

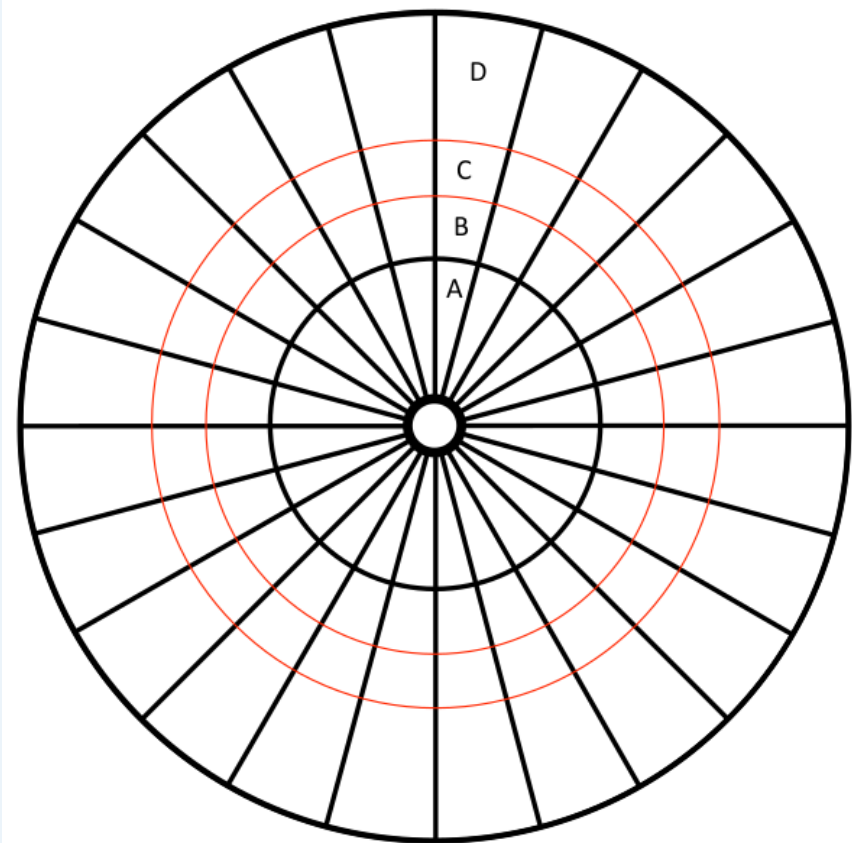


**CREMLIN PLUS**

Connecting Russian and European Measures  
for Large-scale Research Infrastructures

Mechanical design for CMD-3 drift chamber

# Details about the cell structure in chamber sectors.



## SPIDER WEB STRUCTURE

A:  
jet cell axial-layer  
12 sense per cell  
1 cell per sector

B:  
4 single wire cell  
±stereo-layers  
4 cells per sector

C:  
4 single wire cell  
±stereo-layers  
5 cells per sector

D:  
8 single wire cell  
±stereo-layers  
6 cells per sector

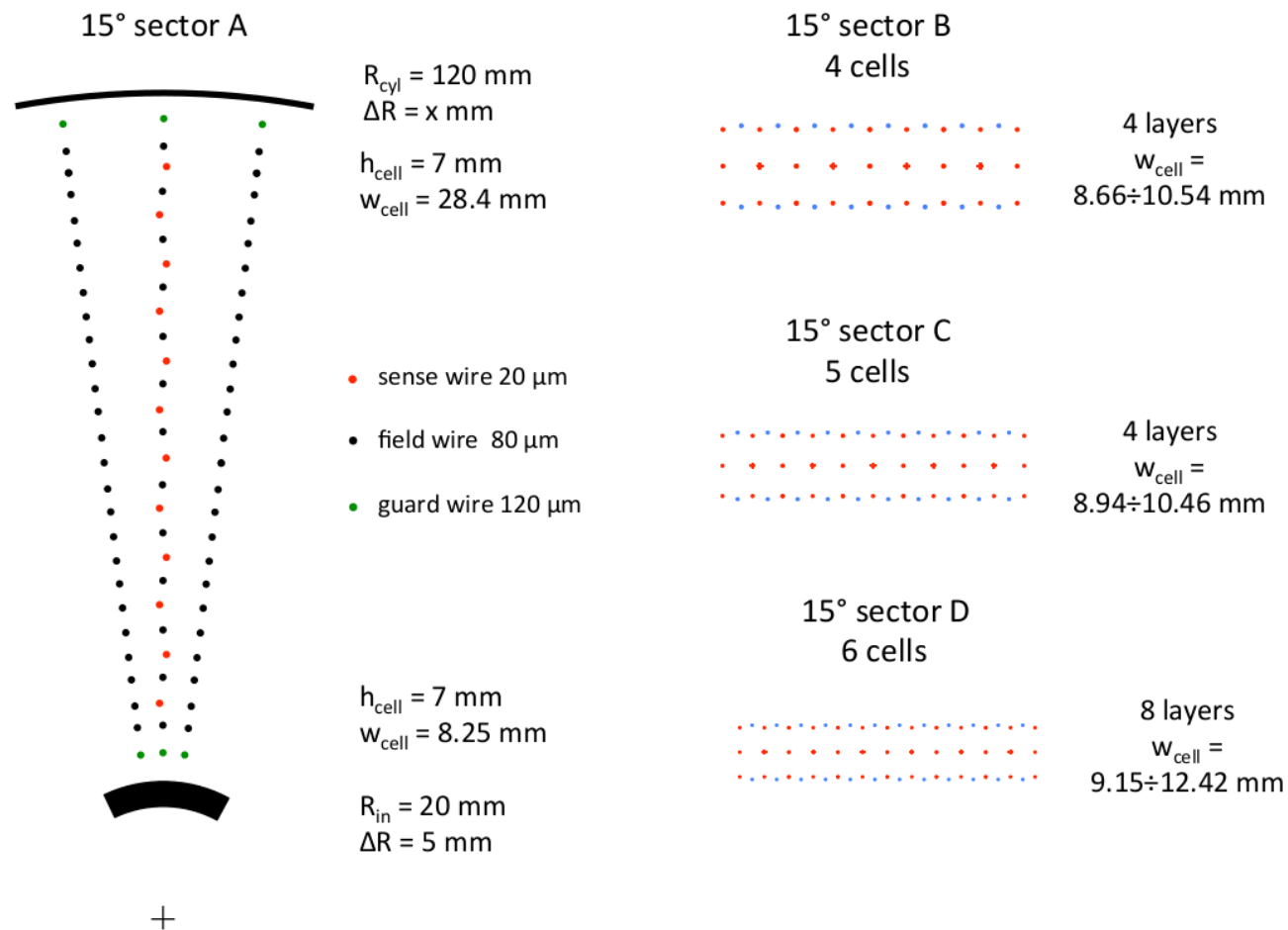
From inside to outside, marked with black circle:

