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on behalf of the SaToR-G experiment

Summary

- Results of the LARASE Experiment: Part IV
- Current activities

Results of the LARASE Experiment: Part IV Summary LAser RAnged Satellites Experiment

- Thermal thrust effects
- Mass and moments of inertia
- The LASSOS Spin Model
- The LATOS thermal model
- Preliminary results
- Conclusions



An intricate role, among the complex nongravitational perturbations, is played by the subtle thermal thrust effects that arise from the radiation emitted from the satellite surface as consequence of the non uniform distribution of its temperature

In the literature of the LAGEOS satellite this problem was addressed since the early 80s' of the past century to explain the (apparently) anomalous behavior of the along-track acceleration of the satellite, characterized by a complex pattern:

Rubincam, Afonso, Ries, Scharroo, Farinella, Metris, Vokrouhlicky, Slabinsky, Lucchesi, Andres, ...

represents a non exhaustive list of the researchers that have successfully worked on this very important issue



Figure 2. LAGEOS 1 anomalous acceleration: observed data points (squares) are based on 15 day fits to laser data by the Center for Space Research, University of Texas at Austin. The vertical bars mark eclipse seasons. N at top of bar denotes season when satellite travels northward through earth shadow; S denotes season with southward travel.



The dynamical problem to solve is quite complex and should account for the following main aspects:

- A deep physical characterization of the satellite
 - emission and absorption coefficients, thermal conductivity, heat capacity, thermal inertia, ...
- Rotational dynamics of the satellite
 - Spin orientation and rate
- Radiation sources
 - Sun and Earth



We have tackled the problem following the two approaches considered in the past in the literature (but with some differences):

- We developed a simplified thermal model of the satellite based on
 - the energy balance equation on its surface
 - a linear approach for the distribution of the temperature with respect to its equilibrium (mean) temperature
- A general thermal model based on
 - a satellite (metallic structure) in thermal equilibrium
 - the CCRs rings are at the same temperature of the satellite
 - for each CCR the thermal exchange with the satellite is computed







LAGEOS II

The main perturbations to be taken into account are:

• The solar Yarkovsky-Schach effect

- an anisotropic emission of thermal radiation that arises from the temperature gradients across the surface produced by the solar heating and the thermal inertia of the various parts (mainly from the CCRs)
- it produces long-term effects when the thermal radiation is modulated by the eclipses

• The Earth Yarkovsky thermal (or Rubincam) effect

- the temperature gradients responsible of the anisotropic emission of thermal radiation are produced by the Earth's infrared radiation
- the bulk of the effect is due to the CCRs and their thermal inertia
- The Earth's Albedo
 - the temperature gradients responsible of the anisotropic emission of thermal radiation are produced by the Earth's visible radiation
 - the bulk of the effect is due to the CCRs and their thermal inertia

Simplified (average) thermal model

Characteristic amplitude:

$$A_{YS} \cong \frac{16}{9} \frac{A}{m} \frac{\varepsilon \sigma}{c} T_0^3 \Delta T$$

Accelerations in body:



$$a_{X} = A_{YS} \frac{\sin z_{\odot}}{1 + (\omega_{spin}\tau)^{2}}$$
$$a_{Y} = A_{YS} \frac{\sin z_{\odot}}{1 + (\omega_{spin}\tau)^{2}} \omega_{spin}\tau$$

$$a_Z = A_{YS} cos z_{\odot}$$

with eclipses

$$a_{X} = A_{YS} \frac{sinz_{\odot}}{1 + (\omega_{spin}\tau)^{2}} \Gamma_{X}$$

$$a_{Y} = A_{YS} \frac{sinz_{\odot}}{1 + (\omega_{spin}\tau)^{2}} \Gamma_{Y}$$

A / **1 I I**

 $a_Z = A_{YS} cos z_{\odot} \Gamma_Z$

Farinella P, Vokrouhlicky D., Thermal force effects on slowly rotating, spherical

artificial satellites - I. Solar heating, Plan. Space Sci. 44, 12 (1996)

We used:

 \circ $\tau \cong 2113 s$

○ $A_{YS} \cong -1.035 \times 10^{-10} \text{ m/s}^2$

Lucchesi D.M., Reassessment of the error modelling of the non-gravitational perturbations on LAGEOS II and their impact in the Lense-Thirring derivation - Part II, Plan. Space Sci. 50 (2002)

