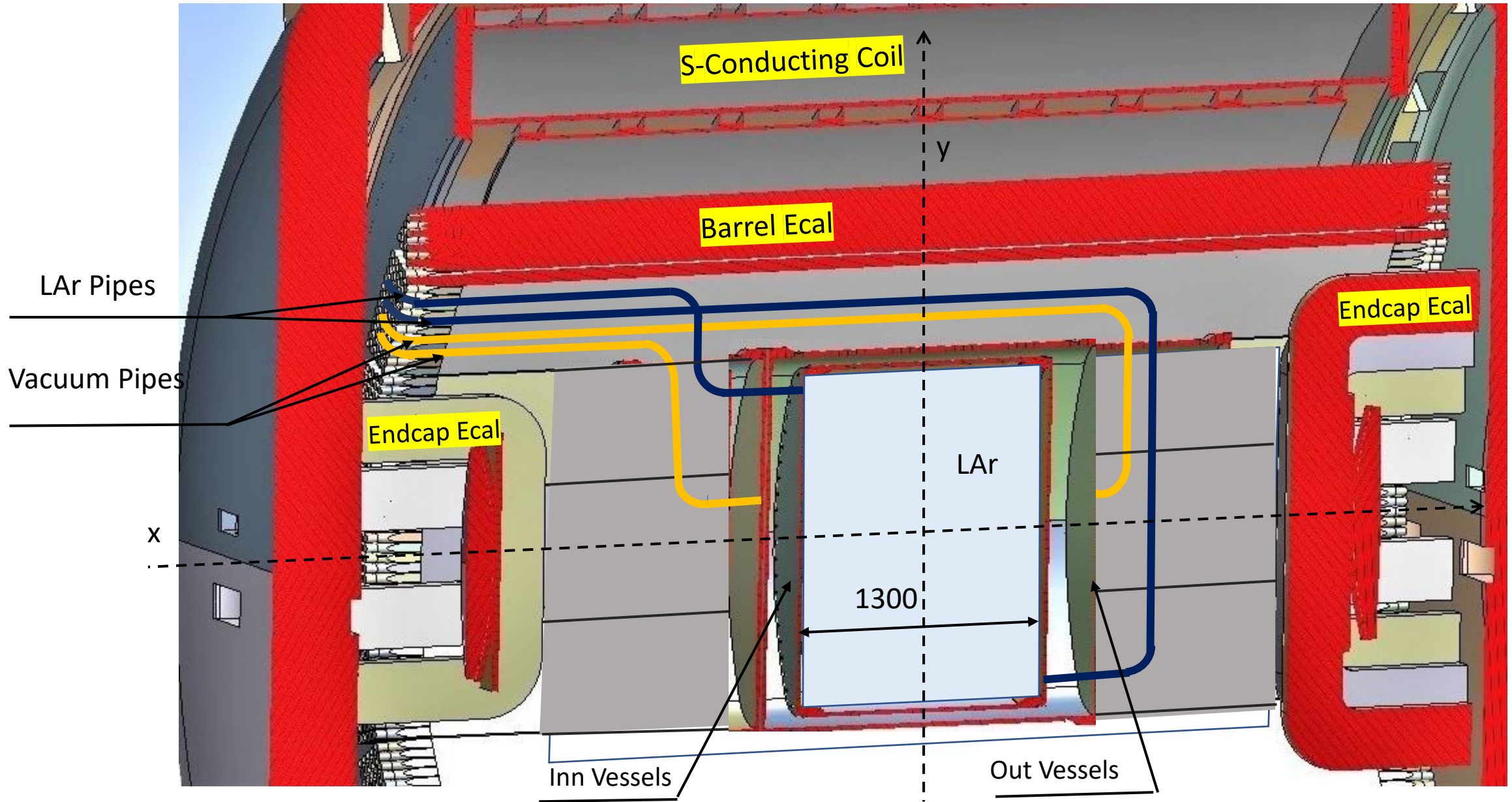
Sup insulated and vacuum

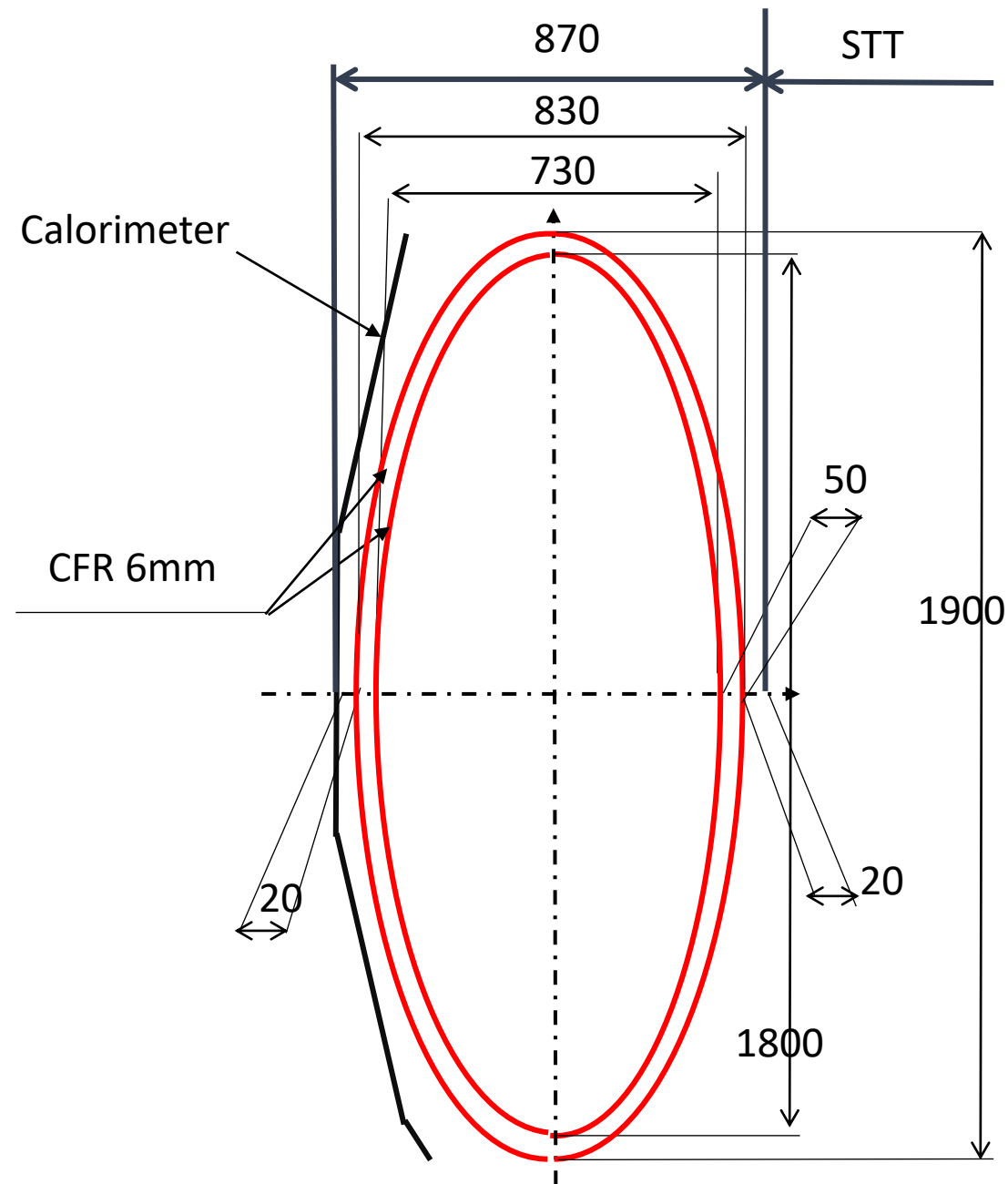
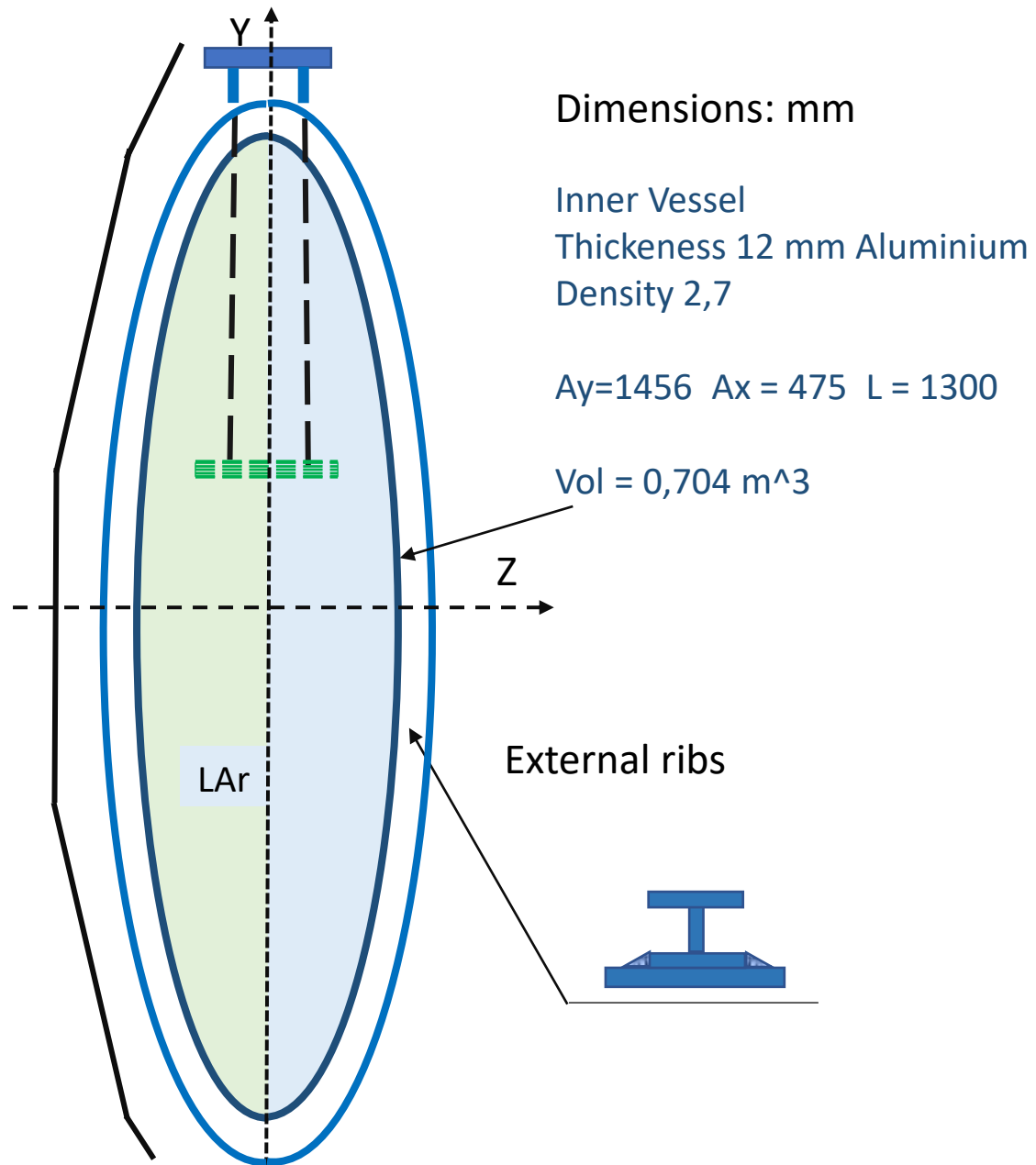
As **Thin** as possible

