

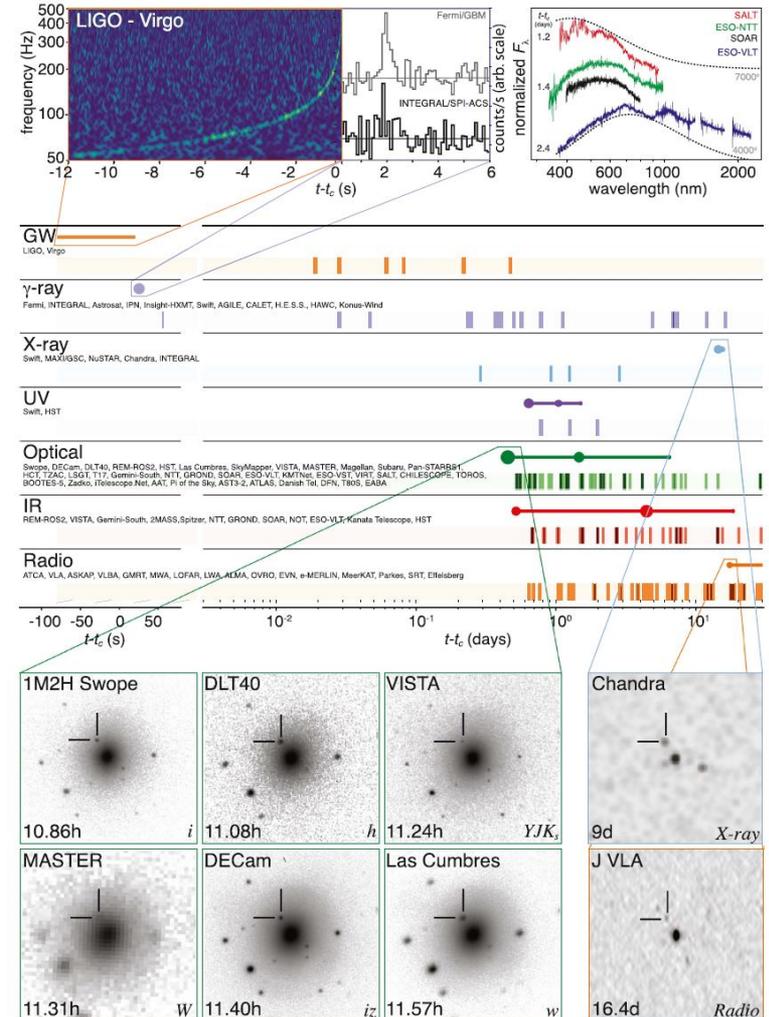
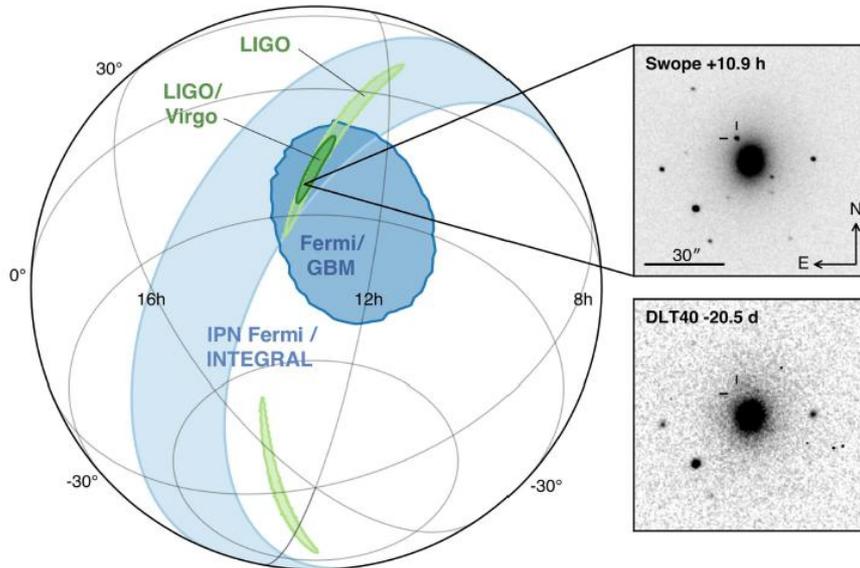


Stray Light Control in Virgo and future  
prospects  
(a very incomplete survey)

A.Chiummo  
May 3rd, 2019

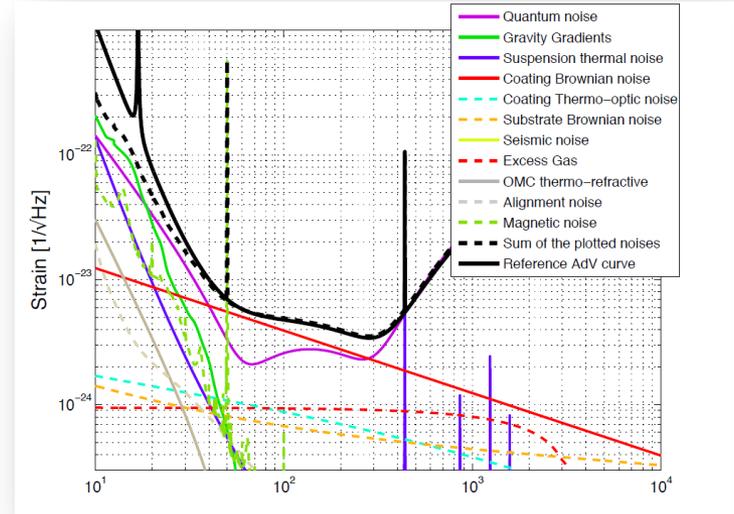
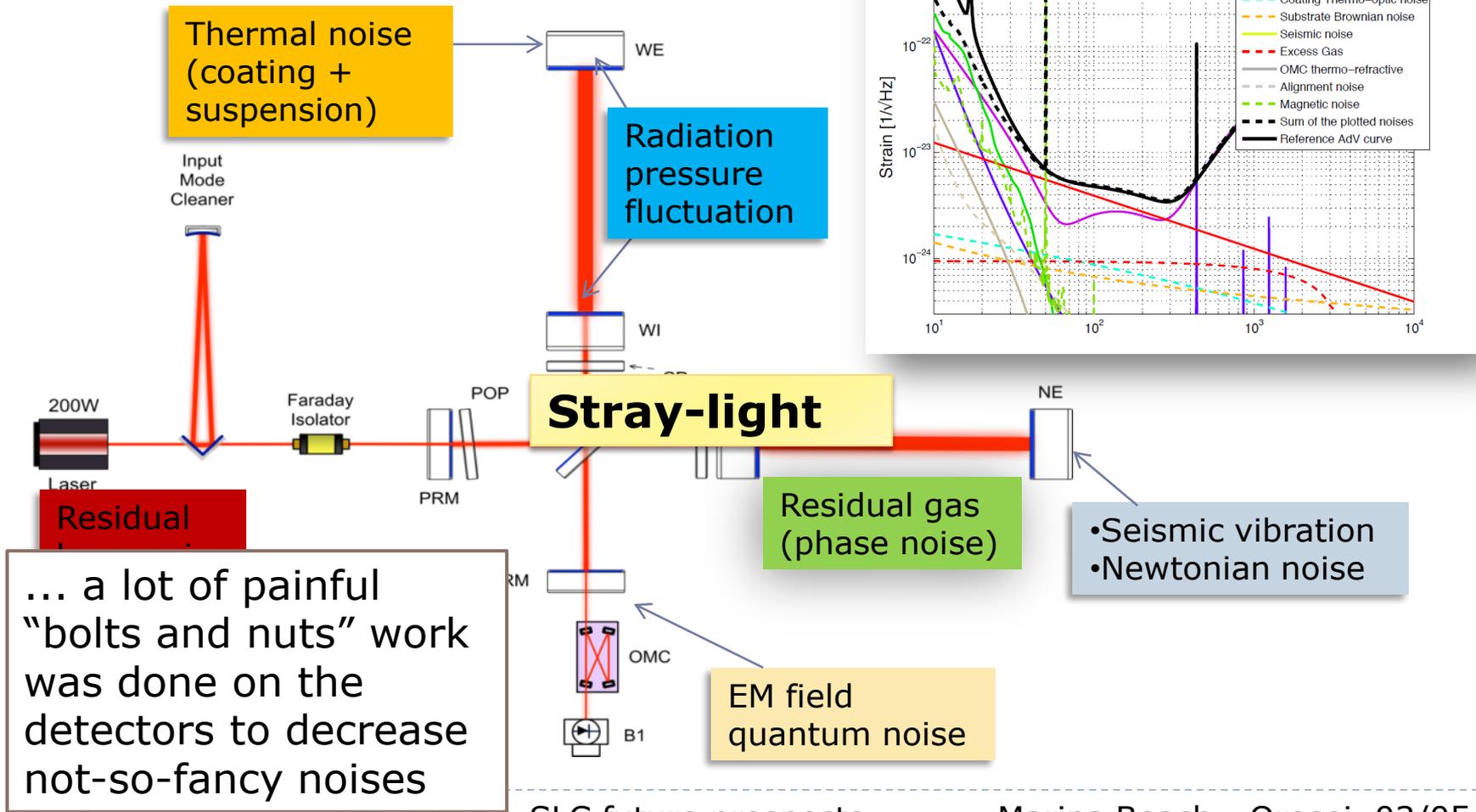
# GW170817: beautiful Physics

The “gold mine” (quite literally) of Multimessenger Astronomy was possible also because...



