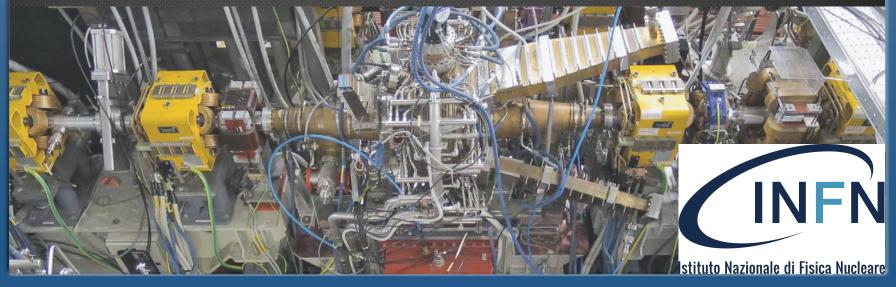


Accelerator Laboratory Magnets in Particle Accelerators

Carlo Ligi, Lucia Sabbatini, Alessandro Vannozzi



Topics

- Magnetization / Ferromagnetism
- Materials for electromagnets: yokes / conductors
- Magnetic design
- Power Supplies for magnets
- Lab experience:
 - Magnetic length measurement
 - Quadrupole gradient measurement
 - Quadrupole excitation curve measurement
 - Measurement of e/m ratio with an electron beam



Materials for electromagnets: Magnetization

The spin of an electron, combined with its orbital angular momentum, results in a magnetic dipole moment and creates a magnetic field.

In many materials (with a filled electron shell), the total dipole moment of all the electrons is zero.

Atoms with **partially filled shells** can experience a net magnetic moment in the absence of an external field. Ferromagnetic materials contain many atoms with unpaired spins.

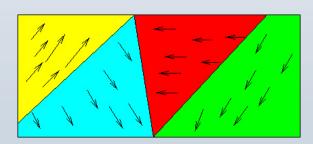
Elettroni 3d spaiati	Atomí	Numero di elettroni		Config	urazione elet orbitali 3 <i>d</i>	tronica		Elettroni 4s
3	V	23	+	+	1			2
5	Cr	24	A	+	4	+	+	1
5	Mn	25	4	4	A	A	+	2
4	Fe	26	* *	4	*	4	4	2
3	Co	27	A ¥	++	4	4	4	2
2	Ni	28	* *	* *	+ +	4	4	2
O	Cu	29	+ +	4 +	* +	* *	+ *	1

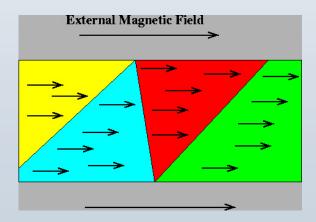


Ferromagnetism is the property of some materials that exhibit a spontaneous magnetization.

In small WEISS domains $(10^{-3} - 10^{-8} \text{ m})$ the magnetic dipole moments of the atoms tends to align. The domains are randomly oriented.

In presence of an external B, all the domains tends to align with it.

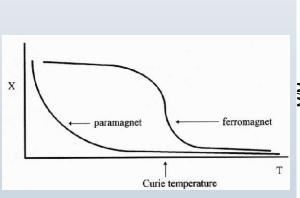


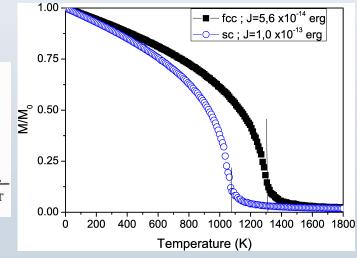




Iron, Cobalt, Nickel (Z = 26, 27, 28) are ferromagnetic elements, as well as some of their alloys and some rare-earth metal compounds.

Ferromagnetism is a function of T and disappears when the material is heated over the *Curie Temperature*, which depends on the material.





Fe:	Tc=1043K
Ni:	Tc=627K
Co:	Tc=1388K
$FeOFe_2O_3$:	Tc=858K
$NiOFe_2O_3$:	Tc=858K
$CuOFe_2O_3$:	Tc=728K
$MgOFe_2O_3$:	Tc=713K
MnBi:	Tc=630K
MnSb:	Tc=587K
$MnOFe_2O_3$:	Tc=573K
$Y_3Fe_5O_{12}$:	Tc=560K
CrO ₂ :	Tc=386K
MnAs:	Tc=318K
Gd:	Tc=292K



High-purity iron (impurities < few 100 ppm) such as ARMCO (American Rolling Mill Company) iron is the most used magnetic steel for yokes, which can be either massive or laminated.