Not too large in Z

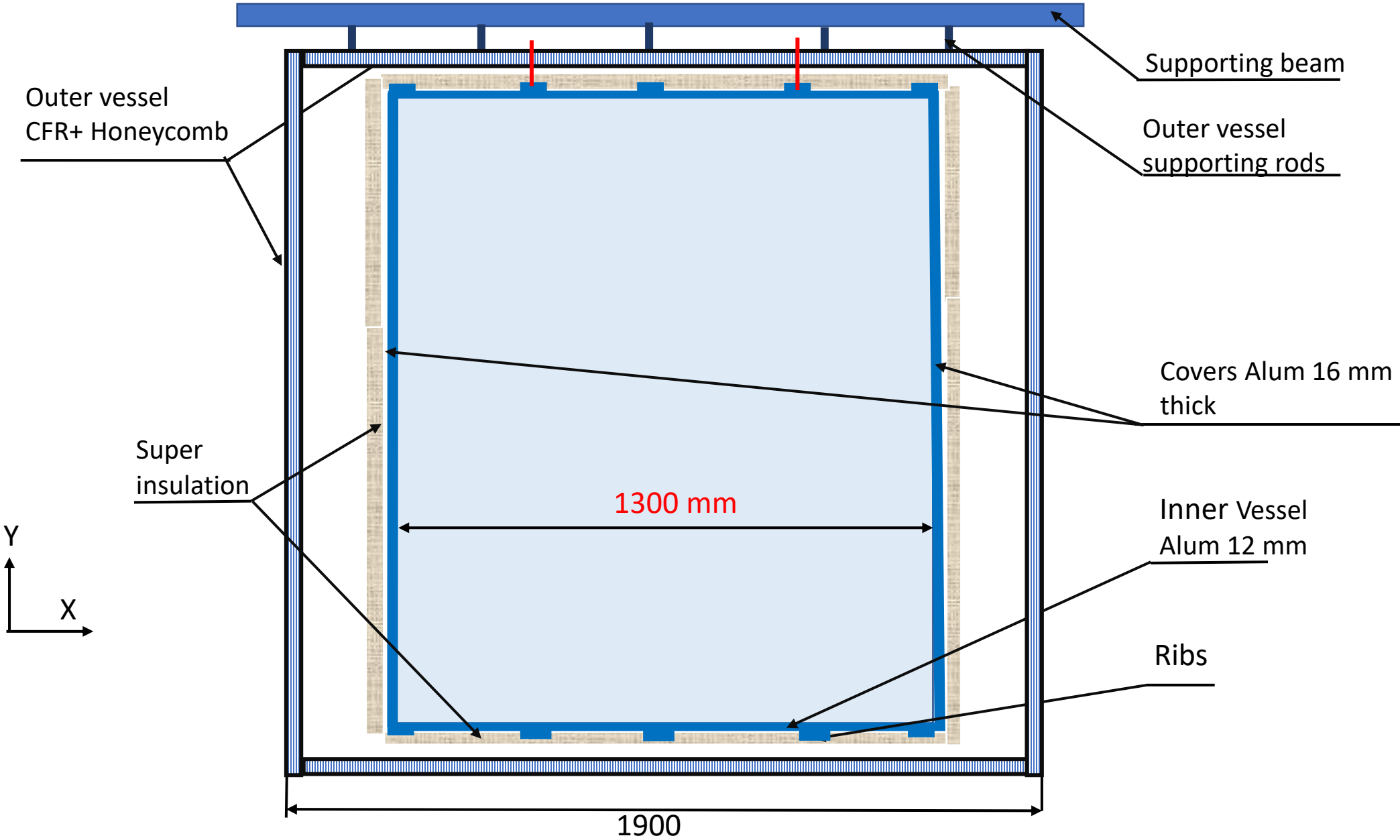
Openable ( detectors inside)