# GW Detectors - Noise

❑ *Not only fundamental noises...*



# An Old Enemy

❑ Stray light gave countless problems during past generation (as long expected)

J. Phys. E: Sci. Instrum., Vol. 12, 1979. Printed in Great Britain

## An argon laser interferometer for the detection of gravitational radiation

H Billing, K Maischberger, A Rüdiger, R Schilling, L Schnupp and W Winkler  
Max-Planck-Institut für Physik und Astrophysik, Munich, Germany

Received 10 April 1979

**Abstract** A gravitational radiation antenna, consisting of a Michelson interferometer illuminated with an argon laser, is being developed. A first stage has been reached with the construction of a small prototype of 3 m arm length. This prototype was used to locate and study various noise sources and other disturbances, which would restrict signal-to-noise ratio. From an analysis of these disturbances, the demands on apparatus components have been estimated. Some constructional details are given, as well as suggestions for improvement aimed at a future interferometer of increased base length, with the prospect of successful operation.

[Billing79] H Billing, K Maischberger, A Rudiger, R Schilling, L Schnupp and W Winkler, "An argon laser interferometer for the detection of gravitational radiation", J. Phys. E: Sci. Instrum. 12 1043 (1979)

21-06-12

J. Marque – Cascina VESF school '12

One of the oldest papers which identified stray light as a serious problem for GW detectors.

### 3.6 Light scattered with long path differences

In an interferometer with long travel times, the frequency jitter  $\delta\nu/\nu$  can enter in yet another way into the measurements. Light scattered back into the direction of the properly returning main beam may have path differences  $\Delta L$  with respect to the main beam which can be of the order of the total path length  $L$ . Such extreme path differences occur for light scattered prior to the delay line, or during early reflections, but also for scattered light making an extra cycle in the delay line.

On interference with the main beam, this scattered light of relative field strength  $r$  will cause a phase jitter corresponding to a spurious path variation  $\delta L$ , roughly approximated by

$$\delta L \approx r \Delta L \frac{\delta\nu}{\nu}. \quad (7)$$

Again, we want this to be below the 1 W shot noise equivalent  $\delta L = 10^{-16} \text{ m Hz}^{-1/2}$ . We hope that the frequency jitter can be reduced by a factor of  $10^3$  with respect to that of our present laser. Even then, but assuming  $\Delta L = L = 100 \text{ km}$ , a back-scattered fraction of only  $r^2 = 10^{-11}$  in intensity is allowed. This will be very hard to achieve, but it does not appear impossible.

### 2.5 The 'parasitic interferometer'

Light scattered at one of the optical surfaces in the interferometer and returning to the laser will be reflected at the laser output mirror. Here, with a phase  $\phi(t)$  determined by the extra path  $2(D_0 + d(t))$ , it interferes with the main beam (figure 6), giving rise to intensity variations. This is what we call the 'parasitic interferometer'.

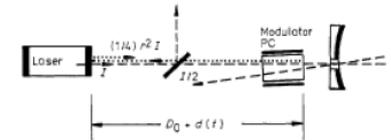


Figure 6 Light paths in a 'parasitic interferometer'.

If the difference nulling method is used, these intensity fluctuations are treated as being merely an additional intensity noise. For the modulation method, however, the 'parasitic interferometer' constitutes a new noise source: backscattered light that has passed the modulator Pockels cell leads to a 10 MHz intensity modulation of the main beam, which the demodulator converts into a spurious interferometer signal.

The relative intensity fluctuations  $\delta I/I$  due to the parasitic interference depend on the fraction backscattered to the laser ( $r^2$  in power, or  $r$  in field strength), and on the distance variation  $d(t)$  between laser mirror and scattering surface, according to, say,

$$\frac{\delta I}{I} \approx r \sin \left( \frac{4\pi}{\lambda} d(t) \right). \quad (6)$$

Extremely small amounts of scattered light could be troublesome. As little as  $r^2 = 10^{-18}$  in intensity, scattered back into the (narrow) laser beam, could cause intensity variations of the order of the signals to be detected ( $10^{-9}$ ).

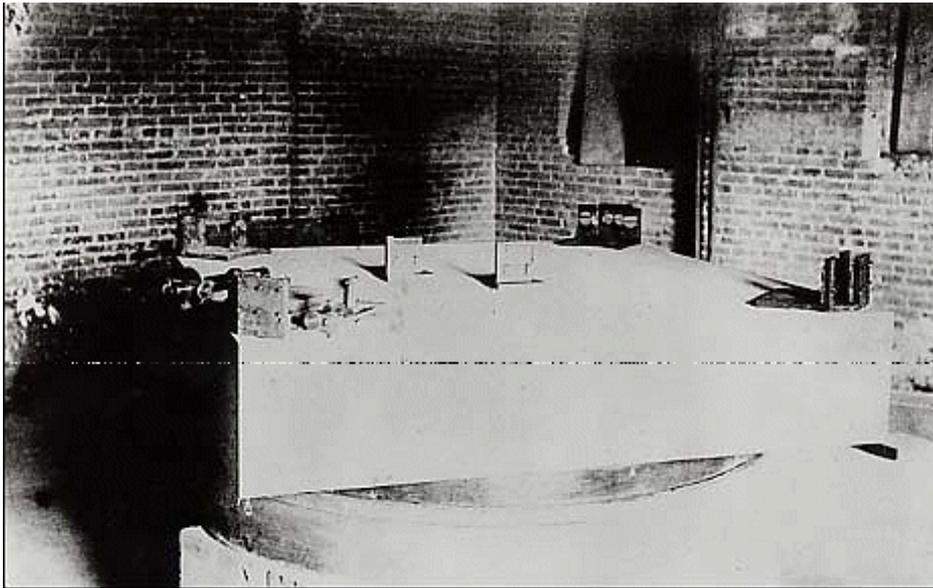
We have to rely on the second factor in equation (6) to reduce the spurious signals. Fortunately, the mechanical motions  $d(t)$  of the optical components involved are very small in our signal frequency range, i.e. above a frequency  $F$  of several hundred hertz.

At very low frequencies  $f$ , however, particularly at the pendulum resonance ( $f \approx 1 \text{ Hz}$ ), we can observe large amplitudes  $a(f)$ , even up to many wavelengths  $\lambda$ . They produce high harmonics  $m f > F$  inside our signal frequency range, which can be described by the Bessel functions  $J_m(4\pi a/\lambda)$  of large order  $m$ . These assume appreciable values only if the argument  $4\pi a/\lambda$  becomes comparable with the order  $m = F/f$ .

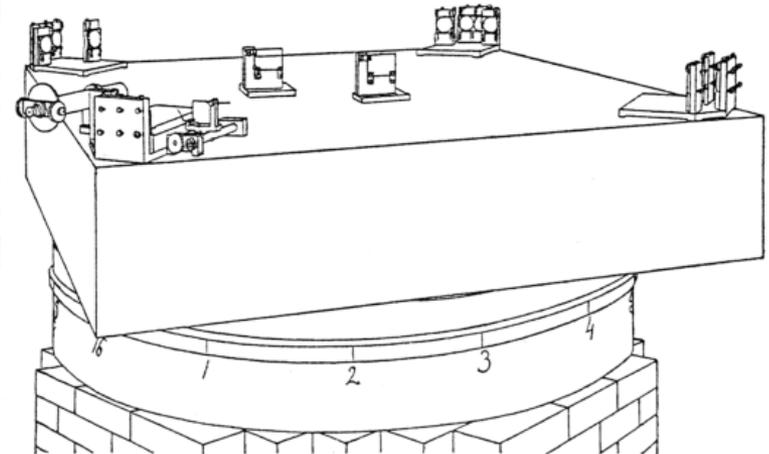
The high- $Q$  resonance of the pendulum had, in fact, led to such large relative motions  $d(t)$ . Therefore, an active damping of the pendulum was introduced (cf §3.1), which practically eliminated the harmonics above  $F$ . Should the need arise, as we proceed to higher sensitivities, one could reduce the backscattered light drastically by the use of a Faraday isolator.

# An Old Enemy

□ ... And even before:

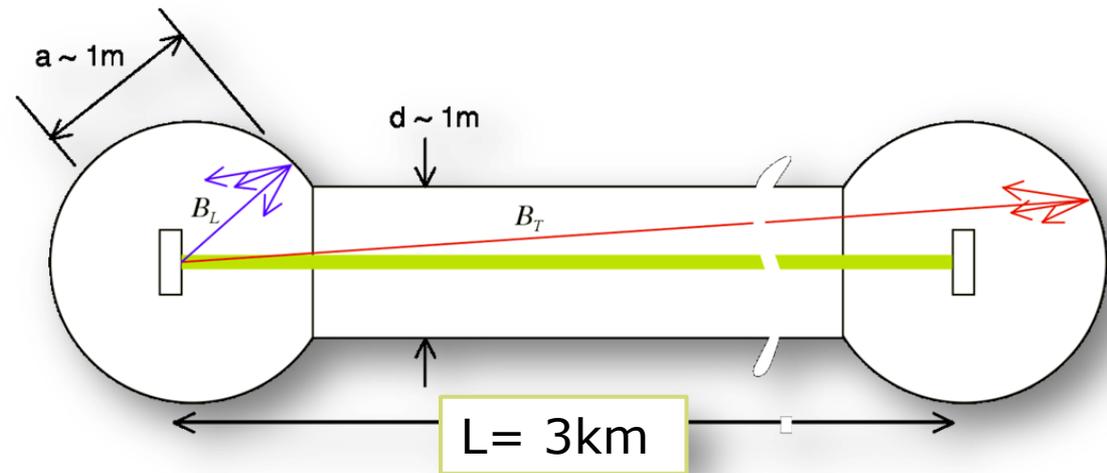


Michelson & Morley's 1887 interferometer  
built in the basement of Western Reserve  
Photo: Case Western Reserve Archive



# An Old Enemy

- ❑ Stray light gave countless problems during past generation (as long expected)
- ❑ A tiny amount of stray light coupling with the fundamental mode after “probing” the vibrations of infrastructures will bury any gravitational signal.