Results for the simplified (averaged) model: LAGEOS II



Results for the simplified (averaged) model: LAGEOS II



Results for the simplified (averaged) model: LAGEOS II





About 27 years POD of LAGEOS II with GEODYN II

Among the main parameters necessary to correctly model the dynamical behavior of an artificial satellite we have to consider:

- mass
- center of mass position
- moments of inertia

If we look to the scientific literature and to the official documents (NASA, ASI, ALENIA) of LAGEOS, we can easily see a number of different values for these fundamental parameters, differences that we have mainly confined within the following categories:

- 1. lack of complete measurements (hence of the flight model knowledge)
- 2. mistakes in information/popularization and its "error propagation..."
- 3. material alloys and manufacturing tolerances

For instance, just to give an example, it is well known the controversy and the consequent very long debate about the material of the inner core of LAGEOS:

- it is of BRASS (NASA-TN 1975; Cohen and Smith 1985)?
- it is of BERYLLIUM and COPPER (Johnson et al. 1976)?
- Still in Slabinski 1997 (more than 20 years after LAGEOS launch), it was reported Be-Cu for the core
- Only 10 years later Andrés concluded that the core was probably made of Brass as that of LAGEOS II, but he wrongly concluded that the dimensions were slightly different

Slabinski, V.J., 1996. A numerical solution for LAGEOS thermal thrust: the rapid-spin case. Celestial Mech. Dyn. Astron. 66, 131–179. Andrés de la Fuente, J.I., 2007. Enhanced Modelling of LAGEOS Non-Gravitational Perturbations (Ph.D. thesis). Delft University Press. Sieca Repro, Turbineweg 20, 2627 BP Delft, The Netherlands.

A second and significant example are the correct dimensions for the stud and the core of LAGEOS: for instance, those reported in Cohen and Smith 1985 are wrong



- We reconstruct information about the structure, the material used and the moments of inertia of the two LAGEOS
- We built a 3D-CAD model of the satellites structure useful for finite element-based analysis
- We also solve for contradictions and overcome several misunderstanding present in the historical literature of the older LAGEOS (carefully re-analyzing the earlier technical documents)





Documents on LAGEOS

- NASA, 1975. LAGEOS Phase B Technical Report, NASA Technical Memorandum X-64915. Technical Report TMX-64915. ٠ Marshall Space Flight Center. Marshall Space Flight Center, Alabama 35812. February 1975
- Siry, J.W., 1975. The LAGEOS system. Technical Report TM-X-73072. NASA •
- LAGEOS Press Kit, 1976. NASA (1976) Project LAGEOS Press Kit release 76/67. Technical Report 76/67. NASA. National • Aeronautics and Space Administration, Washington, DC
- Fitzmaurice, M.W., Minott, P.O., Abshire, J.B., Rowe, H.E., 1977. Prelaunch Testing of the Laser Geodynamic Satellite. ٠ Technical Report TP-1062. NASA
- Wong, C., 1978. Watching the Earth move from space. Sky Telesc., 198–202

Documents on LAGEOS II

- Cogo, F., 1988. Weight discrepancy analysis between LAGEOS 1 and LAGEOS 2 satellites. Technical Report LG-TN-AI-035. Aeritalia
- Fontana, F., 1989. Physical properties of LAGEOS II satellite. Technical Report LG-TN-AI-037. Aeritalia •
- Fontana, F., 1990. Physical properties of LAGEOS II satellite. Technical Report LG-TN-AI-037. Aeritalia •
- Minott, P.O., Zagwodzki, T.W., Varghese, T., Seldon, M., 1993. Prelaunch Optical Characterization of the Laser ٠ Geodynamic Satellite (LAGEOS 2). Technical Report 3400. NASA Technical Paper 3400. National Aeronautics and Space Administration, Washington, DC 17

Satellite	Material density ρ_n (kg/m ³)				
	Hemispheres	Core	Stud		
LAGEOS	AA6061	QQ-B-626 COMP.11	Cu-Be		
	2700 ^a	8440 ^a	8230 ^b		
LAGEOS II	AlMgSiCu UNI 6170	PCuZn39Pb2 UNI 5706	Cu-Be QQ-C-172		
	2740°	8280°	8250°		



 $\frac{M_m}{M}$ $\bar{\rho} = \rho_N$

Table 2

Our conclusions on the materials and shape of the satellites have been validated by re-computing the mass and moments of inertia of the satellites and comparing the results with those reported in the official documentation in the case of the pre-flight configurations

Comparison of masses and moments of inertia for the two LAGEOS satellites. In the notation we follow NASA (1975). The x axis coincides (nominally) with the principal axis of inertia (the angle between the symmetry axis and the principal axis orientation was bound to be below 0.02 radians). Practically, this axis coincides with the initial rotation axis of the satellites.

