

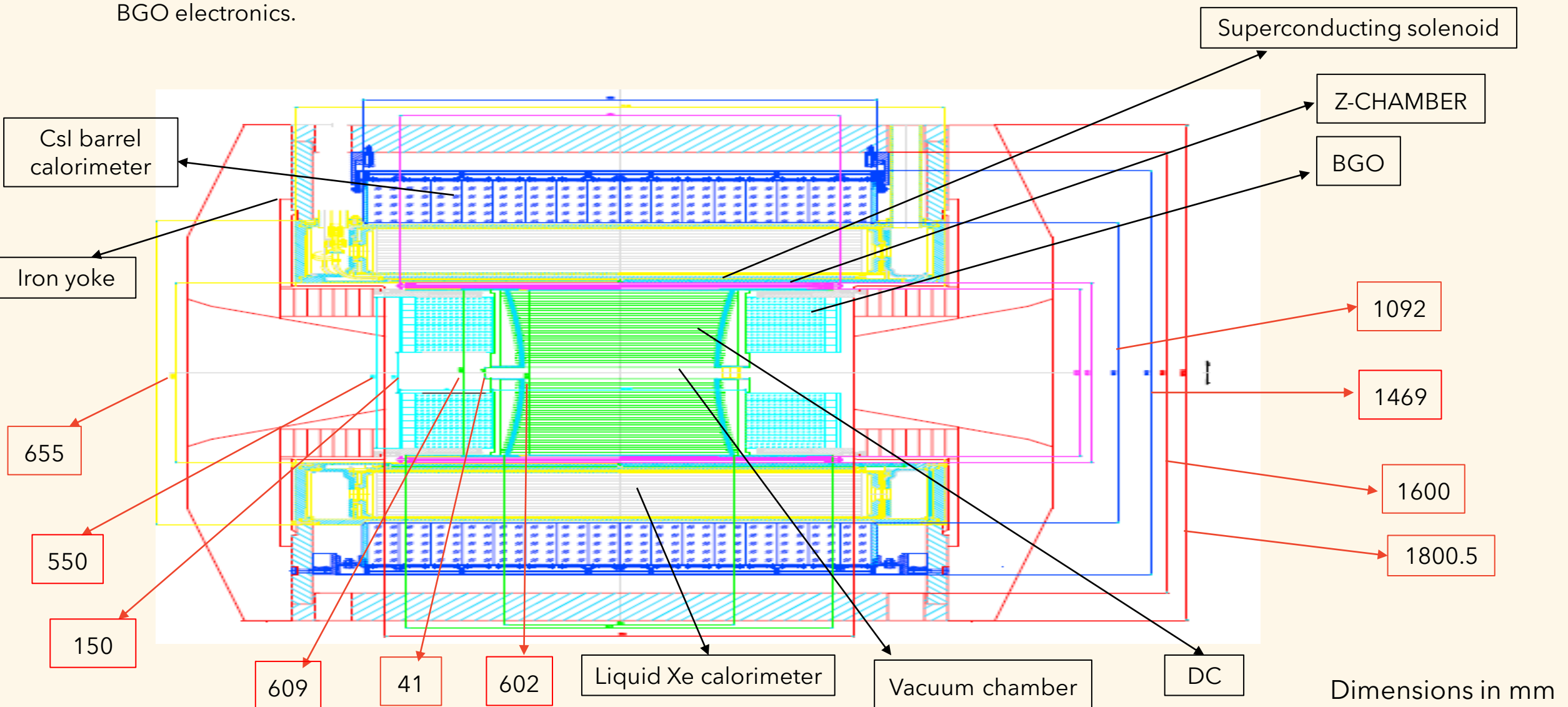


**MECHANICAL DESIGN PROPOSAL
FOR CMD-3 DRIFT CHAMBER**

DIMENSIONS

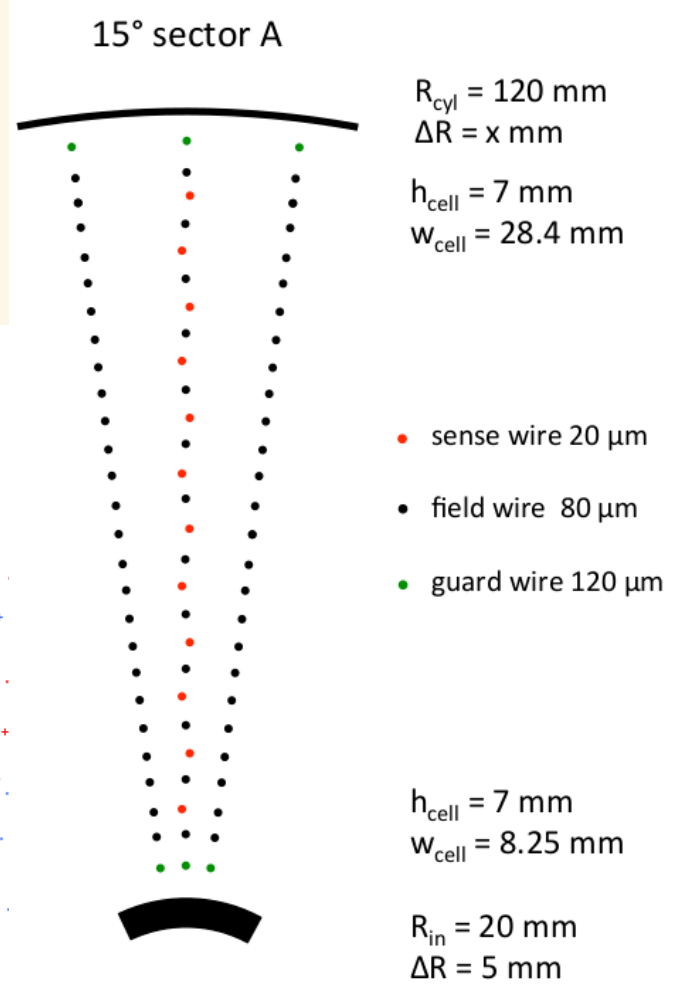
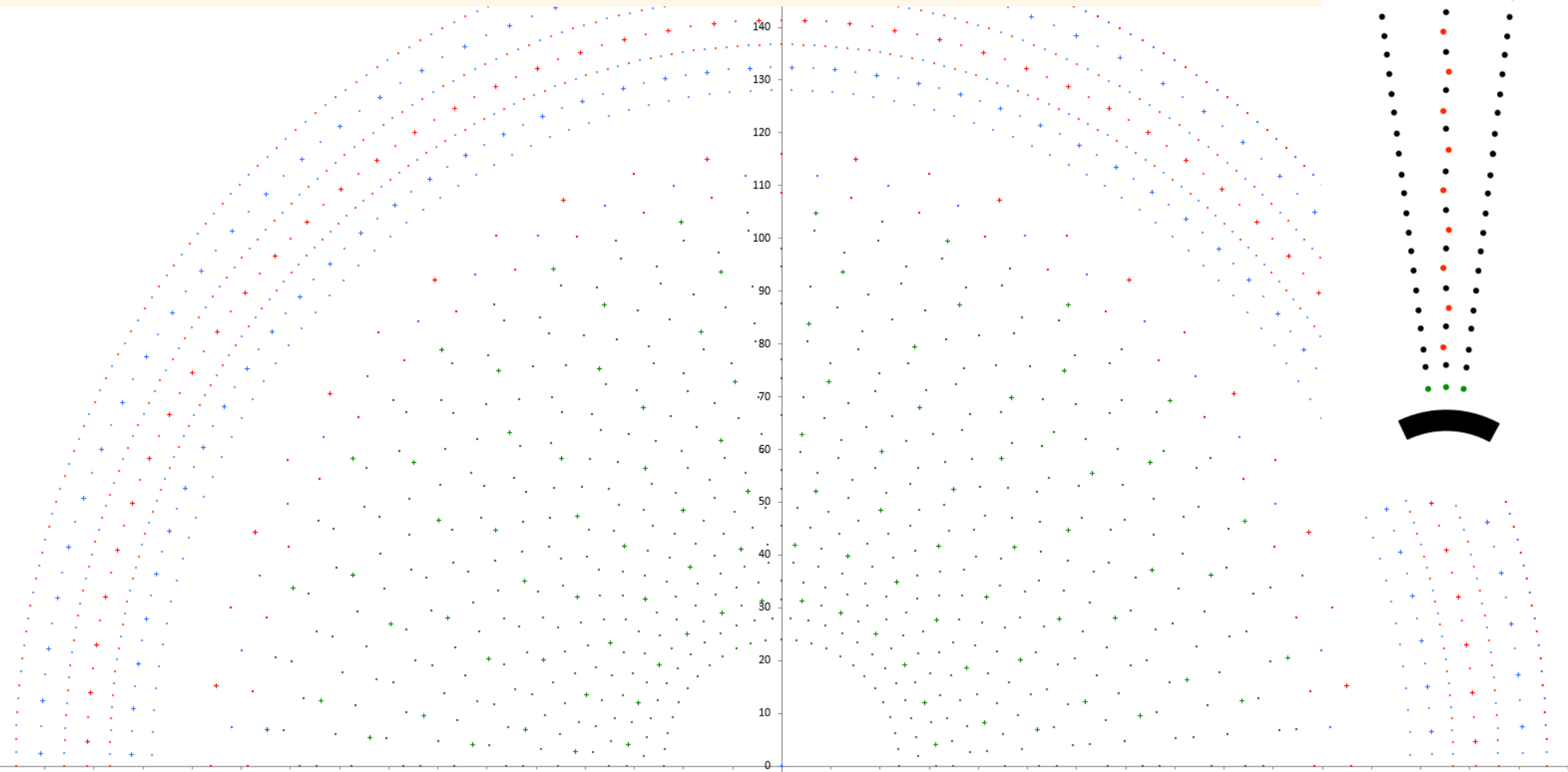
- Along beam axis (distance between end-cap calorimeter) = 609 mm
- Transverse direction (diameter) = 484 mm
- Inner shell= 41 mm

The size along beam will be change not more than **5-15 mm**, due to the optimization of BGO electronics.



Sector A (some remarks)