GRAIN inside SAND

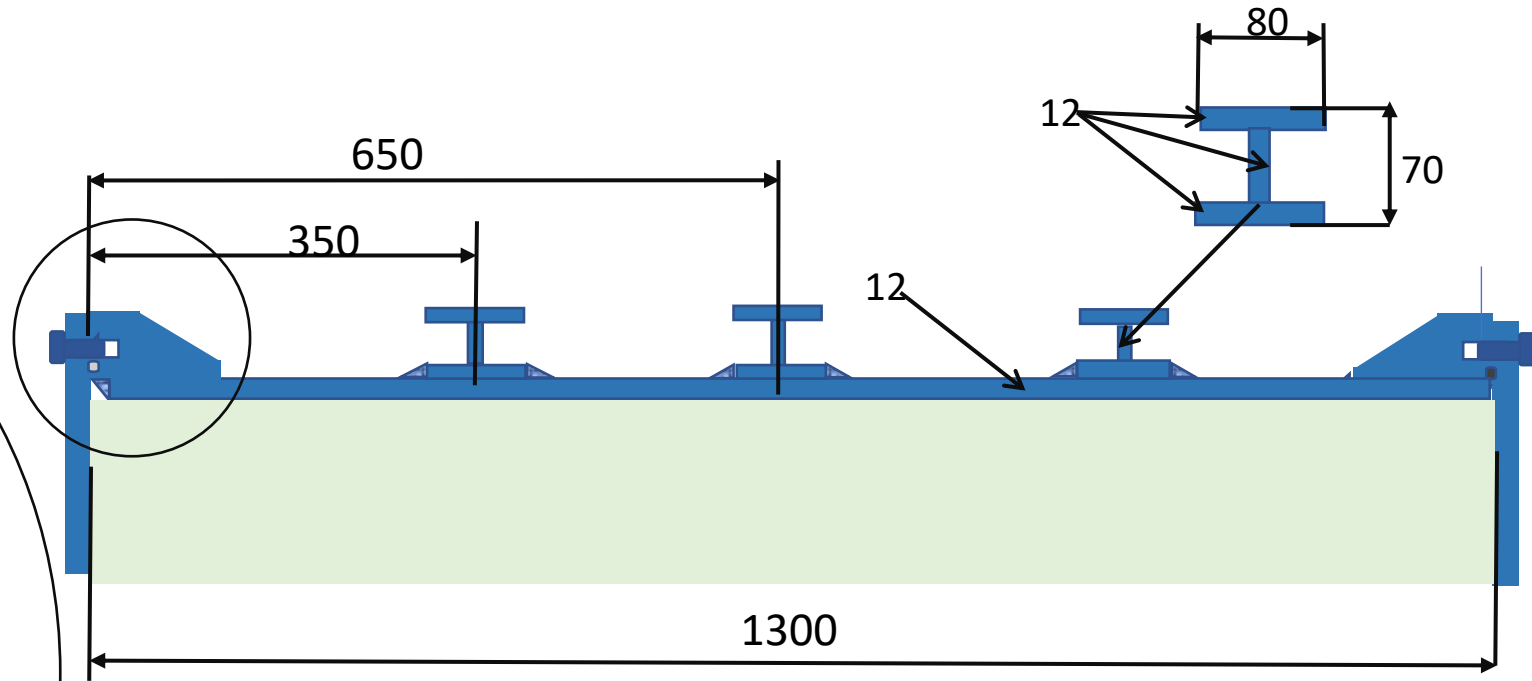
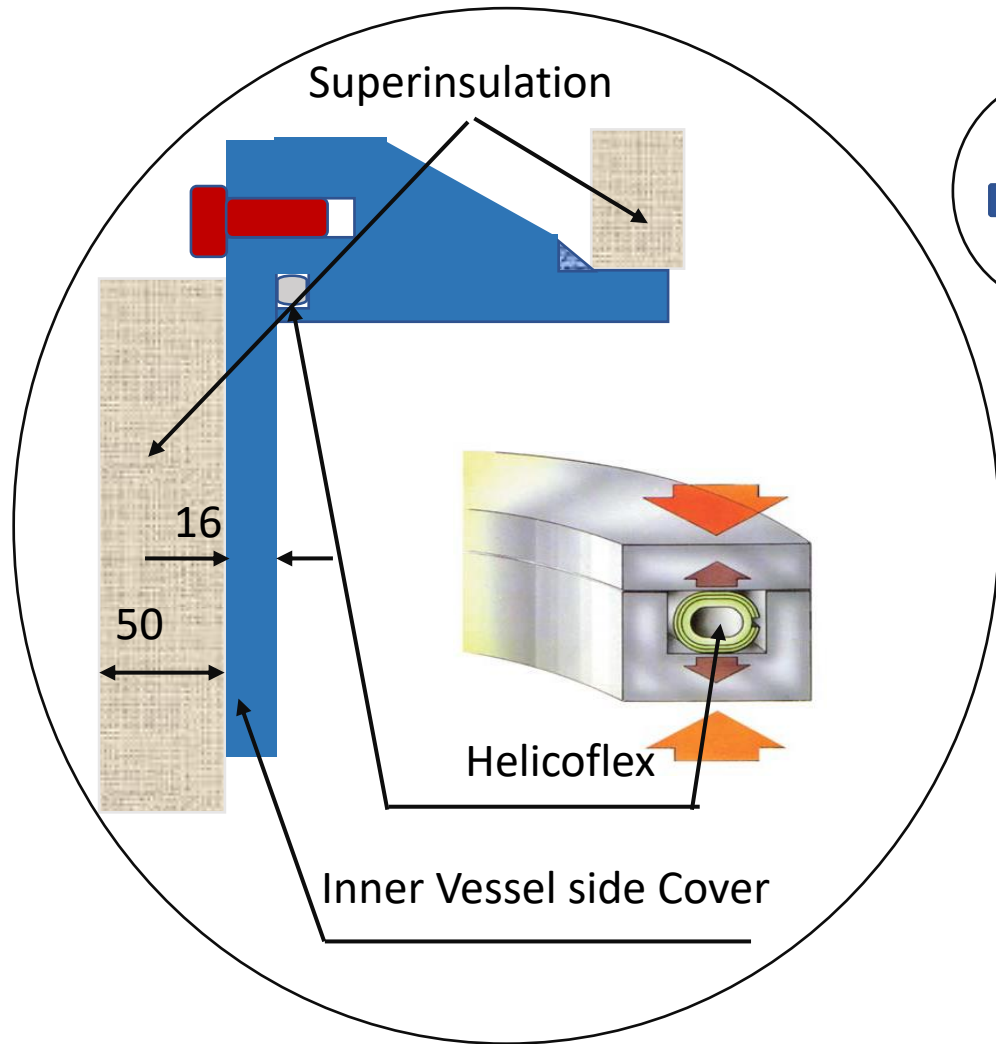