Satellite origin of value	Mass (kg)	Moments of	Moments of inertia (kg m ²)	
	M	I _{xx}	I_{yy}	I_{zz}
LAGEOS flight arrangement				
Computed value in NASA (1975)	409.8	11.516	11.084	11.084
Measured value in NASA (1975)	406.965	_	_	_
Values computed in the present work using nominal density of Table 1	405.93	11.40	10.93	10.93
LAGEOS balance model				
Computed value in NASA (1975)	440.3	13.14	12.71	12.71
Measured value in NASA (1975)	440.0	13.11	12.69	12.71
Value computed in the present work using	437.68	13.09	12.62	12.62
nominal density of Table 1				
Values computed in the present work using normalized density	440.00	13.16	12.68	12.68
LAGEOS II flight arrangement				
Computed values in Fontana (1990)	_	11.45	11.00	11.00
Measured value in Fontana (1990), Fontana (1989) and Cogo (1988)	405.38	_	_	_
Values computed in the present work using nominal density of Table 1	404.97	11.44	10.99	10.99
LAGEOS II without CCRs				
Computed value in Fontana (1989)	386.59	10.39	9.95	9.95
Measured value in Fontana (1989)	387.20	9.67	9.37	9.15
Values computed in the present work using nominal density of Table 1	386.71	10.41	9.95	9.95
Values computed in the present work using normalized density	387.20	10.42	9.96	9.96

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Table 3

Mass and moments of inertia of LAGEOS and LAGEOS II to be used in the future. The masses are the one measured. The moments of inertia are those computed in the present work with normalized densities.

Satellite	Mass (kg) M	Moments of inertia (Moments of inertia (kg m ²)		
		I _{xx}	I_{yy}	I_{zz}	
LAGEOS flight arrangement	406.97	11.42 ± 0.03	10.96 ± 0.03	10.96 ± 0.03	
LAGEOS II flight arrangement	405.38	11.45 ± 0.03	11.00 ± 0.03	11.00 ± 0.03	

This work was also extended to LARES:

Table 1. Principal moments of inertia of LAGEOS, LAGEOS II and LARES in their flight arrangement.

Satellite	Moments of Inertia (kg m ²)			
	I_{zz}	I_{xx}	I_{yy}	
LAGEOS	11.42 ± 0.03	10.96 ± 0.03	10.96 ± 0.03	
LAGEOS II	11.45 ± 0.03	11.00 ± 0.03	11.00 ± 0.03	
LARES	4.77 ± 0.03	4.77 ± 0.03	4.77 ± 0.03	

- The two **LAGEOS** have almost the same oblateness of about 0.04
- LARES is practically spherical in shape, even if an oblateness as small as 0.002 is however possible







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Review and critical analysis of mass and moments of inertia of the LAGEOS and LAGEOS II satellites for the LARASE program

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Spin Models

The rotational dynamics of a satellite represents a very important issue that deeply impacts the goodness of the orbit modeling

Indeed, the modeling of several disturbing effects (like the thermal thrust ones) depends on the knowledge of the spin period and orientation in the inertial space:

- 1. Yarkovsky–Schach effect
- 2. Earth–Yarkovsky (Rubincam) effect
- 3. Asymmetric reflectivity from the satellite surface

Their modelling will greatly improve the POD of the two LAGEOS satellites avoiding the current (and significant) use of empirical accelerations during the data reduction

Spin Models

A general theory is not easy to be developed because the modelling of the spin evolution depends on several factors:

- spacecraft materials, its shape, details of the structure
- space environment: orbit altitude and inclination
- spin rate: kind of equations to be solved, resonances (rotational period, thermal inertia, orbit period)

Past Spin Models

The best spin models developed in the past are:

- 1. Bertotti and less (JGR 96 B2, 1991)
- 2. Habib et al. (PRD 50, 1994)
- 3. Farinella, Vokrouhlicky and Barlier (JGR 101, 1996); Vokrouhlicky (GRL 23, 1996)
- 4. Andrés, 1997 (PhD Thesis): LOSSAM model

All of these studies, with the exception of Habib et al., attack and solve the problem of the evolution of the rotation of a satellite in a terrestrial inertial reference system, in the so-called rapid spin approximation and they introduce equations for the external torques that are averaged over time; their fit to the spin observations was good, especially in the case of the LOSSAM model for the LAGEOS II satellite. Habib et al. use a body-fixed reference system and non-averaged torques; their model does not fit so well the observations

