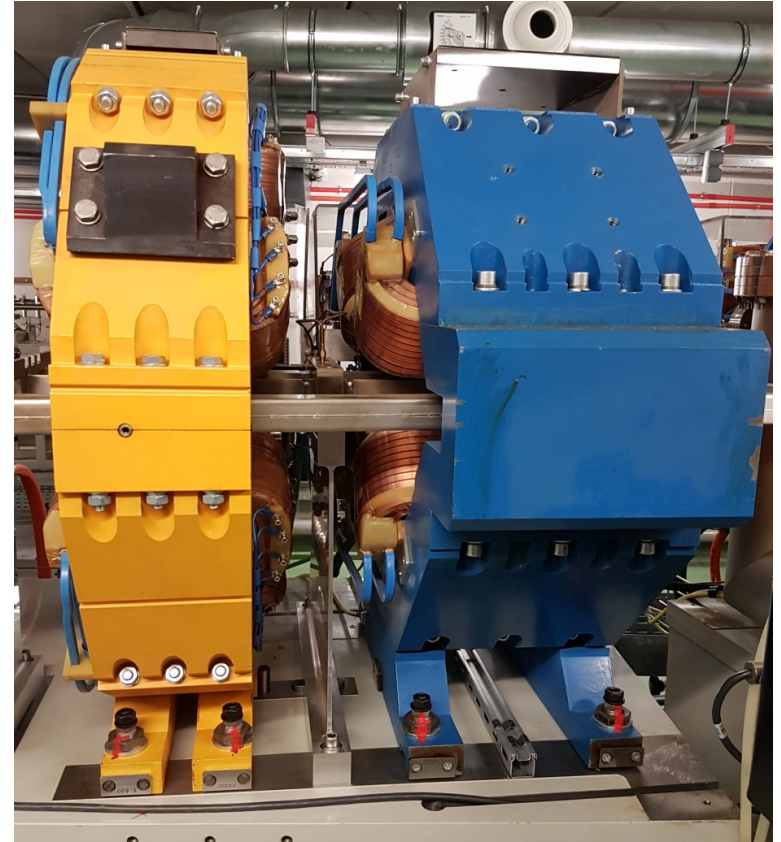


Fast Beam Based Alignment Using AC Corrector Excitations**

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* paper: <https://link.aps.org/doi/10.1103/PhysRevAccelBeams.23.012802>

** Python & Matlab implementations: <https://gitlab.com/fbba>
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BBA

FBBA

ALBA set up

Results

It is needed to:

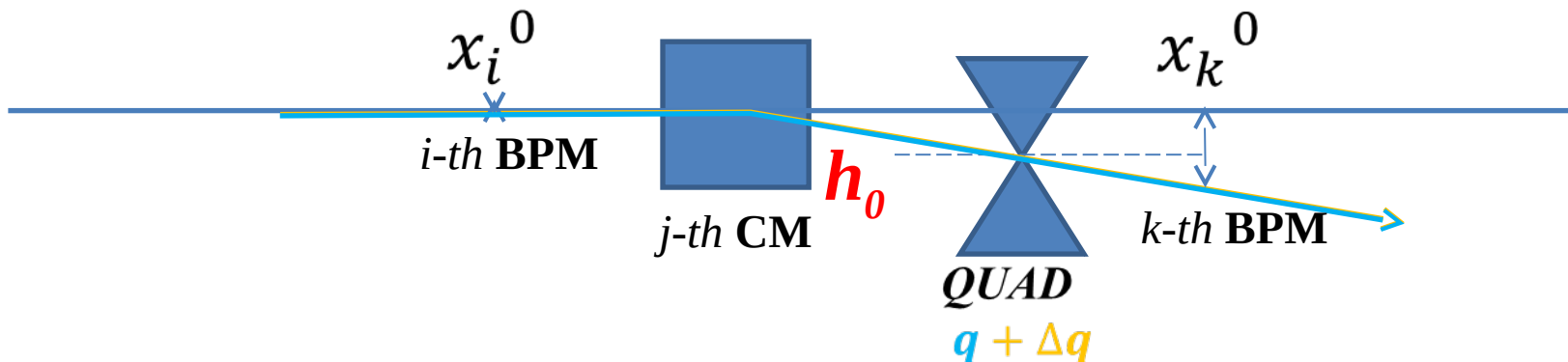
- Minimize **multipole feed down** effect, minimizes the corrector strength needed:
 - **Optic** & coupling errors due to Sextupoles.
 - **Orbit** errors due to Quadrupoles.
- Bring the machine closer to the **model** in-between BPMs.

Misalignments come from:

- Real: mechanical
- Apparent: electronic

Several measurement methods:

- **Beam2quad**: Quad scan: **Fast** but **Model dependent**.
- **BPM2quad**: Quad&CM scan: **Slow** but **Model independent**.
- There is a systematic error (orbit angle):



Instead of scanning sequentially in DC the CM, it uses the FOFB hardware:

- 10kHz **Fast Acquisition Archiver**
- AC CM excitation (quads **could** also be AC)

The FBBA measurable quantities are the same as for the normal **bpm2quad** BBA, but:

- The **two planes** are done at the same time (h_o and v_o)
- **Optics coupling** is taken into account -> **skew** magnets can also be aligned
- BPM gain and **coupling**, CM calibration and **tilt** are also considered