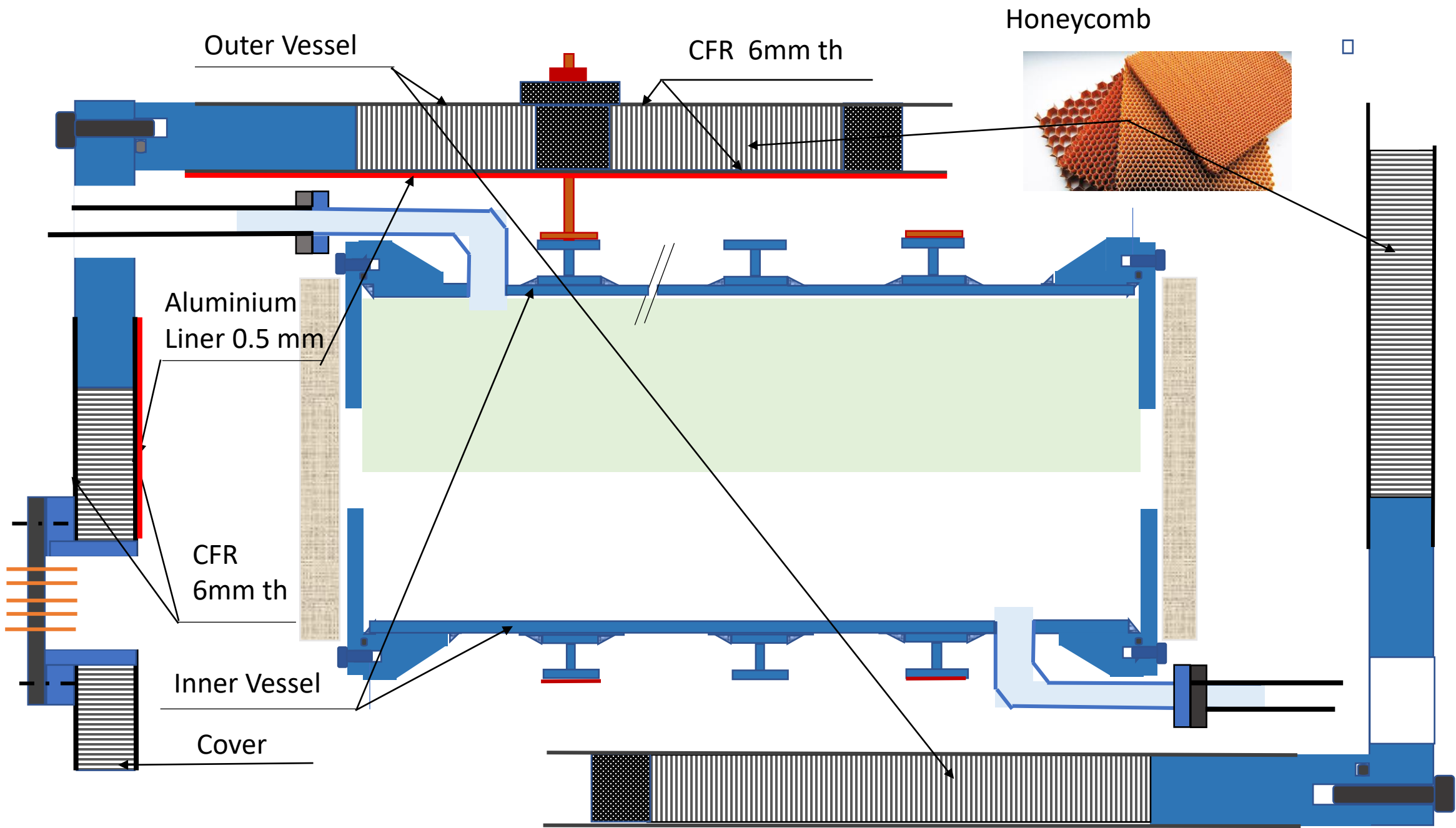


# Schematic XY cross section

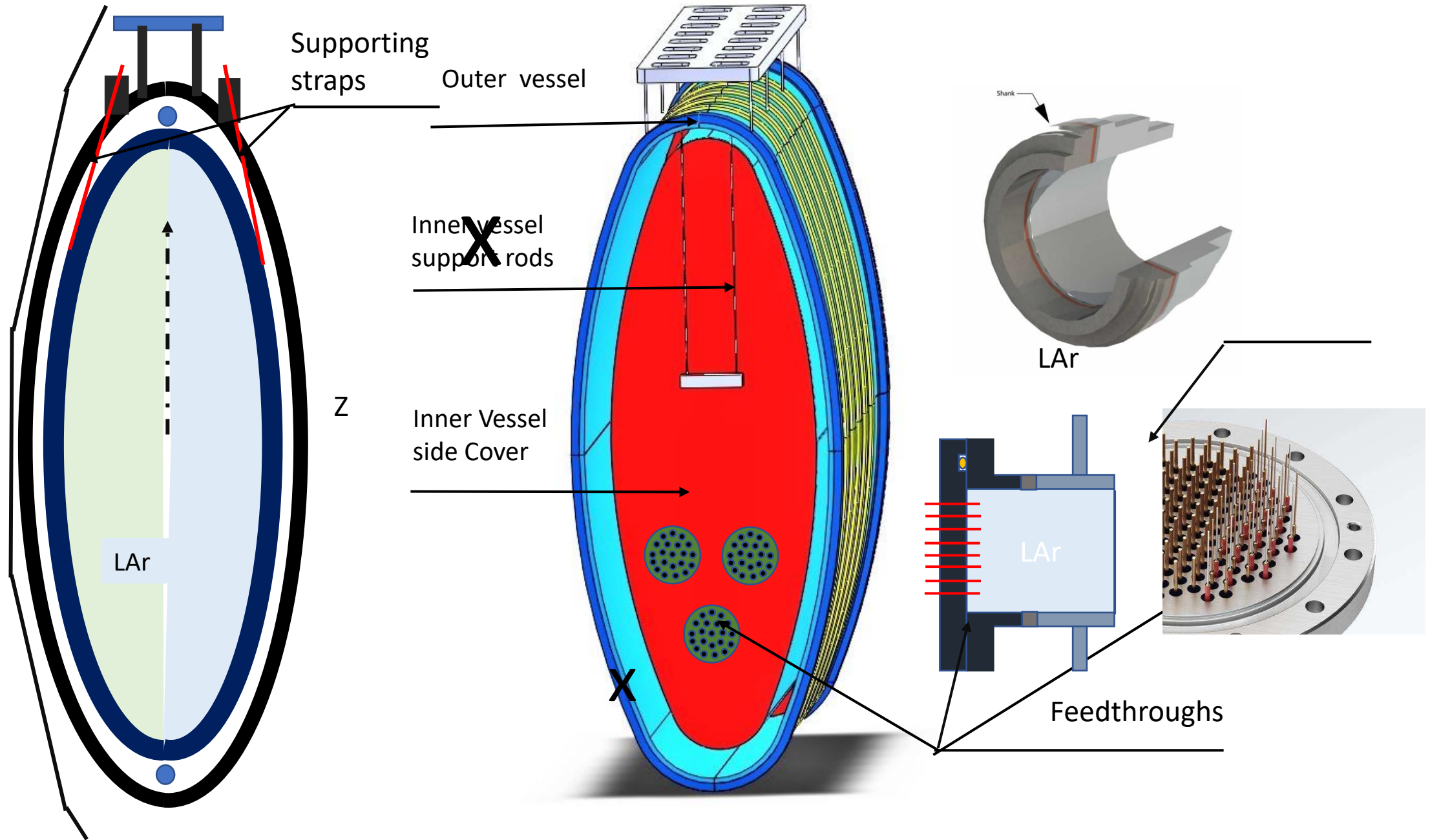


# Inner Vessel Schematic cross sections

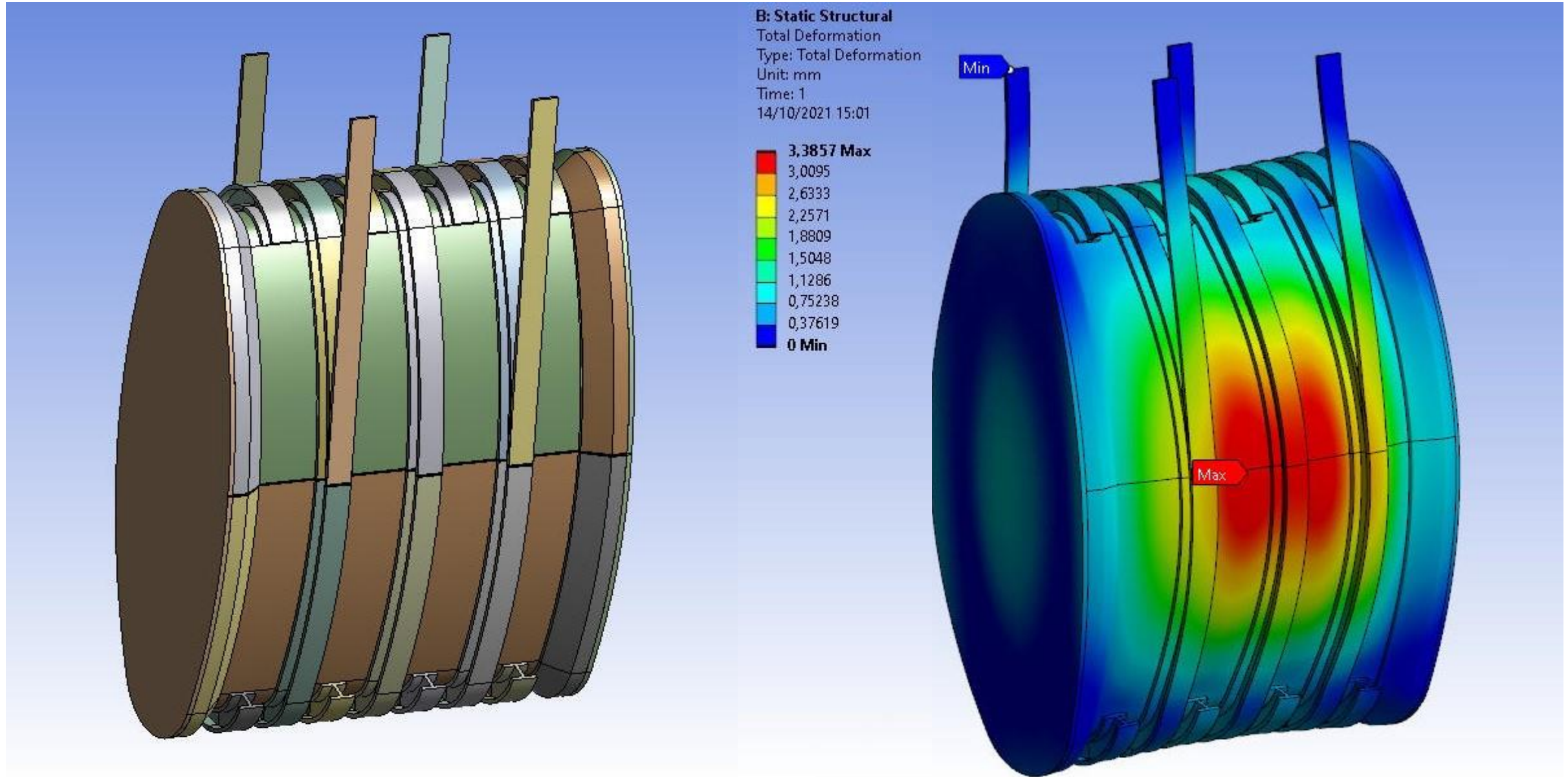






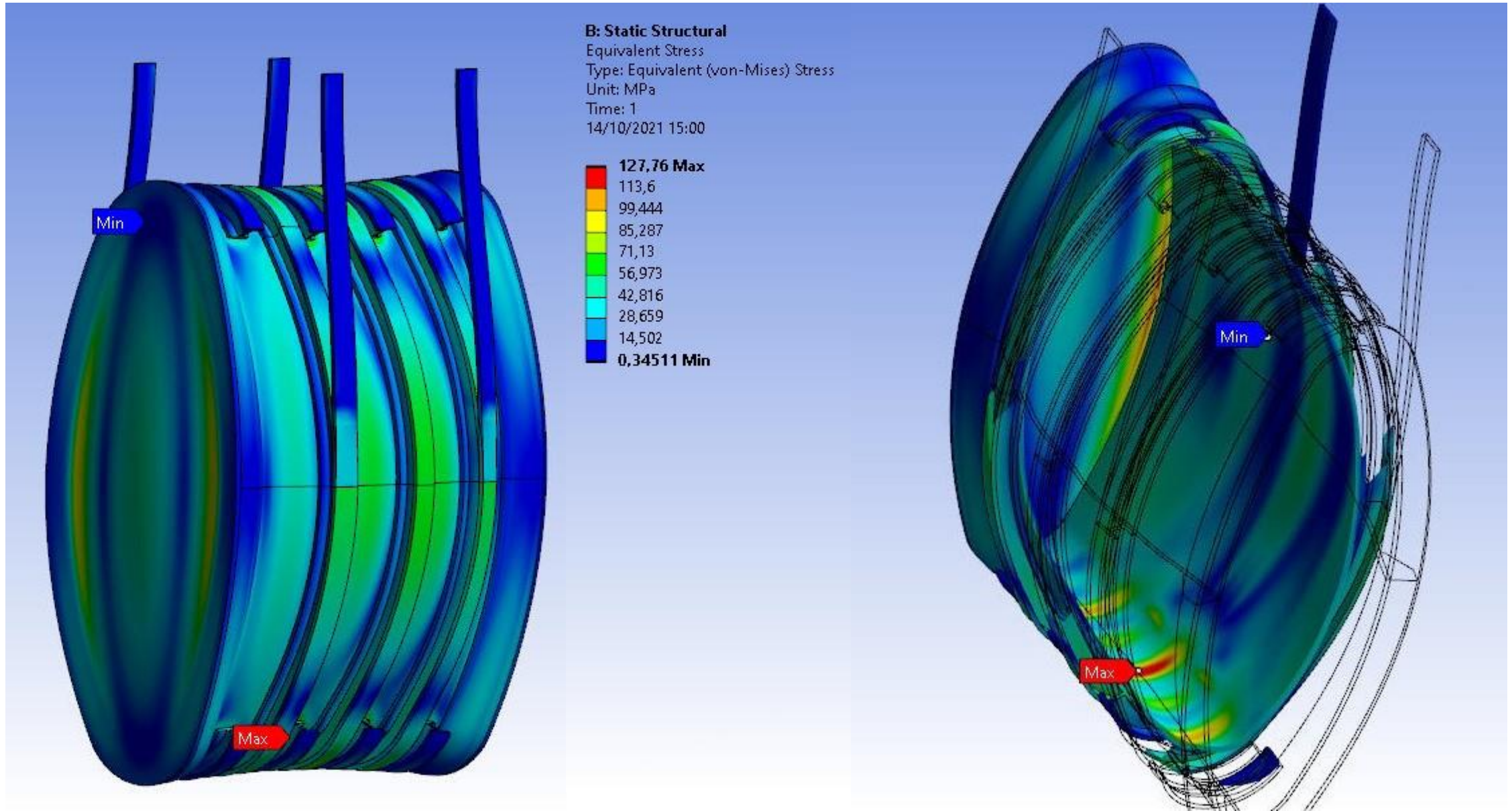


Press = 3 bars





# Alluminio 2024



# Alluminio 6000

Equivalent Stress