We have deeply reviewed previous spin models, in particular we:

- first built our own spin model in the rapid spin approximation
- adopted non-averaged torques in the equations to describe the slow spin approximation: we solved the problem of a metallic sphere rotating in an alternate magnetic field
- introduced in the equations all known possible torques (like in LOSSAM model)
- solved the equations in a body-fixed reference system in order to better describe the misalignment between the symmetry axis and the spin
- included in the equations the terms due to the transversal asymmetry
- carefully studied the satellites moments of inertia

The model for the magnetic torque

Since we are working with conductive satellites moving and rotating in the Earth's magnetic field B, a magnetic moment m will be induced in their body and, consequently, a torque M_{mag} will be applied:

 $M_{mag} = m \times B$

In previous works, LAGEOS was modeled as a conducting sphere rotating in a static magnetic field

• The value of the constant magnetic field was computed averaging the magnetic field over the entire orbit of the satellite

This solution, which is completely valid in a **quasi-stationary** field, can be suitably used as long as the rotation period of the satellite is much shorter than its orbital period as well as of the Earth's rotation period:

 $T_{rot} \ll T_{orb}$ $T_{rot} \ll T_{\oplus}$

but it could produce wrong results when is used in slow-spin conditions

In order to obtain a more general expression of the magnetic torque we faced the problem to find an easily integrable expression for the torque acting on a conducting sphere rotating in an **alternating magnetic** field

The involved torques

We consider in the case of the two LAGEOS satellites four torques:

 $A'_{i} = \frac{\alpha'(\omega_{s}^{E} - \omega_{i}) + \alpha'(\omega_{s}^{E} + \omega_{i})}{2} \qquad D'_{i} = \frac{\alpha'(\omega_{s}^{E} - \omega_{i}) - \alpha'(\omega_{s}^{E} + \omega_{i})}{2}$

 $A_i'' = \frac{\alpha''(\omega_s^E - \omega_i) + \alpha''(\omega_s^E + \omega_i)}{2} \qquad D_i'' = \frac{\alpha''(\omega_s^E - \omega_i) - \alpha''(\omega_s^E + \omega_i)}{2}.$

1. The magnetic torque (eddy currents)

where

Angular velocities of the harmonic components of the magnetic field

 $\alpha(\omega) = \alpha' + j\alpha''$ Fourier transform of the magnetic polarizability

 $\omega_3 = \omega_4 = \omega_{\oplus} + 2n$

 $\omega_5 = \omega_6 = 2n$

 $\omega_7 = \omega_8 = \omega_{\oplus},$

per unit of volume V of the satellite

The involved torques

We consider in the case of the two LAGEOS satellites four torques:

- The magnetic torque (eddy currents) 1.
- The gravitational torque 2.
- The asymmetric reflectivity torque (C_R differences) 3.
- The CoM offset torque (with respect to the center of geometry) 4.
 - $\frac{dL}{dt} = M_{mag} + M_{grav} + M_{ar} + M_{offset}$

Angular momentum evolution

 $V\sum_{i=1}^{9} \frac{\mathbf{B}_{i} \cdot \boldsymbol{\omega}_{s}}{2|\boldsymbol{\omega}_{s}|^{2}} \left\{ \left[\alpha'(\omega_{i}) - A_{i}' \right] \left[1 + \cos(2\omega_{i}t + 2\varphi_{i}) \right] - \left[D_{i}'' + \alpha''(\omega_{i}) \right] \sin(2\omega_{i}t + 2\varphi_{i}) \right\} \left(\boldsymbol{\omega}_{s} \times \boldsymbol{B}_{i} \right) + \left[\sum_{i=1}^{9} \frac{\mathbf{B}_{i} \cdot \boldsymbol{\omega}_{s}}{2|\boldsymbol{\omega}_{s}|^{2}} \left\{ \left[\alpha'(\omega_{i}) - A_{i}' \right] \left[1 + \cos(2\omega_{i}t + 2\varphi_{i}) \right] - \left[D_{i}'' + \alpha''(\omega_{i}) \right] \sin(2\omega_{i}t + 2\varphi_{i}) \right\} \left(\boldsymbol{\omega}_{s} \times \boldsymbol{B}_{i} \right) \right\}$ $V\sum_{i=1}^{9} \frac{B_i \cdot \boldsymbol{\omega}_s}{2|\boldsymbol{\omega}_s|} \left\{ -A_i'' \left[1 + \cos(2\omega_i t + 2\varphi_i) \right] + D_i' \sin(2\omega_i t + 2\varphi_i) \right\} B_i$

$$M^{b}_{grav} = 3\omega_{\oplus}^{2} \left\{ \hat{s}^{b} \times \left[I_{x} (\hat{s}^{b} \cdot \hat{x}^{b}) \hat{x}^{b} + I_{y} (\hat{s}^{b} \cdot \hat{y}^{b}) \hat{y}^{b} + I_{z} \left(\hat{s}^{b} \cdot \hat{z}^{b} \right) \hat{z}^{b} \right] \right\}$$

