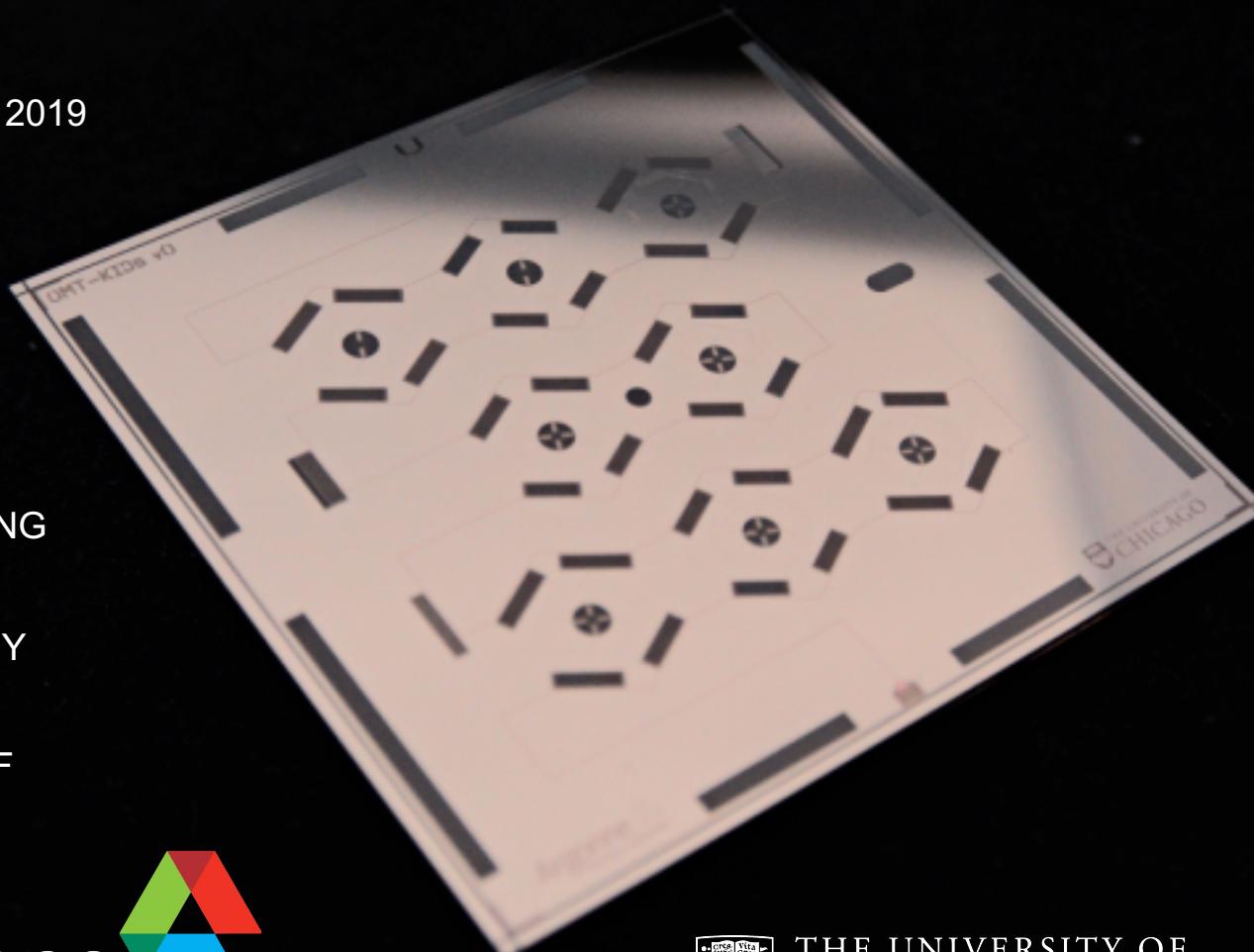


# DESIGN AND OPTIMISATION OF THE MICROSTRIP-COUPLED LUMPED-ELEMENT KID

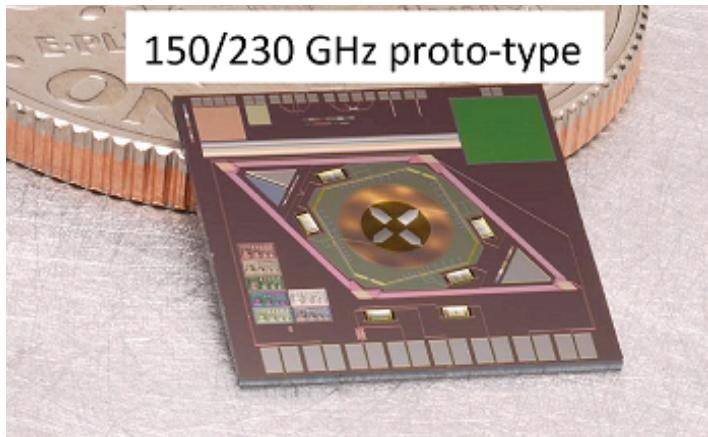
LTD18 – 22<sup>nd</sup> July 2019

PETE BARRY  
TOM CECIL  
CLARENCE CHANG  
SIMON DOYLE  
AMBER HORNSBY  
KIRIT KARKARE  
ERIK SHIROKOFF  
AMY TANG

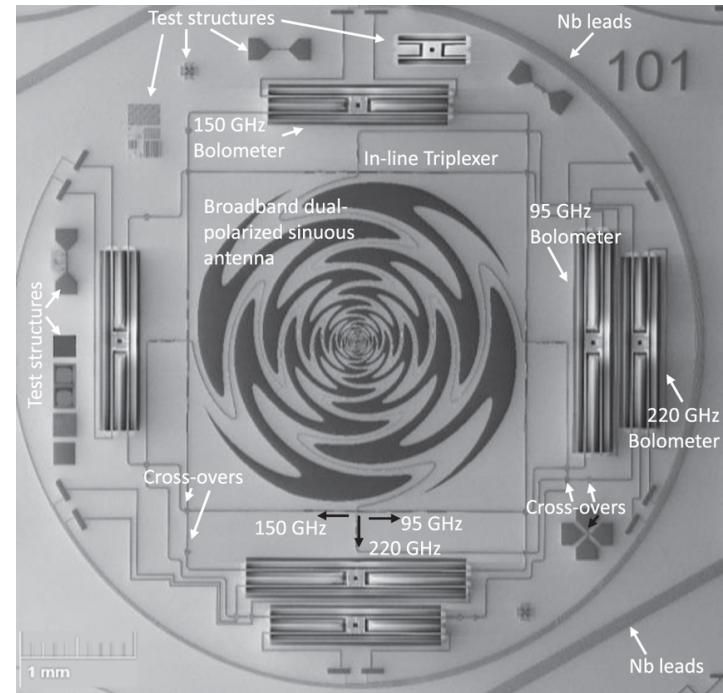


# SOME CONTEXT...

- Motivation: want simple, drop in replacement for TES for multi-chroic detector arrays
- Challenging to readout fully sampled focal planes with TES arrays at high frequency



Adv ACTpol  
(NIST)



SPT-3G (ANL)

BICEP/KECK  
(JPL)

# SOME CONTEXT...

- Motivation: wanted simple, drop in replacement for TES for multi-chroic detector arrays
- Challenging to readout fully sampled focal planes with TES arrays at high frequency
- Example (CMB-S4 DSR RD):**

Bands	Lenses	Field of view	Min. edge taper	Modulation (Pole/Chile)	Detectors / tube	Tubes
30 / 40	2× 55 cm Al	29°	-9.3 dB	scan	576	2
85 / 145	2× 55 cm Al	29°	-6.2 dB	scan / HWP	7048	6
95 / 155	2× 55 cm Al	29°	-8.4 dB	scan / HWP	7048	6
220 / 270	3× 44 cm Si	35°	-13.4 dB	scan / HWP	16876	4
total: 153,232 detectors, 18 tubes						