- inner cylinder
- middle cylinder
- outer cylinder

Red circles show the different sectors in which the chamber is conceptually divided.

Sector A: jet-cells with wires arranged axially.

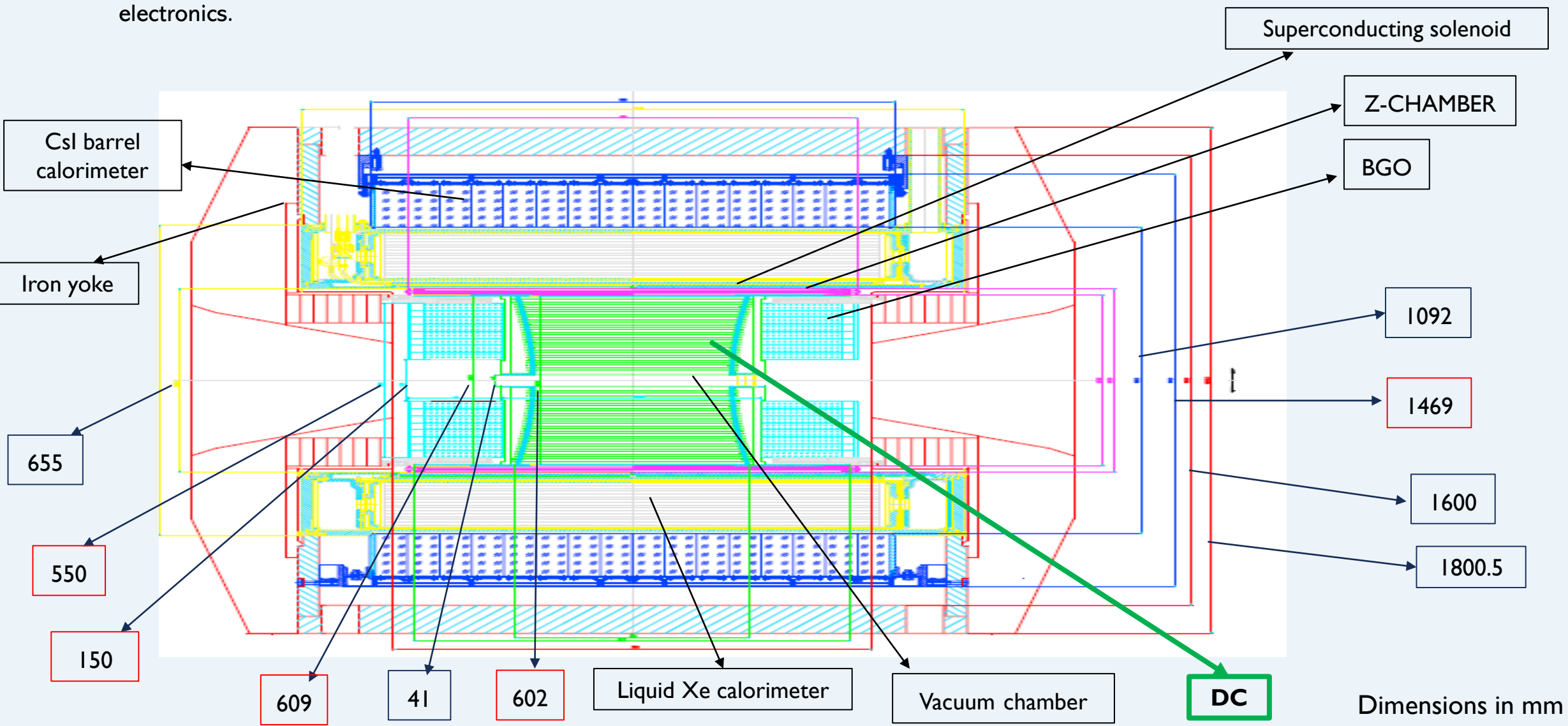
Sector B, C, D: single-wire cells with the wires arranged in stereo angle configuration.



# DIMENSIONS

- Along beam axis ( distance between end-cap calorimeter) = 484 mm
- Transverse direction (diameter) = 609 mm
- Inner shell= 41 mm

The size along beam will be change not more than **5-15 mm**, due to the optimization of BGO electronics.



## Sector A: 24 spokes-48 PCBs

The construction of the chamber is driven by two main purposes:

- 1) The high transparency
- 2) The mechanical stability of the whole structure

Support for PCB

Wire PCB for sector B

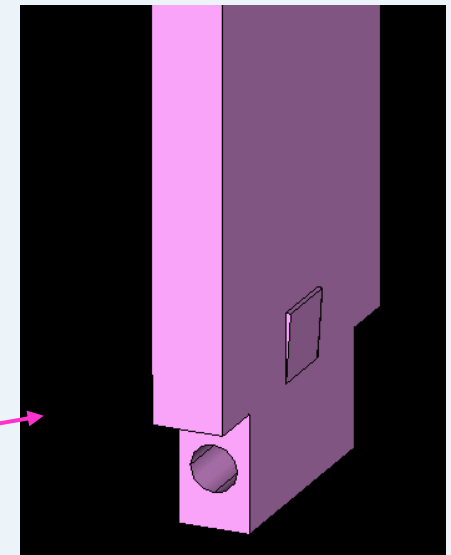
PCB for sector A

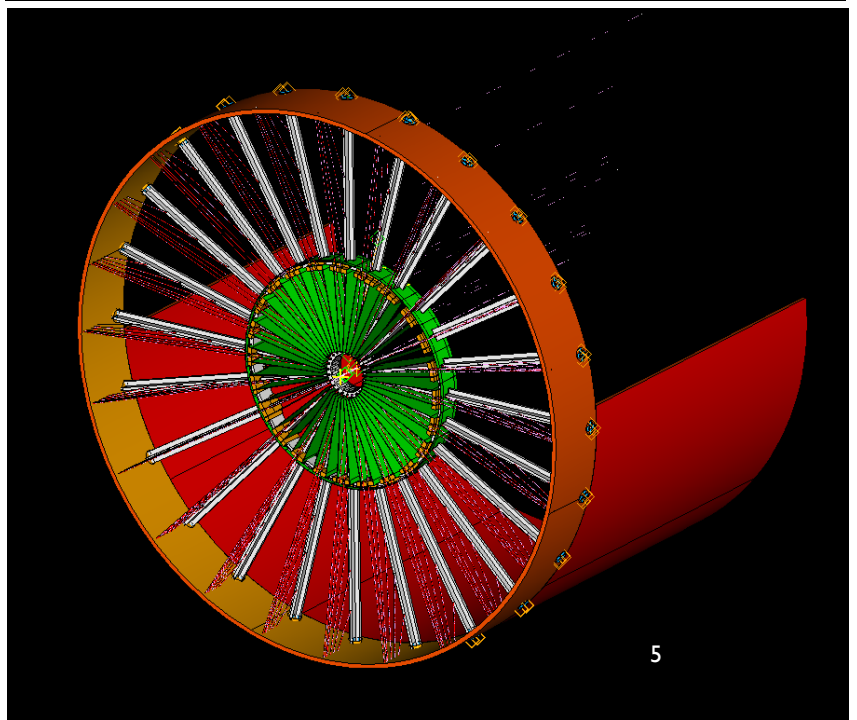
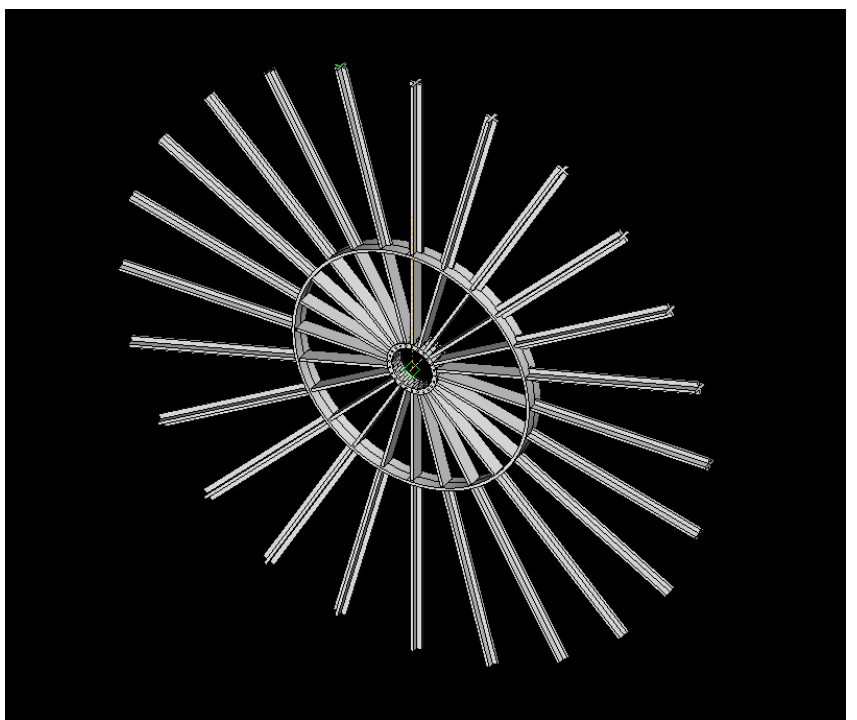
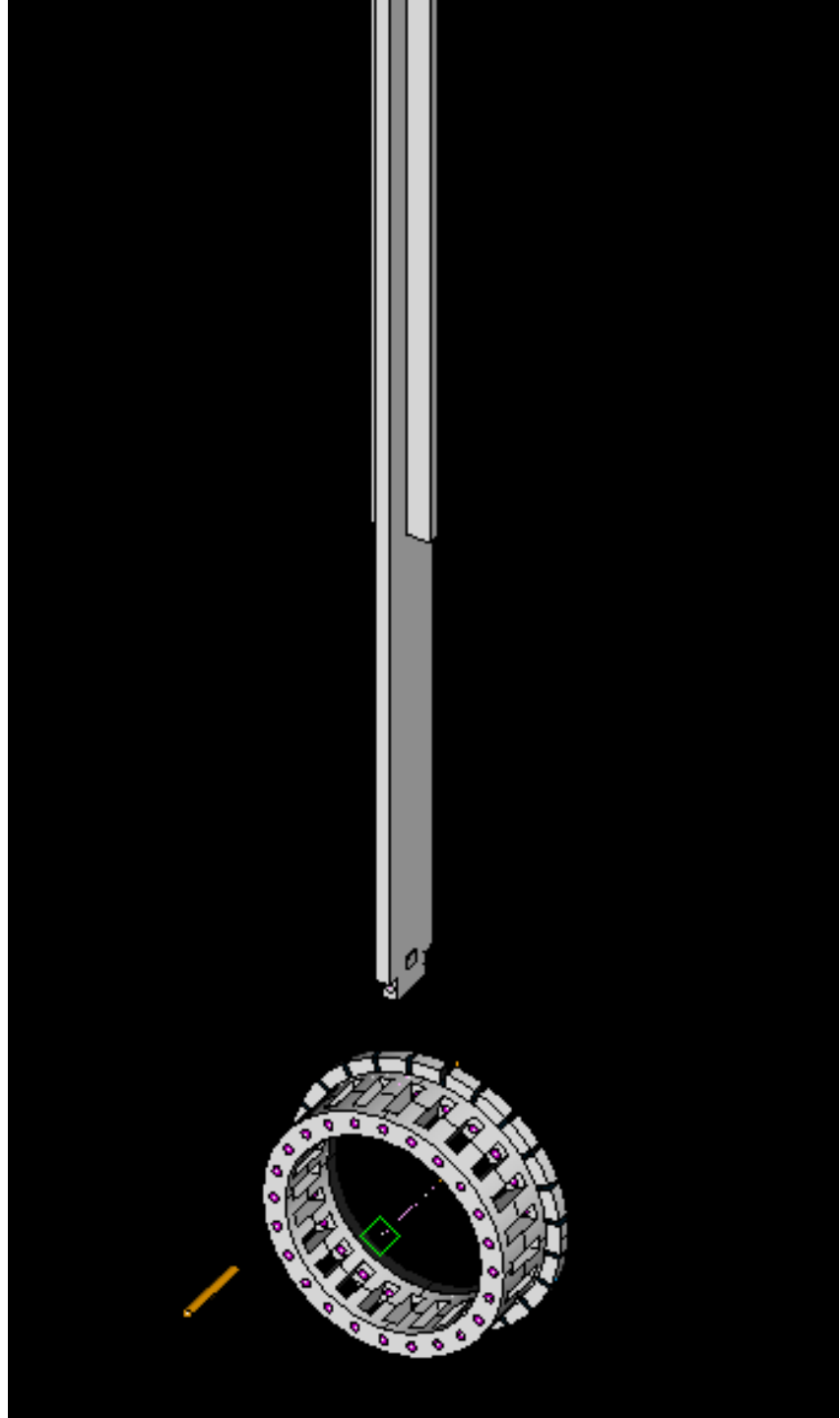
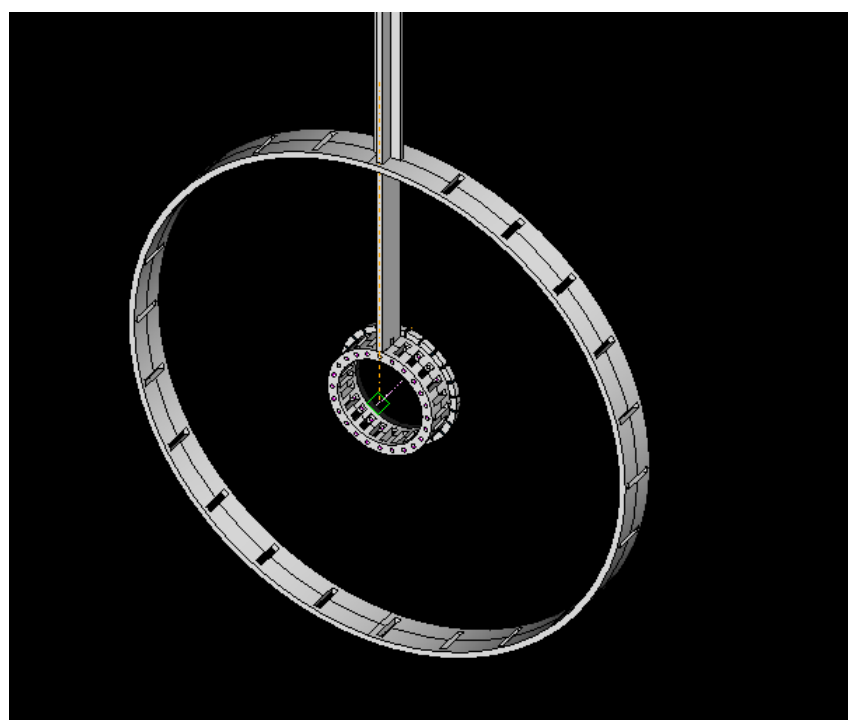
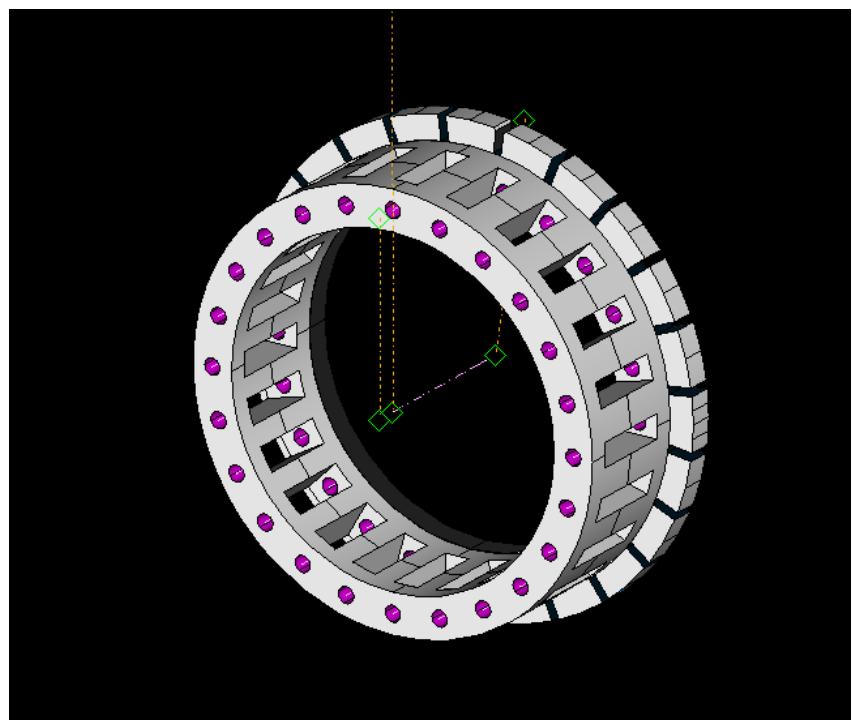
Tie-rod