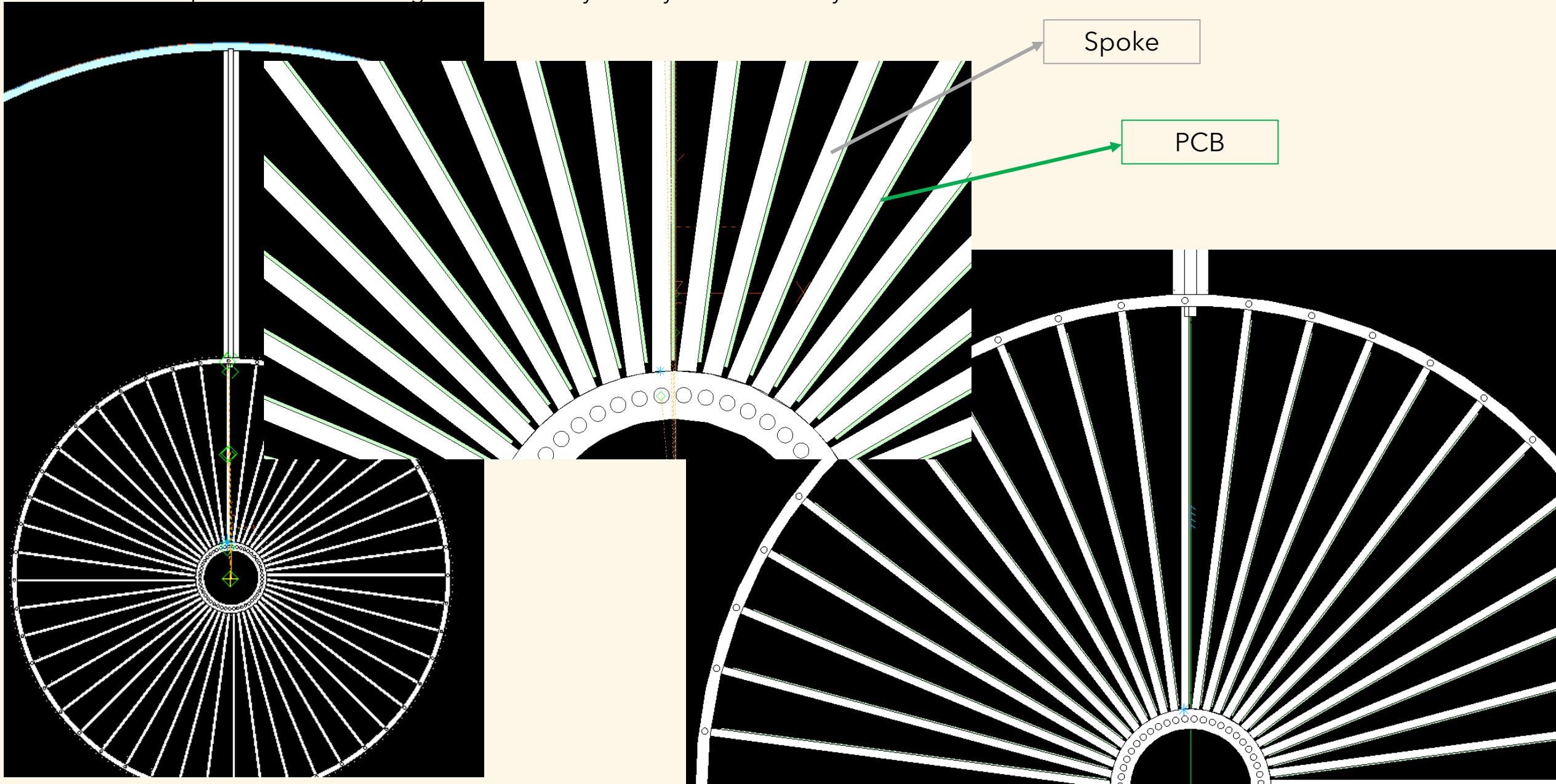
Goal: positioning of wires on the axis of the cylinder to know precisely their position in the space



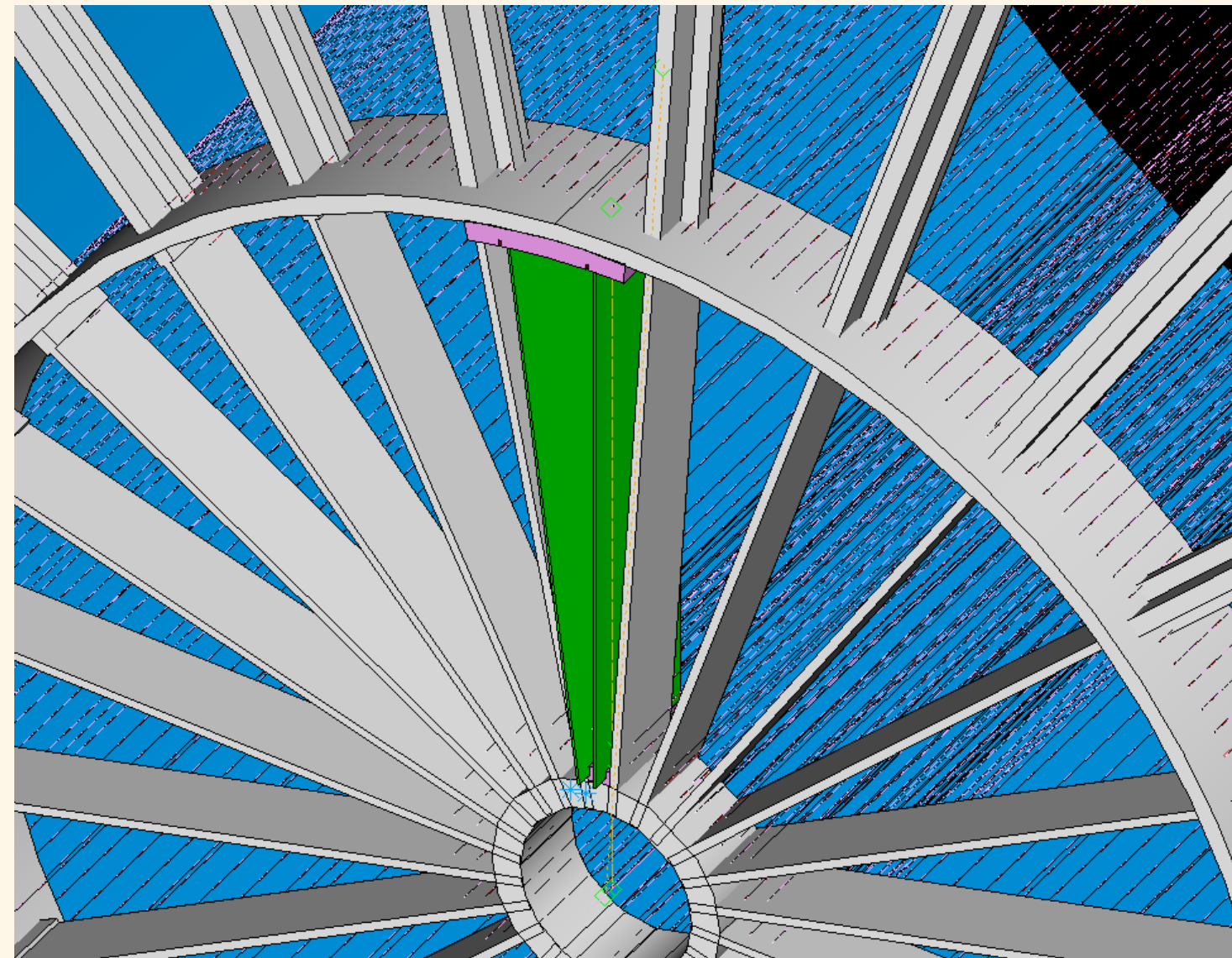
Several attempts to build the sector A

1) Constrain the PCBs to the spokes

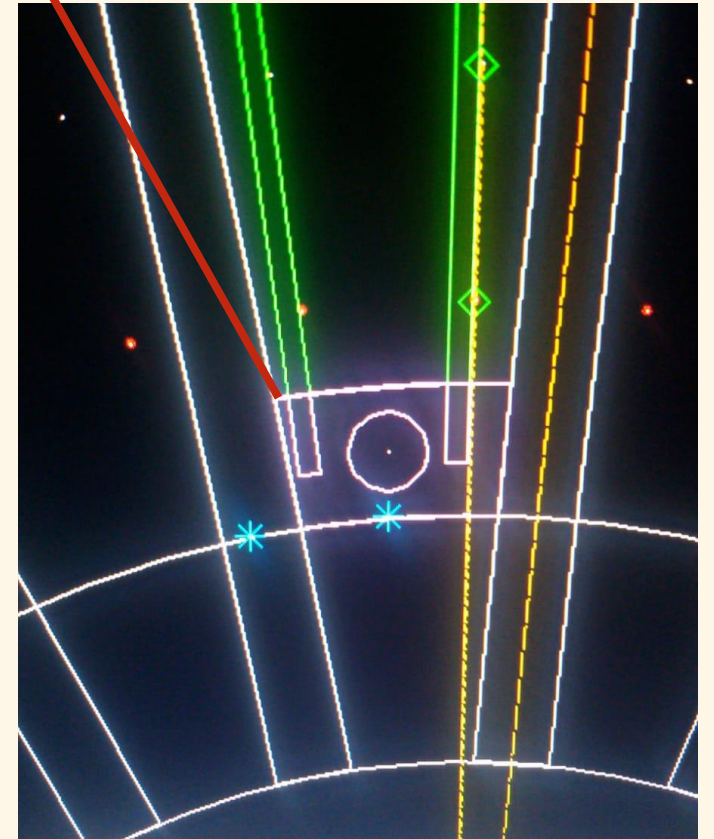
-The spokes will not converge towards the symmetry center of our cylinder



- 2) Put the PCBs between two spokes and use a support to fix them:
- Same problem for the spokes
 - Really tiny dimensions for the support

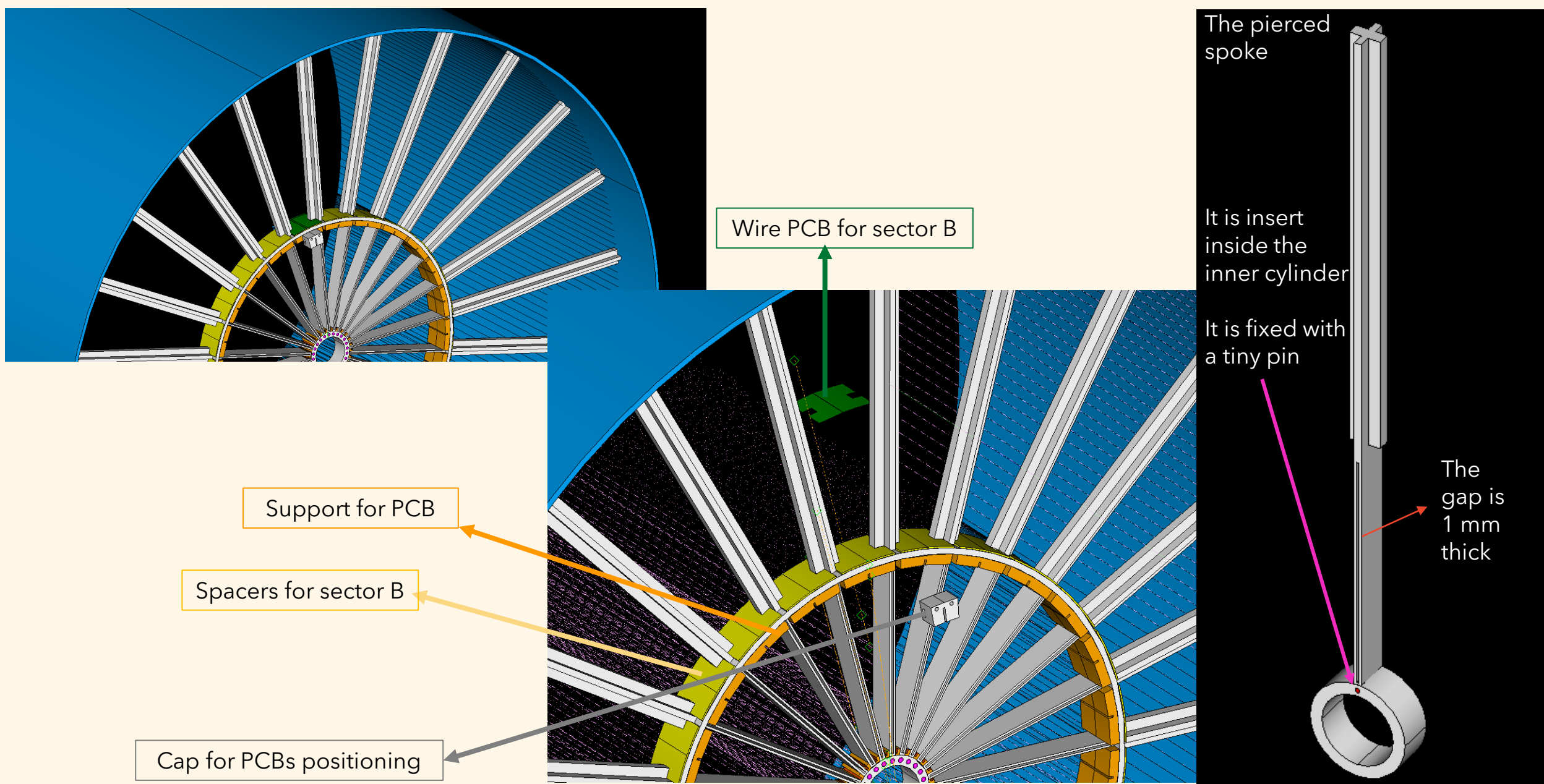


$\approx 150 \mu\text{m}$



The «pierced» spokes

The solution for the correct positioning of wire and the preserving of the geometrical symmetry seems to be the «**pierced**» spokes.

