

25/05/2020



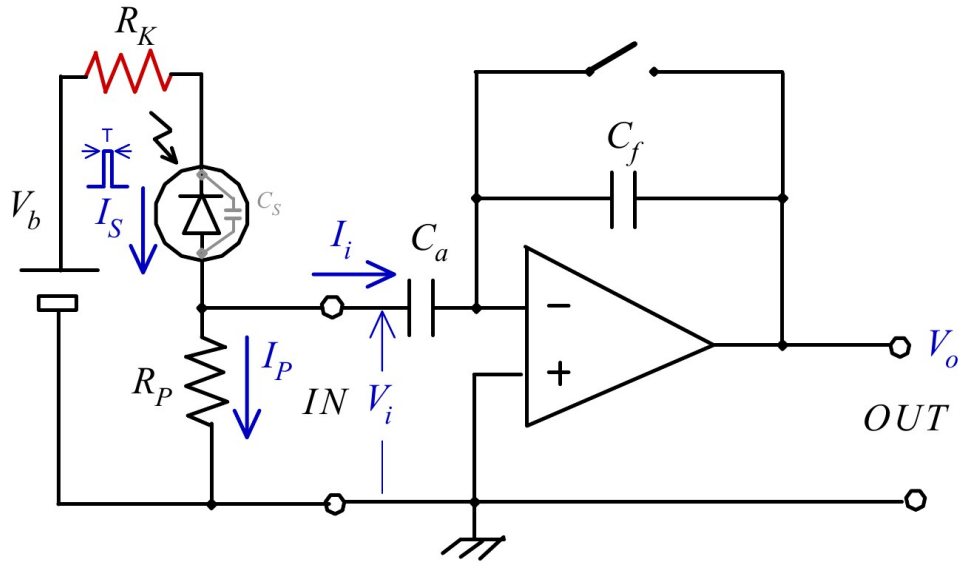
Istituto Nazionale di Fisica Nucleare
SEZIONE DI FIRENZE

HIDRA input circuit study: model and simulation

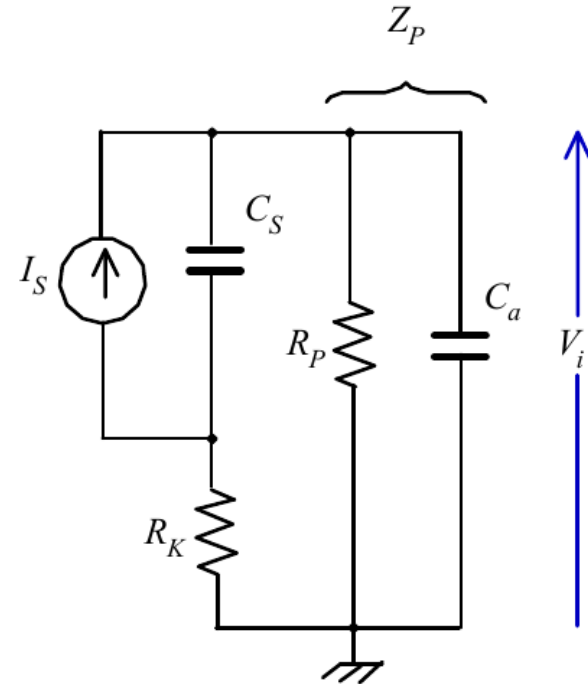
Lorenzo Pacini on behalf of Sebastiano Detti

Approximation of the circuit

Simplified scheme



Equivalent circuit



The exact calculation is described in: “Risposta globale all'impulso Sebastiano Detti”

Results of the calculation: equation

Check Sebastiano's report

$$V_{idG} = \left[V_{iT} \cdot \left(\frac{1}{2} + \frac{\omega_o}{2 \cdot \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}} \right) + \frac{V_{ST} \cdot R_P - V_{iT} \cdot (R_P + R_K)}{\sqrt{\omega_o^2 - 4 \cdot \omega_n^2} \cdot C_a \cdot R_P \cdot R_K} \right] \cdot e^{-\frac{1}{2} \cdot (\omega_o - \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}) \cdot t} +$$

$$+ \left[V_{iT} \cdot \left(\frac{1}{2} - \frac{\omega_o}{2 \cdot \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}} \right) + \frac{V_{ST} \cdot R_P - V_{iT} \cdot (R_P + R_K)}{\sqrt{\omega_o^2 - 4 \cdot \omega_n^2} \cdot C_a \cdot R_P \cdot R_K} \right] \cdot e^{-\frac{1}{2} \cdot (\omega_o + \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}) \cdot t}$$