Each spoke will be inserted inside the inner cylinder

The spider web structure will be built in carbon fiber.

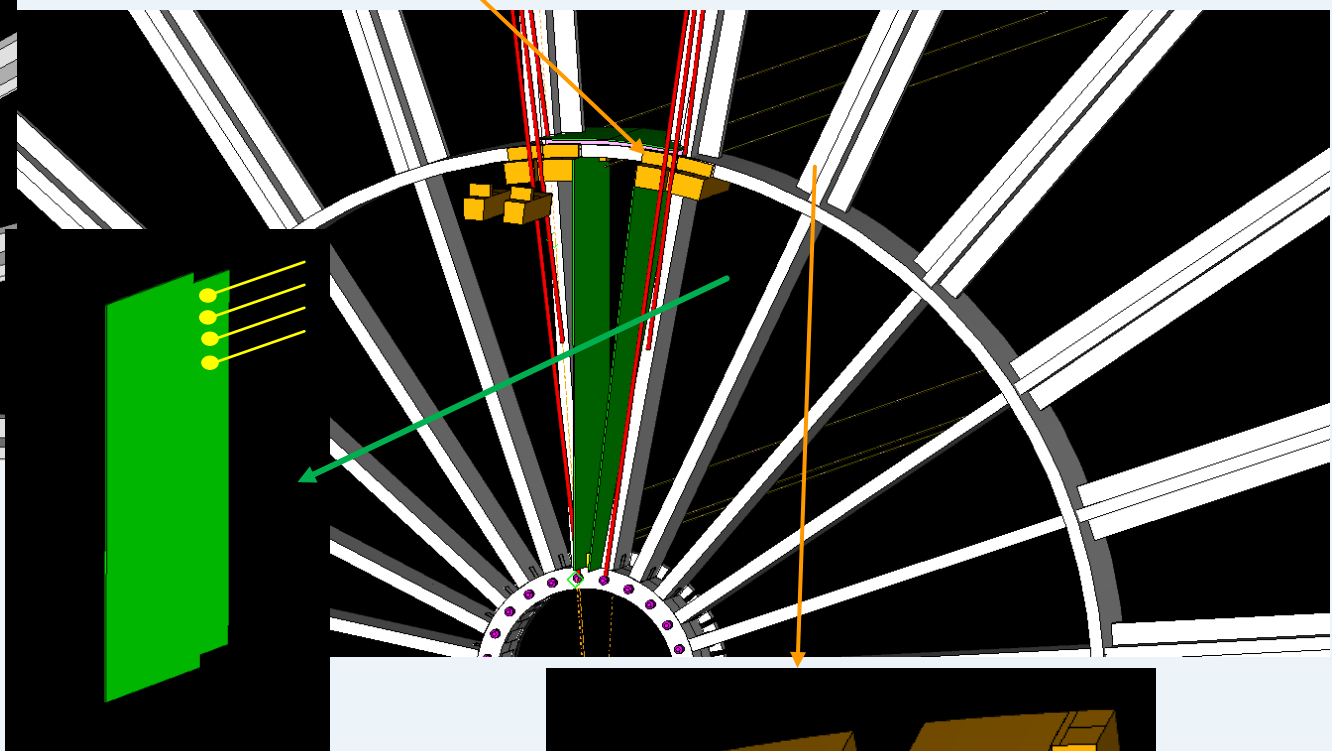
The spoke will be fixed with a tiny pin



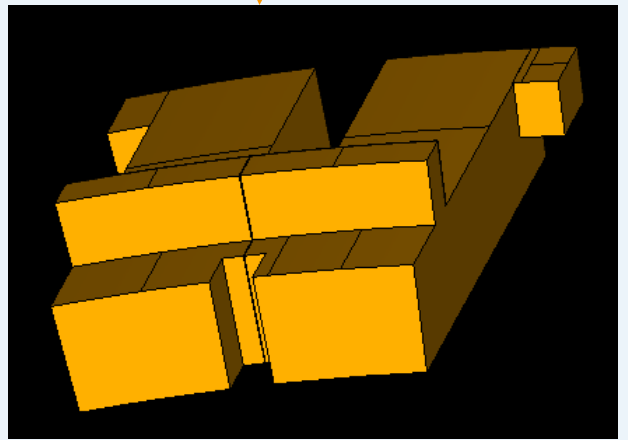
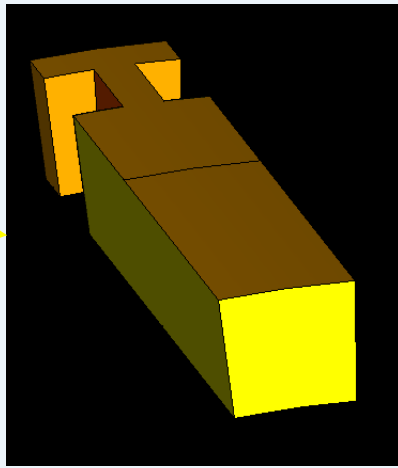
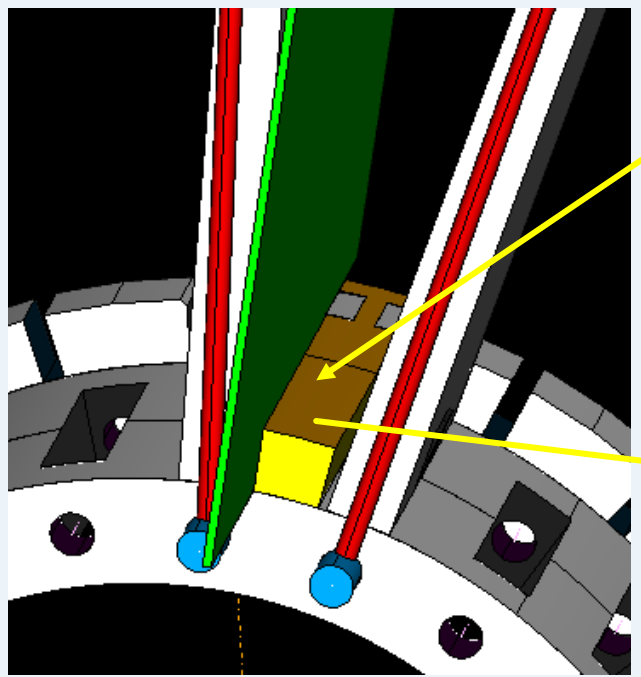


# Details about the positioning of PCBs in sector A

At the intermediate ring, supports will be built with a suitable shape to host the PCBs.