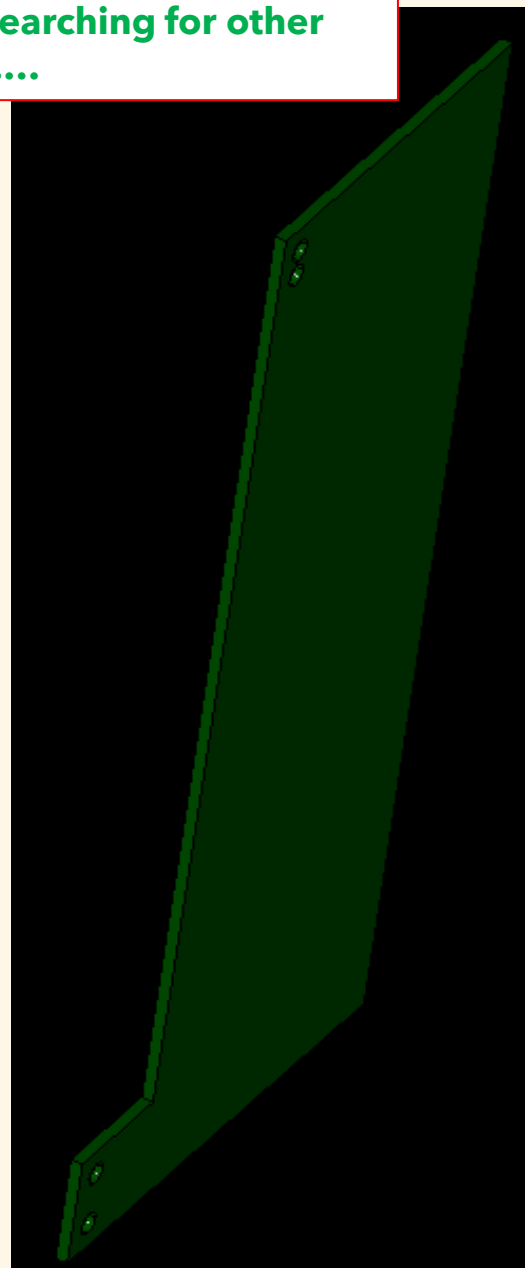
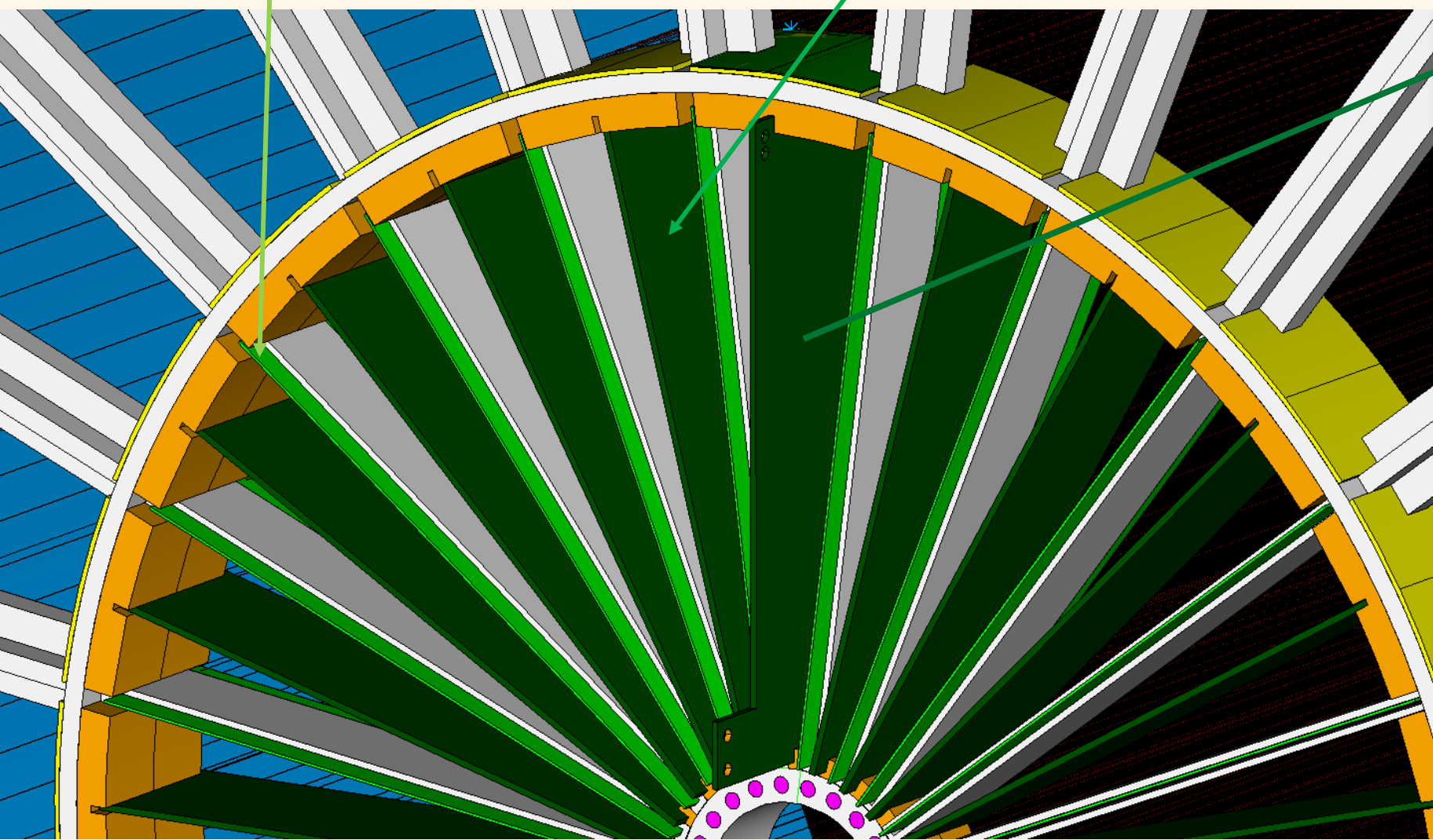


We intend to use two different thickness for PCBs

The ones inside spokes : 400 μm

The ones between two adjacent spokes : 1 mm

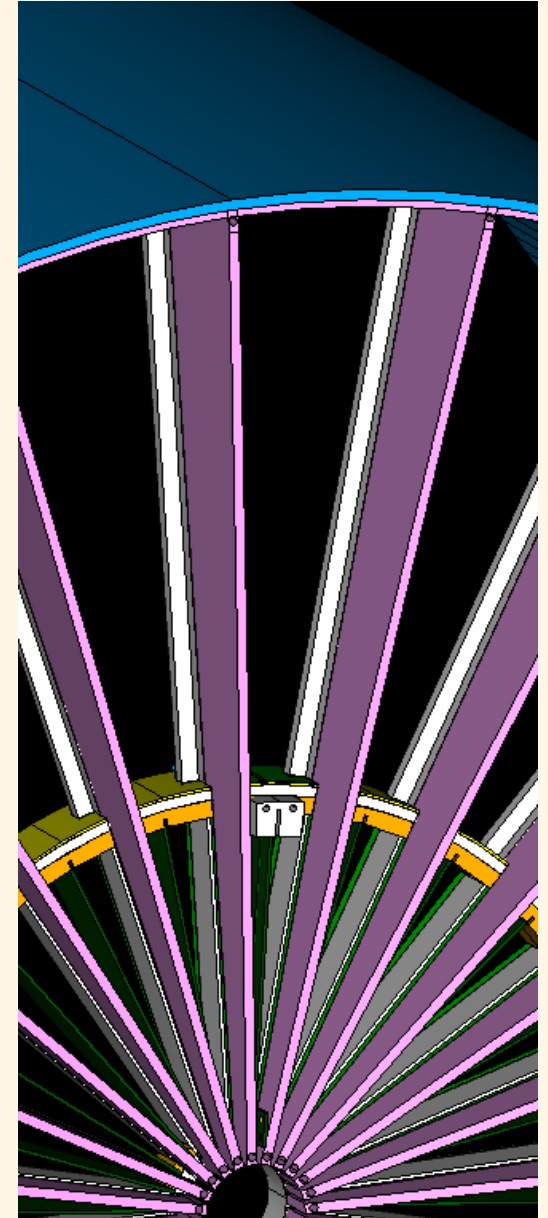
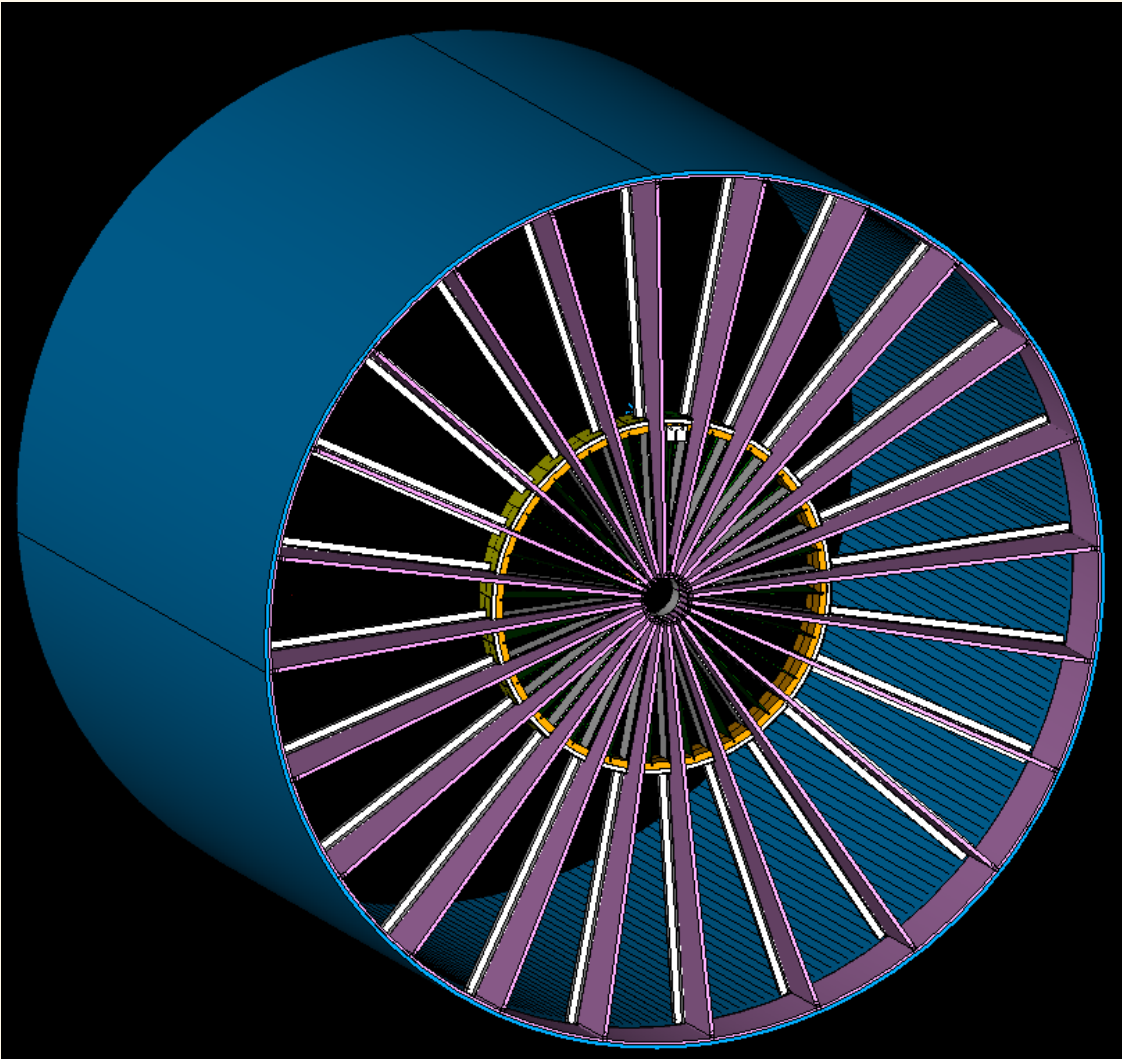
Possible solution to fix the position of PCB between two spokes.
We are searching for other solution....