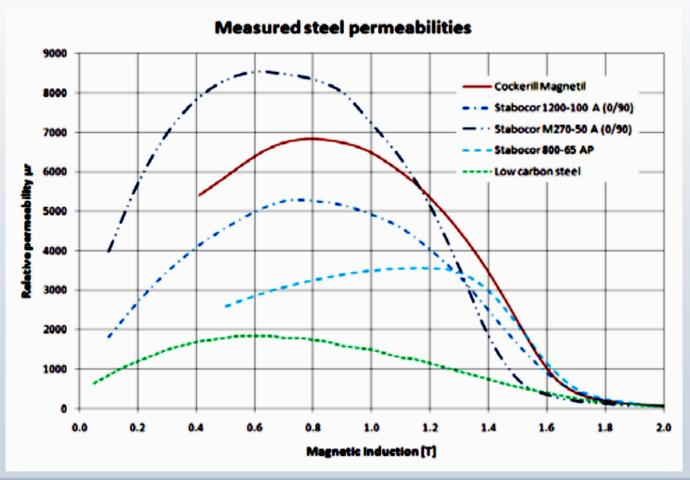
Solid yokes support eddy currents hence cannot be cycled rapidly. Moreover, laminated steel assure better reproducible steel quality.

Laminated steel is generally cheaper than solid steel but require more tooling for the production.

Typical sheet thickness is in the range 0.3 - 1.5 mm, the filling factor being around 97%.



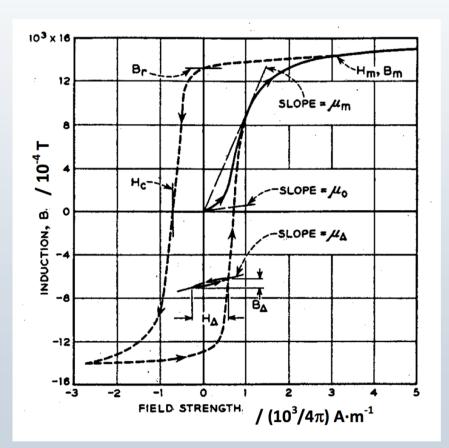
Inside a ferromagnetic material the *permeability* is a function of the magnetic induction B: $B = \mu(B) H = \mu_r(B) \mu_0 H$





The hysteresis loop

 $(B_r = residual induction, H_c = coercive force)$

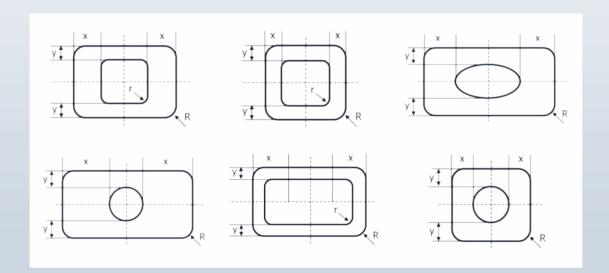




Materials for electromagnets: Conductors

Common materials used for the coil fabrication are basically OFHC Copper and Aluminum (NbTi and Nb₃Sn for superconducting coils)

Property	Aluminium	Copper (OF grade)
Purity	99.7%	99.95%
Resistivity at 20°C	28.3 nΩ m	17.2 nΩ m
Thermal resistivity coefficient	$0.004~{ m K}^{-1}$	$0.004~{ m K}^{-1}$
Density	2.70 kg/dm^3	8.94 kg/dm^3
Thermal conductivity	237 W/m K	391 W/m K
Approx. price	4.7 €/kg	11 €/kg





Materials for electromagnets: Conductors

Coil design should take in account some requirements as:

- Low power consumption, which is related with the yoke design
- Sufficient cooling performance (Water/Air cooling)
- Adequate insulation thickness
- Manufacturing Cost





Magnets in Accelerators:

o D.C.