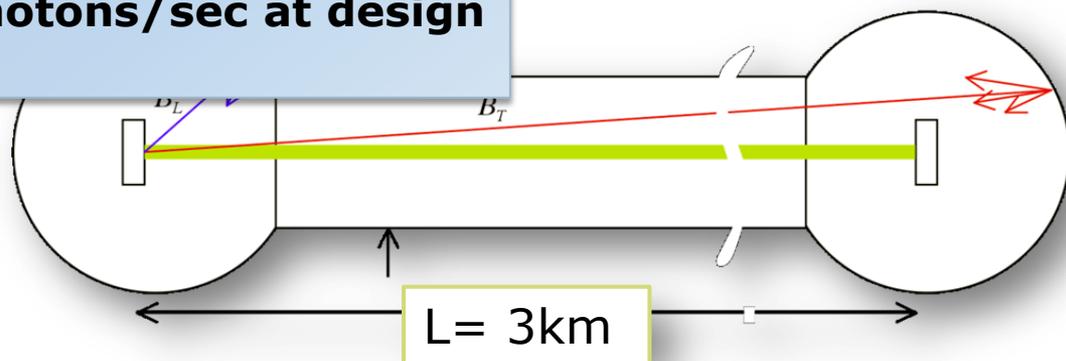
# An Old Enemy

❑ Stray light gave countless problems during past generation (as long expected)

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➤ **1979:** expected troubles when stray light recombines to the main mode with an efficiency of  $10^{-18} \text{ W/W}$

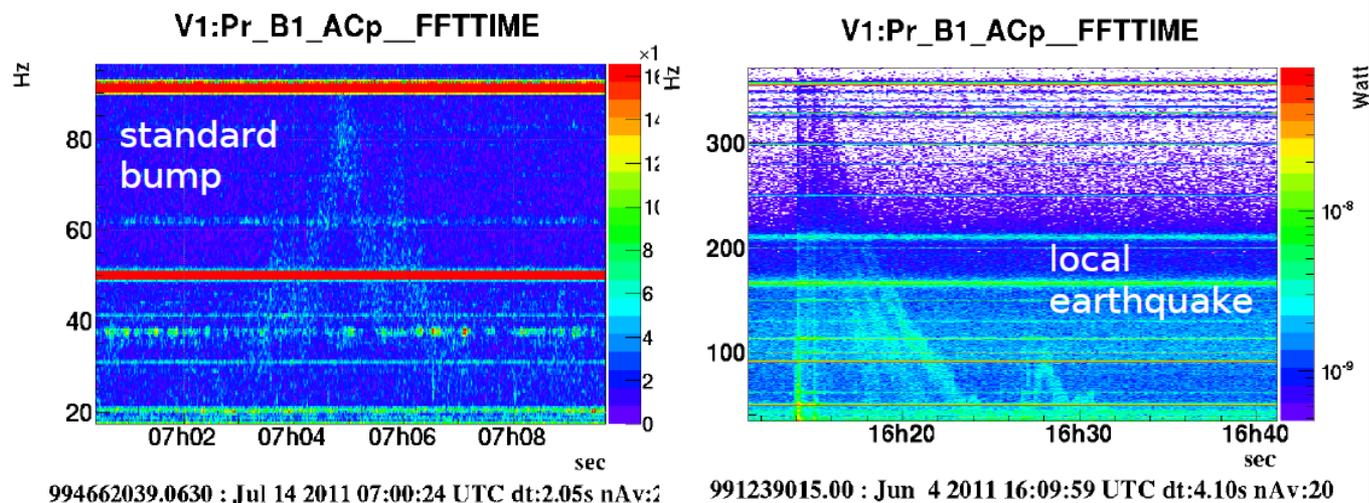
➤ **2015:** expected troubles when stray light recombines to the main mode with an efficiency of  $10^{-24} \text{ W/W}$  ( **$\sim 5$  photons/sec at design configuration**)



# A case study from the past

An annoying noise spoiling Virgo+ sensitivity during VSR4 (2011)

## Baffle-noise?

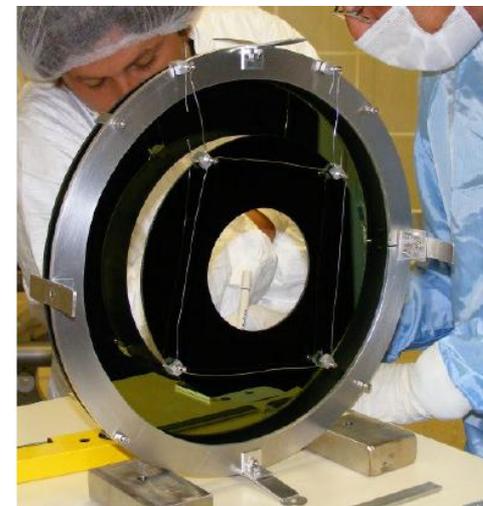
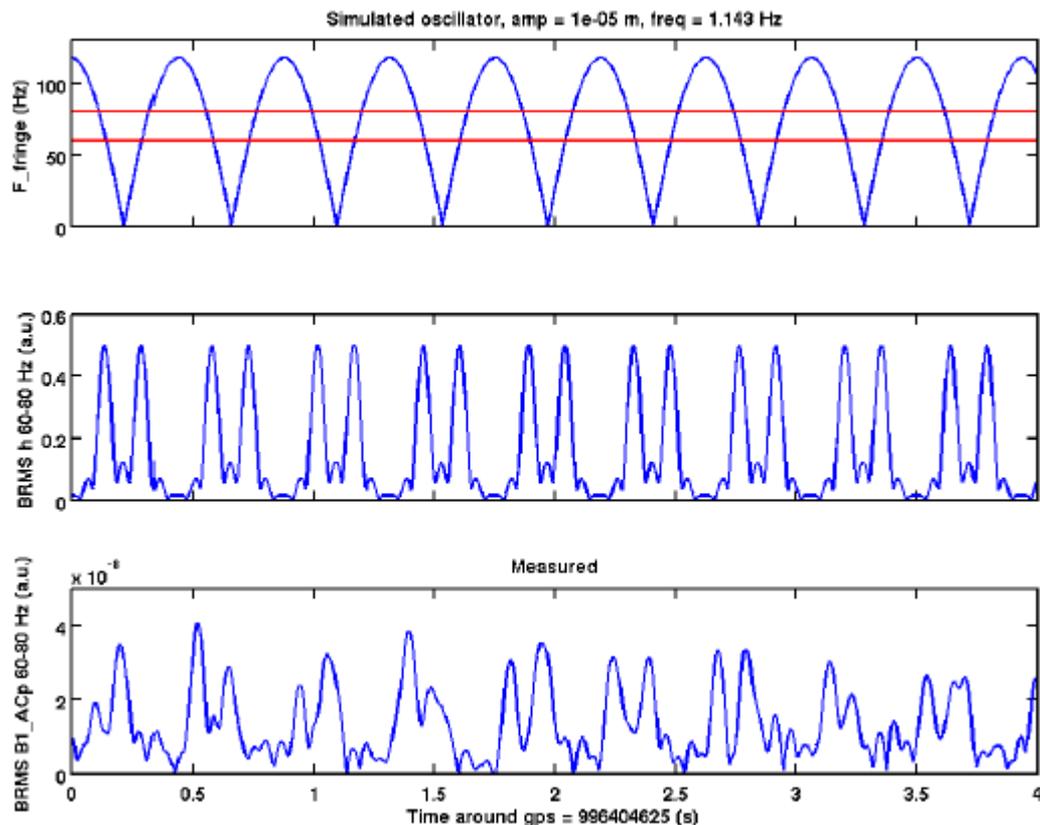


- Noise appears like a bump moving in frequency
- Typical of light scattered by excited baffle

Swinkels et al, VIR-0560A-11

# A case study from the past

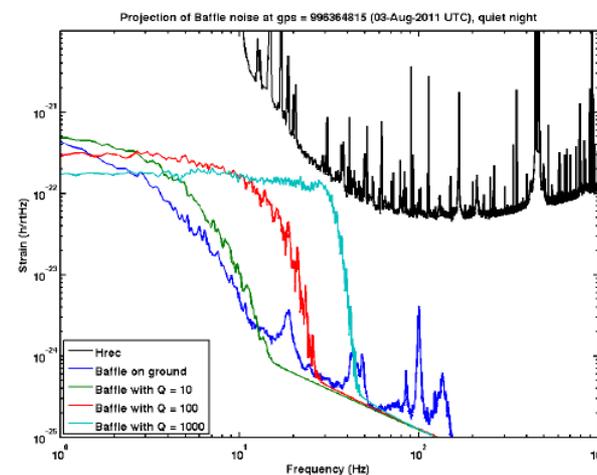
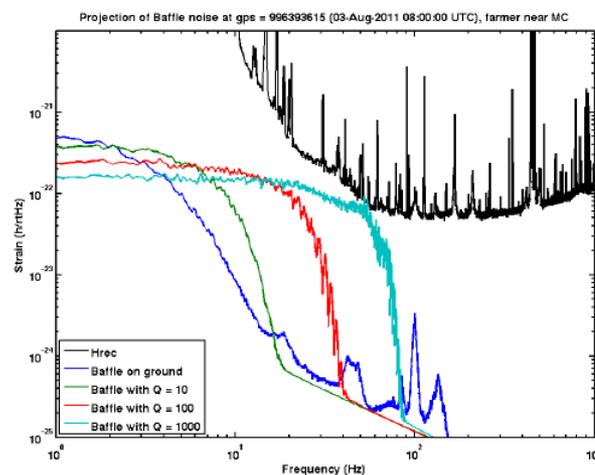
Finally tracked down to the light scattered off a suspended baffle...