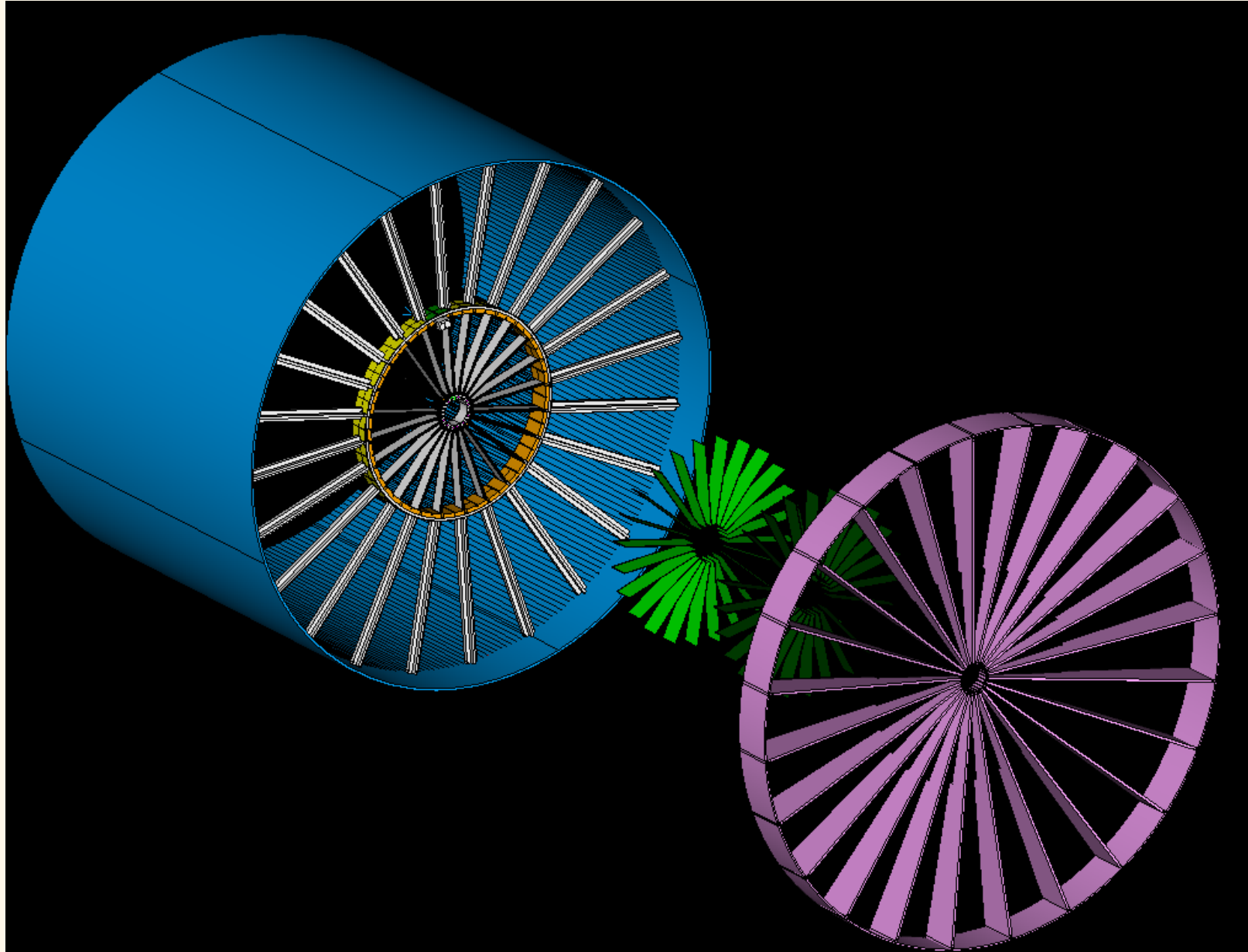
A trapezoidal structure to prevent the endplates deformation instead of tie rods

Previous calculation showed that:

- the load on the tie rods are really high
- the available space to fix the rods on the external cylinder is very small



Exploded view of the total structure



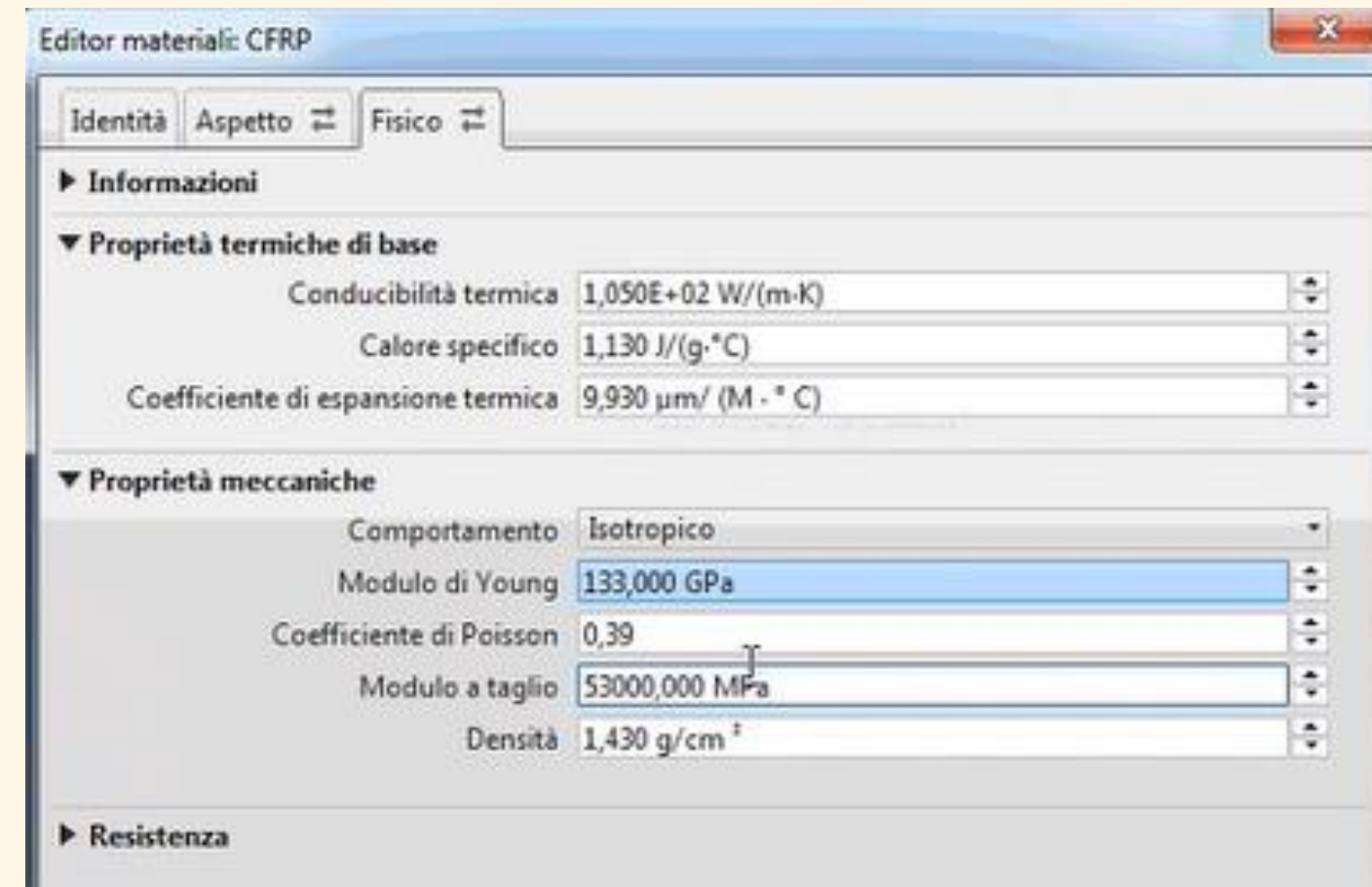
Some details about dimensions:

1. Inner cylinder :
 - Thickness = 5 mm
 - Width = 15 mm
2. Middle cylinder:
 - Thickness = 3 mm
 - Width = 25 mm
3. External cylinder :
 - Thickness = 3 mm
 - Width = 609 mm