**B: nervi piatte e rinforzato**

Equivalent Stress

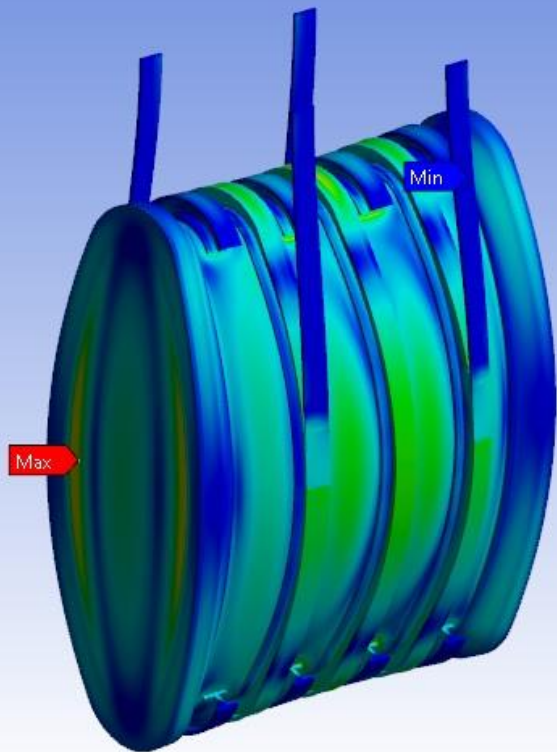
Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 1

14/10/2021 18:46

120,08 Max  
106,78  
93,474  
80,171  
66,867  
53,563  
40,26  
26,956  
13,652  
0,34877 Min