Swinkels et al, VIR-0560A-11

# A case study from the past

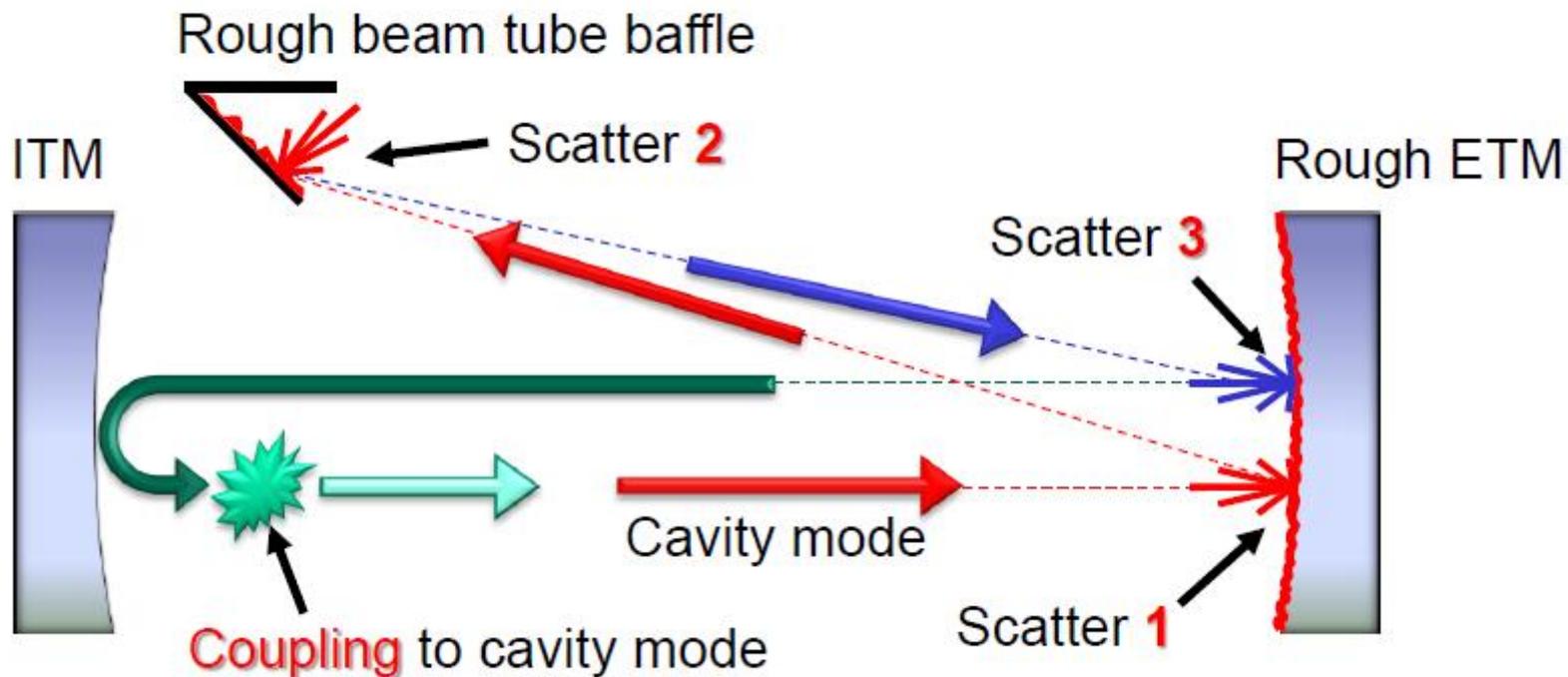
## Noise projection



- Measured data of seismometers, simulated pendulum
- Limiting up to 100 Hz in case of seismic bursts
- Close to limiting around 30 Hz in quiet condition
- Simulated effect of reducing Q or fixing baffle to ground

Swinkels et al, VIR-0560A-11

# Stray Light noise: how does it work?



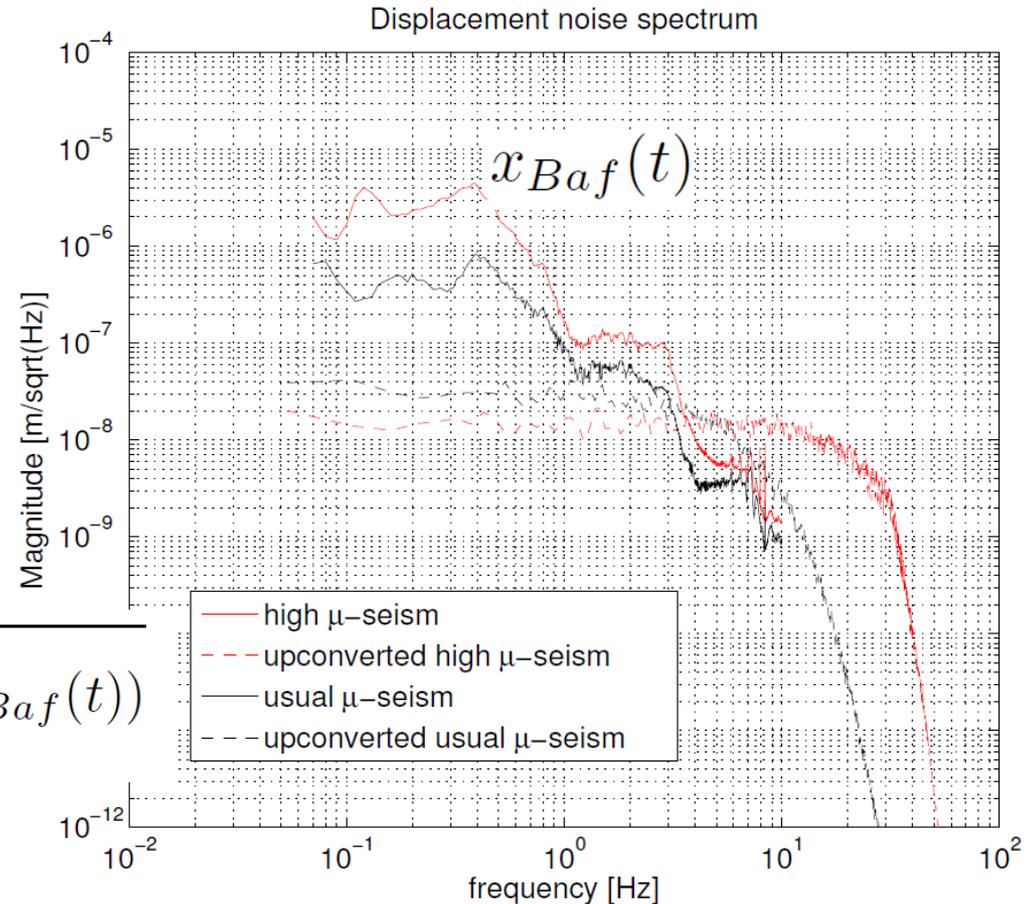
If the scatterer moves wrt the ITF, then the backscattered light is phase modulated before recombining with the ITF main mode

# Stray Light simulations

❑ Non-linear coupling  
(fringe-wrapping)

Regardless of the amplitude of motion of the scatterer, scattered light phase modulation cannot exceed  $2\pi$ . For large amplitude we must use an effective displacement:

$$\tilde{x}_{Baf}(\omega) = \frac{\lambda}{4\pi} \sqrt{PSD\left(\sin\left(\frac{4\pi}{\lambda} x_{Baf}(t)\right)\right)}$$



# Stray Light simulations

❑ Example: how to design new baffles /accept existing ones?

1) Need to evaluate baffle displacement noise and project it to the strain sensitivity.

Recipe for noise projection:

Parameter	Meaning	Estimation method
$ c ^2$	recombination efficiency	FFT (FOG -SIS) /Semi-analytical
Xbaf	(effective) displacement noise of scatterer	Measurement /simulations
Tbaf	Transfer function from Xbaf to dark fringe PD (B1)	Optickle /Finesse /MIST
Tdarm	Transfer function from DARM dof to dark fringe PD	Optickle /Finesse /MIST

$$h_{\text{baf}} = |c| T_{\text{baf}}/T_{\text{darm}} 1/L X_{\text{baf}}$$

# Stray Light simulations

❑ Example: how to design new baffles /accept existing ones?

1) Need to evaluate baffle displacement noise and project it to the strain sensitivity

Recipe for noise projection

Roughness,  
reflectivity,  
shape, position

Parameter	Meaning	Estimation method
$ c ^2$	rec	FOG -SIS) i-analytical
Xbaf	(ef noi	urement /simulations
Tbaf	Transfer function from Xbaf to dark fringe PD (B1)	Optickle /Finesse /MIST
Tdarm	Transfer function from DARM dof to dark fringe PD	Optickle /Finesse /MIST

Mechanics,  
linear /non-linear  
(fringe wrapping)

location

$$h_{baf} = |c| T_{baf}/T_{darm} 1/L X_{baf}$$

# Stray Light simulations

❑ Example: how to design new baffles /accept existing ones?

1) Need to evaluate baffle displacement noise and project it to the strain sensitivity

Recipe for noise projection

Roughness, reflectivity, shape, position

Parameter	Meaning	Estimation method
$ c ^2$	reflectivity	FOG -SIS) / semi-analytical
Xbaf	(effective) noise	Measurement /simulations
Tbaf	Transfer function from Xbaf to dark fringe PD (B1)	Optickle /Finesse /MIST
Tdarm	Transfer function from DARM dof to dark fringe PD	Optickle /Finesse /MIST