At the inner ring, we will insert a wedge-shaped locking plate.

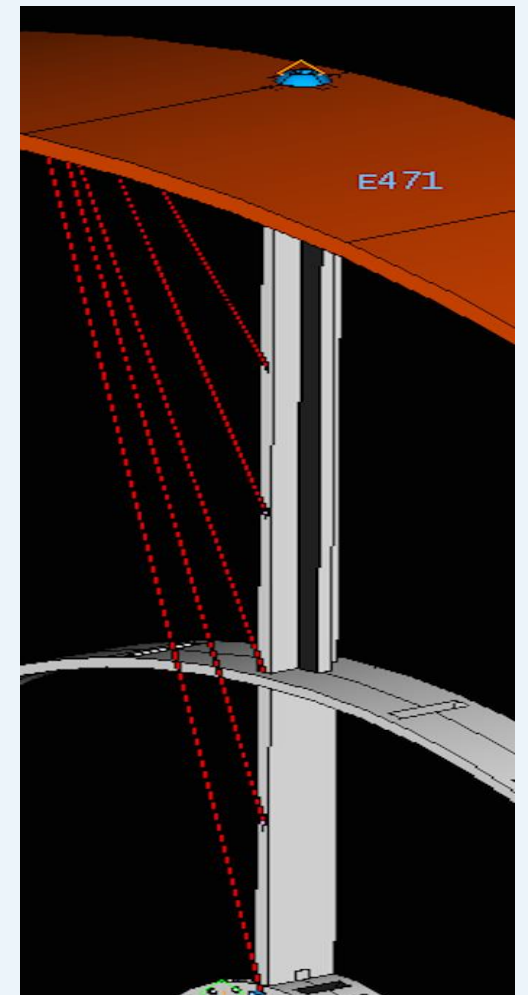
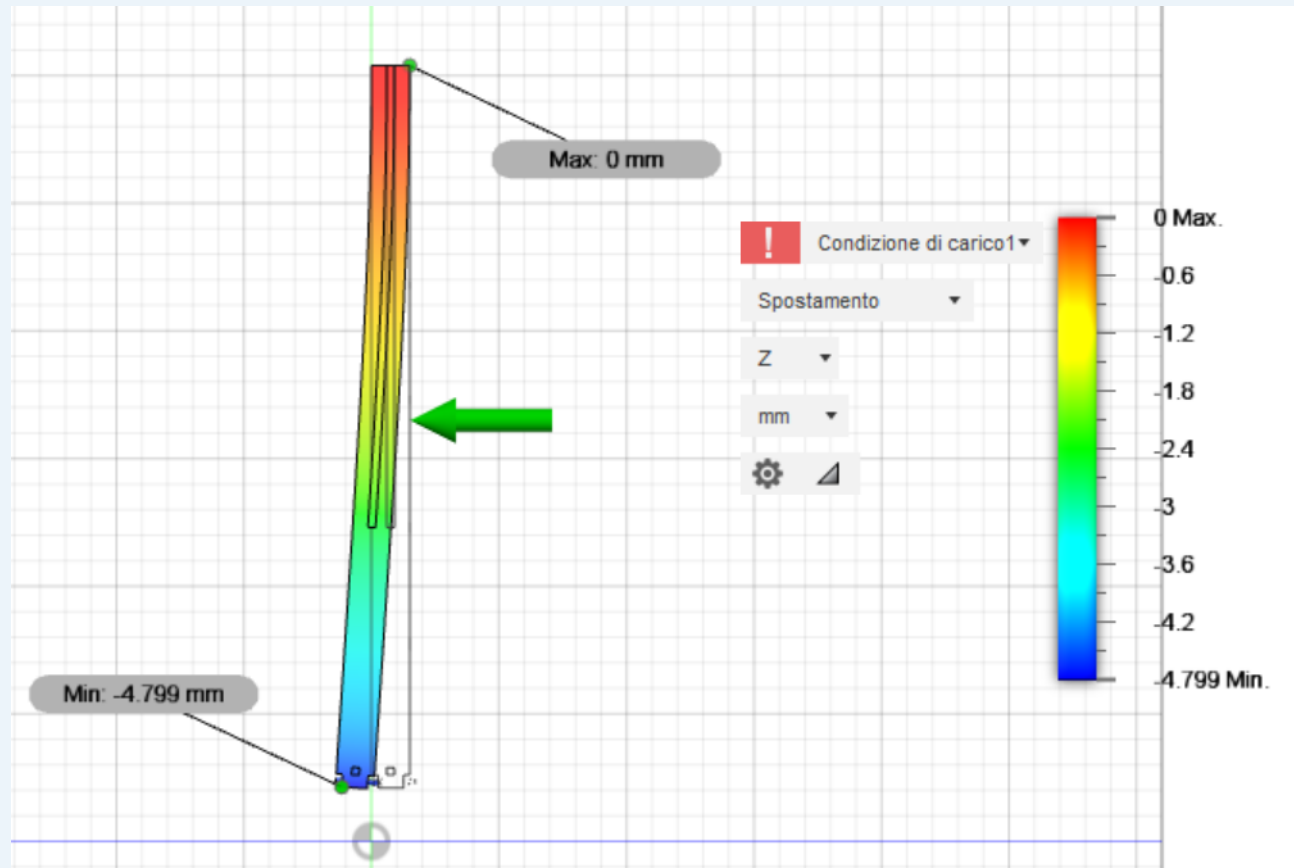