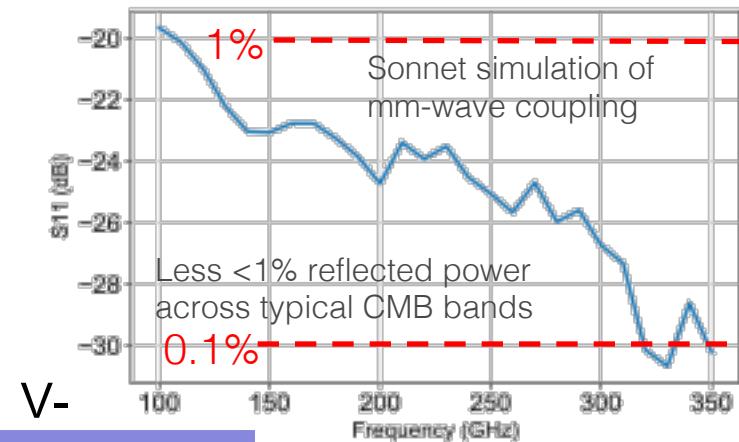
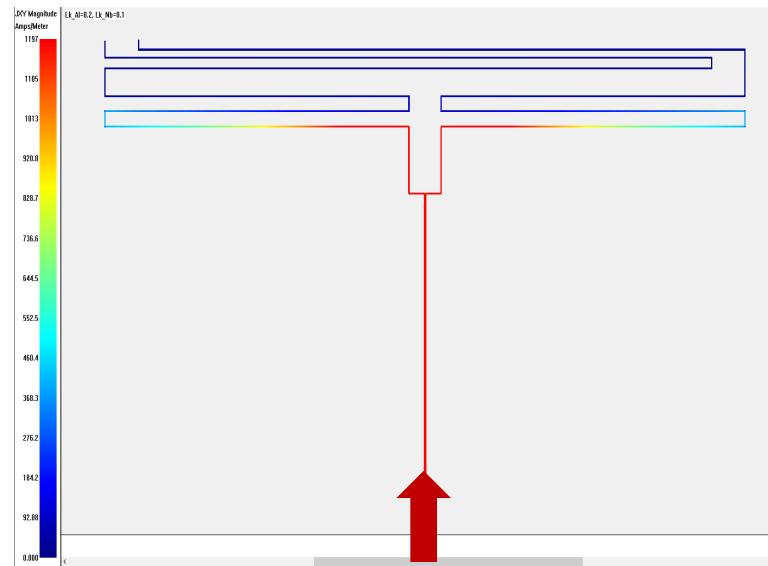
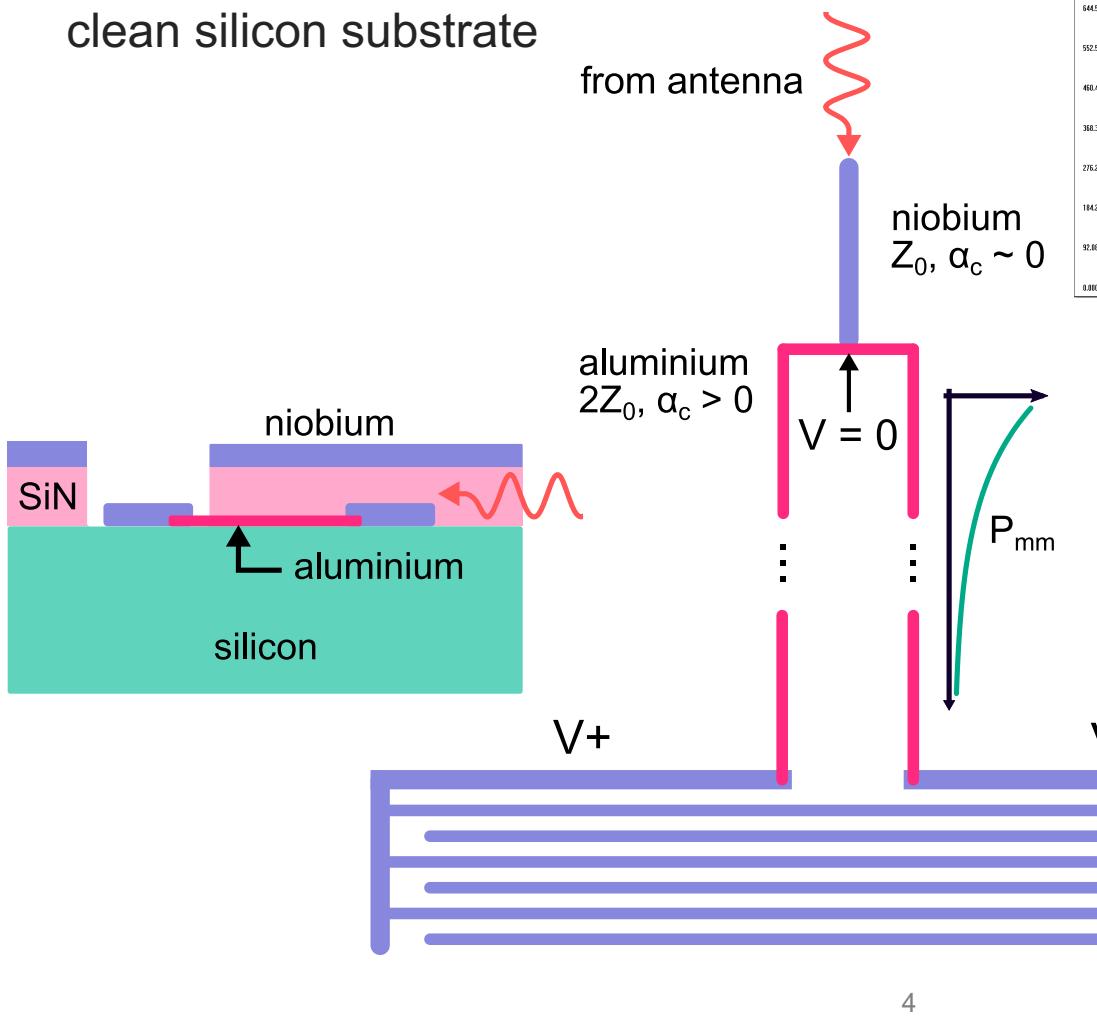
**Table 4-14.** Summary of small-aperture telescopes for the reference design.