Mechanics, linear /non-linear (fringe wrapping)

location

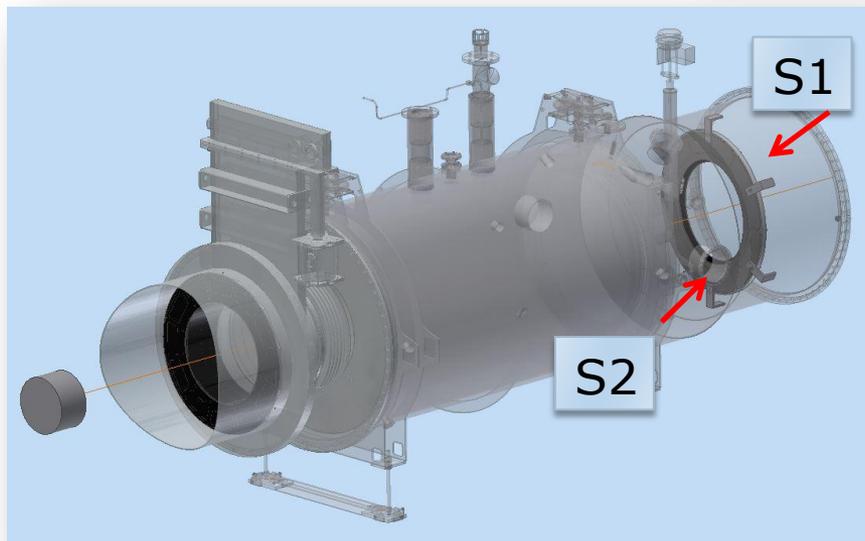
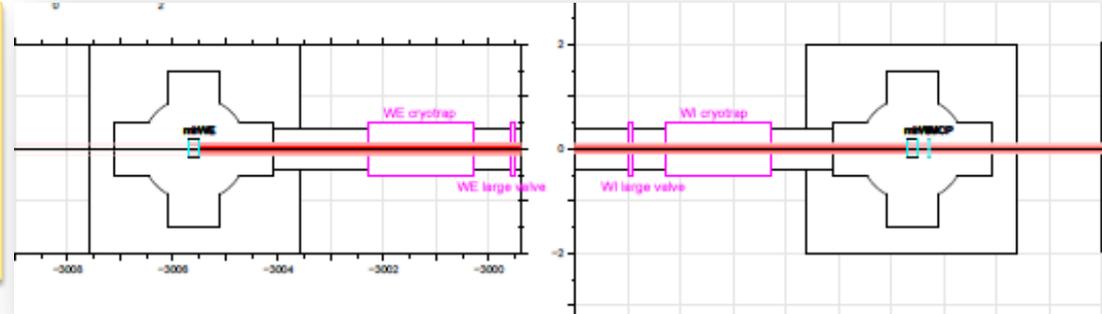
$$h_{baf} = |c| T_{baf}/T_{darm} 1/L X_{baf} < h/10$$

# Stray Light simulations

## □ Example: baffles for arm cryogenic traps

Needed to obscure inner walls of the cryotrap from:

- Farthest test mass (baffle S1)
- Closest test mass (baffle S2)



# Stray Light simulations

□ Design study for baffles in arm cryogenic traps [VIR-0417B-13]:

□ Simulations with:

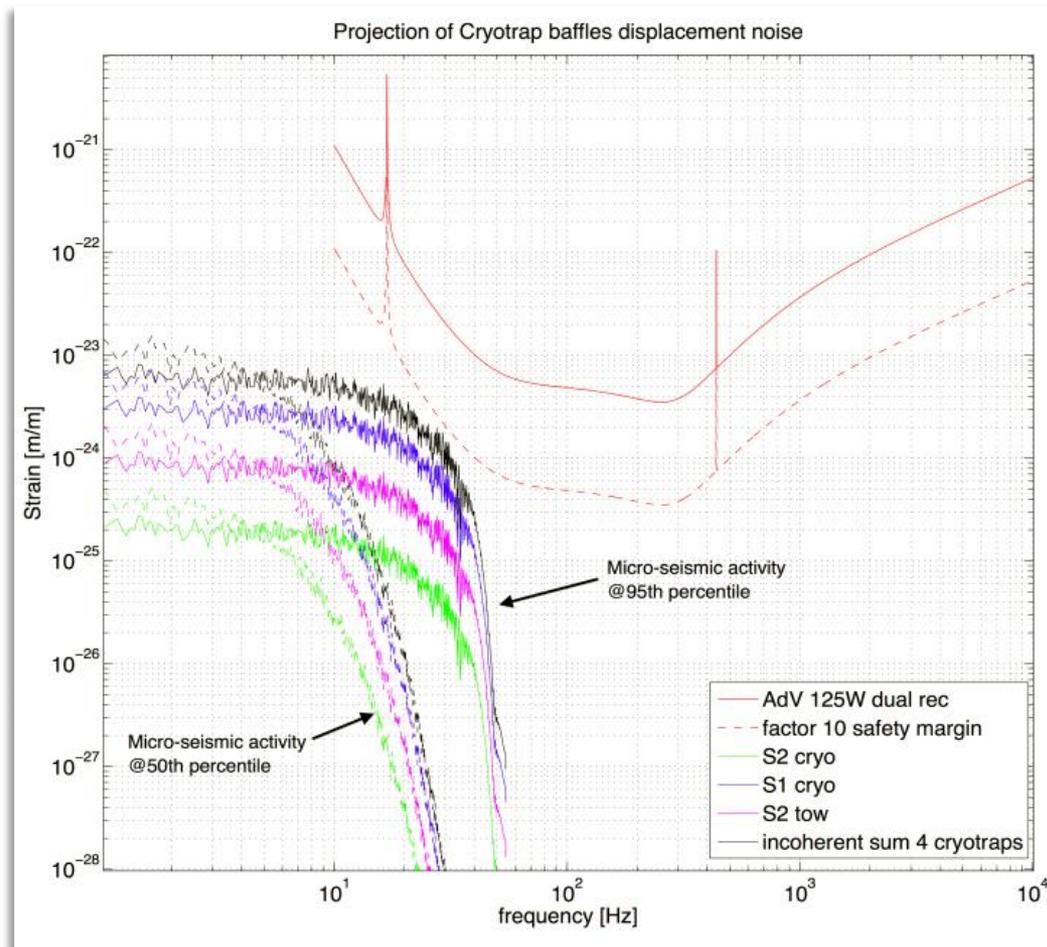
- FFT / BRDF for the coupling,
- Optickle for TFs
- Baffle displacement *caused by micro-seism*

□ Overall expected noise *ok* even for severe seismic conditions

Table 1: BRDFs of baffles for cryotrap

Baffle surface	BRDF [sr <sup>-1</sup> ]	Coupl [W/W]
S2 Baf_Cryo	$3 \times 10^{-2}$	$1.5 \cdot 10^{-27}$
S1 Baf_Cryo	$3 \times 10^{-3}$	$3 \cdot 10^{-25}$
$S_{Cyl}$	$\sim 10^{-2}$	$\sim 10^{-26}$
S2 Baf_Tow	$3 \times 10^{-3}$	$2.6 \cdot 10^{-26}$

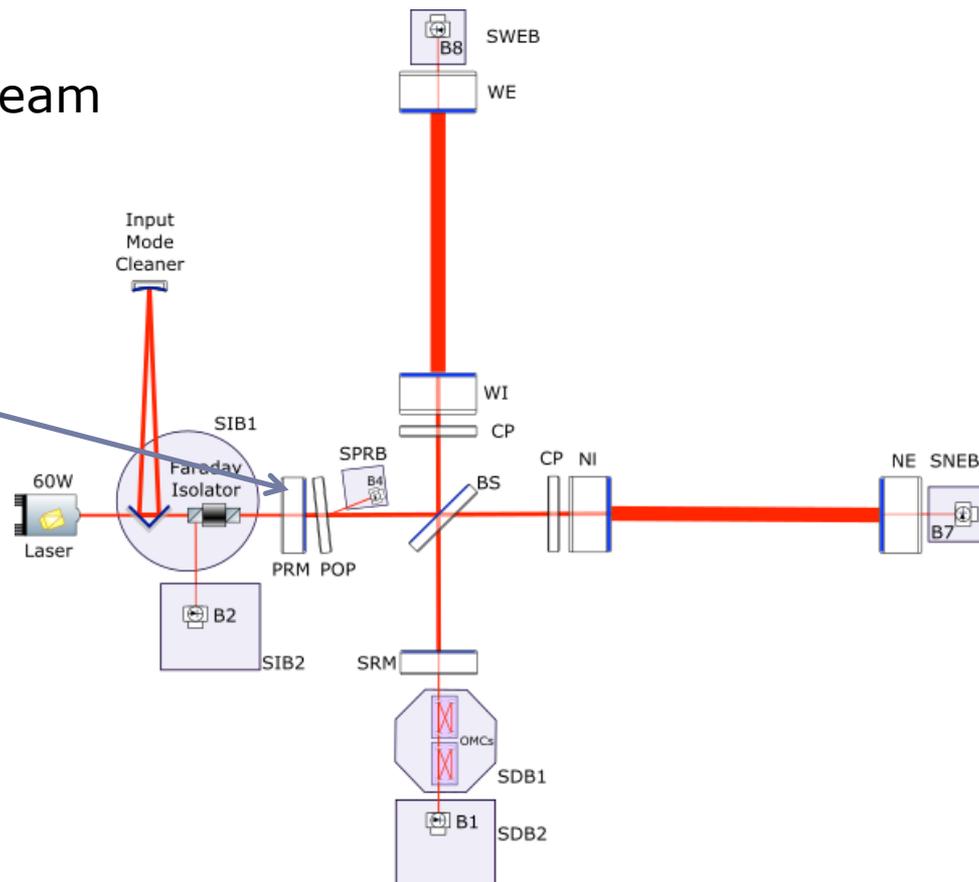
Parameters used for the simulations  
(actual ones *turned out to be better*)



# Stray Light noise measurement

## Case study: the B4 ghost beam

- A pick-off plate (POP) samples the beam circulating in the com branch of the short Michelson
- The pick-off beam is called B4