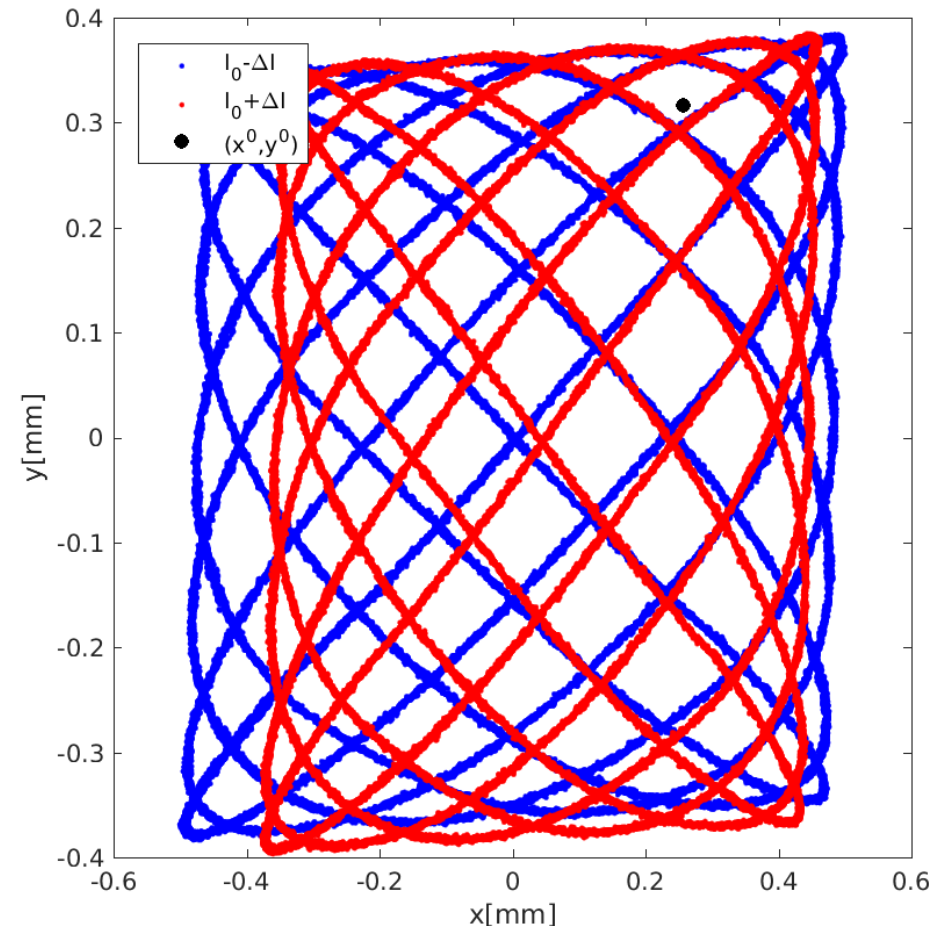
QUAD FBBA-DC BPM data example:

The method is valid for:

- *DC quad*
- *AC quad* (*additional factor 2 faster*)

And also:

- *Normal quad*
- *Skew quad* (*sextupole yoke*)



The method is a **factor 2 faster** if two different **frequencies** are used in each plane.

$$h_j(t_n) = \hat{h}_j \cos(2\pi f_h t_n + \psi_h) = \Re\{(\hat{h}_j e^{i\psi_h}) e^{i2\pi f_h t_n}\}$$

$$v_j(t_n) = \hat{v}_j \cos(2\pi f_v t_n + \psi_v) = \Re\{(\hat{v}_j e^{i\psi_v}) e^{i2\pi f_v t_n}\}$$

The offset is obtained combining the **Fourier components** of each BPM signal.

$$h_j(t_n) = \Re\{(\hat{h}_j e^{i\psi_h}) e^{i2\pi f_h t_n}\} = \frac{1}{2} (\langle h_j | f_h \rangle e^{i2\pi f_h t_n} + \text{c.c.}),$$

$$v_j(t_n) = \Re\{(\hat{v}_j e^{i\psi_v}) e^{i2\pi f_v t_n}\} = \frac{1}{2} (\langle v_j | f_v \rangle e^{i2\pi f_v t_n} + \text{c.c.}).$$

In the linear regime, the BPM readings as a function of CMs change with **coupling** are:

$$x_k(t) - x_k^0 = R_{kj}^{xx} (h_j(t) - h_0) + R_{kp}^{xy} (v_p(t) - v_0)$$

$$y_n(t) - y_n^0 = R_{np}^{yy} (v_p(t) - v_0) + R_{nj}^{yx} (h_j(t) - h_0)$$

DC quad:

$$R_{kj}^{xx} \quad R_{kp}^{xy} \quad R_{np}^{yy} \quad R_{nj}^{yx}$$

have 2 values: **two sets**
of data are acquired.

AC quad:

$$R_{kj}^{xx} \quad R_{kp}^{xy} \quad R_{np}^{yy} \quad R_{nj}^{yx}$$

vary with time: only **one set** of data.

Both for quads and skews the **solution** is:

$$\begin{cases} x_l^0 = \Re \{ \langle x_l | 0 \rangle \} + \mathcal{S} \{ \langle x_l | f_h \rangle \} \mathcal{M}_h + \mathcal{S} \{ \langle x_l | f_v \rangle \} \mathcal{M}_v \\ y_l^0 = \Re \{ \langle y_l | 0 \rangle \} + \mathcal{S} \{ \langle y_l | f_v \rangle \} \mathcal{M}_v + \mathcal{S} \{ \langle y_l | f_h \rangle \} \mathcal{M}_h \end{cases}$$

Where the **observable** (h_o and v_o are not) **relative corrector offsets** are:

$$\begin{cases} \mathcal{M}_h = \frac{h_{0j}}{\hat{h}_j} = - \frac{\mathcal{D}_x \mathcal{D}_{yv} - \mathcal{D}_{xv} \mathcal{D}_y}{\mathcal{D}_{xh} \mathcal{D}_{yv} - \mathcal{D}_{xv} \mathcal{D}_{yh}} = \frac{\mathcal{Y}_{hk}}{\mathcal{X}_{hk}} \\ \mathcal{M}_v = \frac{v_{0j}}{\hat{v}_j} = - \frac{\mathcal{D}_{xh} \mathcal{D}_y - \mathcal{D}_x \mathcal{D}_{yh}}{\mathcal{D}_{xh} \mathcal{D}_{yv} - \mathcal{D}_{xv} \mathcal{D}_{yh}} = \frac{\mathcal{Y}_{vk}}{\mathcal{X}_{vk}}. \end{cases}$$

BPM gain and coupling, CM calibration and tilt are taken into account.

