

Layer 0 Module Support and Cooling

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Outline

- -Microchannel Full Module support design, test results .
- -Microchannel Net Module construction and and test .
- -Net Module Simulation Study
- Further developments to reduce X_0 and improve thermal efficiency. -
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Support Characteristic

Merging Super-B experiment specifications with the thermal and hydraulic concepts, we focused our attention on a CFRP supports with microchannel technology for an heat evacuation through a single phase liquid forced convection .

Several prototypes with different geometries and material have been realized; miniaturization of composites structures have been developed through close collaboration with companies. Prototypes have been submitted to test at the TFD laboratory of the INFN-Pisa.

<u>Main goal :</u> reducing as much as possible X₀ maintaining good cooling performance!

X_0 module support improvement

Planarity tollerance of the microchannel module is 40 ^µm .

Grinding about 40 µm on the top and bottom surfaces of microchannel module obtained a 620 µm-thick structure with further 15% reduction in X_0 .

better thermal interface between CFRP and the Aluminumkapton foil (ground layer of the silicon detector).

Surface roughness

 $700 \mu m \longrightarrow 620 \mu m$

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(X=0.28 X_0 \longrightarrow X_0=0.25\% X_0)
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Module Samples

A kapton heater is glued on the CFRP support structure to dissipate the needed power density.

On the bottom of the heater there is an aluminum foil 300 μ m-thick, in place of the silicon detector. On the top, to read the temperatures, n.5 PT100probes are glued, positioned just laterally to the heater.

 An Aluminum kapton 75 µm-thick is sandwiched between the support structure and the aluminum foil, simulating ground plane in the real detector. There is also a glue layer between each components (30µm-thick on average).

 $\begin{array}{c} 6 \ 0 \end{array}$ There are two kinds of tested configurations: the "double side", where the heat is dissipated both on the upper and the lower external faces, and the "single side" where the power is dissipated only on the upper face.

Test Results

Temperature along the module $(\Delta T = 5 \degree C)$

Net Module support

Assuming further progress in MAPS sensor design, and looking to actual hybrid^pixel, the required Power (analog ⁺ digit), could step down to 1.5-1.0 W/cm2.We choose to design ^a lighter solution for the suppor^t structure . The Net Module is ^a micro-channel suppor^t with vacancies of tubes in the structure .

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We admitted worse cooling performance for strongly gaining in X_{0} .

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Net modules support

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N.2 Prototype produced !

Net module mechanical structure:10 microtube + 5 trasversal comb

Net module support

Epoxy glue used to place microtube on very thin transversal CfRP stiffeners.

Micropositioning and microgluing work required a dedicated gluing mask!

Sealing of the hydraulic interface obtained with epoxy/CFRP .

 $X = 0.15\%$ X_0

The Net Module has the same hydraulic parameter / microtube , already measured for Microchannel module.

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Net module test results

From this experimental data, the Net Module is able to cool power up to about 1.5 W/cm2 at the max required Temperature (50 °C). This goal can also be achieved with a greater safety factor by reducing the inlet coolant temperature.

Tests performed with water-glycol @ 10 °C as coolant.

Net module test results

T_average VS Total Mass Flow (kg/min)

Net module test results

Longitudinal Temperature Drops VS Reynolds

In order to decrease the longitudinal temperature drop along the module (Difference between ${\mathsf T}_{\mathsf{input}}$ and T_{output}) is possible to increase the Reynolds number, that means increase the fluid velocity. '
<mark>*Remark*</mark>: This means the pressure drops grow significantly!!

The hydraulic parameter shows that for the microchannel geometry there is a laminar flow and a good thermal film coefficient (h)

Thermal Simulation

In order to validate the experimental tests we have been performedsimulation studies on the Net micro-channel Module .

Boundary conditions values:Power density: 1 W/cm2 Water film coefficient*: 3275 W/m2KCoolant Temperature: 10 $^\circ\!{C}$ Air film coefficient: 5 W/m2KAir Temperature: 22 °C

Thermal conductivity of the materials:CFRP: 2 W/mK PEEK: 0.25 W/mK Kapton: 0.15 W/mK Aluminum: 210 W/mKGlue: 0.22 W/mK

*: it is derived from experimental and geometrical data.

Case study: 1 W/cm² (the same Boundary values used for microchannel module) We consider the entrance region of the module. Heat flux

There are several lines to follow for further enhancing the performance of the microchannel support:

1) Further miniaturization of the base microtube profile: CFRP thickness = 500 µm, peek tube inner diameter = 200/50 th µm. (at present we are developing prototypes with the companies: it is possible but it is difficult !)

2) Use of thermoplastic technology and/or composite material with higher conductive thermal coefficient. (collaboration with companies needful)

3) Opposite flow directions of the coolant in the module in order to minimize the temperature variation along the module (feasible: it requires a special design of the hydraulic interfaces)

Net Module

Remarks :

The Net Module is a support structure well suited for variable specific power request .

 In fact it is possible to build a structure by adding single microtubes according to the sensor power amount, with means minimum material budget without change dramatically the design of the project.

• We performed studies for a light mechanical/cooling support structure suited for the L0 of the Super-B experiment and in general also for detectors with high power dissipation in the active region (order of 2 W/cm²).

• Our prototypes design for the L0 Super-B detector, based on microchannel technology ins ingle phase forced convection, matches the requirements for pixel MAPS (P= 2W/cm², X = 0.25%) and for pixel hybrid sensors (P= 1.5-1,0 0 $\textsf{W/cm^2}$, $\textsf{X}_{\textsf{0}}$ = 0.15%) .

• Further enhancement are still possible within this technology, gaining in X_0 and thermal efficiency.

BACK UP

Test Procedures

The power dissipated by the kapton heater could be tuned from 1.0 to 3.0 $\,$ W/cm 2 .

The tests have been performed in standard way for both kinds of module. During the tests the average temperature of the environment was 22.0 $^{\circ} \mathcal{C}$ (for these kind of test there is no need to avoid environment free convection and irradiation).

The test was performed by setting the fluid pushing pressure 1.5 atm, the (suction) pressure 0.5 atm, the fluid temperature 10 $^\circ$ C. The electrical power was then switched on and set to the lower specific power (1.0 W/cm2). The maximum pressure was set 3 atm and the heater power tuned up according to the experimental program (1.0 to 3.0 W/cm²)

In all conditions, the DAQ system is able to record up to 24 parameters at the same time.

Test and set-up at TFD lab

Thermal Simulation