- ✓ Electromagnets
- Normal Conducting
- o A.C.
- Superconducting
- ✓ Permanent Magnets

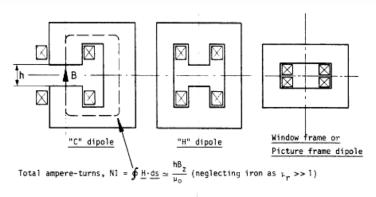
Accelerator's Magnets

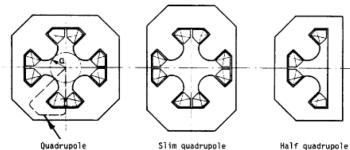
- Dipoles (& Correctors)
- Quadrupoles
- Sextupoles
- Octupoles
- Wigglers
- Solenoids
- Combined-function, etc.

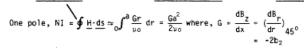


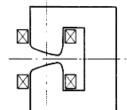


Magnets in Accelerators:









- NI = number of ampere-turns [A]
- h = dipole gap height [m]
- a = inscribed circle radius [m]
- s = integration path [m]
- H = magnetic field strength [A m⁻¹]

Lorentz force

$$\vec{F} = e(\vec{v} \times \vec{B} + \vec{E})$$

Energy vs Field

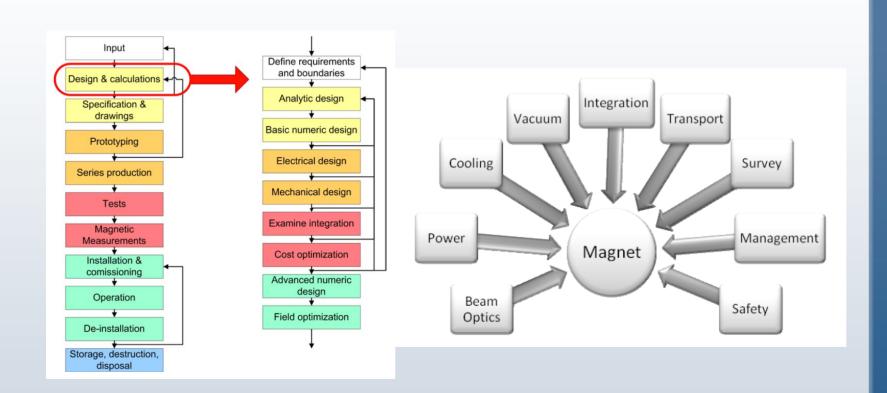
$$E(GeV) \approx 0.3 \cdot B(T) \cdot R(m)$$

Emission by sinchrotron radiation

$$\Delta E = \frac{1}{3\epsilon_0} \frac{e^2 E^4}{(m_0 c^2)^4 R}$$

$$\propto \frac{E^4}{m_0^4 R}$$

Magnetic design



Keyword: integration between services!



Magnetic design

General requirements

- Beam parameters (mass, charge, energy, deflection angle...)
- Magnetic field (integrated field or integrated gradient)
- Aperture (physical aperture and good field region)
- Operation mode (continuous, pulsed, fast pulsed, ramped...)
- Field quality (field uniformity)
- Available space



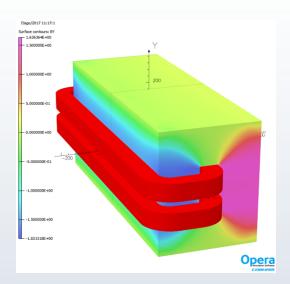
2-D and 3-D Simulations

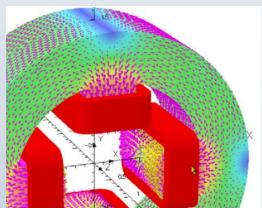
Some finite elements computational codes:

- POISSON (2-Dimensional)
- OPERA, ANSYS (2 and 3-Dimensional)
- ROXIE (2 and 3D superconducting)



Magnetic design – Finite Element Analysis (F.E.A.) Softwares





Opera 3D simulations

Pre-Processing

- Define geometry of all the regions (Coil, Iron, Air)
- Define material properties (B-H curve)
- Define mesh (region discretization)
- Define Ampere-Turns in the coils region
- Define symmetries

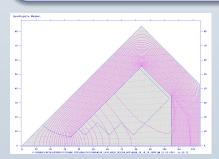
Solver

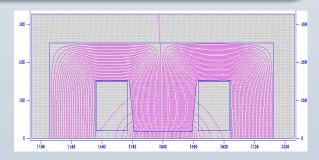
- Linearization of Maxwell Equation
- Definition of magnetic potential (thus flux density) in the mesh nodes

Post-Processing

Results analysis:

- Flux density in the air gap
- Flux density in the iron
- Gradient (for a quadrupole) etc. ...