DC Quad/skew (1&2 measurements)

$$\begin{cases} \mathcal{D}_x = \Re \{ \langle x_{k2} | 0 \rangle \} - \Re \{ \langle x_{k1} | 0 \rangle \} \\ \mathcal{D}_y = \Re \{ \langle y_{k2} | 0 \rangle \} - \Re \{ \langle y_{k1} | 0 \rangle \} \\ \mathcal{D}_{xh} = \mathcal{S} \{ \langle x_{k2} | f_h \rangle \} - \mathcal{S} \{ \langle x_{k1} | f_h \rangle \} \\ \mathcal{D}_{yv} = \mathcal{S} \{ \langle y_{k2} | f_v \rangle \} - \mathcal{S} \{ \langle y_{k1} | f_v \rangle \} \\ \mathcal{D}_{xv} = \mathcal{S} \{ \langle x_{k2} | f_h \rangle \} - \mathcal{S} \{ \langle x_{k1} | f_h \rangle \} \\ \mathcal{D}_{yh} = \mathcal{S} \{ \langle y_{k2} | f_h \rangle \} - \mathcal{S} \{ \langle y_{k1} | f_h \rangle \} \end{cases}$$

AC Quad (at f_s : 1 measurement)

$$\begin{cases} \mathcal{D}_x = \mathcal{S} \{ \langle x_k | f_s \rangle \} \\ \mathcal{D}_y = \mathcal{S} \{ \langle y_k | f_s \rangle \} \\ \mathcal{D}_{xh} = \mathcal{S} \{ \langle x_k | f_h + f_s \rangle \} + \mathcal{S} \{ \langle x_k | f_h - f_s \rangle \} \\ \mathcal{D}_{yv} = \mathcal{S} \{ \langle y_k | f_v + f_s \rangle \} + \mathcal{S} \{ \langle y_k | f_v - f_s \rangle \} \\ \mathcal{D}_{xv} = \mathcal{S} \{ \langle x_k | f_v + f_s \rangle \} + \mathcal{S} \{ \langle x_k | f_v - f_s \rangle \} \\ \mathcal{D}_{yh} = \mathcal{S} \{ \langle y_k | f_h + f_s \rangle \} + \mathcal{S} \{ \langle y_k | f_h - f_s \rangle \} \end{cases}$$

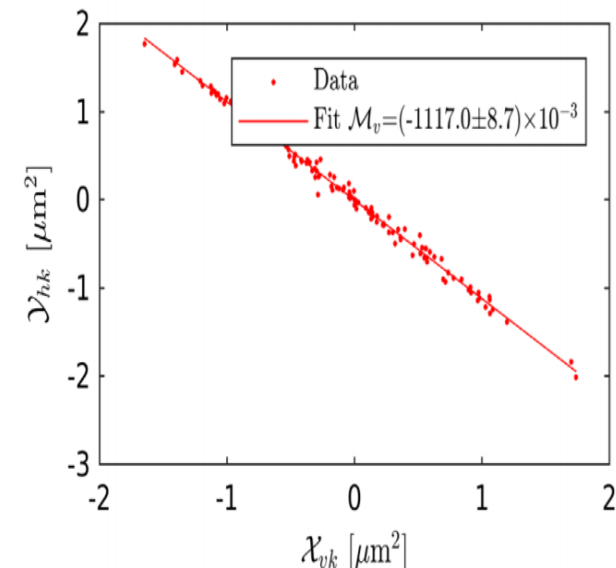
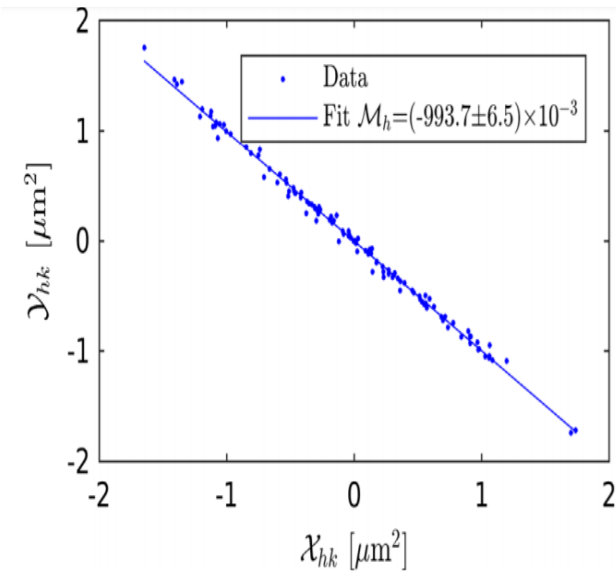
Example: a 90° rotation ($x \Rightarrow y$ & $y \Rightarrow -x$) changes $\mathcal{D}_x \Rightarrow \mathcal{D}_y$, $\mathcal{D}_y \Rightarrow -\mathcal{D}_x$, $\mathcal{D}_{xh} \Rightarrow \mathcal{D}_{yh}$, $\mathcal{D}_{yh} \Rightarrow -\mathcal{D}_{xh}$, $\mathcal{D}_{xv} \Rightarrow \mathcal{D}_{yv}$ and $\mathcal{D}_{yv} \Rightarrow -\mathcal{D}_{xv}$ leaves \mathcal{M}_h and \mathcal{M}_v unchanged: **Any linear coupling** is automatically taken into account.