 $M_{mag}^{E} = V \sum_{i=1}^{9} \frac{|B_{i}|^{2}}{2|\omega_{s}|} \left\{ A_{i}^{\prime\prime} \left[1 + \cos(2\omega_{i}t + 2\varphi_{i}) \right] - D_{i}^{\prime} \sin(2\omega_{i}t + 2\varphi_{i}) \right\} \omega_{s} +$

$$M_{ar}^{b} = \nu \frac{2}{3} \rho^{3} \frac{\Phi}{c} \Delta \rho C_{R} \left(\hat{z}^{b} \times \hat{s}_{\odot}^{b} \right) \left| \hat{z}^{b} \times \hat{s}_{\odot}^{b} \right|$$

$$M^b_{off} =
u \pi \rho^2 \frac{\Phi}{c} C_R \left(h^b \times \hat{s}^b_{\odot} \right)$$

$$M_{ar}^{b} = \nu \frac{2}{3} \rho^{3} \frac{\Phi}{c} \Delta \rho C_{R} \left(\hat{z}^{b} \times \hat{s}_{\odot}^{b} \right) \left| \hat{z}^{b} \times \hat{s}_{\odot}^{b} \right|$$

The Euler equations

 $I_x \dot{\omega}_{sx}^b - \omega_{sy}^b \omega_{sz}^b (I_y - I_z) = M_x$ $I_y \dot{\omega}_{sy}^b - \omega_{sx}^b \omega_{sz}^b (I_z - I_x) = M_y$ $I_z \dot{\omega}_{sz}^b - \omega_{sx}^b \omega_{sy}^b (I_x - I_y) = M_z$

We wrote the Euler equations in the body frame using the Euler angles with respect to the Earth Centered Inertial (ECI) reference frame:

$$\begin{split} \ddot{\theta} &= \frac{M_x}{I_x} \cos \psi - \frac{M_y}{I_y} \sin \psi - \frac{I_z}{I_y} \dot{\phi} \dot{\psi} \sin \theta + \frac{I_y - I_z}{I_x} \dot{\phi}^2 \frac{\sin(2\theta)}{2} \\ &+ \frac{I_x - I_y}{I_x} \Lambda_y \left[\dot{\theta} (\dot{\psi} + \dot{\phi} \cos \theta) \frac{\sin(2\psi)}{2} + \dot{\phi}^2 \frac{\sin(2\theta)}{2} \sin^2 \psi - \dot{\phi} \dot{\psi} \sin \theta \left(\frac{I_y - I_z}{\Lambda} - \sin^2 \psi \right) \right] \end{split}$$
(4)
$$\begin{split} \ddot{\phi} &= \frac{M_y \cos \psi}{I_y} \frac{M_x \sin \psi}{\sin \theta} + \frac{I_z}{I_x} \frac{\dot{\psi} \dot{\theta}}{\sin \theta} - \frac{\Lambda}{I_x} \frac{\cos \theta}{\sin \theta} \dot{\phi} \dot{\theta} \\ &+ \frac{I_x - I_y}{I_y} \Lambda_I \left[\frac{1}{\sin \theta} \left(\sin^2 \psi - \frac{I_x}{\Lambda} \right) \dot{\psi} \dot{\theta} - \frac{\sin(2\psi)}{2} (\cos \theta \dot{\phi} + \dot{\psi}) \dot{\phi} - \frac{\cos \theta}{\sin \theta} \dot{\phi} \dot{\theta} \cos^2 \psi \right] \end{aligned}$$
(5)
$$\begin{split} \ddot{\psi} &= \frac{M_z}{I_z} - \frac{\cos(\theta)}{\sin(\theta)} \left(\frac{M_y}{I_y} \cos(\psi) + \frac{M_x}{I_x} \sin(\psi) \right) + \dot{\phi} \dot{\theta} \frac{1}{\sin \theta} \left(\frac{I_y - I_z}{I_x} \cos^2 \theta + 1 \right) - \frac{I_z}{I_y} \dot{\psi} \dot{\theta} \frac{\cos \theta}{\sin \theta} \\ &+ (I_x - I_y) \left[\frac{1}{I_z} \dot{\phi} \dot{\theta} \frac{1}{\sin \theta} \left(\sin^2 \theta \cos(2\psi) + \frac{\Lambda}{I_x I_y} \cos^2 \psi \cos^2 \theta \right) - \dot{\theta}^2 \frac{1}{2I_z} \sin(2\psi) - \dot{\phi}^2 \frac{1}{2I_z} \sin(2\psi) \left(\frac{\Lambda I_z}{I_x I_y} \cos^2 \theta - \sin^2 \theta \right) \\ - \dot{\psi} \dot{\theta} \frac{1}{I_y} \frac{\cos \theta}{\sin(\theta)} \left(\frac{\Lambda}{I_x} \sin^2 \psi - 1 \right) + \frac{\Lambda}{2I_x I_y} \dot{\phi} \dot{\psi} \cos \theta \sin(2\psi) \right], \qquad \Lambda = I_x + I_y - I_z \end{aligned}$$
(6)