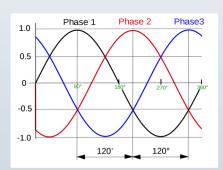




Power Supplies for Magnets

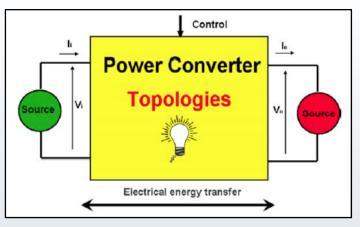


Voltage Source (Power Grid) 3 Phase 50 Hz – 60 Hz



Voltage Source

Imposes a voltage independently of the current flowing through it.



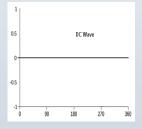
Power Converter Performance

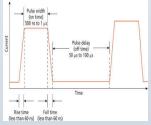


- Stability
- Accuracy
- Reproducibility
- Resolution
- Efficency
- EMC
- Reliability (MTBF), Reparability (MTTR)



Magnets DC or Pulsed. Current Source needed



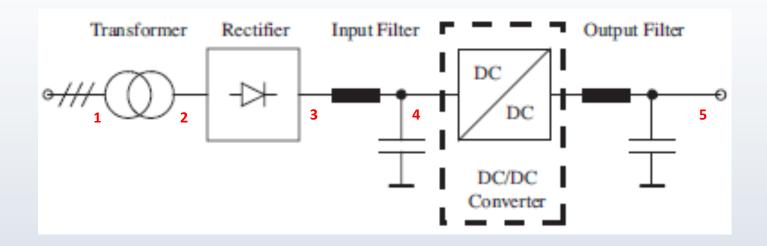


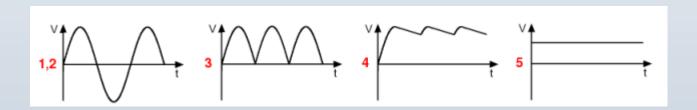
Current Source

Imposes a current independently of the voltage at its terminals.



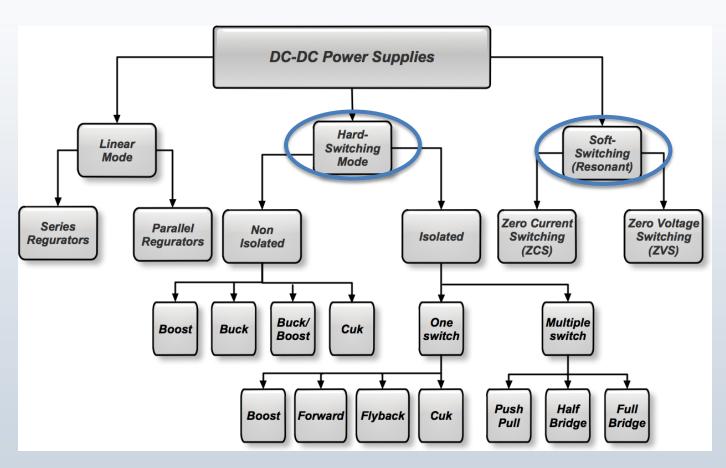
Power Supply: General Layout





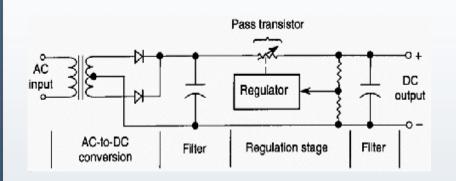


Power Supplies for Magnets





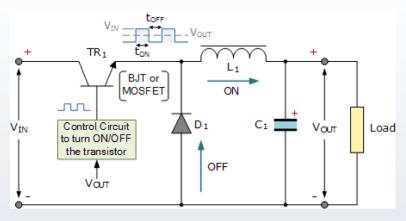
Linear mode Converter vs Switched Mode Converter



Linear Converter

- High dynamic for the output voltage regulation
- © Poor output voltage ripple
- \odot Low Efficency \rightarrow Loss proportional to I_{LOAD} and non-zero $V_{TRANISITOR}$)

Mainly used in low-power application



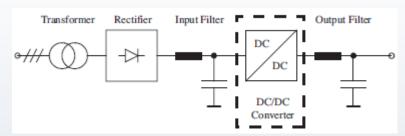
Switched-Mode Converter

- ⊕ High Efficency and High power density → Loss related only to the swittching losses and low conduction losses
- ⊗ EMC emission
- Needed output filter to reduce output voltage ripple

Used in low and high power applications.