Sintesi rete d'ingresso

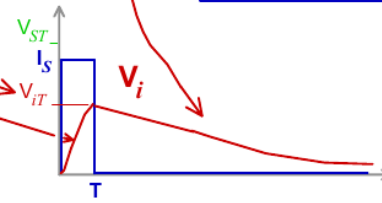
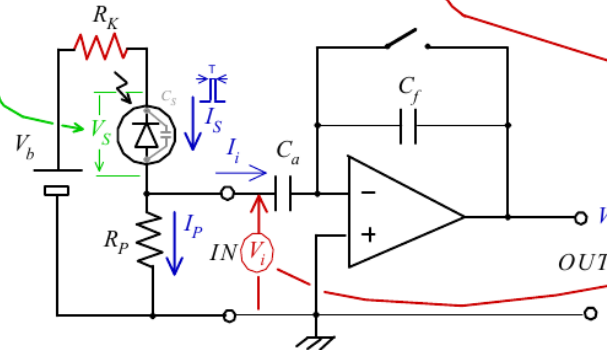
$$V_{ST} = I_S \cdot \left\{ \frac{[2 - C_S \cdot (R_P + R_K) \cdot (\omega_o + \sqrt{\omega_o^2 - 4 \cdot \omega_n^2})] \cdot e^{-\frac{1}{2}(\omega_o - \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}) \cdot T} + [C_S \cdot (R_P + R_K) \cdot (\omega_o - \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}) - 2] \cdot e^{-\frac{1}{2}(\omega_o + \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}) \cdot T}}{2 \cdot C_S \cdot \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}} + R_P + R_K \right\}$$

$$V_{iG} = I_S \cdot R_P \cdot \left[\frac{2 \cdot \omega_n^2}{\sqrt{\omega_o^2 - 4 \cdot \omega_n^2}} \cdot \left(\frac{e^{-\frac{\omega_o + \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}}{2} \cdot t}}{\omega_o + \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}} - \frac{e^{-\frac{\omega_o - \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}}{2} \cdot t}}{\omega_o - \sqrt{\omega_o^2 - 4 \cdot \omega_n^2}} \right) + 1 \right]$$

$$V_{iT} = V_{iG} \Big|_{t=T}$$

$$\omega_o = \frac{R_P \cdot (C_a + C_S) + C_S \cdot R_K}{C_S \cdot C_a \cdot R_P \cdot R_K}$$

$$\omega_n^2 = \frac{1}{C_S \cdot C_a \cdot R_P \cdot R_K}$$



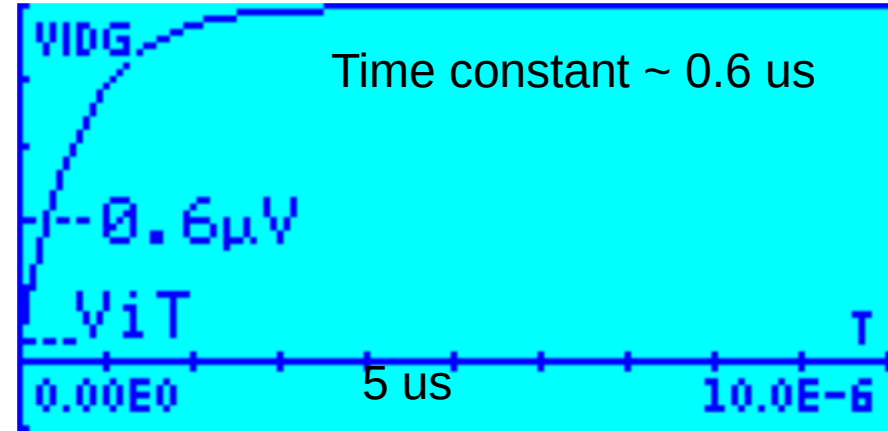
Results of the calculation: some plots

Vi vs Time

Current pulse
parameters:

Width : 50 ns
Amplitude: 300 nA
Charge: 15 fC

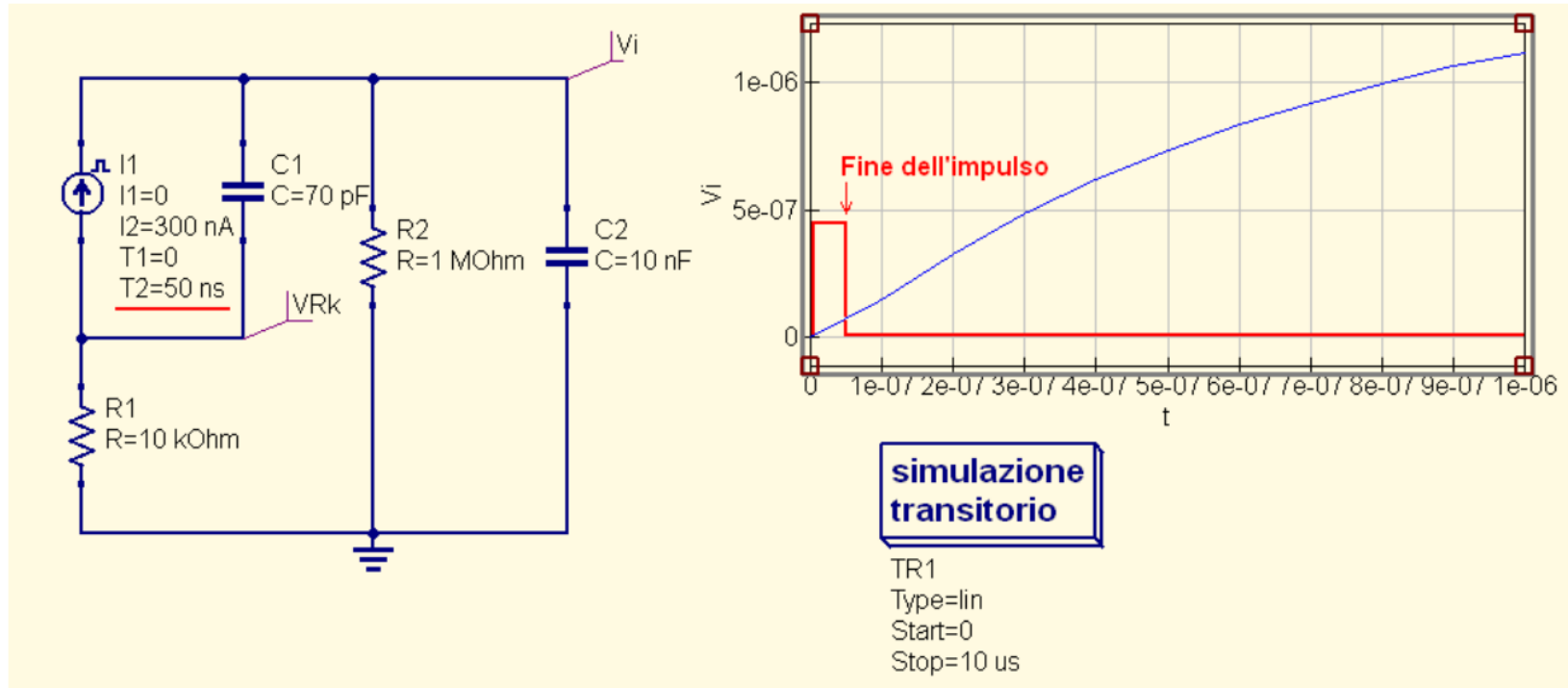
$$\left\{ \begin{array}{l} R_K = 10 K\Omega \\ R_P = 1 M\Omega \\ C_S = 70 pF \\ C_a = 10 nF \end{array} \right.$$



The input voltage of the HIDRA chip increases for a long time ($\sim 1 \mu s$) after the end of the input current.