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TABLE I.	Mechanical	parameters	used in	the equations:	mo-
ments of ind	ertia I, ray R	and offset	h of th	e satellites.	

	LAGEOS	LAGEOS II	LARES
$I_{\rm r}[{\rm kg}{\rm m}^2]$	10.96 ± 0.03	11.00 ± 0.03	4.76 ± 0.03
$I_{v}[\text{kg}\text{m}^{2}]$	10.96 ± 0.03	11.00 ± 0.03	4.76 ± 0.03
I_z [kg m ²]	11.42 ± 0.03	11.45 ± 0.03	4.77 ± 0.03
R[cm]	30.0	30.0	18.2
h_x [cm]	0.000	0.000	0.000
$h_{y}[cm]$	0.000	0.000	0.000
h_z [cm]	0.040	0.055	0.000

TABLE III. Optical parameters used in the equations: radiation coefficient C_R and reflectivity difference between the hemispheres $\Delta \rho$ of the satellites.

	LAGEOS	LAGEOS II	LARES
C_R	1.13	1.12	1.07
Δho	0.013	0.012	0

TABLE II. Electromechanical parameters used in the equations: dimensionless magnetic factors β' and β'' , electrical conductivity σ and the relative magnetic permeability μ_r .

	LAGEOS	LAGEOS II	LARES
β'	< 10 ⁻²	$< 10^{-2}$	1
β''	0.22	0.23	1
$\sigma[s]$	2.37×10^{17}	2.38×10^{17}	5.1×10^{16}
$\mu_r - 1$	2.2×10^{-5}	2.2×10^{-5}	3.3×10^{-7}

TABLE IV. Spin initial conditions: reference epoch in Modified Julian Date (MJD), rotational period P_s , right ascension RA and declination dec.

	LAGEOS	LAGEOS II	LARES
Epoch [MJD]	42913.5	48918	55970
P_s [s]	0.48	0.81	11.8
RA [degree]	150	230	186.5
dec [degree]	-68	-81.8	-73

LArase Satellites Spin mOdel Solutions (LASSOS)

LASSOS Spin Model: results for LAGEOS

Blue = LARASE model for the rapid-spin Red = LARASE general model

Andrés de la Fuente, J.I., 2007. Enhanced æ Modelling of LAGEOS Non-Gravitational æ Perturbations (Ph.D. thesis). Delft University Press. Sieca Repro, Turbineweg 20, 2627 BP Delft, The Netherlands. Kucharski, D., Lim, H.C., Kirchner, G., Hwang, J.Y., 2013. Spin parameters of LAGEOS-1 and LAGEOS-2 spectrally determined from Satellite Laser Ranging data. Adv. Space Res. 52, 1332–1338.