Switched Mode Converter

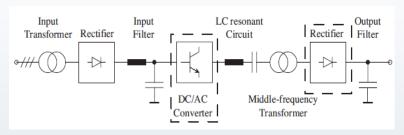


Direct DC/DC converter

Direct DC/DC Converter

Only SINGLE stage is used to adjust voltage levels. They are classified according to the galvanic insulation of a transformer

- Insulated
 - Forward DC/DC converter
 - Flyback DC/DC converter
- Non insulated
 - Buck
 - Boost
 - Buck/Boost
 - Cuk



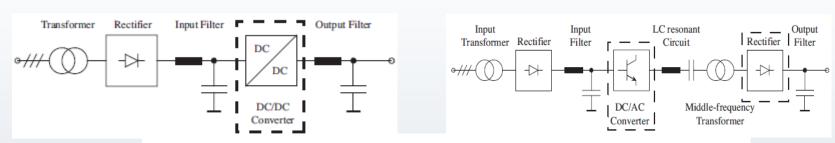
DC/DC Converters with an intermediary AC stage

DC/DC Converters with an intermediary AC stage

- Output voltage regulation achieved by the control of the DC/AC converter
- LC resonant circuit should be used to enable soft-switching condition for te DC/AC converter in order to maximise its efficency



Switched Mode Converter



Optimization of Switched Mode Power Converter

age

Reduction of switch stress

Only SINGLE stag

Reduction of conduction loss

Optimization of switch frequency

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Insulated

They are classifie

insulation of a tra

- Forward DC/DC converter
- Flyback DC/DC converter
- Non insulated
 - Buck
 - **Boost**
 - Buck/Boost
 - Cuk

LC resonant circuit should be used to enable soft-switching condition for te DC/AC converter in order to maximise its efficency

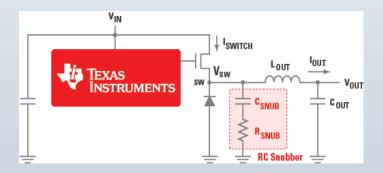


Hard Switching vs Soft Switching Power Supplies

Hard Switching

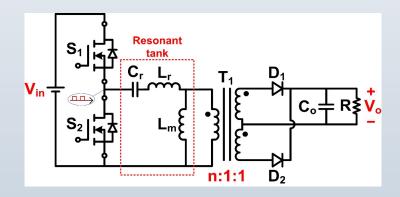
- Switching losses reduction
- Magnetics parts size reduction
- Higher efficency
- Attenuation of harmonics in the range of tens of kHz
- Increased control complexity

- ② Overall Power supply efficiency doesn't change respect to the configuration without snubber



Soft Switching

- Higher efficency
- Switching losses reduction
- Magnetics parts size reduction
- ② Attenuation of harmonics in the range of tens of kHz
- Increased control complexity
- High cost





Hard Switching vs Soft Switching Power Supplies

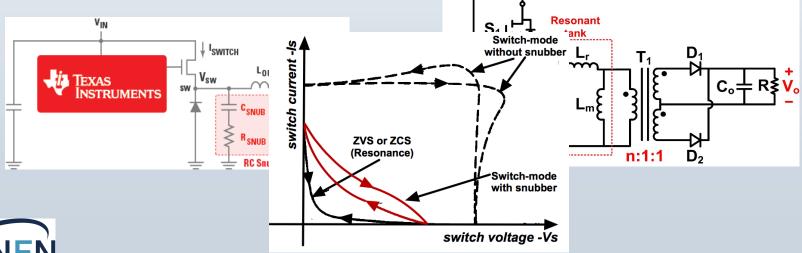
Hard Switching

- Switching losses reduction
- Magnetics parts size reduction
- Higher efficency
- Attenuation of harmonics in the range of tens of kHz
- Increased control complexity