Simulations

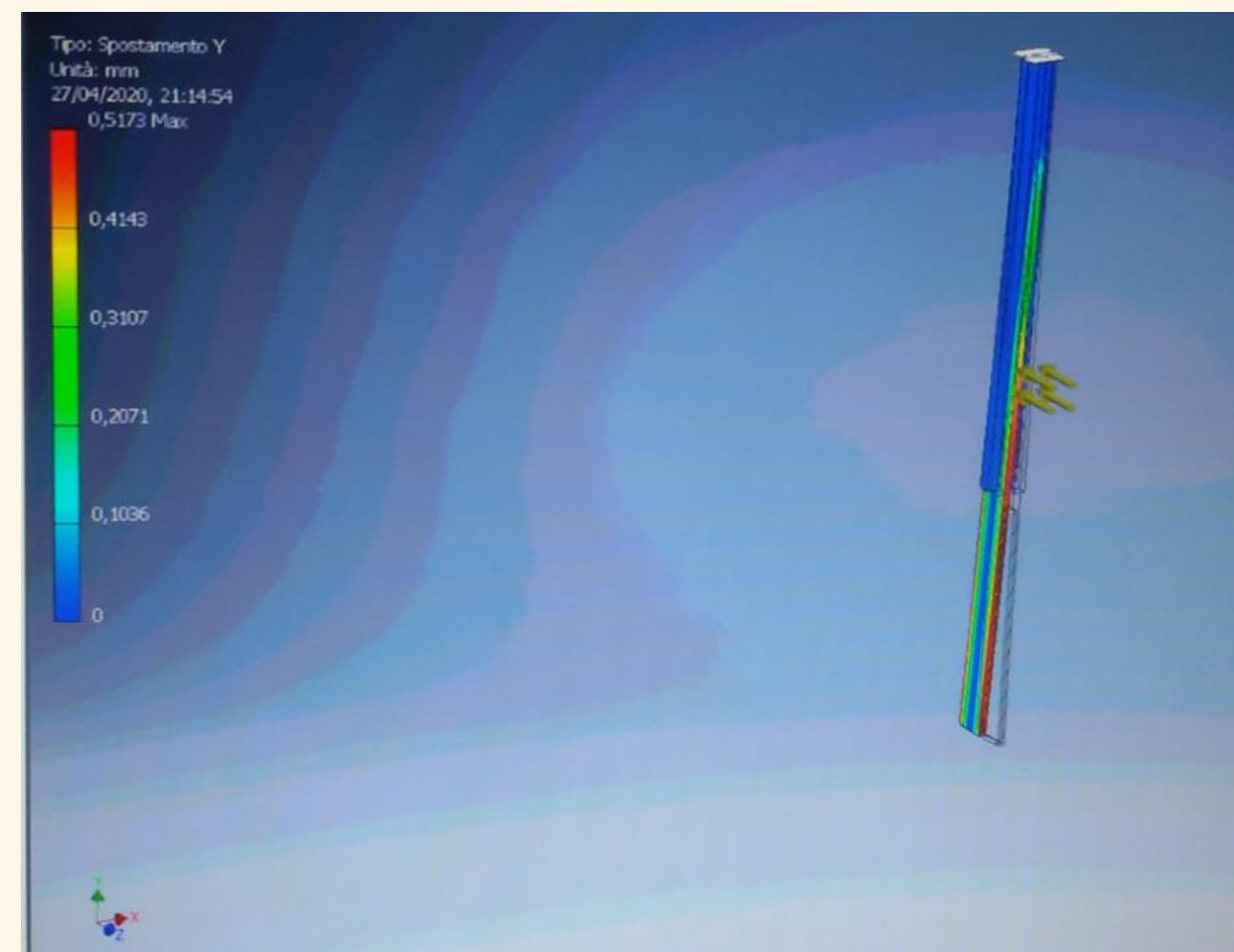
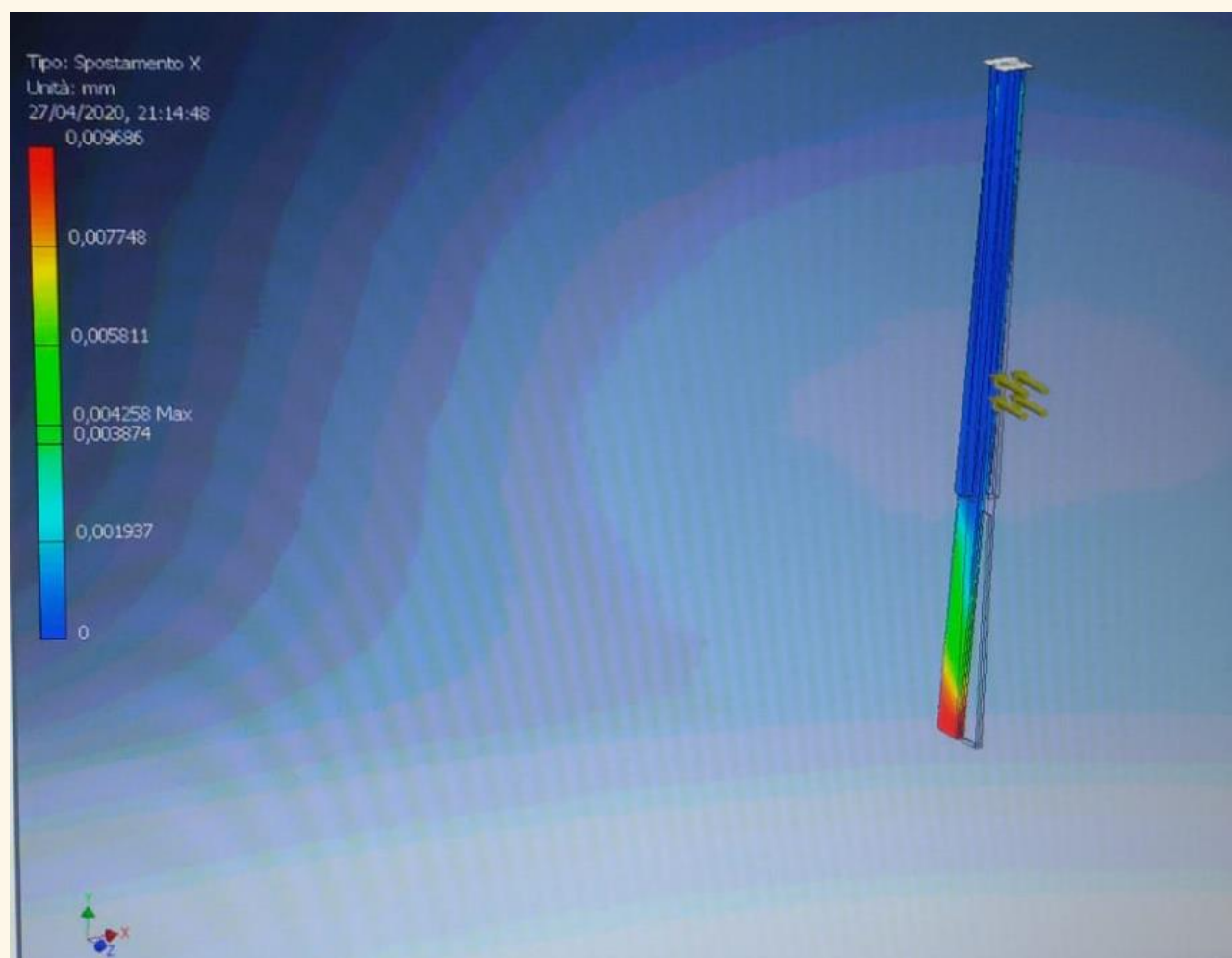
To perform simulations about the mechanical stability, we choose, as first approach, the **worst possible conditions**:

- we apply a stress about 85 Kg, higher than the expected one.
- We choose a «standard» material, with not particular features



In the future simulations we will implement the real conditions of the mechanical structure:
We will put the correct stress value and use a material with better features

Spokes simulations (x and y displacement)

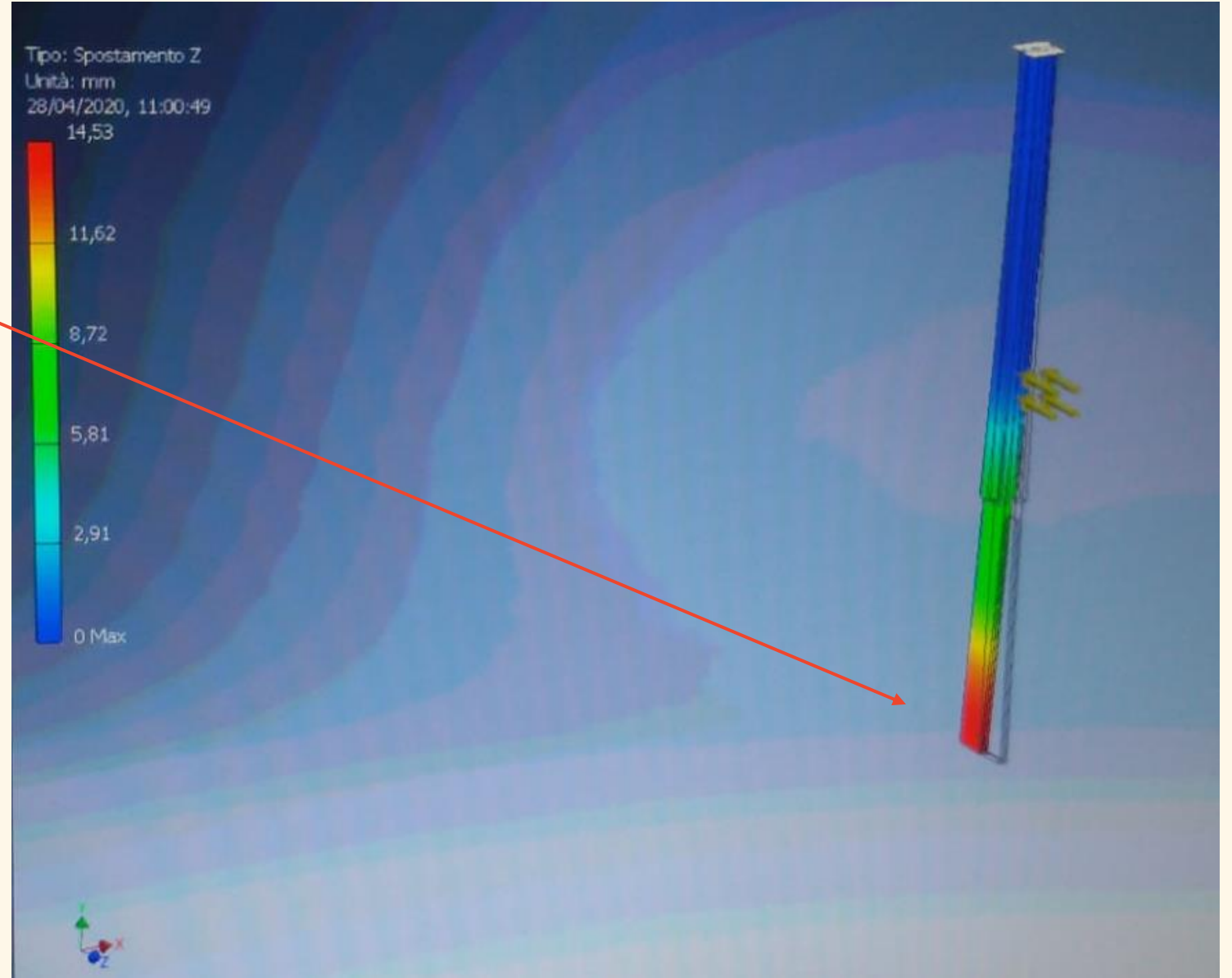


Spokes simulations (z displacement)

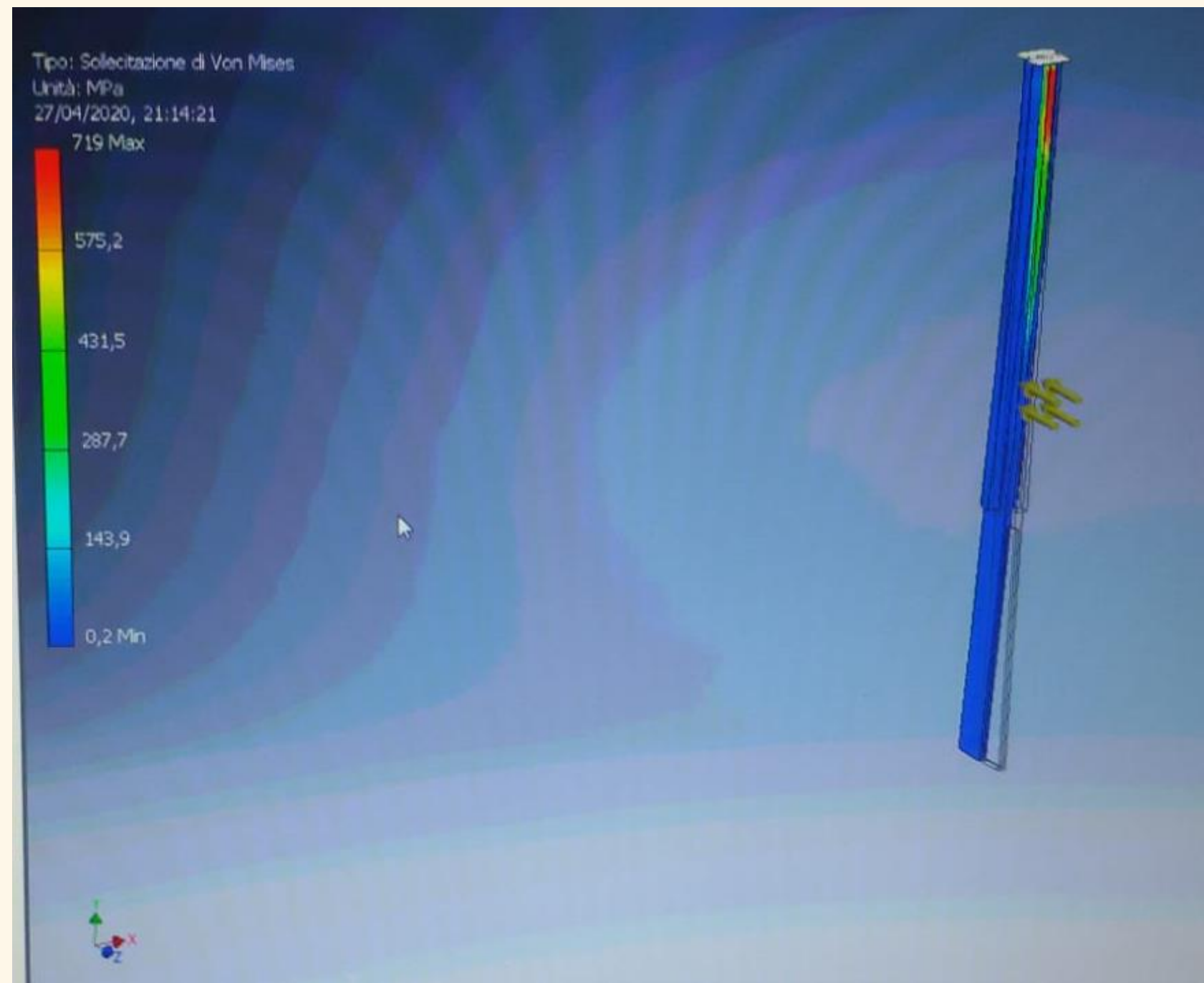
Note :

we have a shift of about 14 mm along z axis.