Spin Orientation: α , δ

LASSOS Spin Model: results for LAGEOS

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LArase Satellites Spin mOdel Solutions (LASSOS)

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Rotational Period: P

LArase Satellites Spin mOdel Solutions (LASSOS)

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Spin Orientation: α , δ

LASSOS Spin Model: results for LAGEOS II

Blue = LARASE model for the rapid-spin **Red** = LARASE general model

LArase Satellites Spin mOdel Solutions (LASSOS)



Rotational Period: P



LASSOS Spin Model: results for LARES



LArase Satellites Spin mOdel Solutions (LASSOS)

Blue = LARASE model for the rapid-spin Red = LARASE general model



• The spin evolution is almost due to the magnetic torque

• The gravitational torque is almost null, we fit the data with an oblateness of about: $\frac{C-A}{C} < 10^{-4}$

LASSOS Spin Model: results for LAGEOS II

Blue = LARASE model for the rapid-spin Red = LARASE general model

LArase Satellites Spin mOdel Solutions (LASSOS)

Cartesian components in J2000





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Comprehensive model for the spin evolution of the *LAGEOS* and *LARES* satellites

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We have developed LATOS a new thermal model for LAGEOS satellites

LArase Thermal mOdel Solutions (LATOS)

Motivation:

Necessity of improved models for the NGP

- Thermal drag/thrust effects (Yarkovsky effect, Yarkovsky-Schach effect)
- Albedo
- Asymmetric reflectivity (LAGEOS, LAGEOS II)

Previous models:

Rubincam, D.P., 1987. LAGEOS orbit decay due to infrared radiation from Earth. J. Geophys. Res. 92, 1287–1294. Rubincam, D.P., 1988. Yarkovsky thermal drag on LAGEOS. J. Geophys. Res. 93, 13805–13810. Rubincam, D.P., 1990. Drag on the LAGEOS satellite. J. Geophys. Res. 95, 4881–4886. Farinella, P., Nobili, A.M., Barlier, F., Mignard, F., 1990. Effects of thermal thrust on the node and inclination of LAGEOS. Astron. Astrophys. 234, 546–554. Farinella, P., Vokrouhlicky, D., 1996. Thermal force effects on slowly rotating, spherical artificial satellites-I. Solar Heating. Plan. Space Sci. 44, 1551–1561. Vokrouhlicky, D., Farinella, P., 1996. Thermal force effects on slowly rotating, spherical artificial satellites-II. Earth infrared heating. Plan. Space Sci. 45, 419–425. Slabinski, V.J., 1996. A numerical solution for LAGEOS thermal thrust: the rapid-spin case. Celestial Mech. Dyn. Astron. 66, 131–179. Andrés de la Fuente, J.I., 2007. Enhanced Modelling of LAGEOS Non-Gravitational Perturbations (Ph.D. thesis). Delft University Press. Sieca Repro, Turbineweg 20, 2627 BP Delft, The Netherlands.

The thermal thrust force:

 $\mathbf{dF_T} = -\frac{2}{3}\frac{\epsilon\sigma T^4 dA}{c}\mathbf{n}$



The force, normal to each surface element dA, depends from the temperature T and emissivity ε of the part considered

It is necessary to know the temperature distribution inside the satellite and the satellite position with respect to the external heat sources (Sun and Earth)

The thermal equations:



The input to the system of differential equations are:

- Attitude of the satellite (from LASSOS model)
- Thermal and optical parameters of the satellite (from technical documentation and tests) that contribute to the different constants in the system

- The satellite is divided into several parts which are assumed to have no thermal gradient within them. For the two LAGEOS: the CCRs, the two hemispheres and the core. The rings that block the CCRs are considered isothermal to the hemispheres
- The conduction constant between the **CCRs** and the hemisphere in which they are inserted was numerically calculated using a **FEM** model



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We considered three external heat sources:

Clouds and Earth's Radiant Energy System (CERES)

- The <u>direct Sun radiation</u> using the standard value of ϕ_{\odot} = 1360.8 $\frac{W}{m^2}$ at 1 A.U.
- The Sun radiation reflected from Earth (Albedo)

We use <u>CERES</u> monthly averaged SW radiation data at the top of the atmosphere taking into account nightday alternance, satellite attitude and orbital position. The grid is 1°x1° Latitude-Longitude

The infrared radiation from the Earth

We take into account the temperature of the different parts of the Earth using the monthly averaged data from Land + Ocean 1°x1° Latitude-Longitude grid from <u>Berkeley Earth Organization</u> and from <u>CERES</u>. Attitude and orbit of the satellite are considered





- We developed two versions of the model (LATOS), an averaged one, usable for fastspin conditions, and a general one, not averaged, to be used when the spin is slow with respect to the orbital period
- By integrating the thermal equations we get the temperature distribution in the satellite and from this distribution we calculate the thermal thrust accelerations
- We then calculated the effects of the thermal accelerations (via Gauss equations) on the rate of the Keplerian elements. The results can be compared with the corresponding rate residuals from a precise orbit determination (POD)