# Stray Light noise measurement

## Case study: the B4 ghost beam

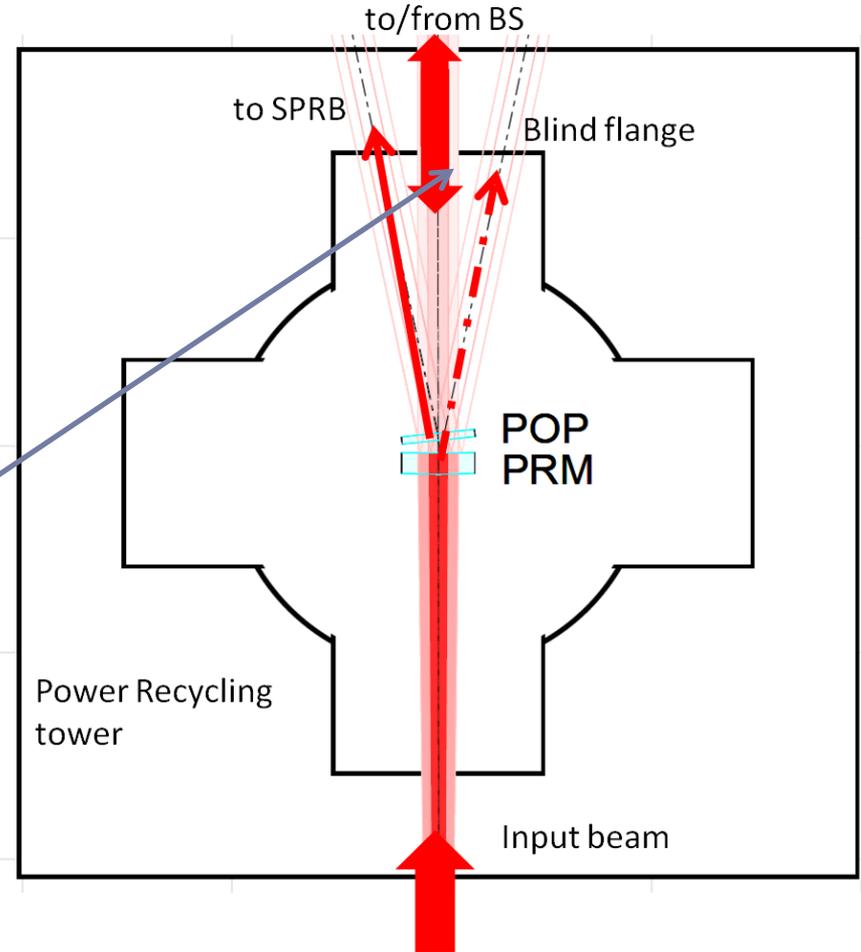
- A pick-off plate (POP) samples the beam circulating in the com branch of the short Michelson

- The pick-off beam is called B4

- B4 is sent to a bench (SPRB)

- the spurious reflection (B4 ghost) goes to a blind flange

- B4 ghost was not properly dumped during O2



# Stray Light noise measurement

## Case study: the B4 ghost beam

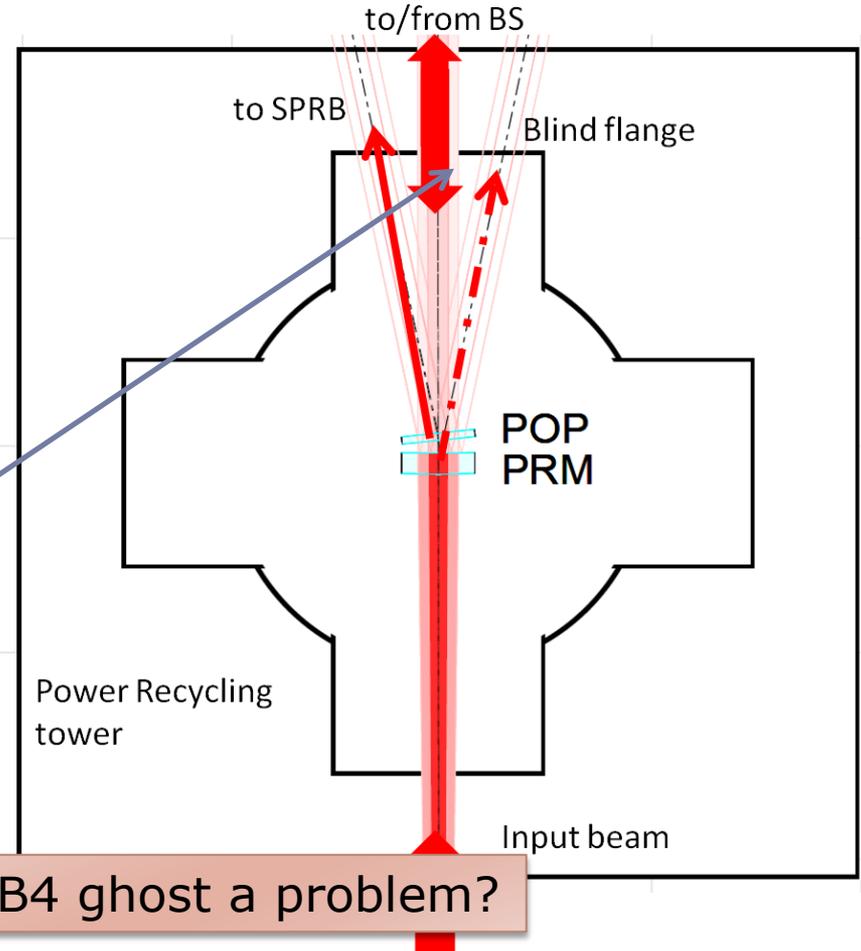
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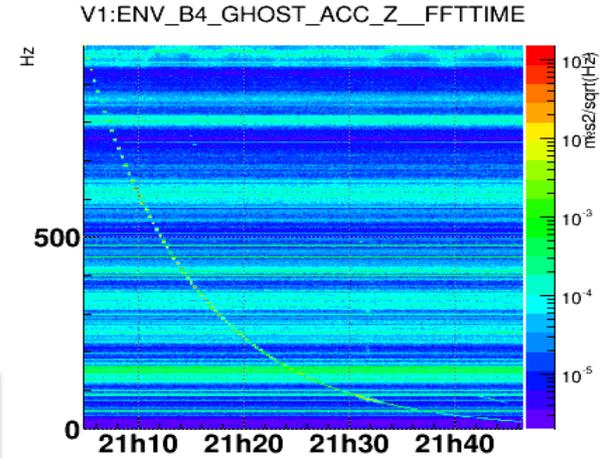


# Stray Light noise measurement

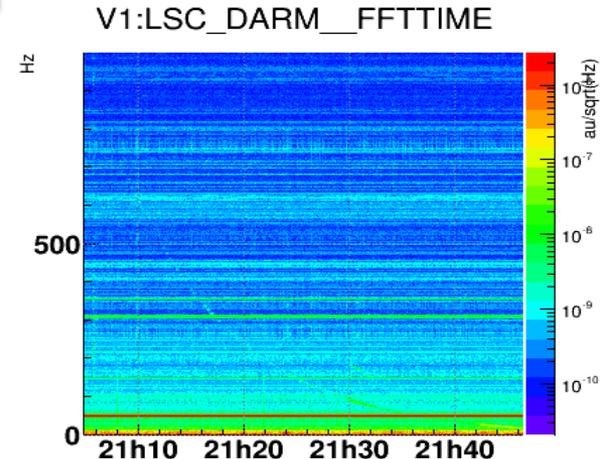
## □ Case study: the B4 ghost beam

To quantify the scattered light we used a shaker, injecting mechanical sinusoidal noise.

The injection is registered by the closest accelerometer, and the effect on the ITF is recorded



1182200709.00 : Jun 22 2017 21:04:51 UTC dt:1.00s nAv:6



1182200709.00 : Jun 22 2017 21:04:51 UTC dt:1.00s nAv:6

# Stray Light noise measurement

## □ Case study: the B4 ghost beam

- Using the estimated transfer functions, the noise due to scattered light is estimated on  $DARM$  and  $H_{rec}$ . The Theoretical value of  $h_{SC}(f)$  is estimated using the accelerometer recording ( $z(t)$ ) during quiet time. It is further multiplied with the transfer function and compared with the  $DARM$  and  $H_{rec}$  during the same quiet period.
- From Fig. 7 it is clear that  $DARM$  and  $H_{rec}$  are limited around 45 Hz, and 92 Hz due to scattered light noise.