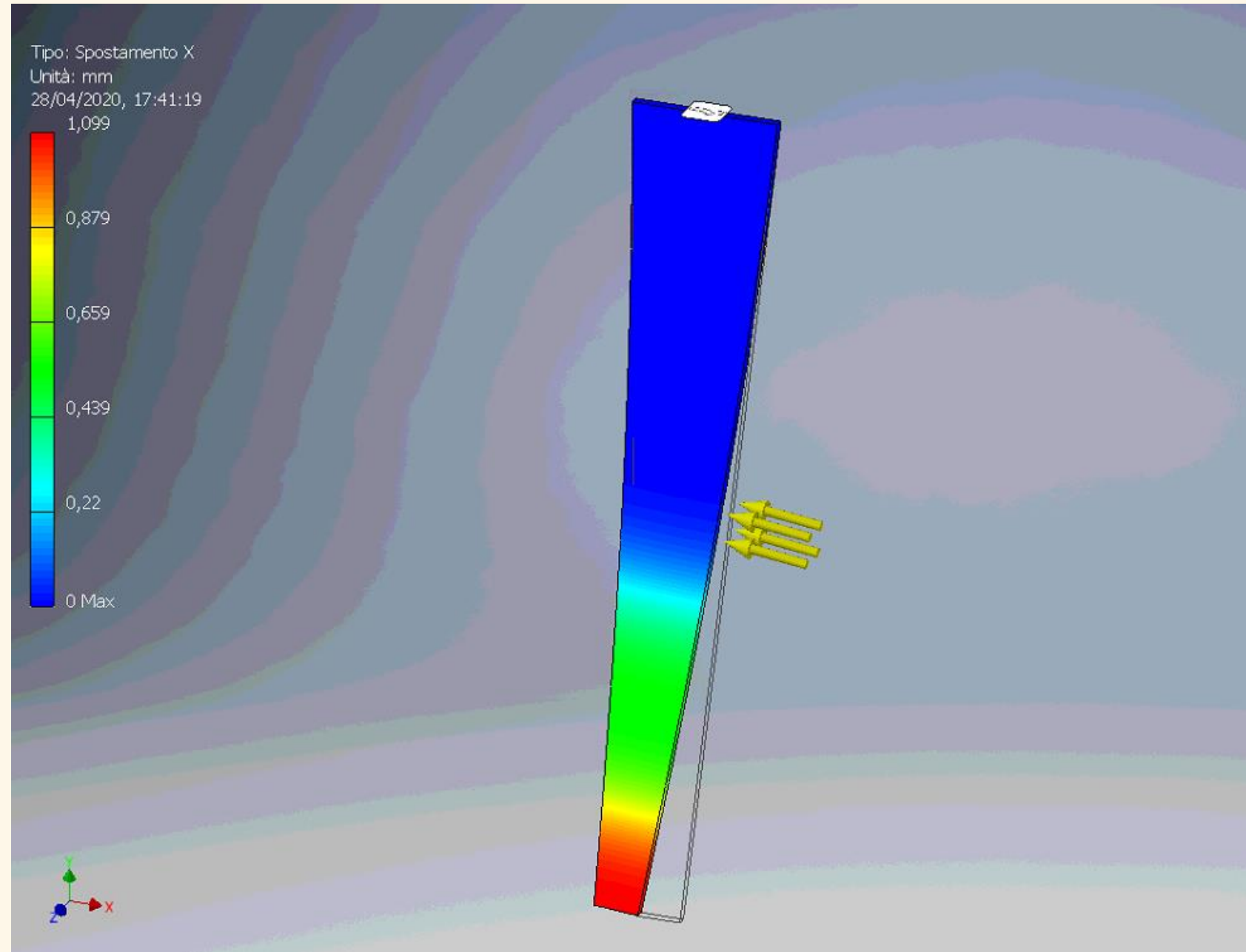
This shift will be corrected with the trapezoidal structure



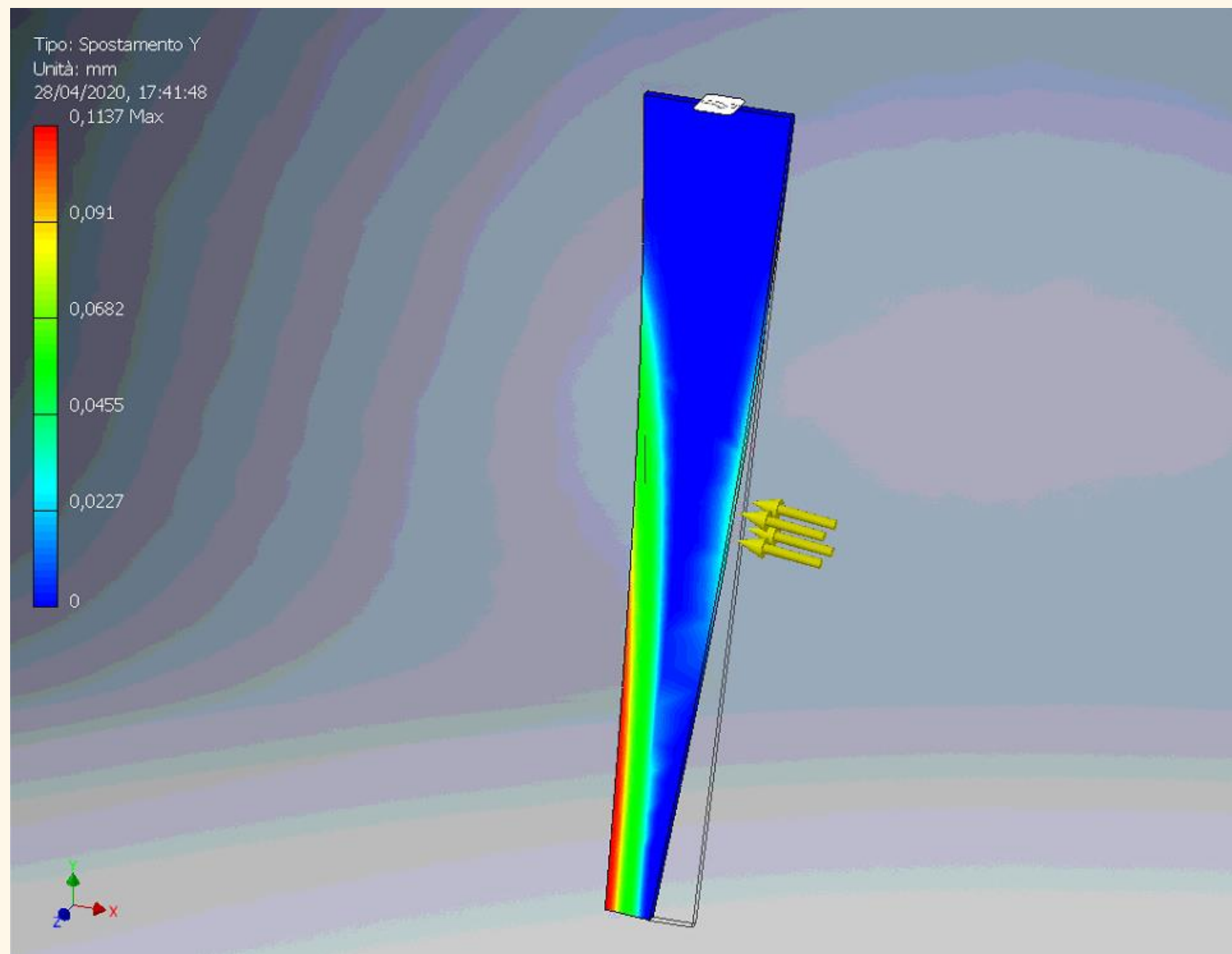
Spokes simulations «Von Mises»



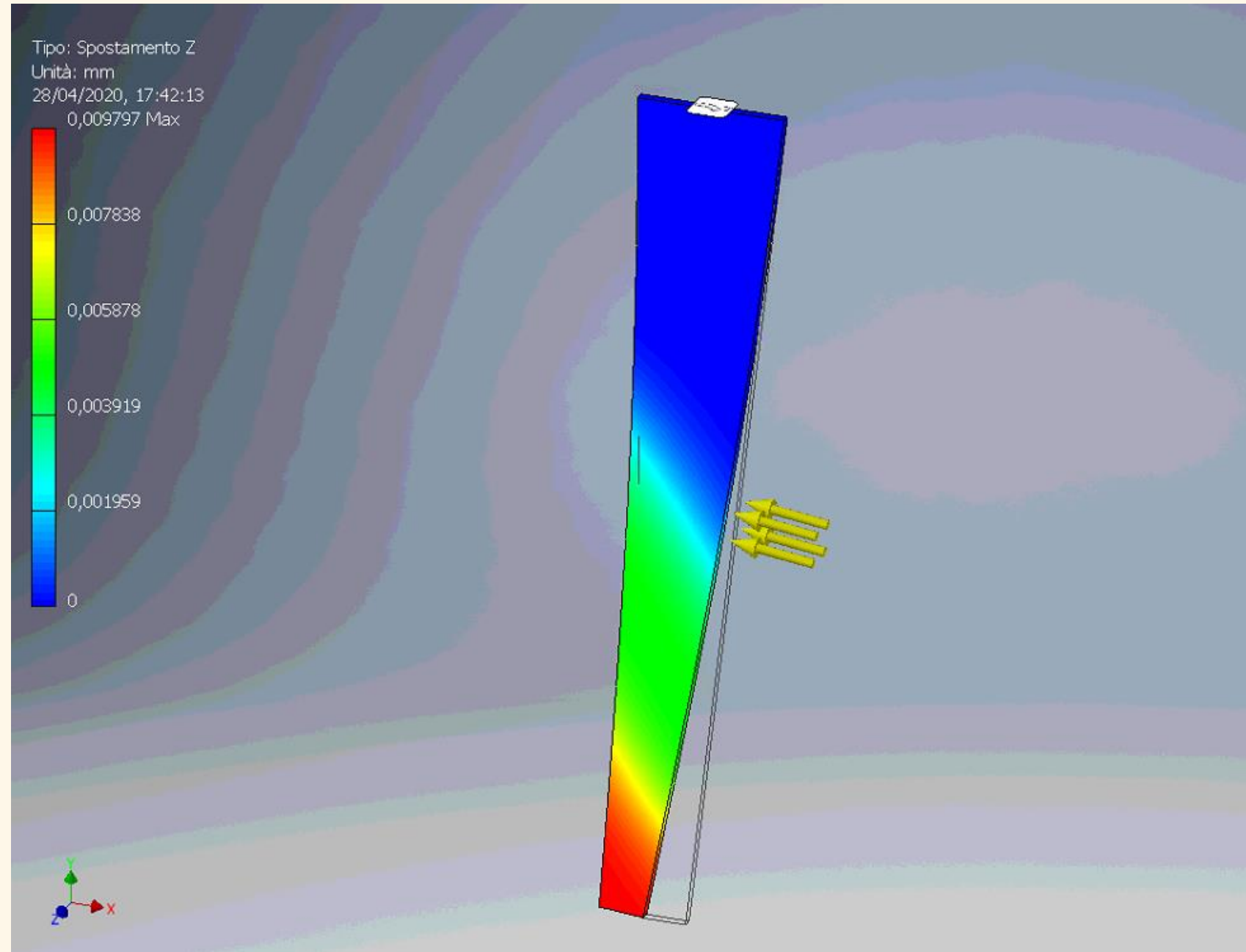
Simulations of the trapezoidal structure (x displacement)