- With proposed mc-lekid design → 2 cryostats

**Use additional focal plane space to increase sensitivity at primary CMB bands**

# MICROSTRIP-COUPLED LE-KID

- Simple broadband galvanic mm-wave coupling
- Feed center of le-KID resonator at the virtual ground
- Inverted microstrip allows le-KID fabrication on clean silicon substrate

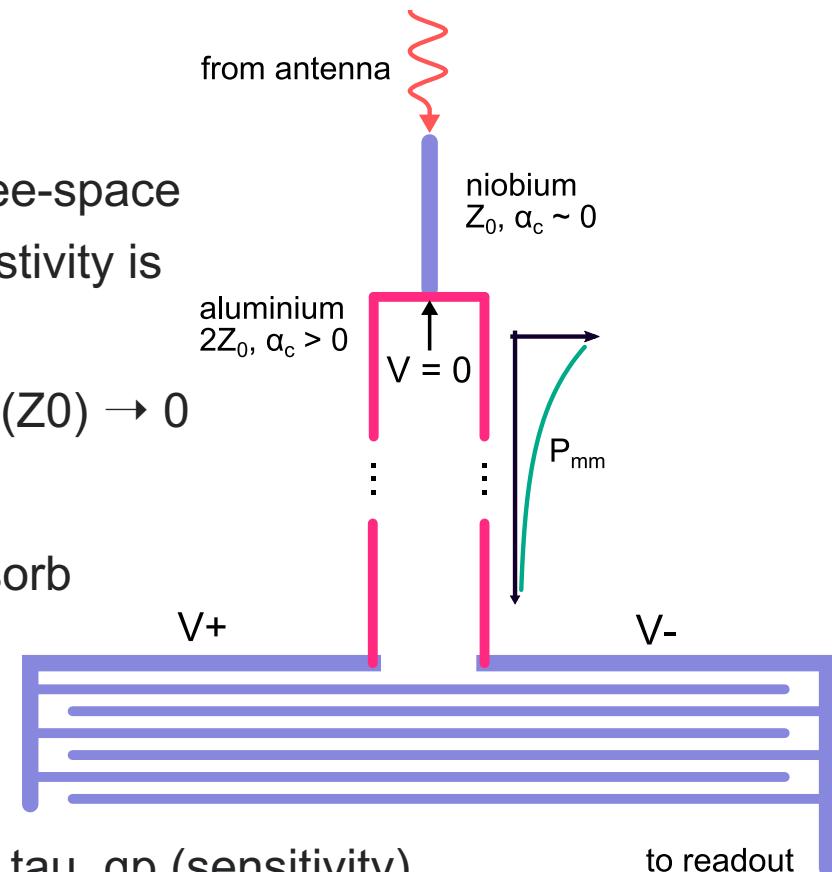


# DETECTOR OPTIMISATION

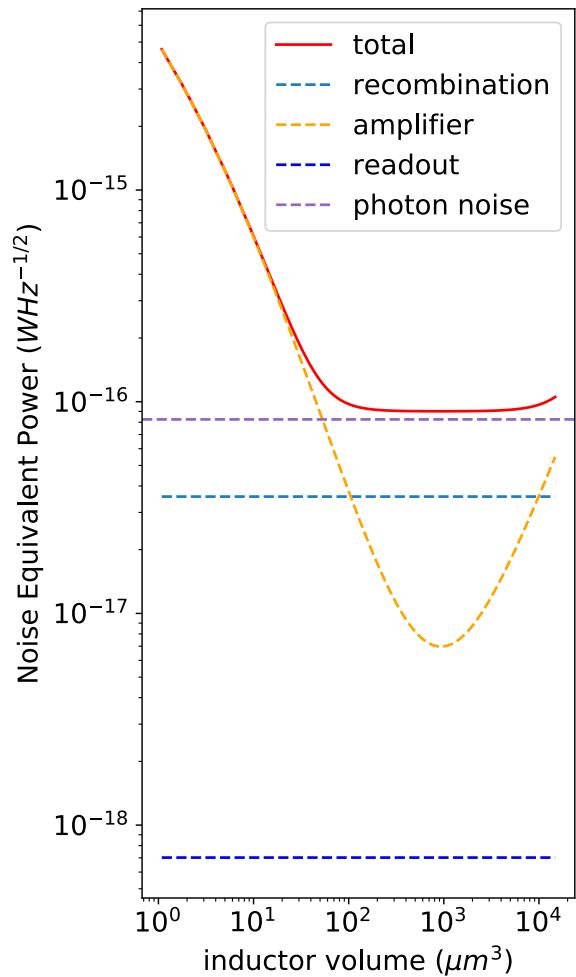