From VIR-0730A-17

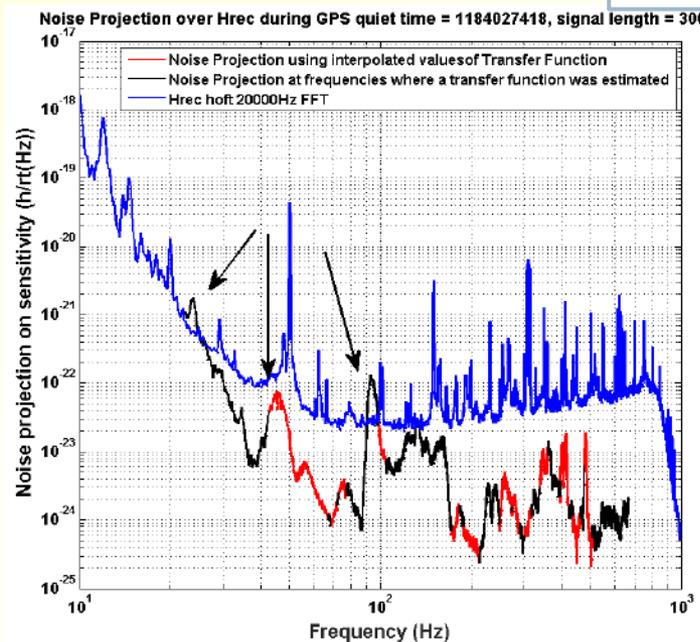
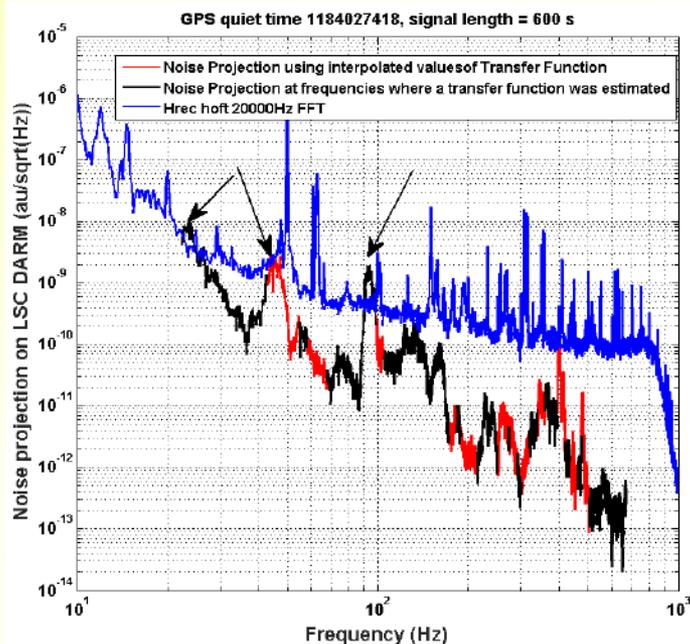
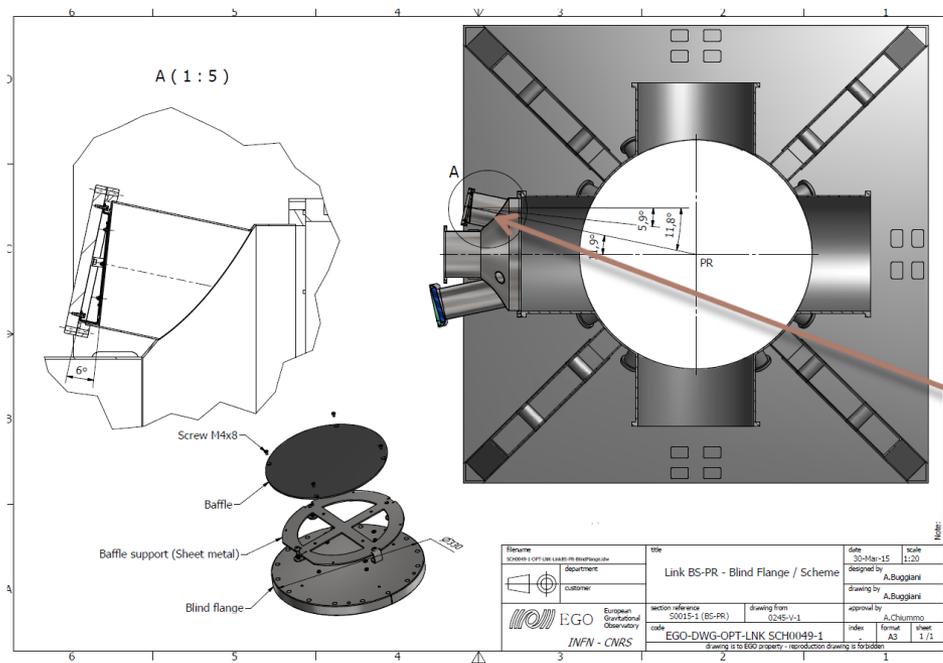


Figure 7. Noise projection on DARM (left), and on Hrec (right). The black part of the projection curve are estimated reliably, whereas the red parts are obtained by interpolating transfer function within those frequency bands.

# Stray Light noise measurement

## Case study: the B4 ghost beam

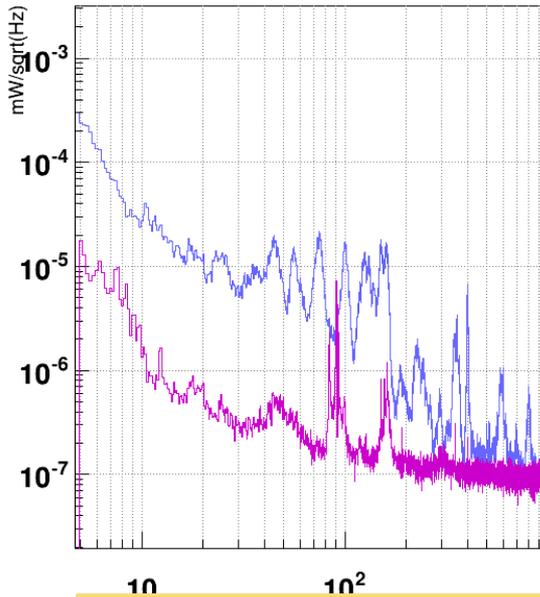


Adding an absorbing baffle solved the issue

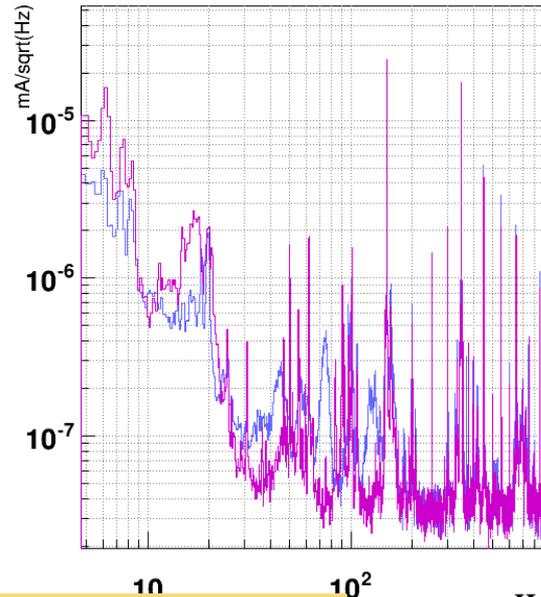
# Stray Light noise measurement

dataDisplay v10r8 : started by chiummo on Oct 24 2017 13:23:00 UTC

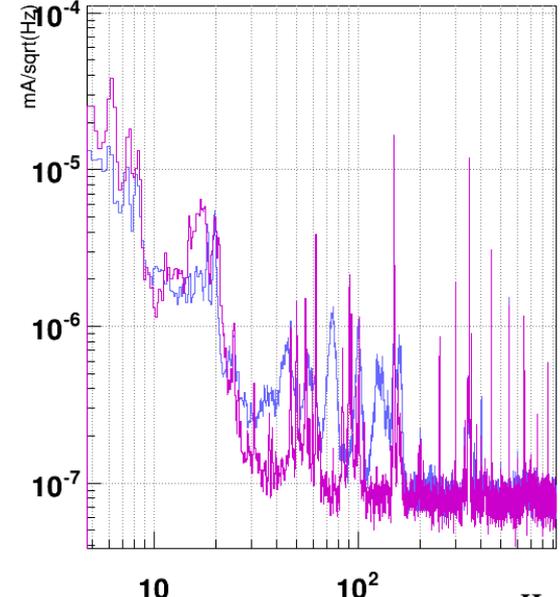
V1:LSC\_B4\_DC\_\_FFT



V1:LSC\_B4\_56MHz\_I\_\_FFT



V1:LSC\_B4\_56MHz\_Q\_\_FFT



The problem was not only the contamination of GW signal, but also spoiling the control signals of ancillary dofs

Adding an absorbing baffle solved the issue

# Materials

❑ Some materials were short-listed for validation:

- Choice based on past generation experience

- Main features tested:
  - Absorption
  - in-vacuum LIDT
  - TIS
  - UHV compatibility
  - ...

- **Cost** was also a key parameter!



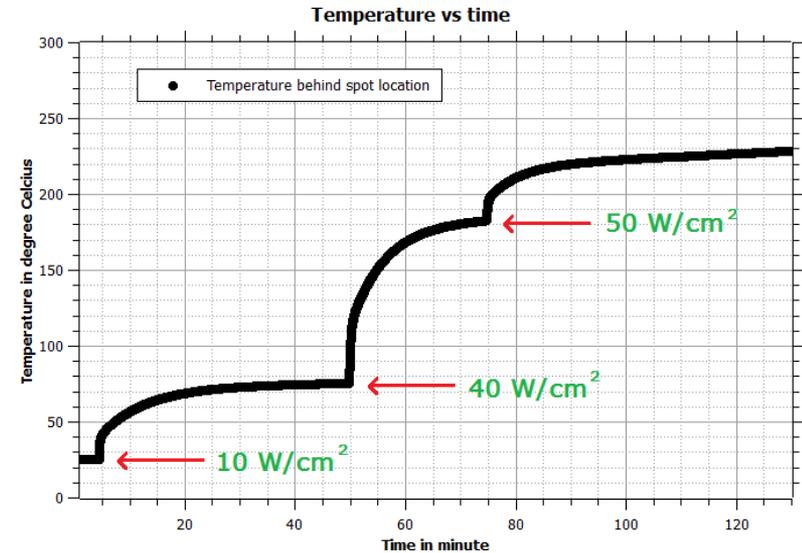
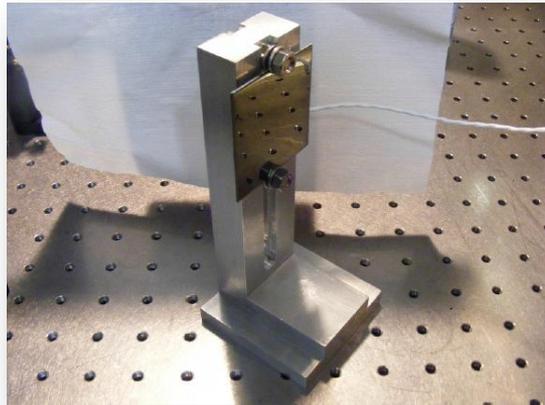
The image shows three overlapping document covers from EGO - VIRGO. Each cover has the EGO logo (European Gravitational Observatory) and the VIRGO logo. The documents are:

- Top document:** "AdV SLC: Characterization of AR coatings on stainless-steel for construction of baffles and beam dumps in AdV". VIR-0482A-14. Authors: V.Bavigadda\*<sup>1</sup>, G.Pillant<sup>1</sup>, A.Magazzu<sup>1</sup>, and A.Chiummo<sup>1</sup>. Date: December 10, 2014.
- Middle document:** "AdV SLC: Characterization of Diamond-Like Coatings for baffles and beam dumps in AdV". VIR-0127A-13. Authors: Antonino Chiummo\*, Benjamin Canuel, Andrea Magazzu, and Julien Marque. Date: April 11, 2013.
- Bottom document:** "AdV SLC: Characterization of Silicon Carbide for constructing baffles and beam dumps in AdV". VIR-0460A-12. Authors: Antonino Chiummo\*, Benjamin Canuel, Andrea Magazzu, and Julien Marque. Date: November 22, 2012.