The **signed amplitude** of a signal x at a frequency f_z is defined as:

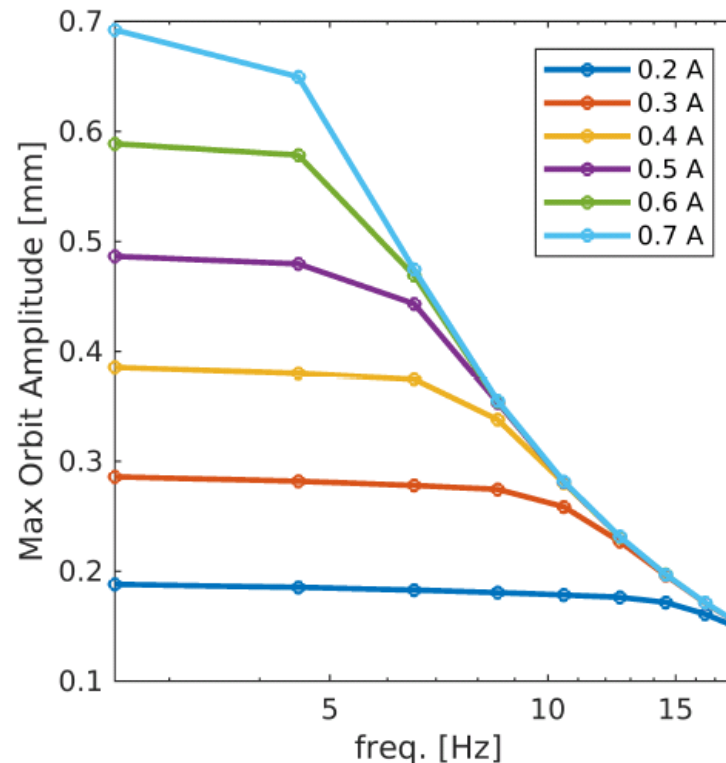
$$\mathcal{S} \{ \langle x | f_z \rangle \} = |\langle x | f_z \rangle| \text{sgn} \left\{ \cos(\psi_x^{(z)} - \psi_z) \right\}$$

Relative corrector offset fit: $\frac{h_{0j}}{\hat{h}_j}$

For every BPM, a point in the \mathcal{X}_{hk} and \mathcal{Y}_{hk} plane is calculated. Then, the fit result is used to calculate the offsets of a single BPM- l : x_l^0 and y_l^0 .



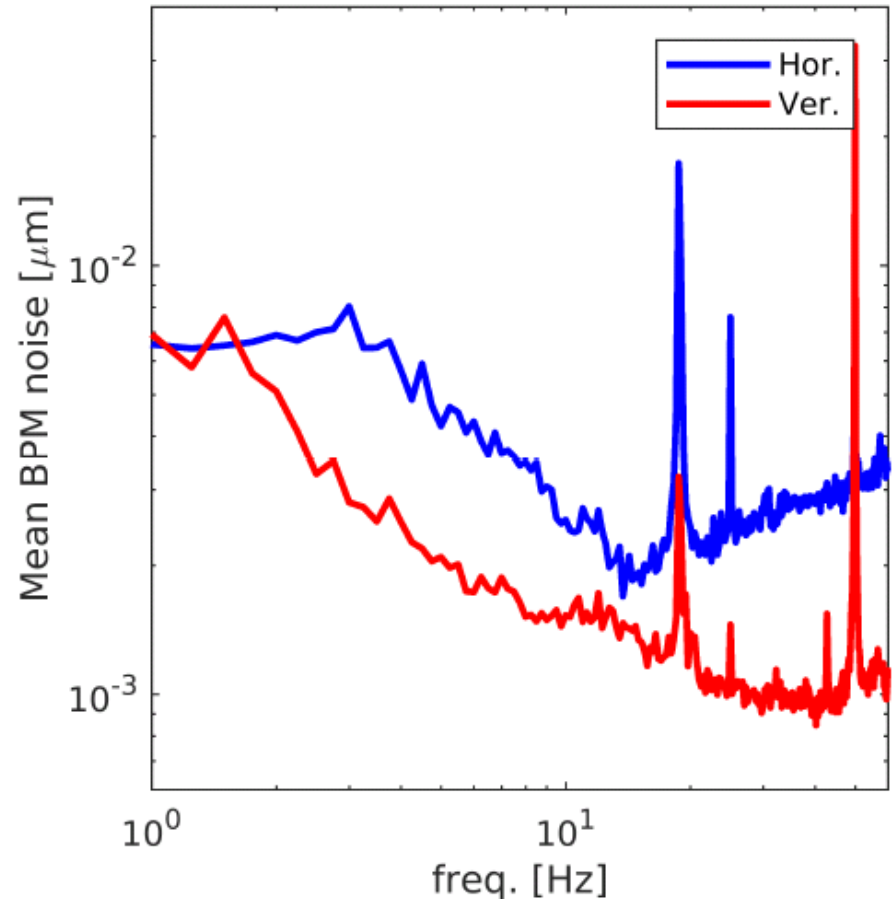
Frequency choice: The CM waveforms have a limited effective kick as a function of the frequency:



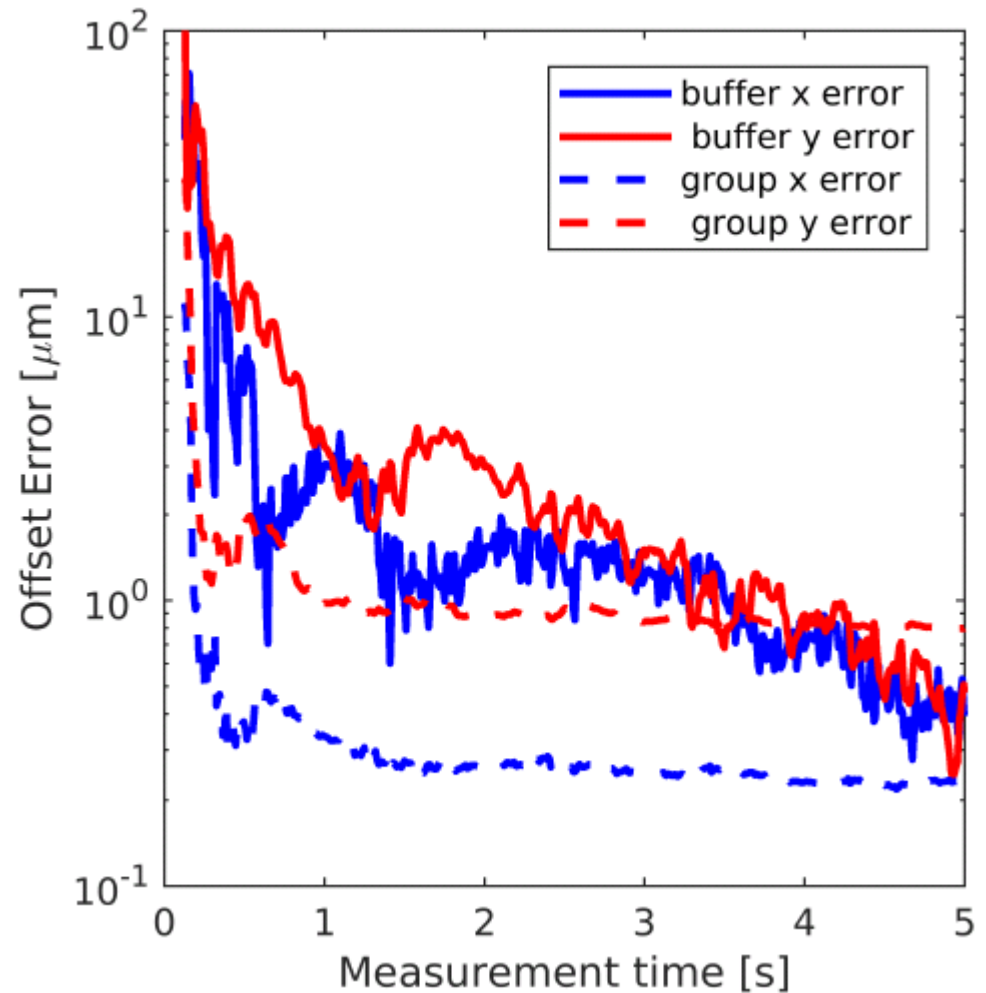
A minimum of **0.5 A** is needed to properly measure large offsets.

Also, we study the BPM noise as a function of the frequency. It gets better the higher the frequency, in the 0 Hz-18 Hz range:

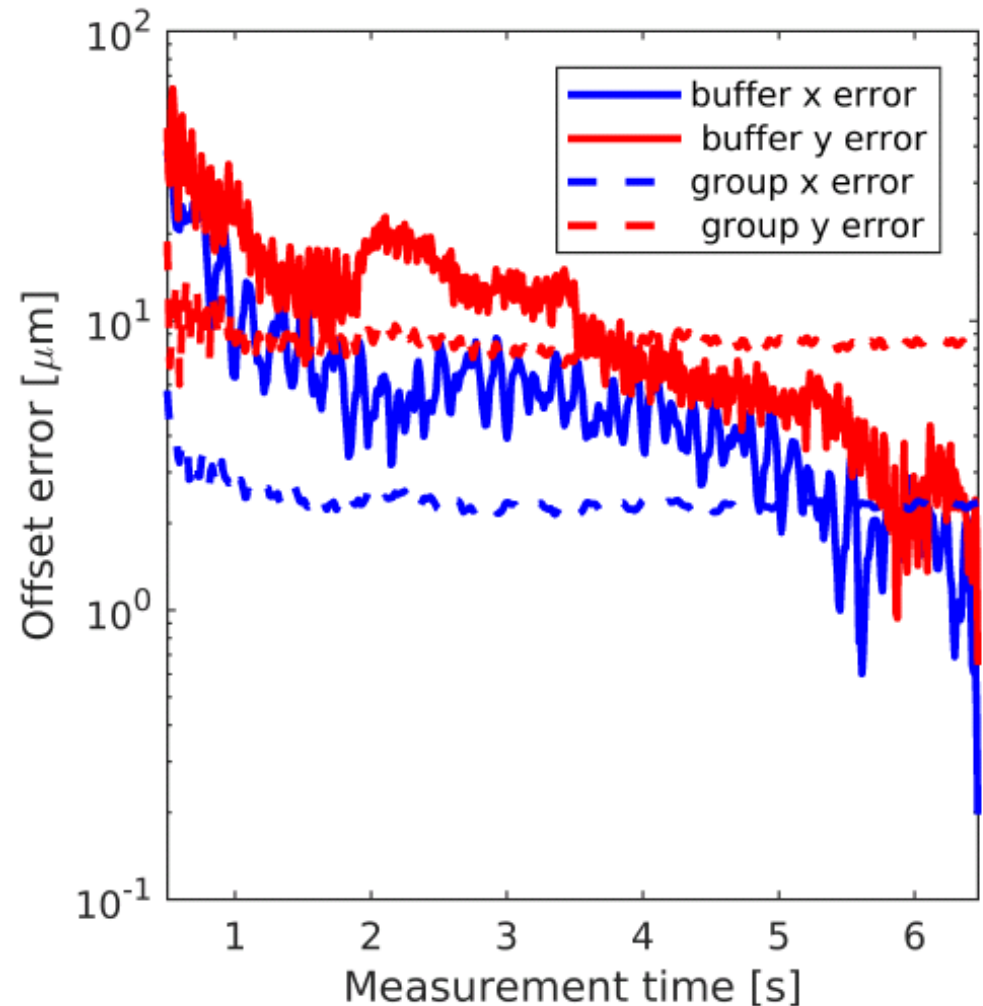
We decided to use **6 Hz** and **7 Hz** for the vertical and horizontal plane respectively (0.5mm).