ANSYS  
2019 R2

Total Deformation

**B: nervi piatte e rinforzato**

Total Deformation

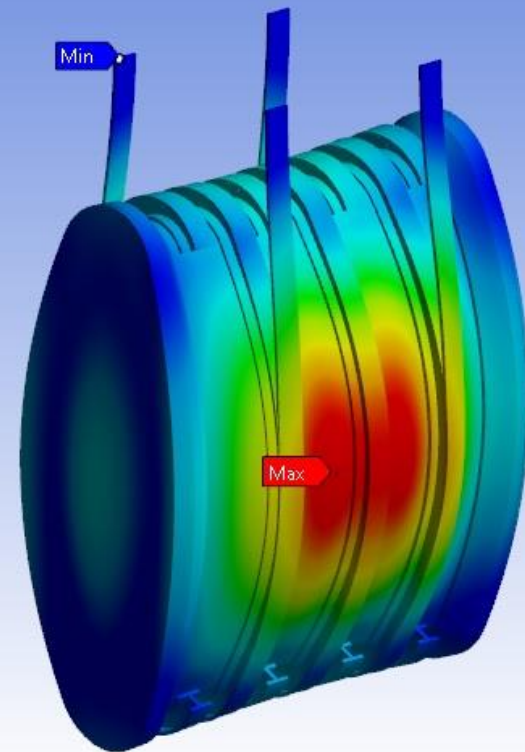
Type: Total Deformation

Unit: mm

Time: 1

14/10/2021 18:46

3,1256 Max  
2,7783  
2,431  
2,0837  
1,7364  
1,3892  
1,0419  
0,69458  
0,34729  
0 Min



ANSYS  
2019 R2

## 3.2 Verifiche Normative

Tenendo conto che l'approccio di verifica proposto è quello che, in ASME Section VIII Div. 2 Parte 5, compete all'Elastic Stress Analysis Method, dopo che saranno state condotte le analisi meccanico-strutturali corrispondenti ai casi di carico definiti in precedenza, si procederà alle verifiche normative tenendo conto della categorizzazione delle tensioni (General Primary Membrane Equivalent Stress -  $P_m$ , Local Primary Membrane Equivalent Stress -  $P_L$ , Primary Bending Equivalent Stress -  $P_b$ , Secondary Equivalent Stress -  $Q$ ) e dei limiti di riferimento relativi.

Oltre alle disequaglianze:

- $P_m < S_a$
- $P_L < 1.5 S_a$
- $P_m + P_b < 1.5 S_a$  (o  $P_L + P_b < 1.5 S_a$ )
- $P_m + P_b + Q < 3 S_a$  (o  $P_L + P_b + Q < 3 S_a$ ) (verifica a stress Ratcheting)

verrà verificata anche la disequaglianza secondo cui deve essere che:

- $S_1 + S_2 + S_3 < 4 S_a$  (Protection against Local Failure – Elastic Analysis)

dove  $S_1$ ,  $S_2$  ed  $S_3$  sono le somme delle tensioni locali principali membranali primarie e bending e  $S_a$  è la tensione ammissibile della lega d'alluminio con cui sarà costruito il Criostato.

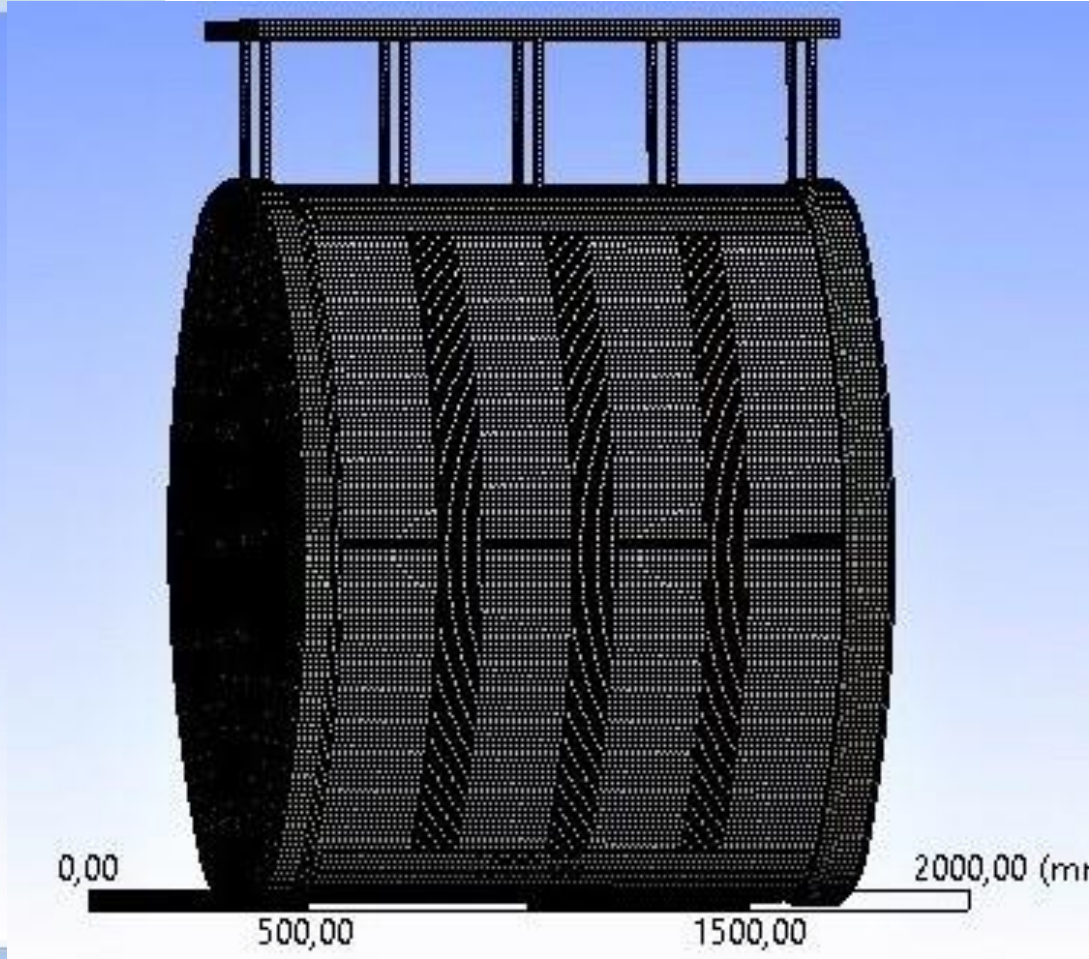
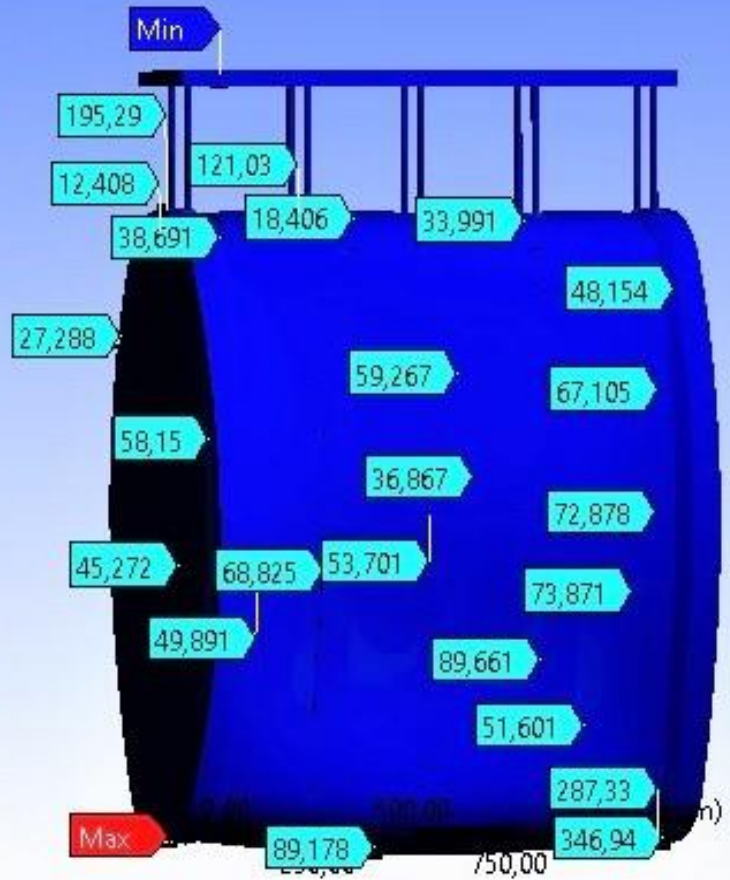
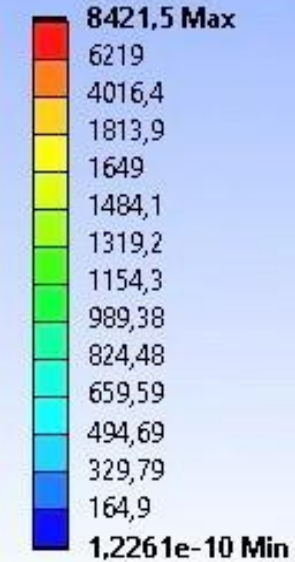
In merito ai collegamenti bullonati, in accordo ad ASME VIII Div. 2, para. 5.7.2, si verificherà che, sul gambo della vite, agli effetti di precarico e di sforzo assiale corrisponda una tensione media di valore non superiore a  $2 S_b$  e che, sempre sul gambo della vite, agli effetti di precarico, di sforzo assiale e di momento flettente corrisponda una tensione massima di valore non superiore a  $3 S_b$ , dove  $S_b$  è la tensione ammissibile del materiale delle viti.