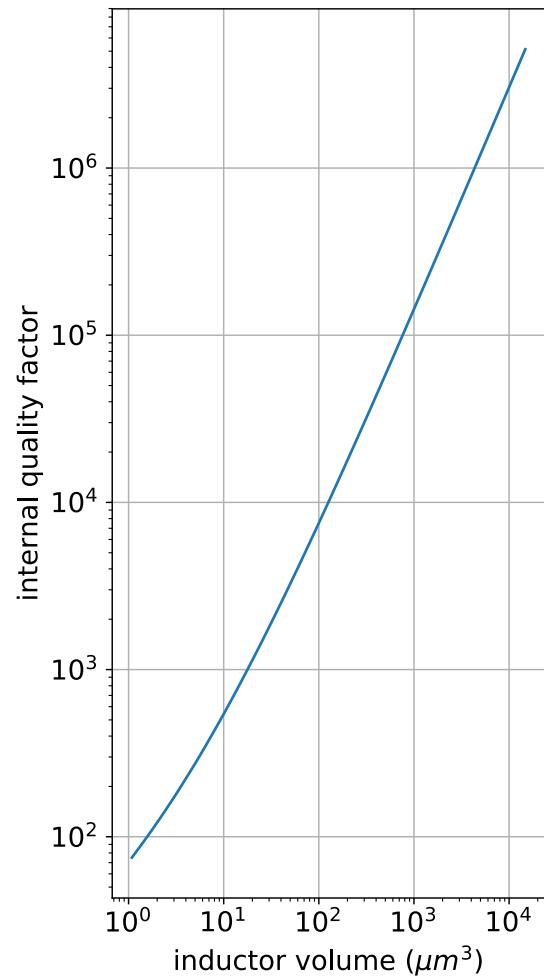
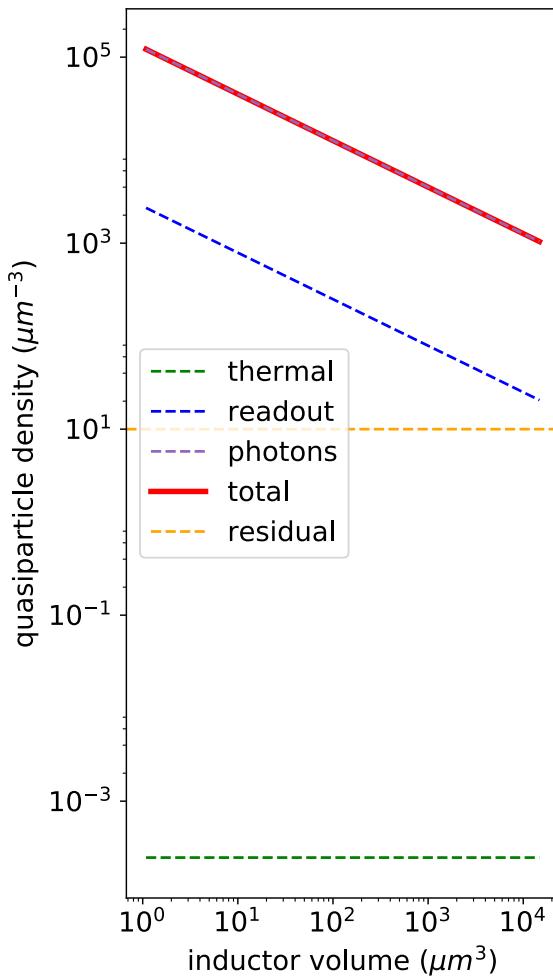
- Unlike traditional direct absorbing le-kid, the constraints on the film resistivity are relaxed
  - Couple to microstrip mode  $Z_0$  instead of free-space
  - From a mm-wave perspective, a lower resistivity is favorable
    - $\text{Al}$  is lossy  $\rightarrow$  as thickness increases,  $\text{Im}(Z_0) \rightarrow 0$   
 $\rightarrow$  better mm-wave match