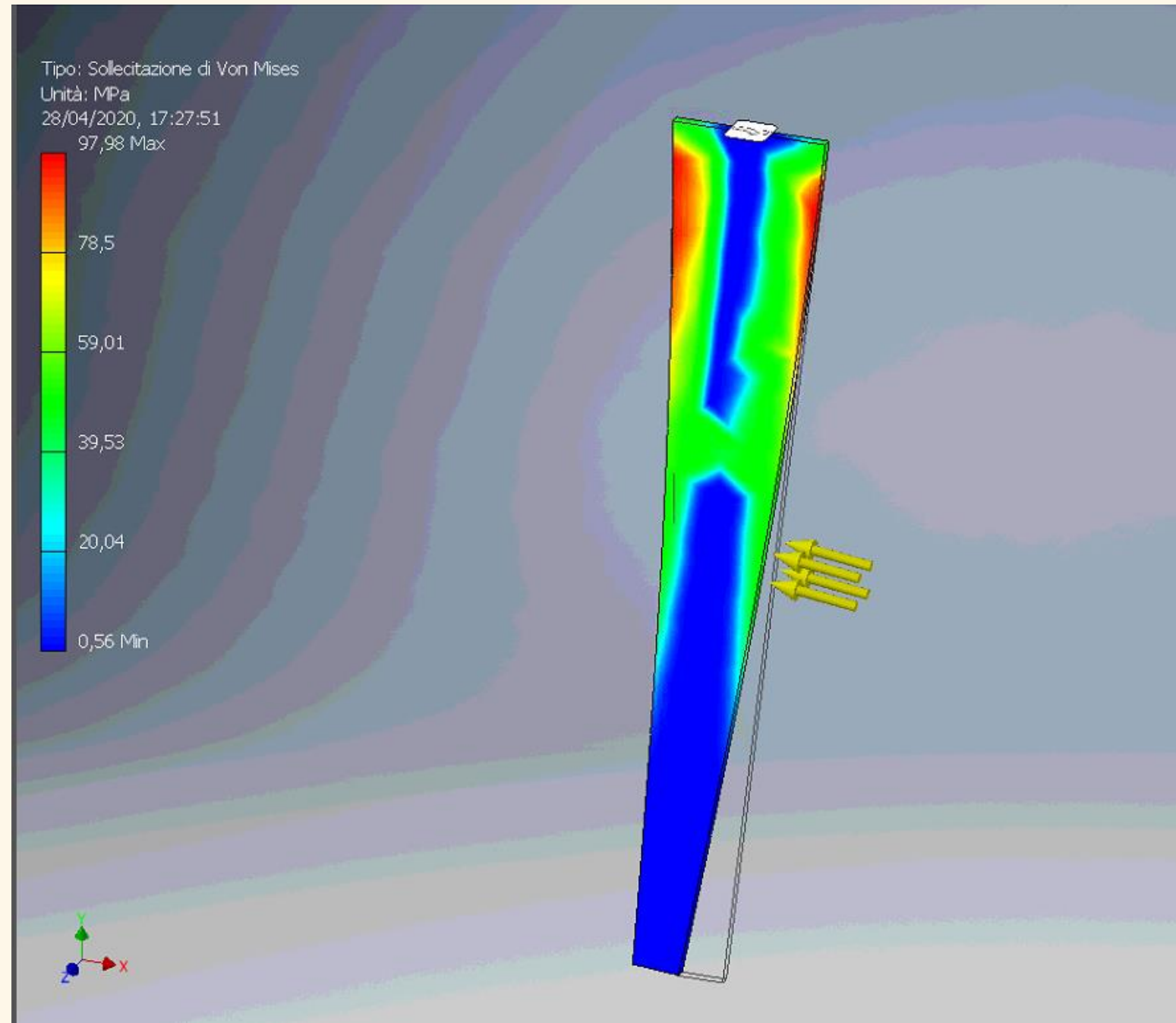
Simulations of trapezoidal structure (y displacement)



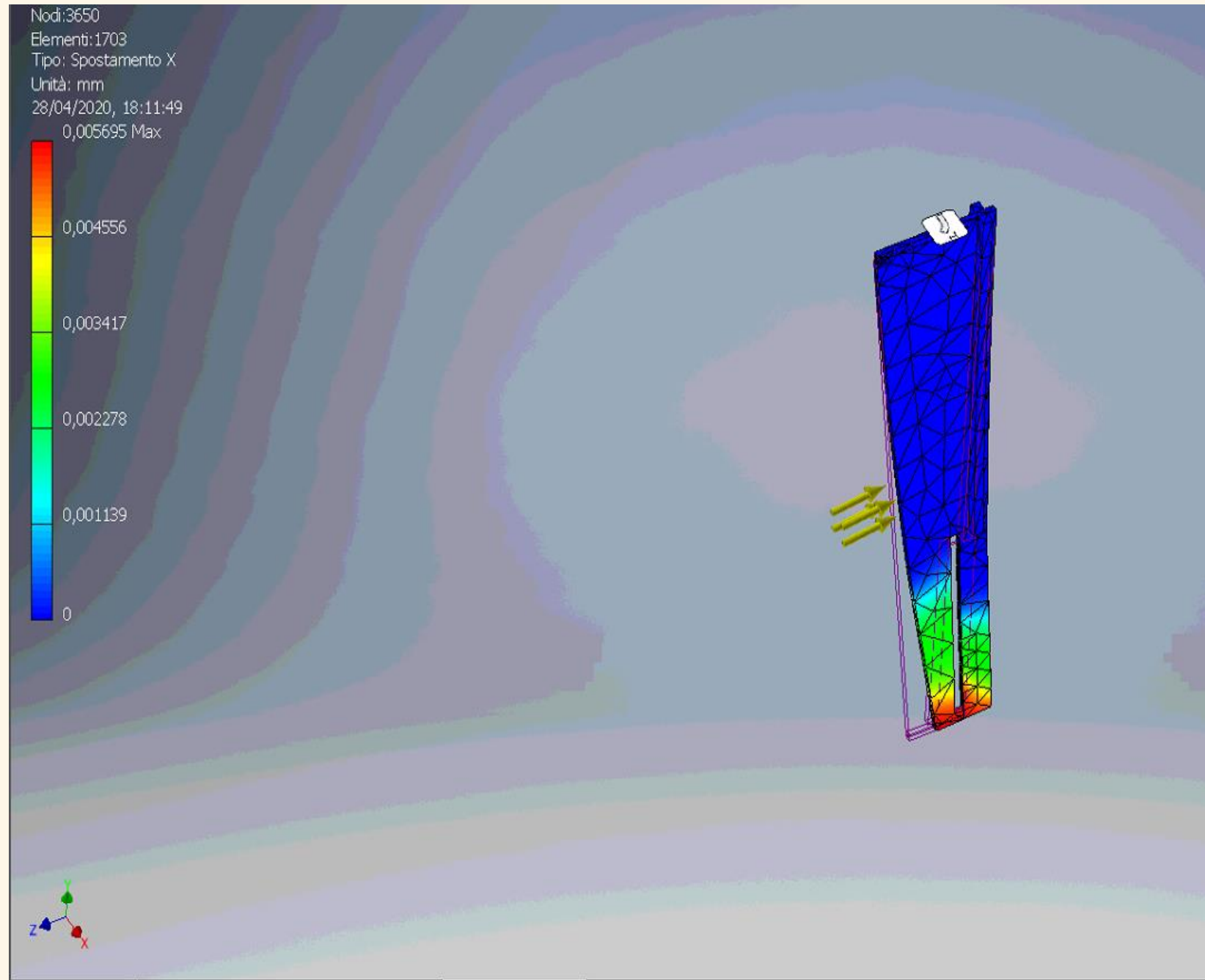
Simulations of trapezoidal structure (z displacement)



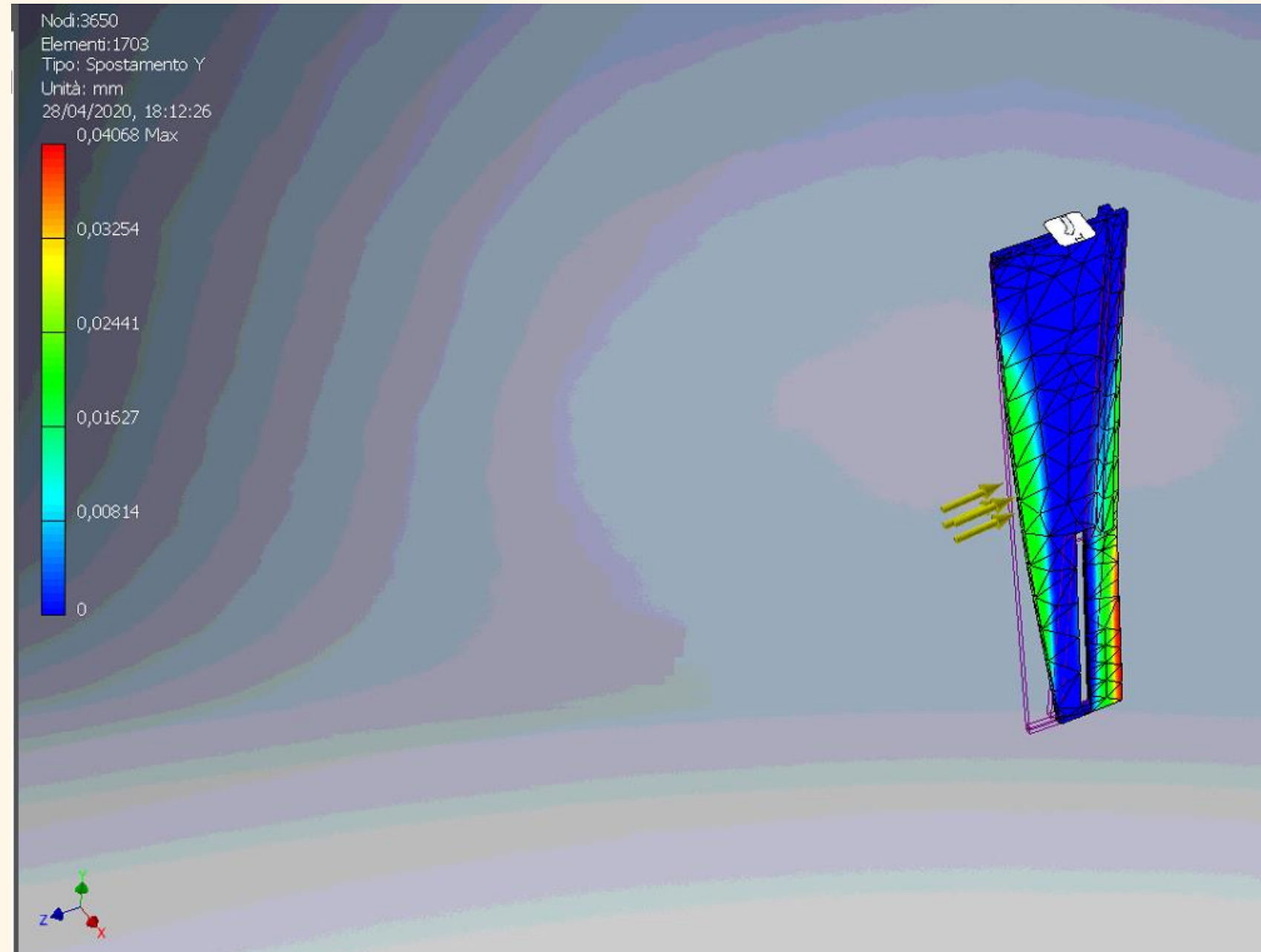
Simulations of trapezoidal structure «von Mises»