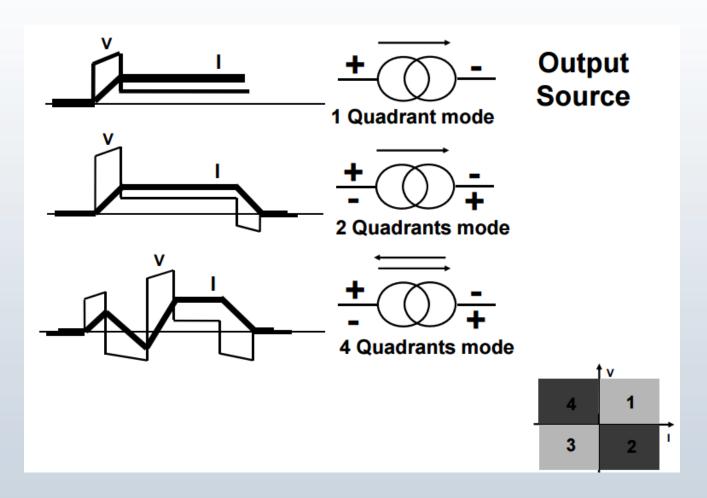
- Overall Power supply efficiency doesn't change respect to the configuration without snubber

Soft Switching

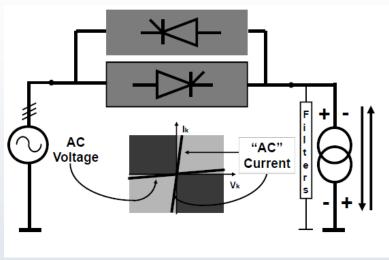
- Higher efficency
- Switching losses reduction
- Magnetics parts size reduction
- Attenuation of harmonics in the range of tens of kHz
- Increased control complexity
- High cost



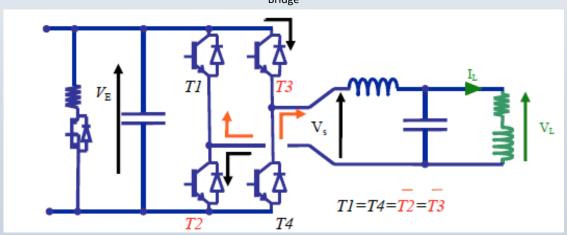
Operating Modes



Power Supply - 4 Quadrants mode



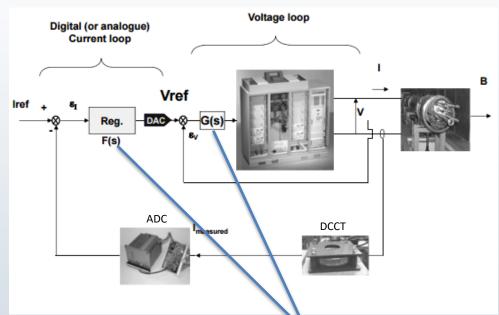
Direct Converter: Antiparallel Thyristor Bridge

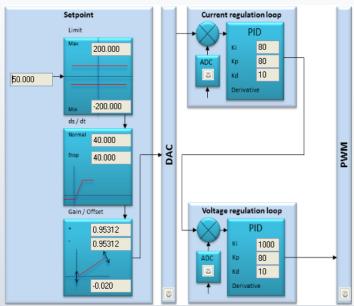






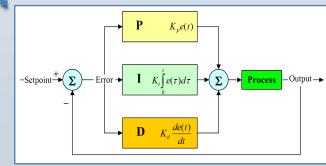
Power Converter Control





Power Converter Control Diagram

Power Converter Control GUI

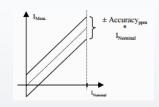


P.I.D. Block Scheme

P R E C I S I O N

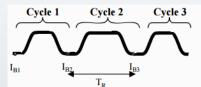
Accuracy

Long term setting or measuring uncertainty taking into consideration the full range of permissible changes of operating and environmental conditions.



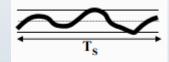
Reproducibility

Uncertainty in returning to a set of previous working values from cycle to cycle of the machine.



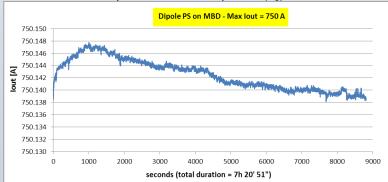
Stability

Maximum deviation over a period with no changes in operating conditions.