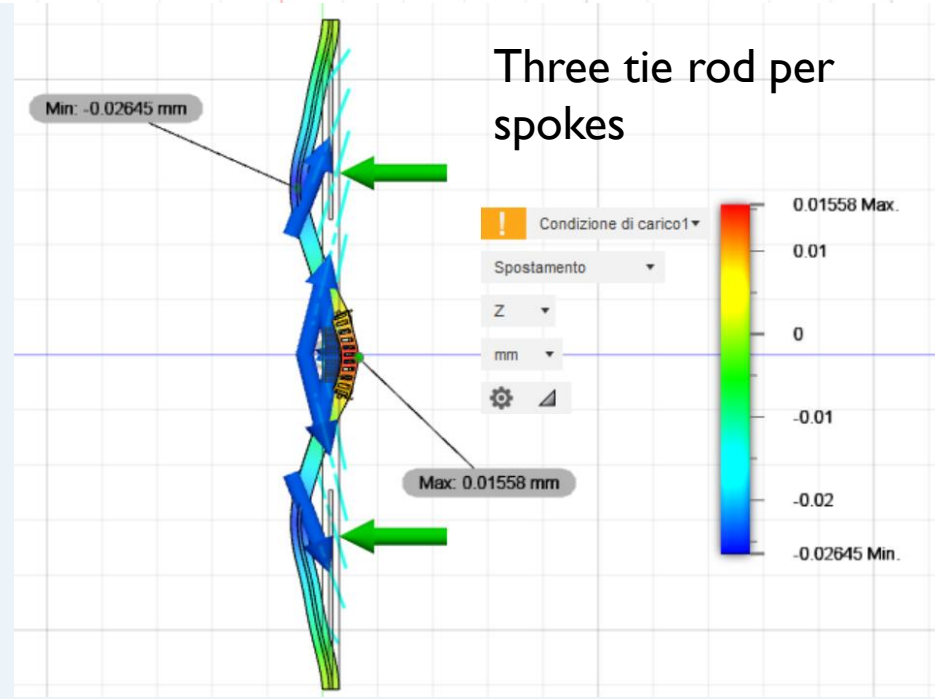
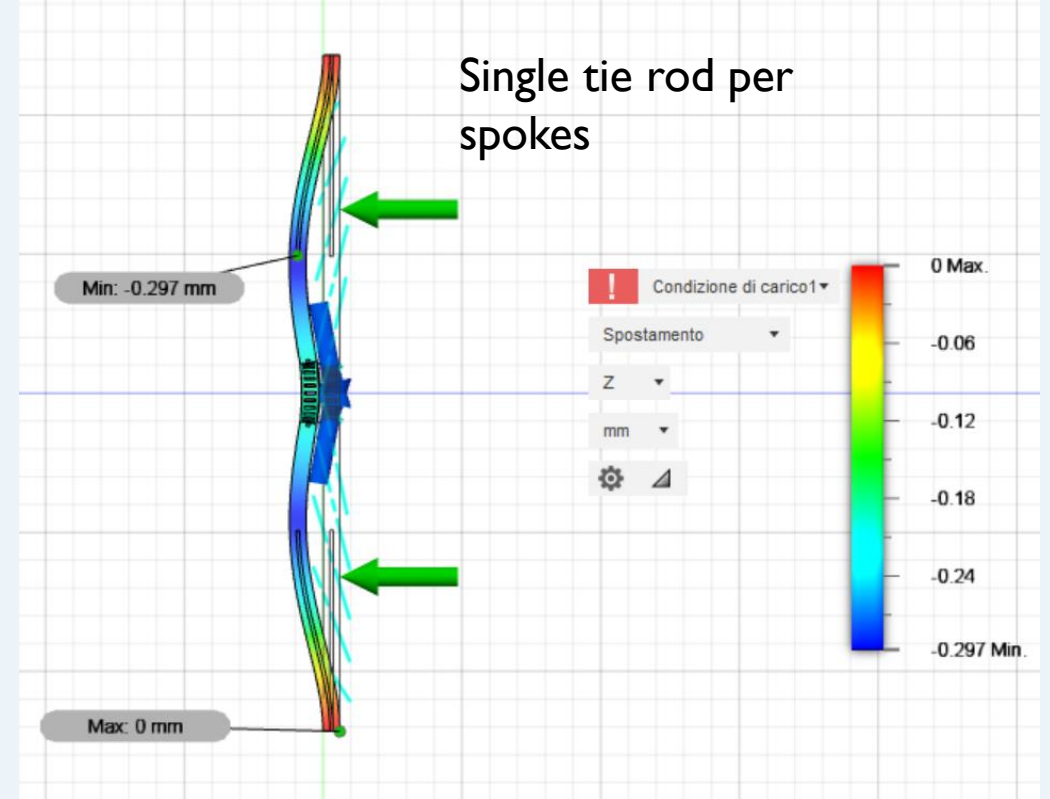
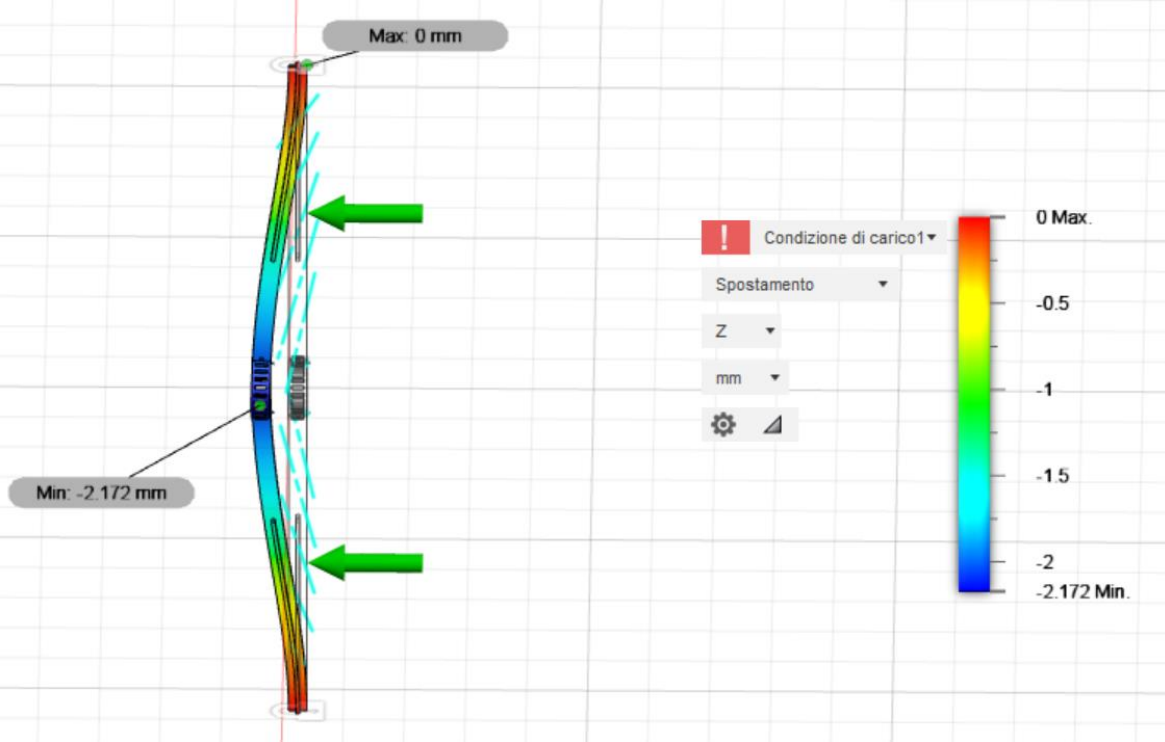
## Tie rod to prevent deformations