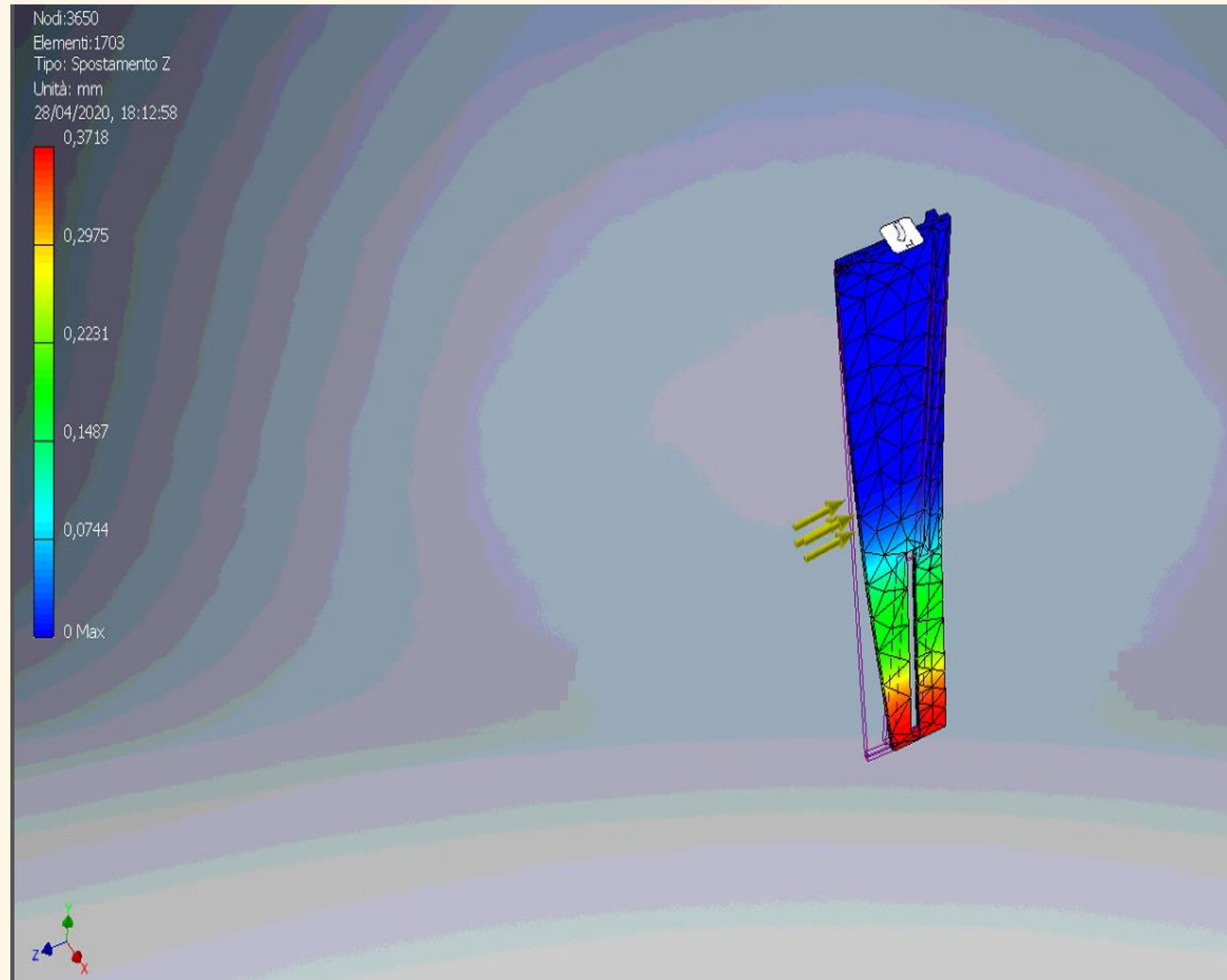
Simulations of the complete structure (x displacement)



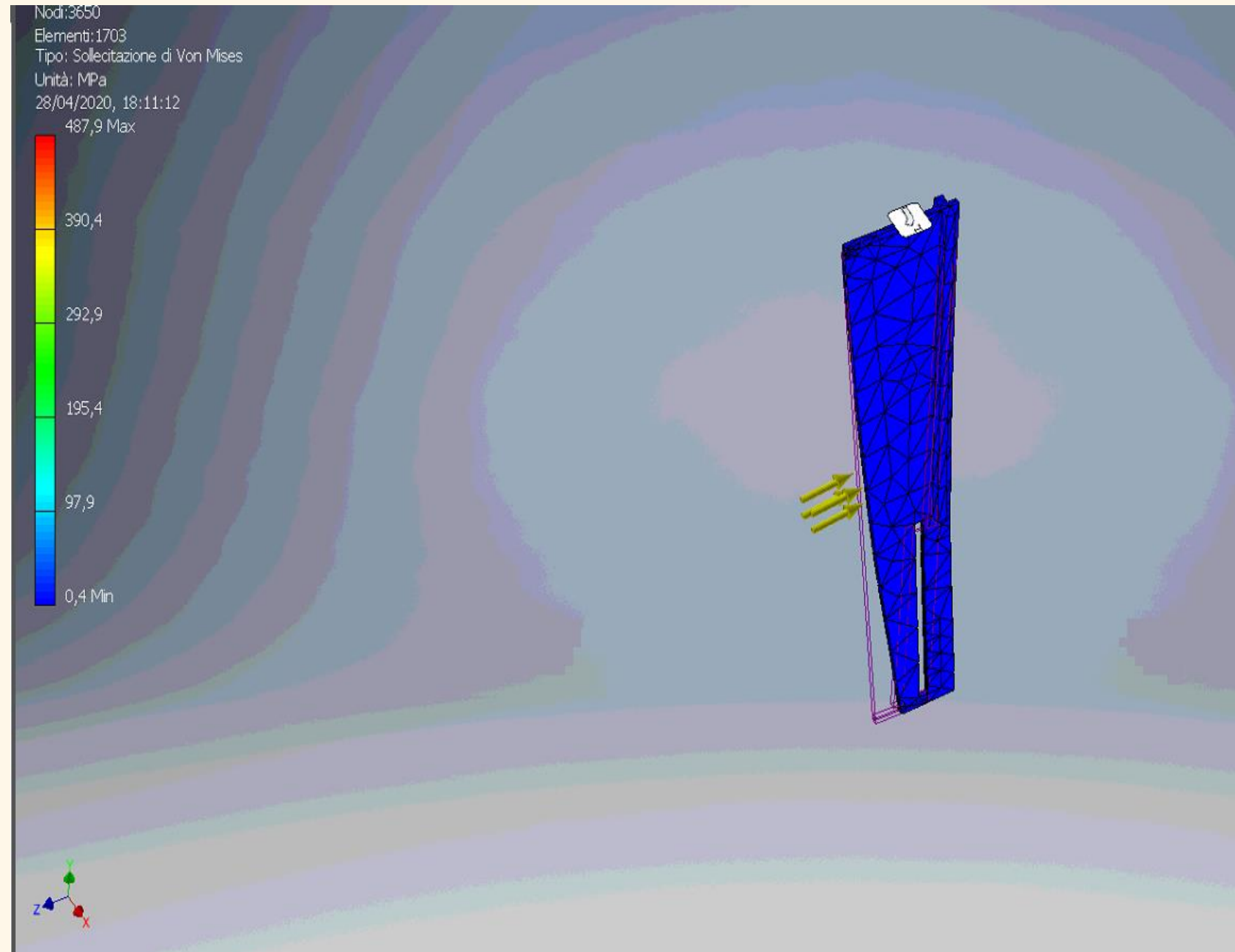
Simulations of the complete structure (y displacement)



Simulations of the complete structure (z displacement)



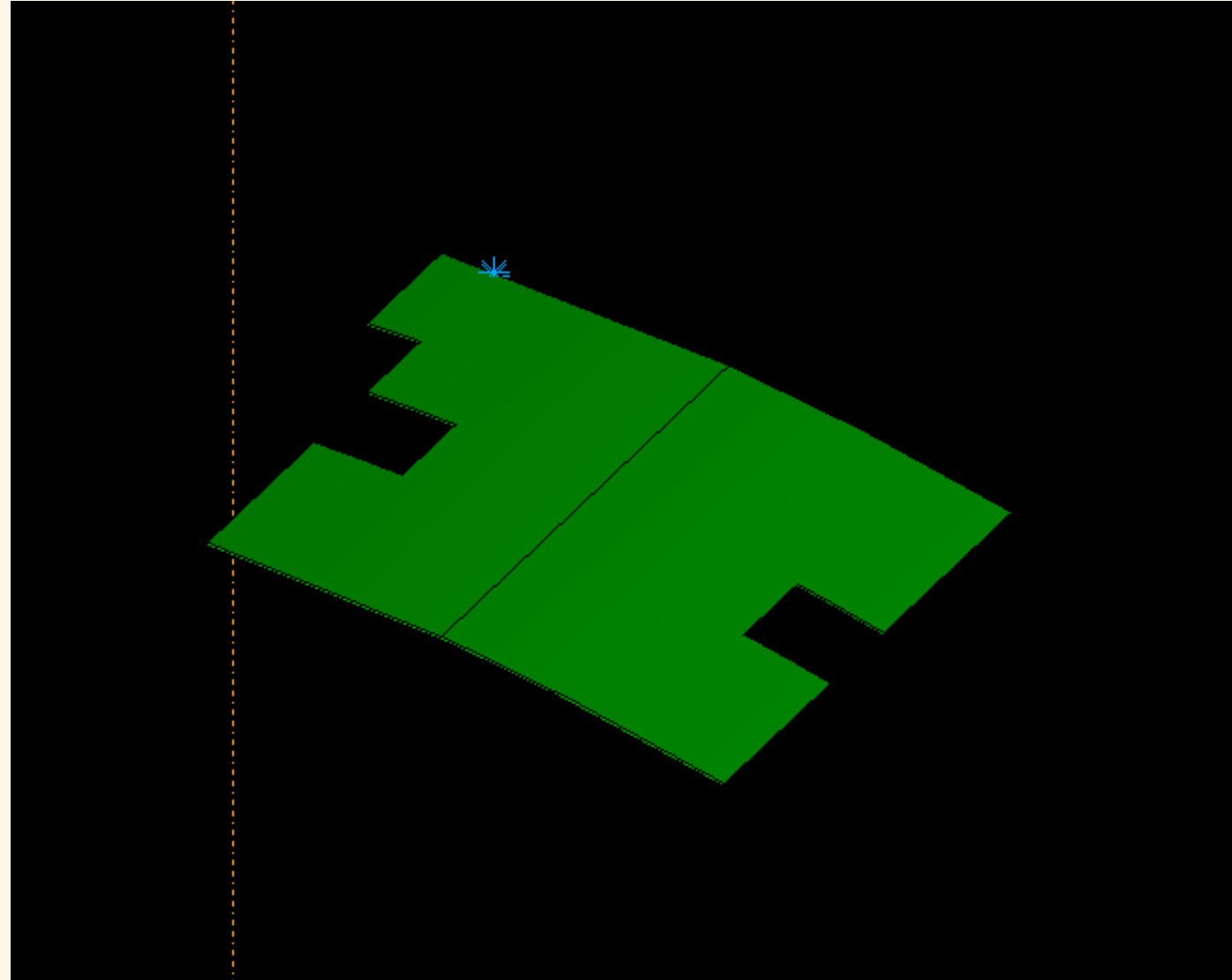
Simulations of the complete structure (Von Mises)



Sector B

Sector B has a structure similar to MEG

PCB with asymmetrical shape for the correct positioning of the wires



BACKUP SLIDES

Simulation Von Mises

Von Mises stress is a value used to determine if a given material will yield or fracture.

It is mostly used for ductile and isotropic materials, such as metals, when subjected to a complex loading condition.

The von Mises yield criterion states that if the von Mises stress of a material under load is equal or greater than the yield limit of the same material under simple tension – which is easy to determine experimentally –, then the material will yield.

The simulations tell us the position in which the spokes have the higher deformation!

For more details: <https://www.simscale.com/docs/content/simwiki/fea/what-is-von-mises-stress.html>