Accuracy, Reproducibility and Stability are quantitative parameters (measured in p.p.m. of In)

They're defined for a period (T_s)

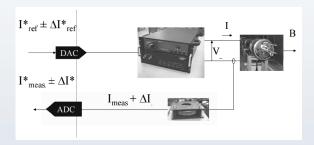


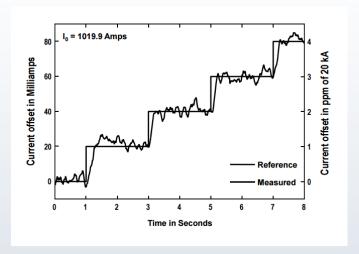
Power Supply Long term stability test

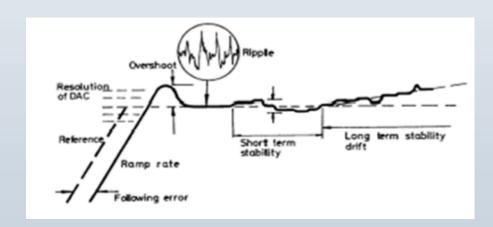
Power Converter for Magnets – Performance Requirements

Resolution

Minimum set current step of power supply It is expressed in ppm of In Directly linked to A/D system





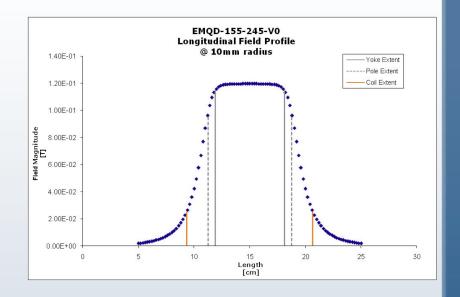




Magnetic length

Magnetic length (*effective* length) is always larger than the actual iron length (*mechanical* length):

$$L_{mag} = \frac{\int_{-\infty}^{+\infty} B_z(y) dy}{B_0}$$



Dipole: $l_{mag} \approx l_{iron} + 2hk$

h: magnet gap

k: geometrical factor, typically 0.3÷0.6

Quadrupole: $l_{mag} \approx l_{iron} + 2rk$

r: aperture radius

k: geometrical factor, typically ~0.45)



Quadrupole: Gradient

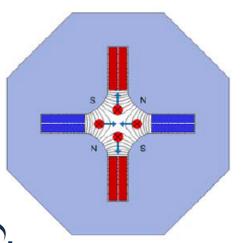
In a quadrupole, the components of the ideal magnetic field in the plane transverse to the beam are given by (general equations):

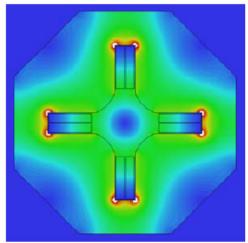
$$B_z = Gx$$

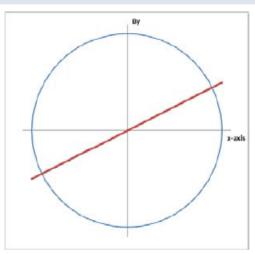
$$B_x = Gz$$

G (T/m) is the field gradient of the vertical component in the horizontal direction (or equivalently, the gradient of the horizontal component in the vertical direction). Sign of G: the quadrupole focuses or defocuses.

In our coordinate system: $G = \frac{dB_z}{dx}$



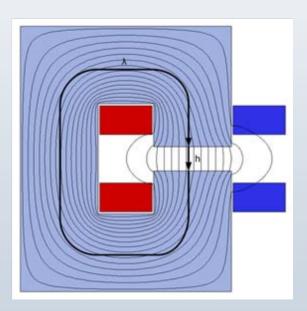




B vs I (dipole)

The flux density in the air gap is proportional to the excitation current.

$$NI = \oint \overrightarrow{H} \overrightarrow{dl} = \oint \frac{\overrightarrow{B}}{\mu} \overrightarrow{dl} = \int_{gap} \frac{\overrightarrow{B}}{\mu_{air}} \overrightarrow{dl} + \int_{yoke} \frac{\overrightarrow{B}}{\mu_{iron}} \overrightarrow{dl} = \frac{Bh}{\mu_{air}} + \frac{B\lambda}{\mu_{iron}} \approx \frac{Bh}{\mu_0}$$



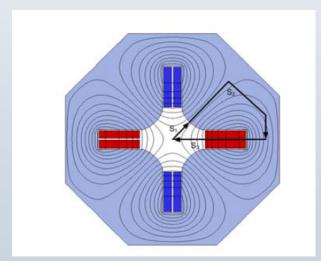
B vs I (quadrupole)

The gradient in the air gap is proportional to the excitation current.