Nel caso in cui, a seguito delle verifiche normative, il Criostato dovesse presentare delle zone critiche, verranno proposte delle modifiche alla struttura. Ad esempio si potrà intervenire sullo spessore del guscio del Criostato o sulle nervature di rinforzo



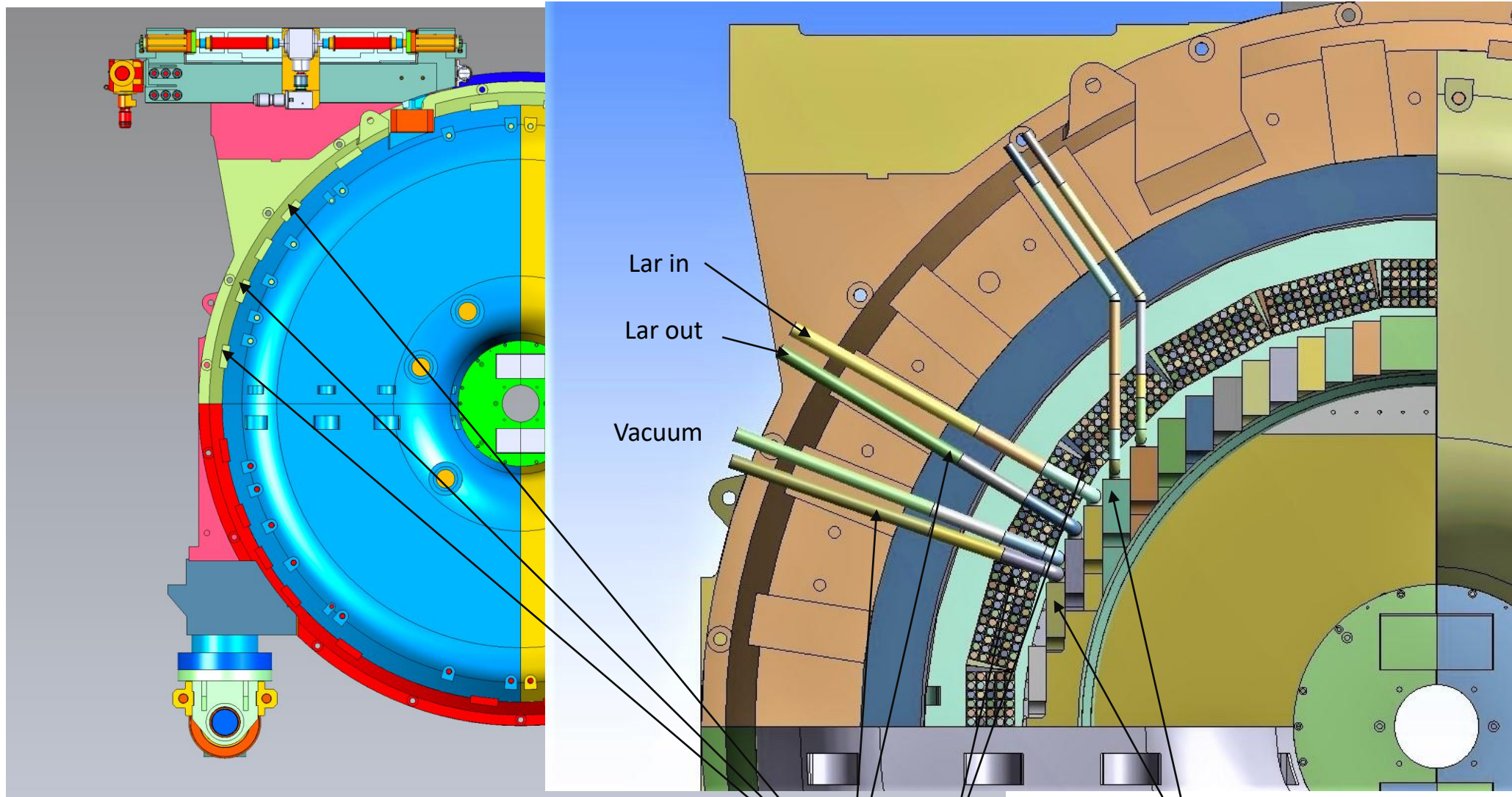
# Equivalent Stress

**E: vessel-est.CF3I**  
Equivalent Stress  
Type: Equivalent (von-Mises) Stress (Unaveraged)  
Unit: MPa  
Time: 1  
21/12/2020 17:05