- Reduction in  $R_s$  requires longer length to absorb mm-wave signal

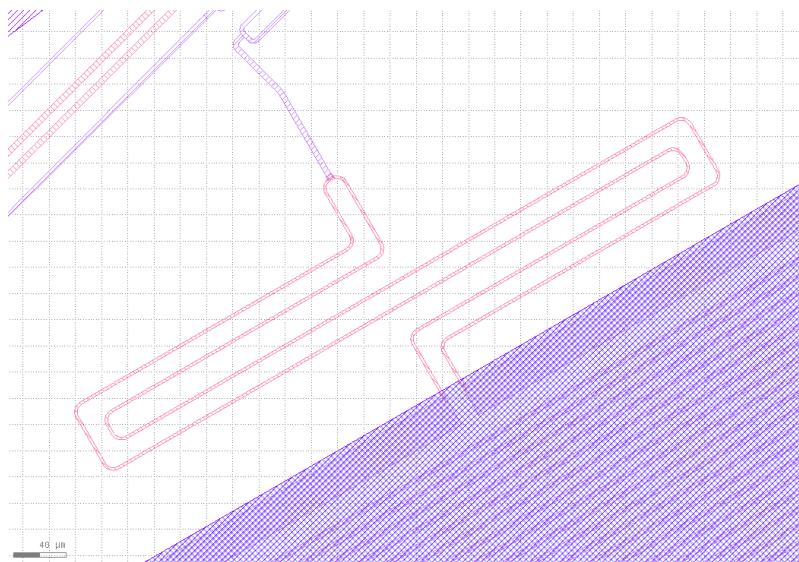
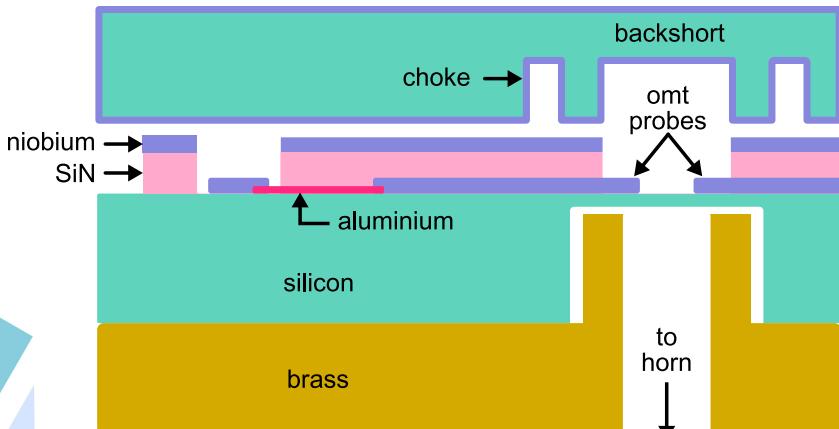
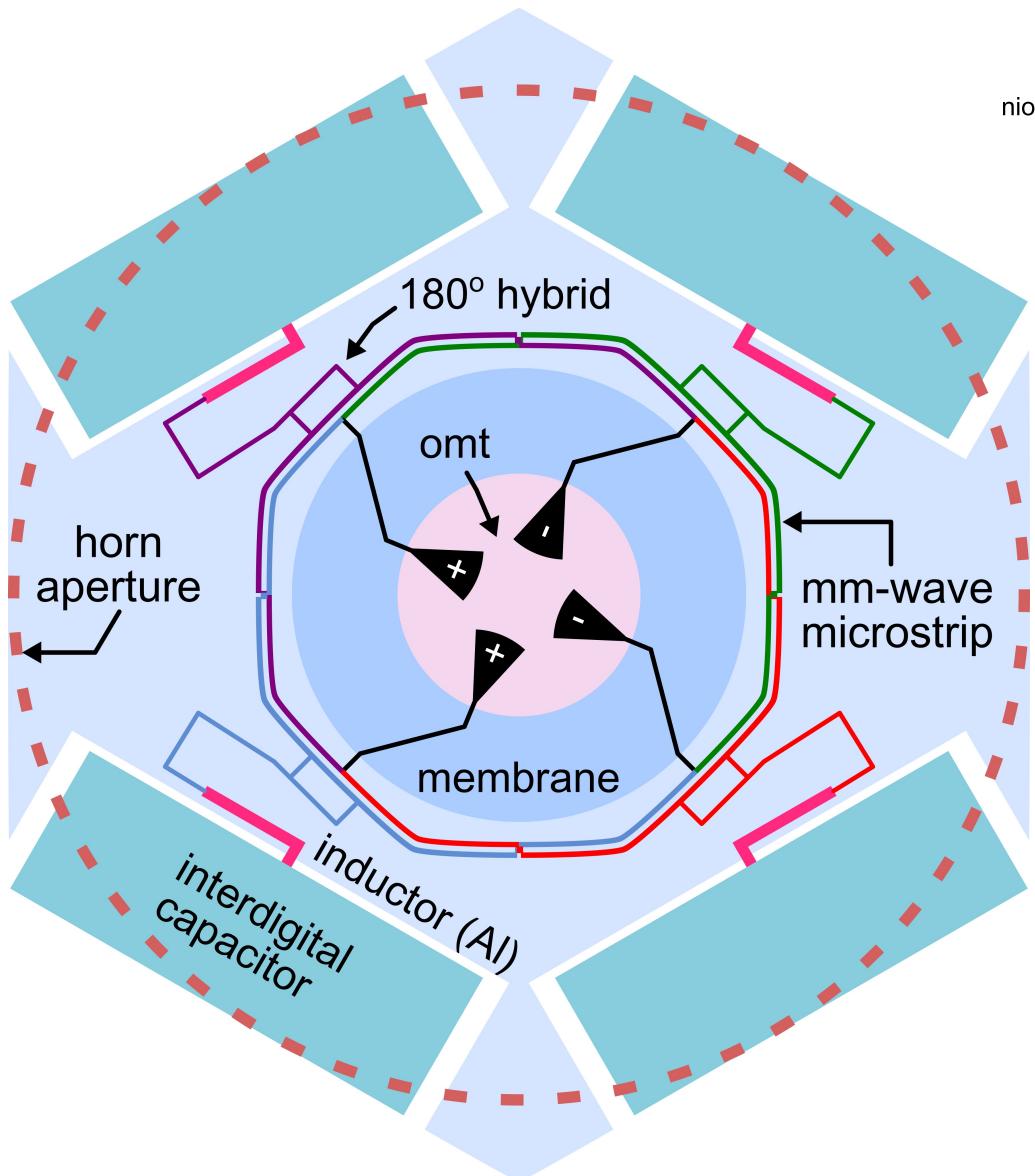
- Resonator frequency increased due to lower  $L_k$ , but reduced for given  $Z_0$
- In addition, increases  $Q_i$  (multiplexing) and  $\tau_{qp}$  (sensitivity)
- $L_k \sim R_s$ 
  - $\alpha_k$  reduces  $\rightarrow$  OK/required for high loading!!
- Take away point:
  - All quantities are interrelated – **require holistic approach to optimization**