Due to the wire loads, ( $\approx 20$  kg per spokes), the end-plates are affected by **deformations**.

We intend to install an appropriate number of tie rods per spoke to minimize the deformations due to the wire load.

C-fiber (low modulus, 133 GPa) 4.8 mm deflection  
Al 9.4 mm deflection  
Ss 3.3 mm deflection





Just by adding symmetry reduces to 2.2 mm deflection

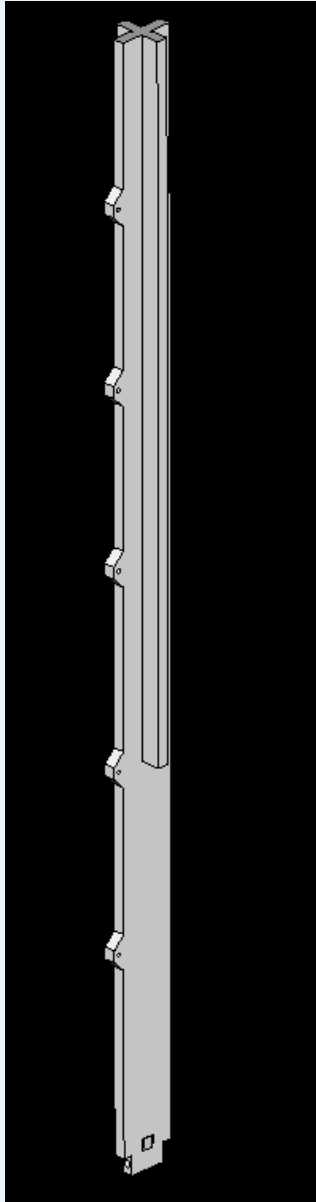
Single tie-rod at inner radius loaded with 450 N at 10°: max deflection < 300  $\mu$ m

Three tie rods loaded with : 140 N at 10°, 240 N at 14°, 200 N at 21°: max deflection <  $\pm 25 \mu$ m

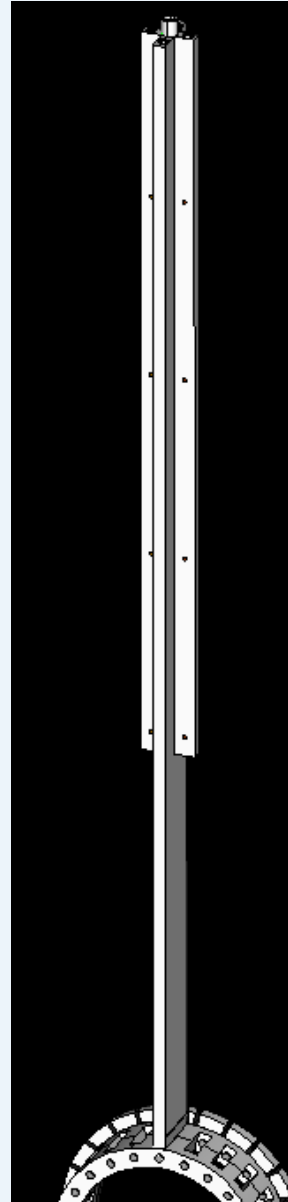


## Possible ways to attach the tie rods on the spokes

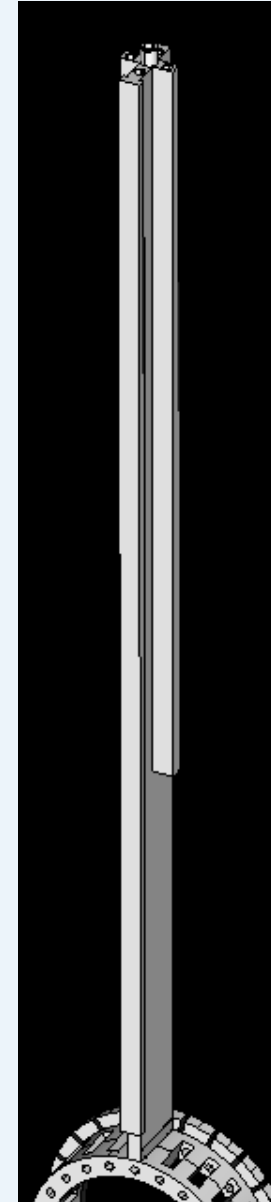
First proposal:  
create buttonholes,  
insert an eyelet and  
hook the tie rod.



Second proposal:  
create two  
buttonholes, insert  
an eyelet and hook  
the tie rod.



Third proposal:  
use a “cart”, like the  
mast of a sailboat



## Conclusion

We started a collaboration with the technicians from University and Polytechnic of Bari, planning the following steps:

1. Finite elements simulation of the inner cylinder and spokes
2. Analysis and choice of suitable materials
3. Building of a prototype