LArase Thermal mOdel Solutions (LATOS)

LAGEOS II: accelerations in Gauss reference frame



LAGEOS II



About 27 years POD of LAGEOS II with GEODYN II

LAGEOS II



About 27 years POD of LAGEOS II with GEODYN II

LAGEOS II



$$\frac{d\omega}{dt} = \frac{\sqrt{1-e^2}}{nae} \left[-R\cos f + T\left(\sin f + \frac{\sin u}{\sqrt{1-e^2}}\right) \right] - \frac{W}{H\sin i} r\sin(\omega + f)\cos \theta$$

Being able to clean up this parameter has a particular importance for us: it contains a secular effect from **General Relativity**, due to the **Gravitoelectric** field (M) and to the **Gravitomagnetic** field (J)

About 27 years POD of LAGEOS II with GEODYN II



LAGEOS



About 27 years POD of LAGEOS with GEODYN II

LAGEOS



About 27 years POD of LAGEOS with GEODYN II

LAGEOS



About 27 years POD of LAGEOS with GEODYN II

Time [MJD]

 $imes 10^4$

Conclusions

Within the many activities of **LARASE** we developed:

- 1. a 3D cad of the satellites for a correct handling of their structure • Masses and moments of inertia have been computed
- 2. a new general spin model (LASSOS) for the two LAGEOS and LARES satellites
 - The results for the spin are in very good agreement with the available observations (orientation and rate)
 - The spin model can be used in synergy with kHz laser observations to capture the current attitude of the satellites (LAGEOS and LAGEOS II)
- 3. a new general model (LATOS) to account for the thermal thrust acceleration acting on LAGEOS II and LAGEOS
 - preliminary results for the orbital effects due to the thermal thrust accelerations on the two satellites are in good agreement with the orbital residuals
 - Thermal accelerations determined from a reliable model may reduce the use of empirical accelerations in the satellites' **POD**, with possible improvements in
 - Geophysical products
 - Fundamental physics measurements

Current activities

- 1. GEODYN II software update
- 2. NGP models improvements
- 3. Models for the Gravitational field of the Earth
- 4. Relativistic effects due to the nonlinearity of the gravitational interaction
- 5. Constraints to alternative theories of gravitation
- 6. Measurement of the GR shift of the argument of pericenter

GEODYN II software update

- update of the Normal Points Data Base and their conversion in TDF
- update of control scripts (Bash): **GEODYN** and ancillary
- update of the post-processing scripts (Python)
- creation of new arcs and new PODs (routine)
- creation of interface files

• ITRF2014:

- $\ensuremath{\circ}$ identification of the reference files
- \circ generation of a new routine for coordinate conversion
- preparation of the files import procedure, their pre-processing and consequent generation of GEODYN cards (Python)
- \circ validation with specific PODs series

NGP models improvements

- Thermal model for LARES
 - Several differences with respect to LAGEOS



LARES



NGP models improvements

- Thermal model for LARES
 - Several differences with respect to LAGEOS
- Neutral drag:
 - Extension of the analysis of the decay of LARES semi-major axis to the full solar cycle #24
 - Comparison of the effects on LARES and Ajisai



NGP models improvements

- Thermal model for LARES
 - Several differences with respect to LAGEOS
- Neutral drag:
 - Extension of the analysis of the decay of LARES semi-major axis to the full solar cycle #24
 - Comparison of the effects on LARES and Ajisai
- Spin model for dissemination
 - General model
 - Averaged model





Models for the Gravitational field of the Earth

As we have shown during the presentation concerning the measurement on the **Lense-Thirring** effect, a correct modeling of the gravitational field (**GF**) of the Earth (in particular of the even zonal harmonics) that takes into account the time dependence of the different coefficients is fundamental to obtain accurate measurements:

- GF for the joint analyses with LAGEOS and LAGEOS II
 - Starting from November 1992
- GF for the joint analyses of the two LAGEOS with LARES
 - Starting from February 2012

Relativistic effects due to the nonlinearity of the gravitational interaction

The precision of the measurements obtained on the relativistic precessions requires taking into account, in certain circumstances, effects related to the nonlinearity of the gravitational interaction

Constraints to alternative theories of gravitation

The recent precise and accurate measurement of the **Lense-Thirring** effect will allow us to constraint the predictions of some alternative theories of gravitation

Measurement of the GR shift of the argument of pericenter

A new measurement of the overall **GR** precession of the argument of pericenter of **LAGEOS II** and, possibly, of that of the older **LAGEOS**

LARASE: publications

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