# DETECTOR OPTIMISATION - NEPS

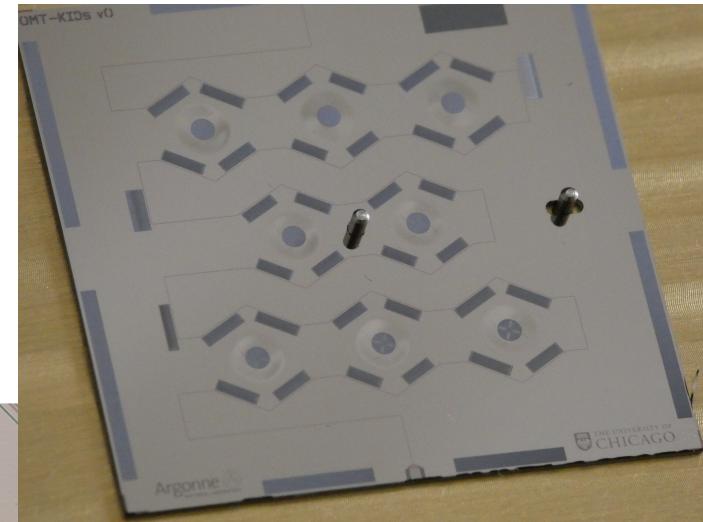
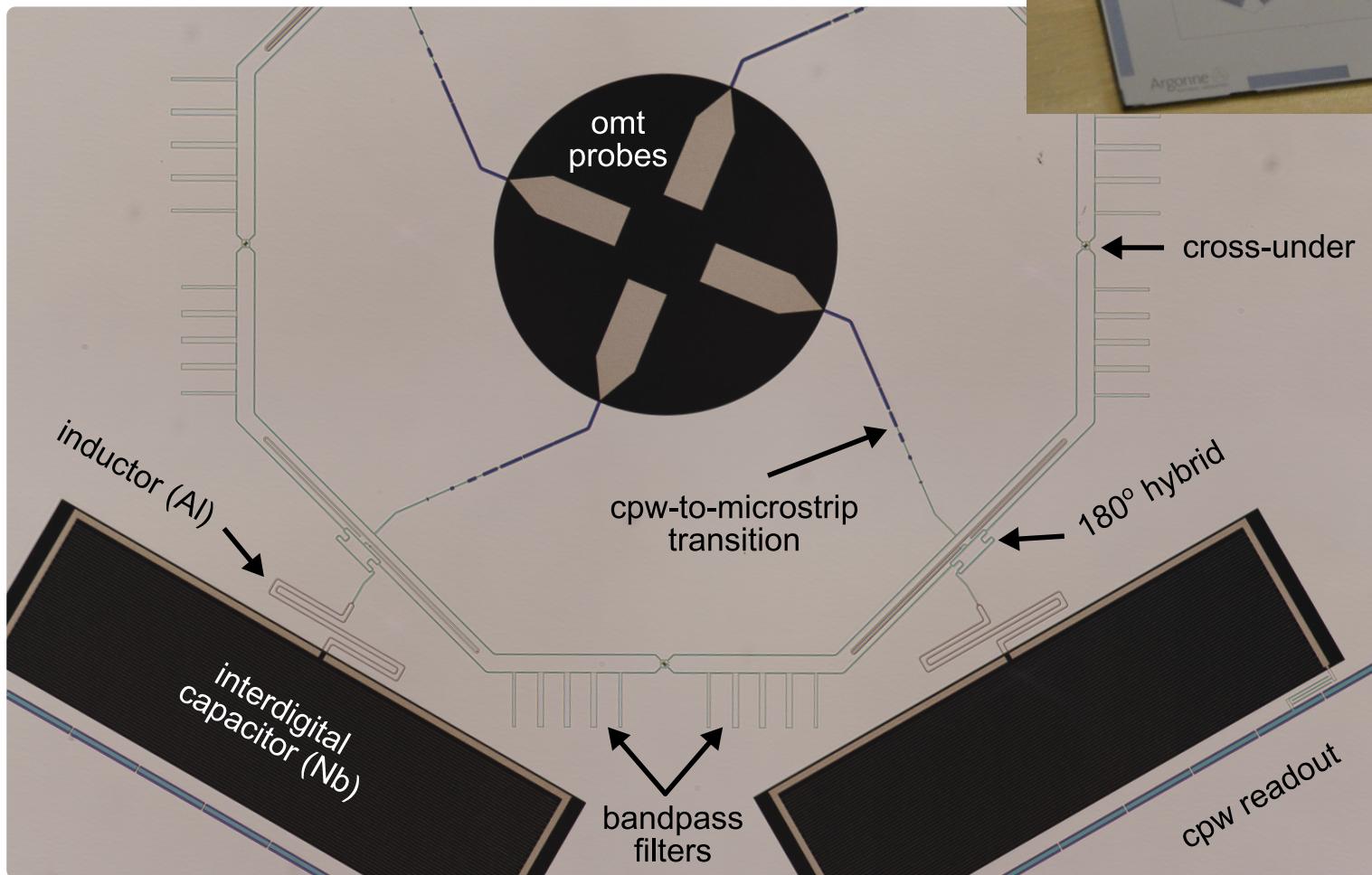