This feature is not present when the R_k is ~ 0 .

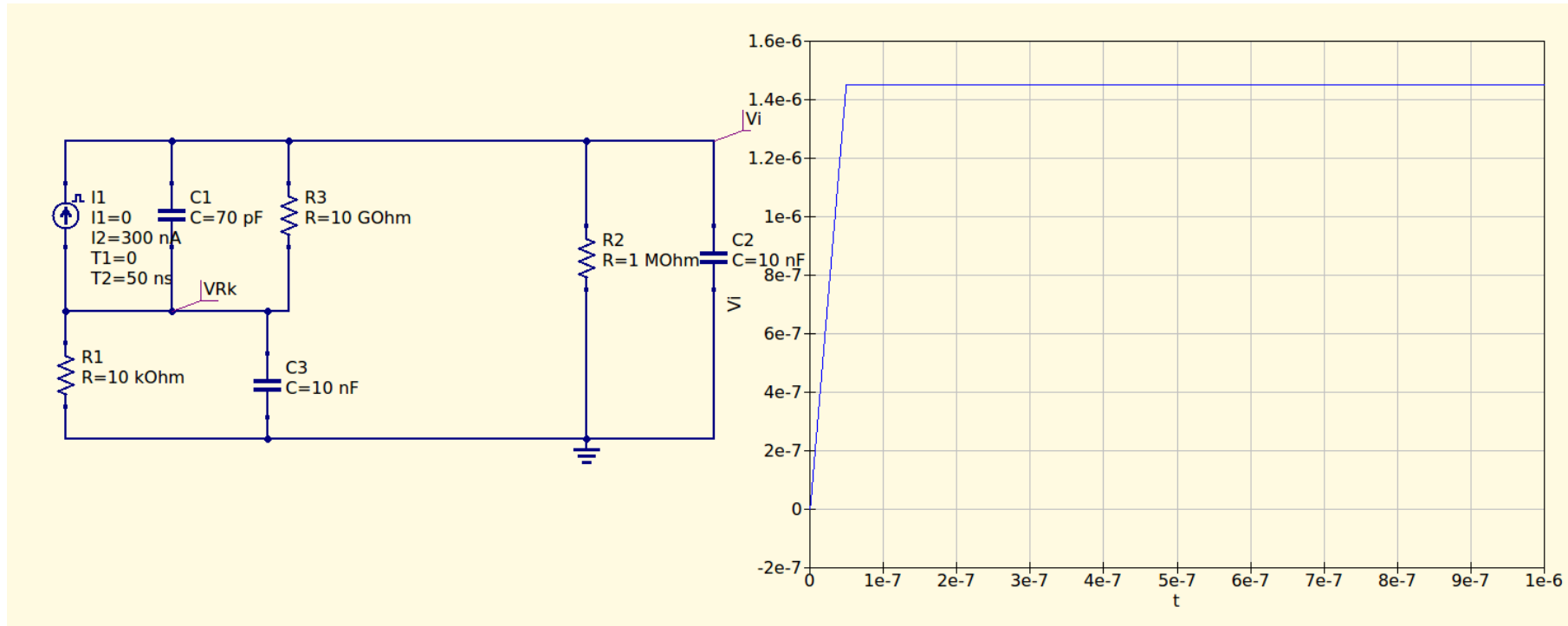
QUCS simulation confirmation



QUCS simple simulation confirm the model.

How to solve: remove Rk (of course), add a big capacitance after Rk

QUCS: test of the 10 nF capacitance



Both solutions seems to completely remove the issue.

Real case: a residual dependence steel remains, is it due to a parasitic R? Unknown effect?

Summary

R_k separates the diode capacitor and C_i . This allows a different voltage of C_i and C_s during the injection of the current. A long time is needed to recover from this difference, since C_s discharges through R_k ($C_s * R_k \sim 0.7$ us as observed by simulation and calculation)

Removing R_k or adding a big capacitor solves the issue.

Residual dependence remains: to be understood.

Next step:

- confirm the residual dependence with MIP (using SiPMs in parallel to the PD to select true MIP signals).
- check the LED light tentative slow talis.