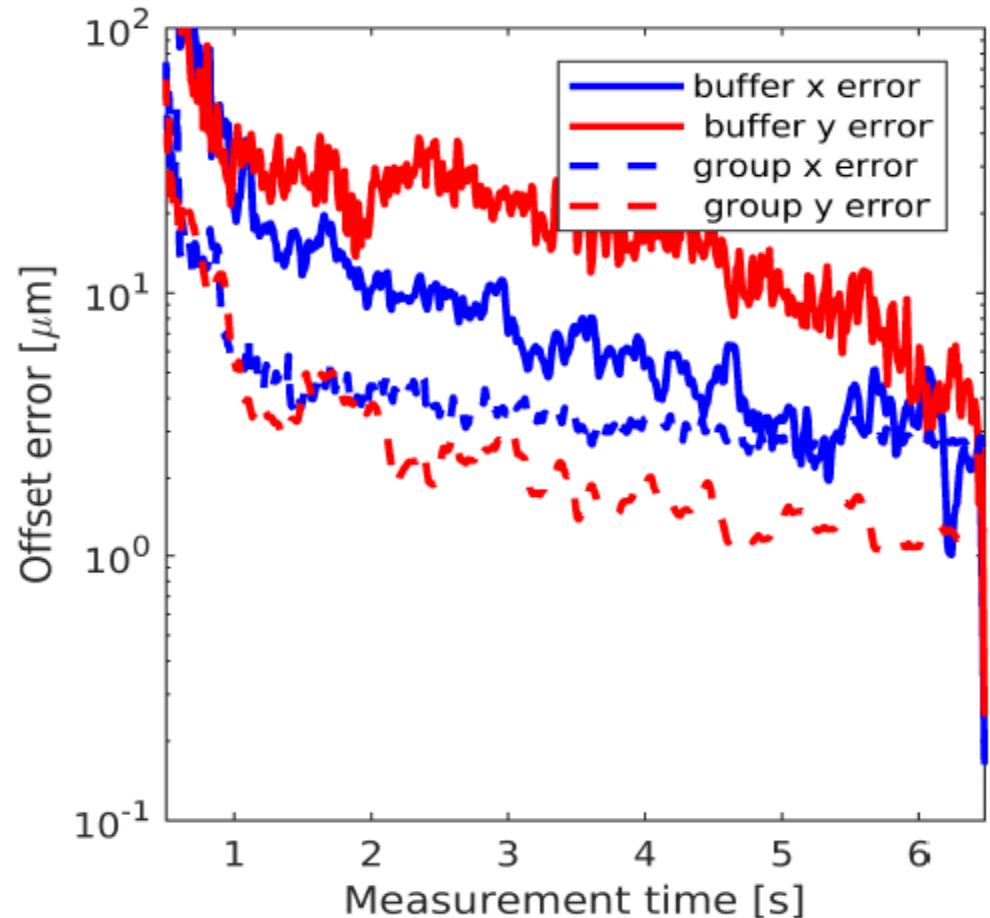
For a DC quad change of 2.5A, the **acquisition time** is optimized:
1.5 seconds (3 s/meas.)



For a DC skew change of 2.5A, the acquisition time is optimized: 6 sec (12s/meas)

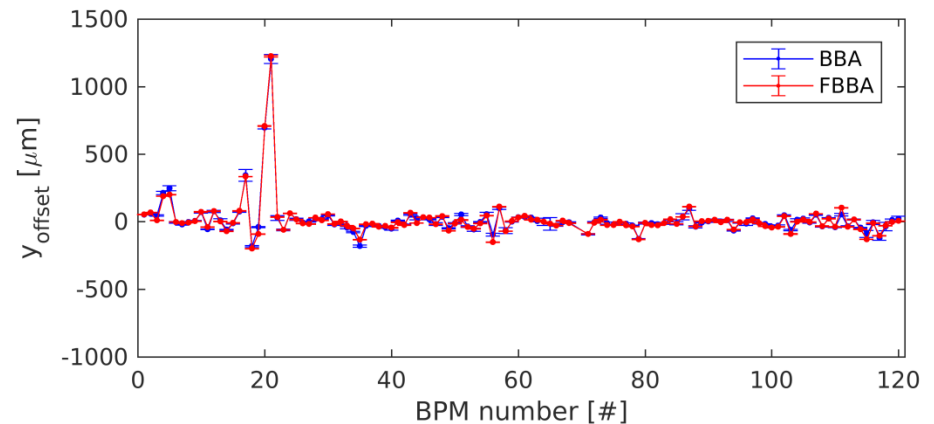
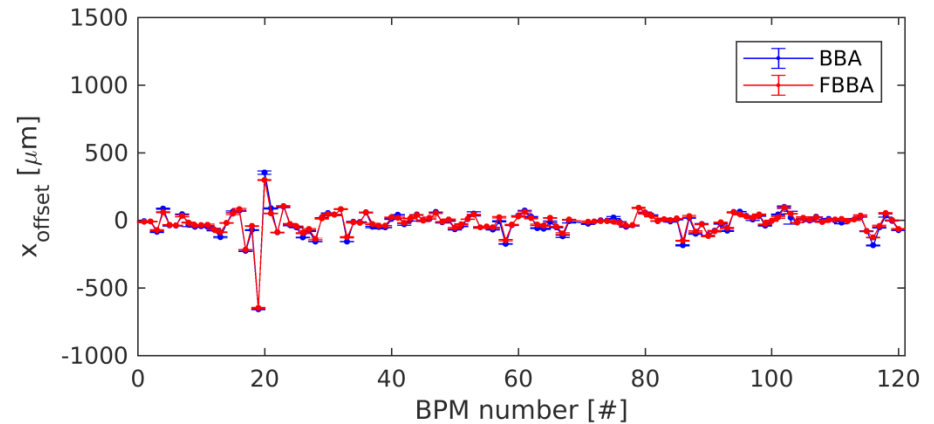