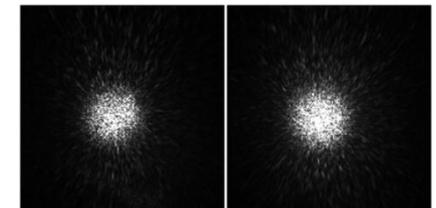
# Materials

❑ Some materials were short-listed for validation:

AR-on-steel  
characterization



Material	LIDT	TIS
SiC + AR	30kW/cm2	~20-50ppm
DLC + AR	500W/cm2	~500-1000ppm
AR-on-steel	> 50W/cm2	~300-500ppm
Absorbing glass	~1W/cm2	~100ppm



2 min

59 min

# Materials

❑ Some materials were short-listed for validation:

Material	LIDT	TIS
SiC + AR	30kW/cm <sup>2</sup>	~20-50ppm
DLC + AR	500W/cm <sup>2</sup>	~500-1000ppm
AR-on-steel	>50W/cm <sup>2</sup>	~300-500ppm
Abs. Glass + AR	~1W/cm <sup>2</sup>	~100ppm



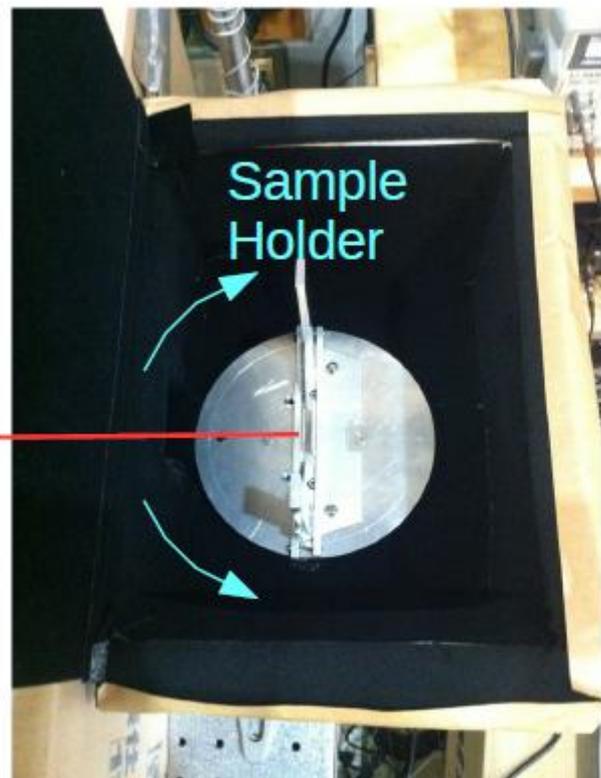
Cost increase

Selection of material driven by:

- location-dependent requirements
- validation of solution
- trade-off with budget needs

# Materials

□ Some materials were short-listed for validation:



## Measured materials:

- **Ti plate** (unpolished)
- **Si plate** (polished)
- **DLC**
- **SiC**
- **“Sol-Black”** (on polished Al)
- **“Specral Black”** (“Acktar”)
- **“Metal Velvet”** (“Acktar”)
- **“Vanta Black”** (“Surrey NanoSystems”)

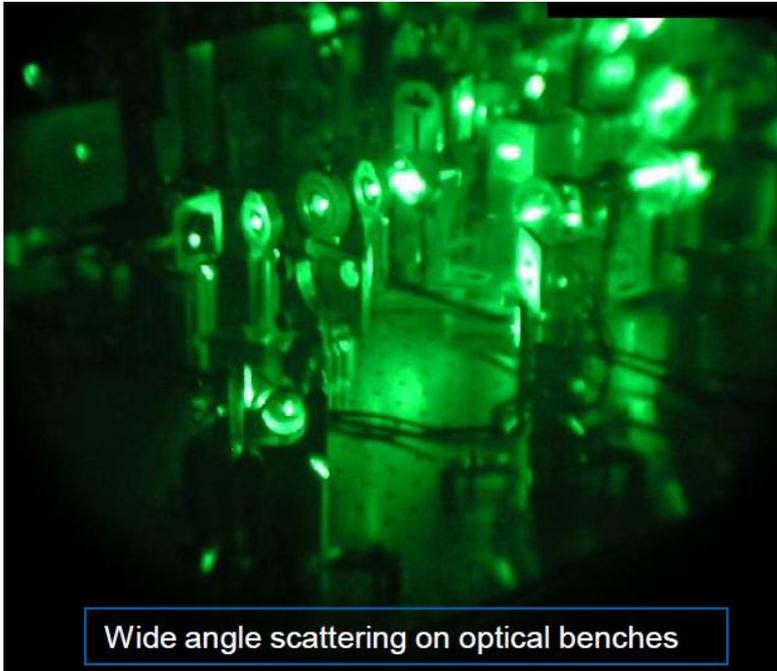
Cost increase

KAGRA colleagues investigated many other materials, some of them were tried up to some extent in Virgo with ambiguous results

From JGW-G1503403-v5

# Stray light noise from benches

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A different class of problem:  
Differently from the scattering off the core mirrors, where a 3-scattering process is needed to recombine with the main beam, here a single-scattering process (backscattering off tilted components) could also play a role.

Very difficult to simulate, and therefore to control by design

Both analytical and monte-carlo approaches employed to simulate the benches, but a full *coherent* simulation of the scattered field is still missing

# Conclusion

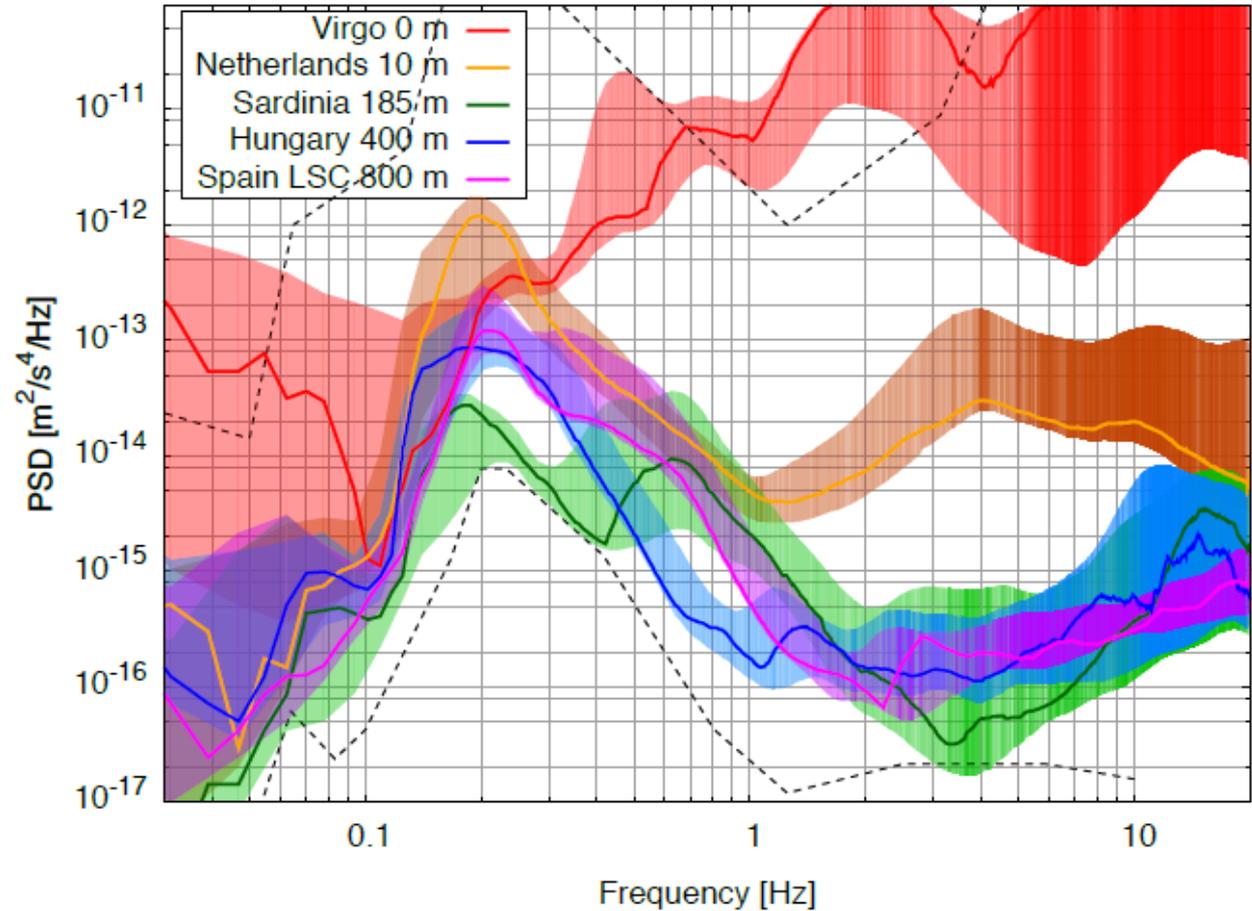
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- ▶ Stray-light is an old enemy of GW interferometric antennas
  - ▶ It comes from a diversity of possible defects
  - ▶ It can probe seismically excited mechanical structures and recombine with the ITF main beam burying GW signals
  - ▶ It is difficult to simulate
  - ▶ It is inherently non-linear
- ▶ Despite huge efforts, it threatens the achievement of design sensitivity
- ▶ Further advances in prediction, mitigation and monitoring are needed
- ▶ New materials with lower BRDF are to be explored for 3rd gen, and possibly chose a site that is...

# Future prospects: what is needed

... A quiet place

Horizontal spectral motion at various sites



Orosei, 3/5/19  
Grazie!  
Antonino