$$H(r) = \frac{B'}{\mu}r$$
 (B' costant in ideal quadrupole)

$$NI = \oint \overrightarrow{H} \overrightarrow{dl} = \frac{B'}{\mu_0} \int_{gap} r \overrightarrow{dr} + \frac{B'}{\mu_{iron}} \int_{yoke} r \overrightarrow{dr} + \frac{B'}{\mu} \int_{X \ axis} r \overrightarrow{dr} \approx \frac{B'}{\mu_0} \int_0^R r \overrightarrow{dr} = \frac{B'r^2}{2\mu_0}$$

$$B_z = B'_z \cdot x \propto I$$



Field quality estimation

A simple method to judge the field quality of a magnet is to evaluate the homogeneity of the field (for dipoles) or of the gradient (for quadrupoles) in the defined good field region (GFR):

Dipole:

$$\frac{\Delta B}{B_0} = \frac{B_Z(x, z) - B_Z(0, 0)}{B_Z(0, 0)} \le 0.01\%$$

Quadrupole:

$$\frac{\Delta B'}{B_0'} = \frac{B_Z'(x,z) - B_Z'(0,0)}{B_Z'(0,0)} \le 0.1\%$$



Magnetic measurements

Equipment:

- Quadrupole
- Axes movement control system
- Hall probe
- Power supply
- PC (Labview, Excel...)

We will evaluate the following parameters:

1. magnetic length

longitudinal scans at different x

2. magnetic gradient

radial scan at magnet center

3. B vs I

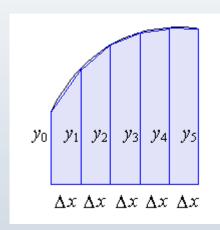
current scan at a fixed position

QUADRUPOLE	Mag No 91544.4
Aperture	53 mm
Gradient	?? T/m
Effective length	?? mm
Focussing power	0.41 T
Nominal voltage	2.2 V
Nominal current	15.5 A



Trapezoidal rule to evaluate with Excel the general integral

$$\int ydx = \frac{\Delta x}{2} (y_1 + 2y_2 + 2y_3 + \dots + 2y_{n-2} + 2y_{n-1} + y_n)$$





Measurement of the e/m ratio

An electron gun, placed inside a glass bulb filled with neon gas, emits an electron beam. The gas atoms are ionized and a straight luminescent beam is produced.

When a homogeneous magnetic field is applied, the electrons deflect, and the trajectory radius can be measured





Helmholtz coils

Two narrow coils with radius R are placed in parallel at a distance R. Combining the magnetic fields produced, we get a volume with a reasonably uniform magnetic field

$$B = kI_H = \left(\frac{4}{5}\right)^{\frac{3}{2}} \frac{\mu_0 NI_H}{R}$$

In our setup:

$$k \cong 0.756 \, mT/A$$

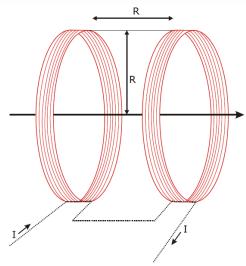
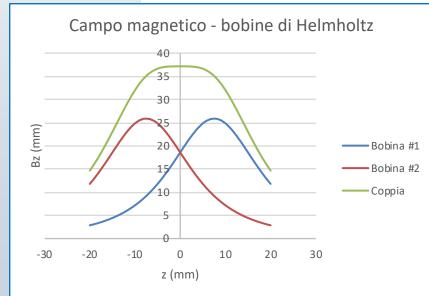


Fig. 1 Bobine nella geometria di Helmholtz





Measurement of the electron specific charge

• Lorentz force:
$$\vec{F} = q\vec{v}x\vec{B}$$

• Centripetal force:
$$F = m \frac{v^2}{r}$$

$$\Rightarrow \qquad m\frac{v^2}{r} = evB$$

• v is related to the gun accel. voltage: $\frac{1}{2}mv^2 = q\Delta V = eU$

So, we get:
$$v = \sqrt{\frac{2eU}{m}}$$

Putting v in the equation:

$$\frac{e}{m} = \frac{2U}{r^2 B^2}$$



Measurement of the electron specific charge

$$\frac{e}{m} = \frac{2U}{r^2 B^2} \qquad (B = kI_H)$$

A variation of U and/or B will modify the radius r.

- Fix a certain r_0 .
- For different U (in the range 200-300 V), move B to get the desired r_0 .
- Graph 2U vs B^2 .
- Calculate e/m.