For an AC skew change of 2.5A at 1.6Hz, the acquisition time is optimized: 6 sec (6s/meas)



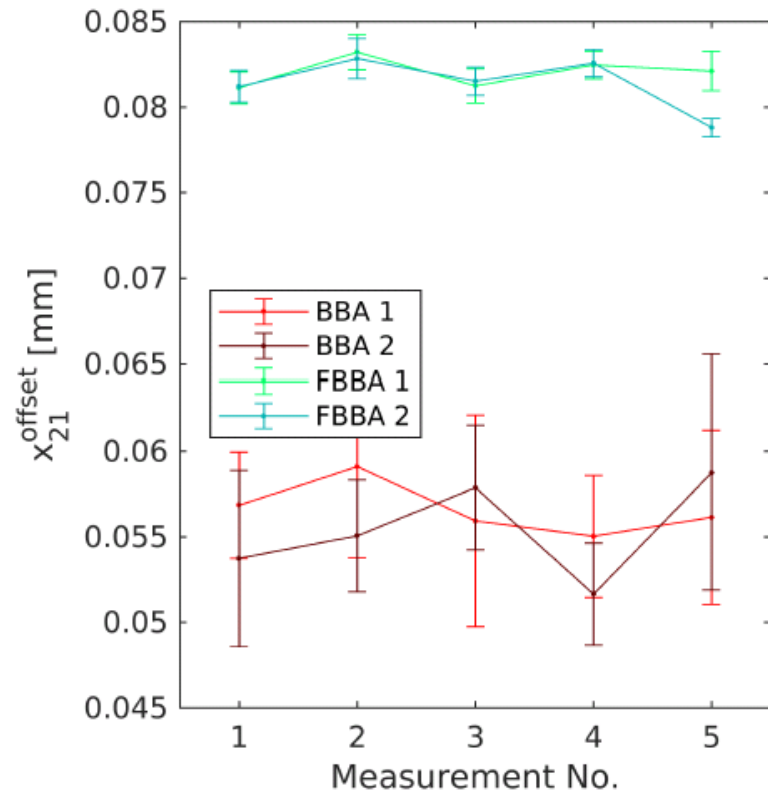
BBA vs FBBA:

- The presented FBBA is **~30 times faster** (10 min vs 5h) than the standard BBA.
- The level of precision is similar.



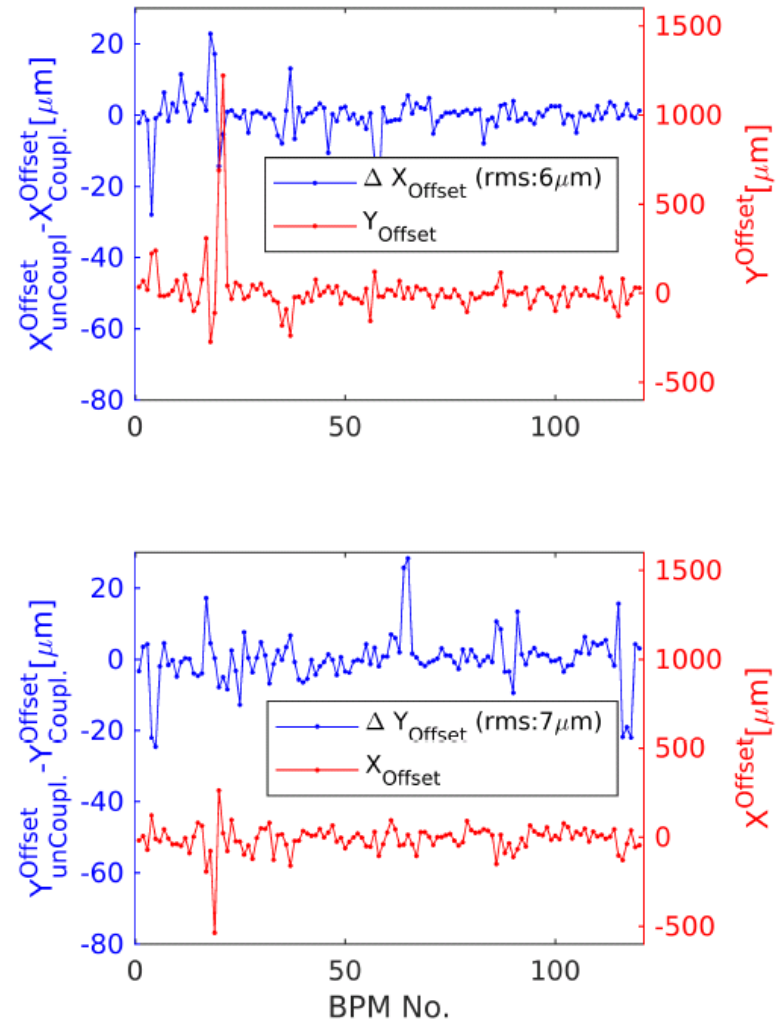
For some BPMs, there are some **systematic** discrepancies effects **not** related to **quad hysteresis**...

The measurements were performed with (1) and without (2) quad hysteresis cycles before the measurement.