**CFR Outer Vessel (Aluminium lining inside)**



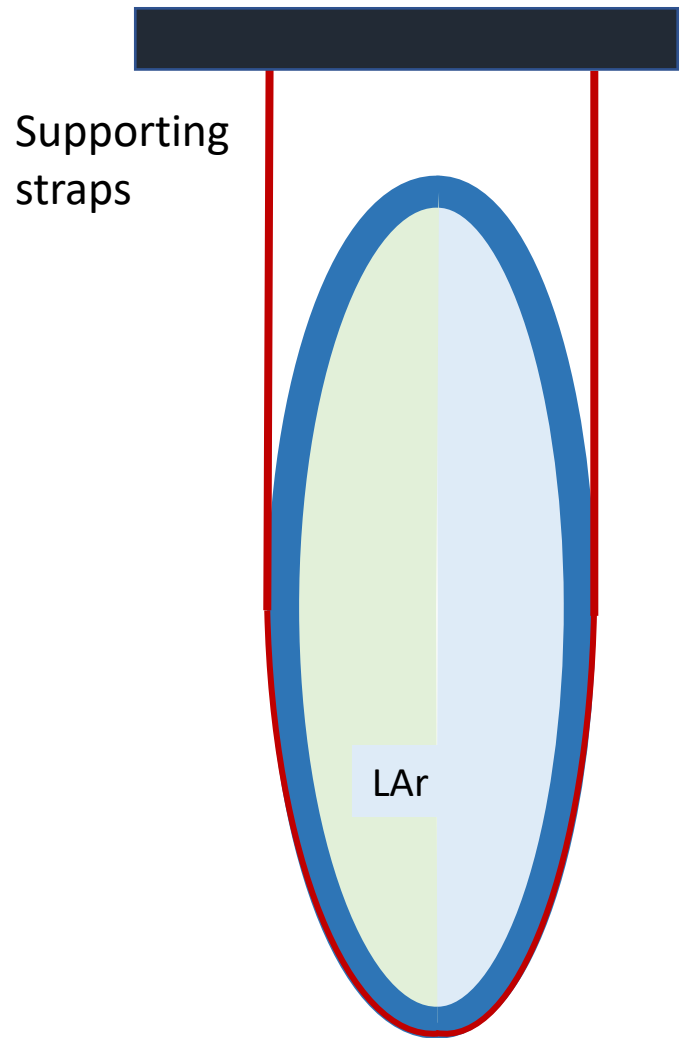


Lar & Vacuum Pipes exit through existing grooves

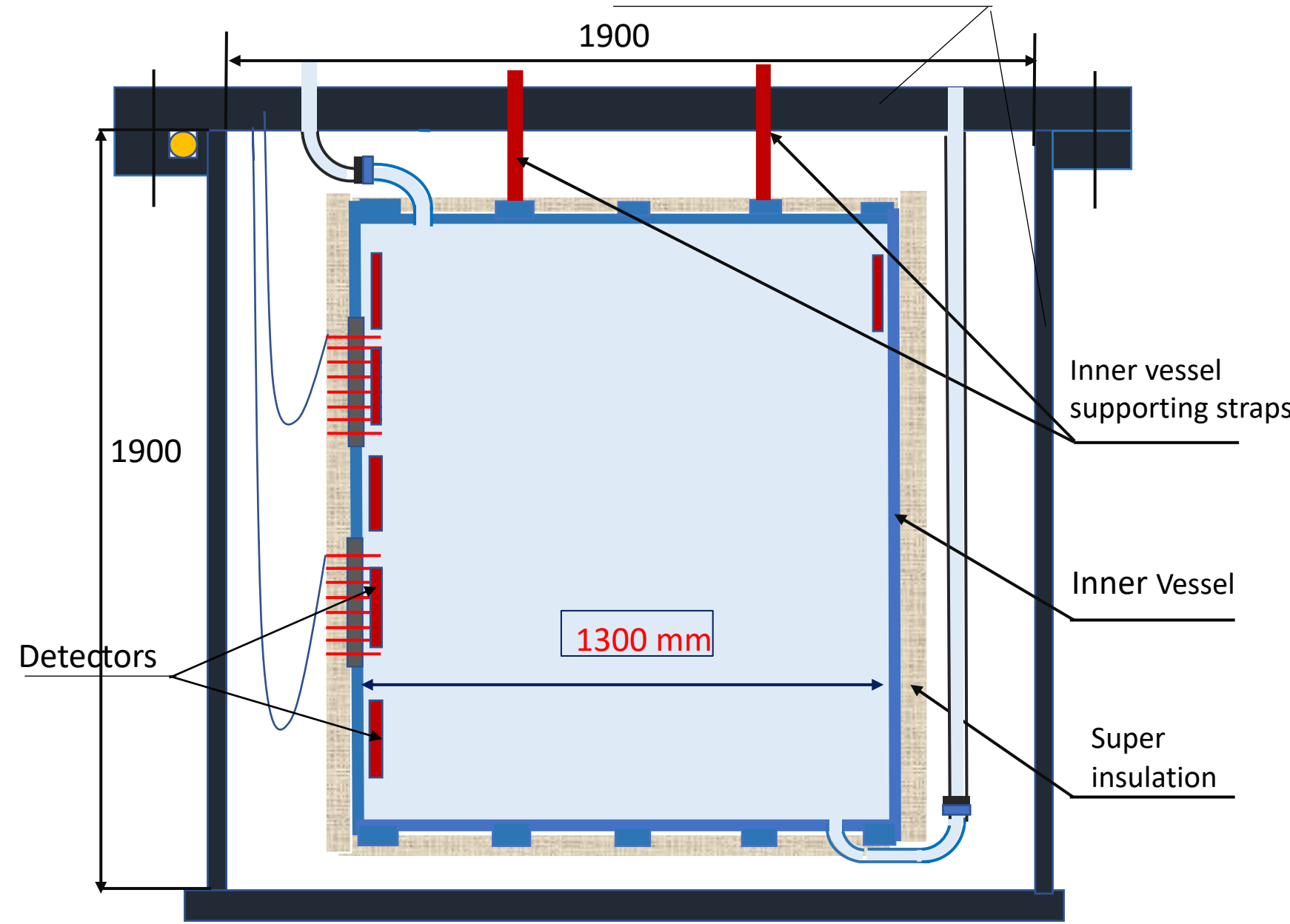
Barrel Ecal

Endcap Ecal

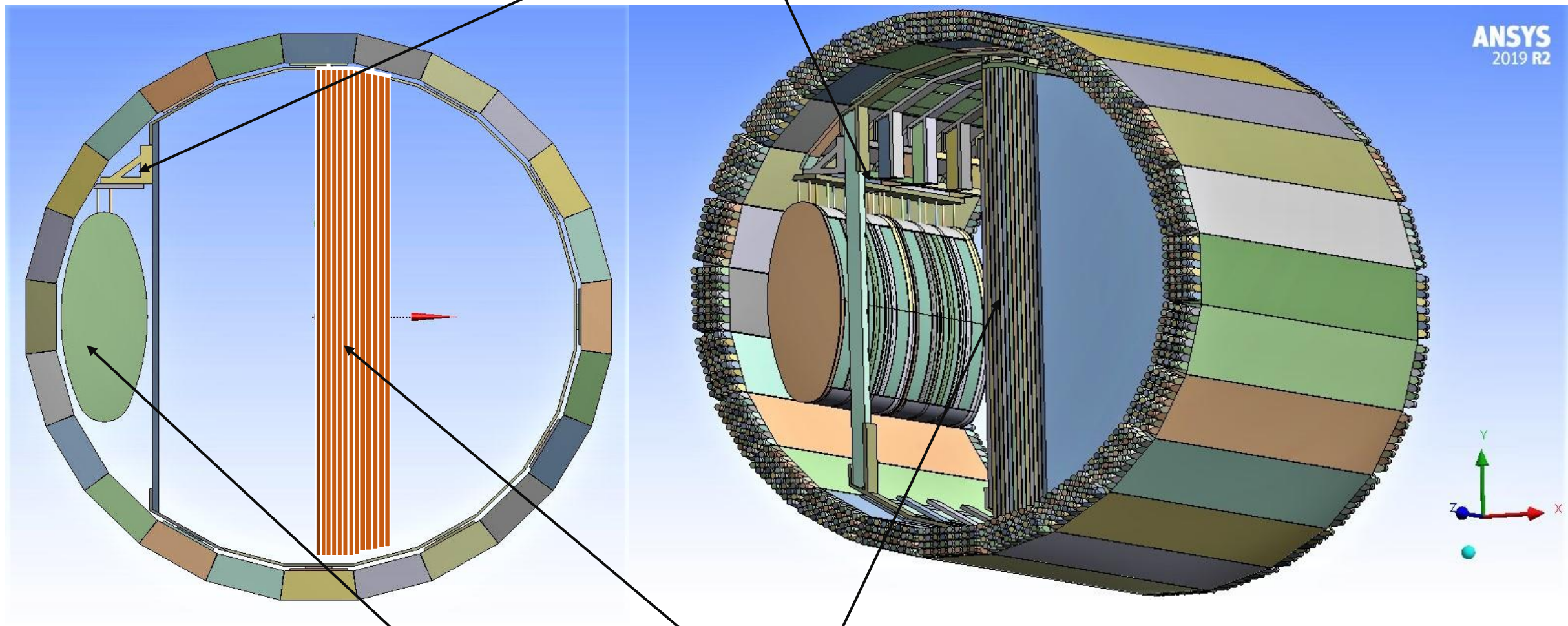
# Grain Inner Vessel prototype



# Temporary Vacuum Vessel



Supporting Structure



GRAIN

STT Central supermodule

GRAIN & STT inside SAND