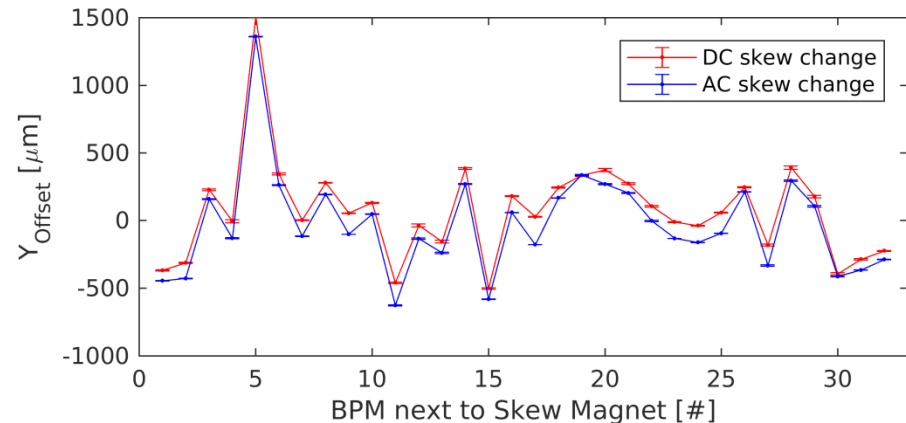
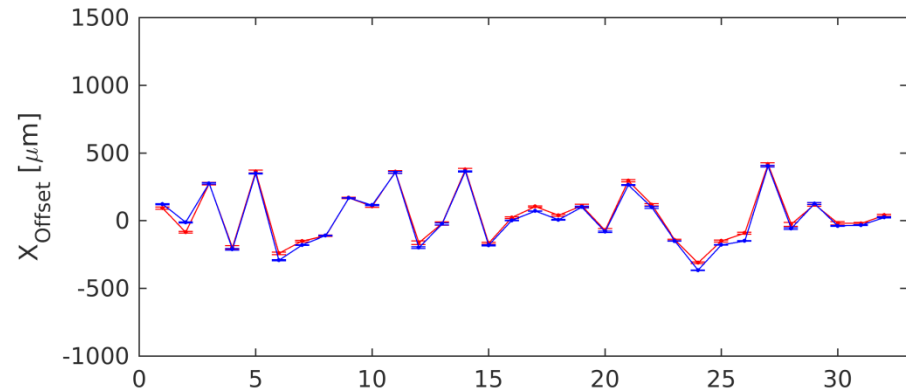
Regarding to **coupling** effects, they are of similar order.

It seems **not very relevant** except in the case of large coupling or for **skew quads**...

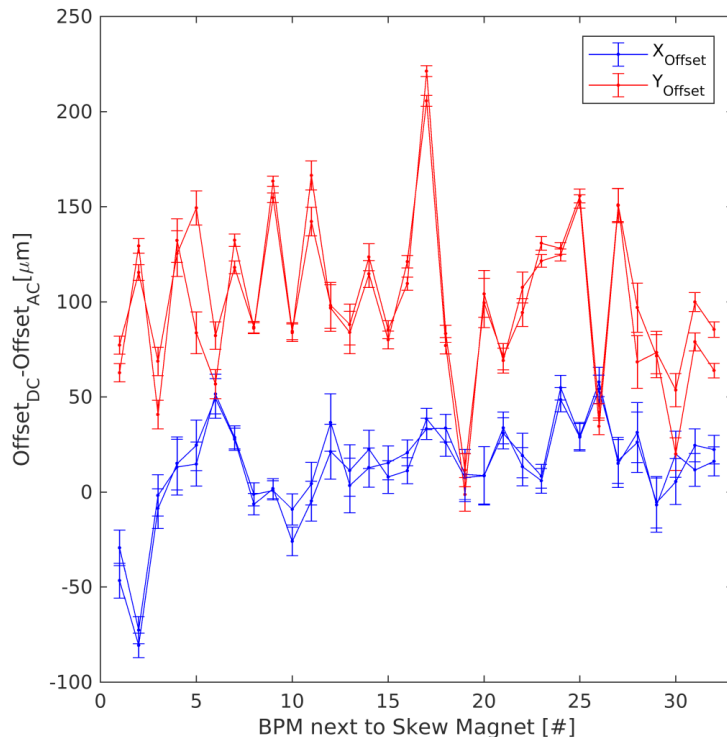


AC and DC magnet excitation give **quite consistent results**.

The AC is about **2 times faster**, but there is a **systematic difference (unexplained)** of around 100 μm .



We have performed **random realistic simulations** of FBBA at ALBA on skew quadrupoles and this effect is **not expected**.



	Horizontal	Vertical
Model rms quadrupole offset	150 μm	150 μm
Mean difference between offsets:		
(Normal quad.) BBA vs model	15 μm	12 μm
(Normal quad.) dc FBBA vs model	16 μm	12 μm
(Normal quad.) ac FBBA vs model	16 μm	13 μm
(Skew quad.) dc FBBA vs model	19 μm	9 μm
(Skew quad.) ac FBBA vs model	19 μm	6 μm
(Normal quad.) dc FBBA vs BBA	4 μm	2 μm
(Normal quad.) ac FBBA vs BBA	4 μm	3 μm
(Normal quad.) ac FBBA vs dc FBBA	0 μm	3 μm
(Skew quad.) ac FBBA vs dc FBBA	0 μm	5 μm

- Using the FOFB hardware, we have developed a method to perform quadrupole BBA which is **30times faster** than standard BBA and achieves even better **precision** (not sure about accuracy).
- The FBBA allows to perform simultaneous analysis of both planes, and accounts for any level of optics **coupling**, **BPM roll and CM tilt**.
- This novel approach allows also a **skew** quadrupole BBA (**sextupole** yoke).
- Some small **differences** between AC and DC modes remain **unexplained** (~30um for the quads case, and ~100um for the skews case).