# HORN COUPLED OMT DESIGN



# PROTOTYPE DEVICES

- Fabrication of first released devices now completed ( **see A. Tang poster for all the details...**)
- Optical testing to begin immediately



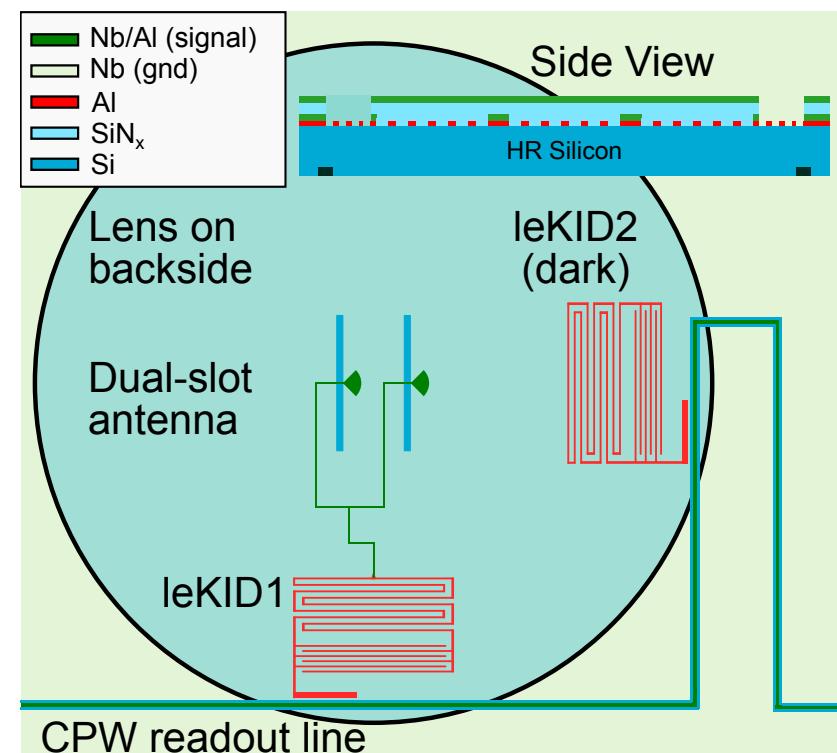
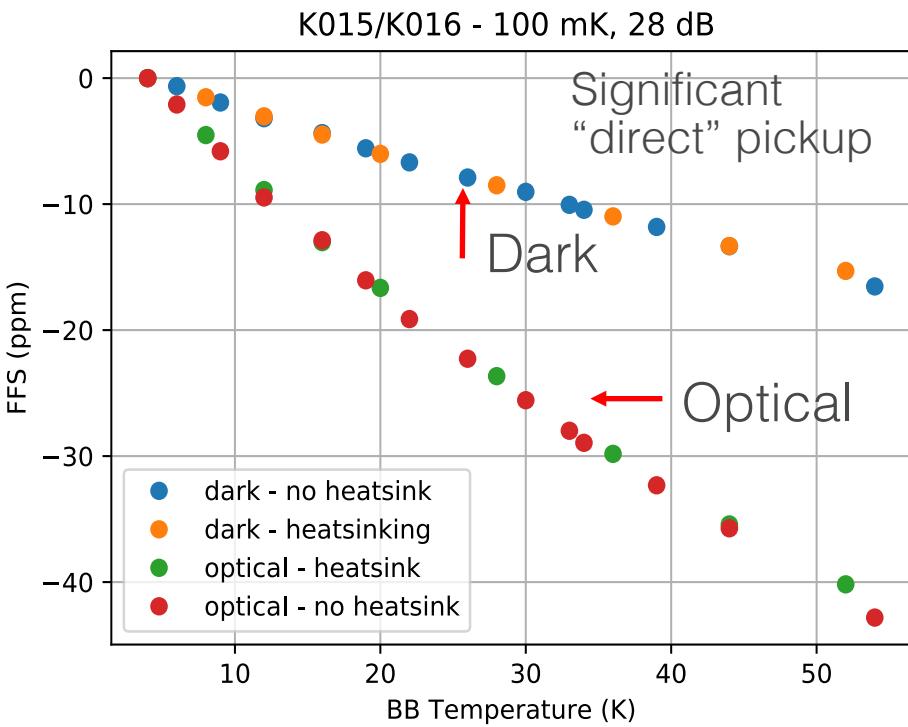
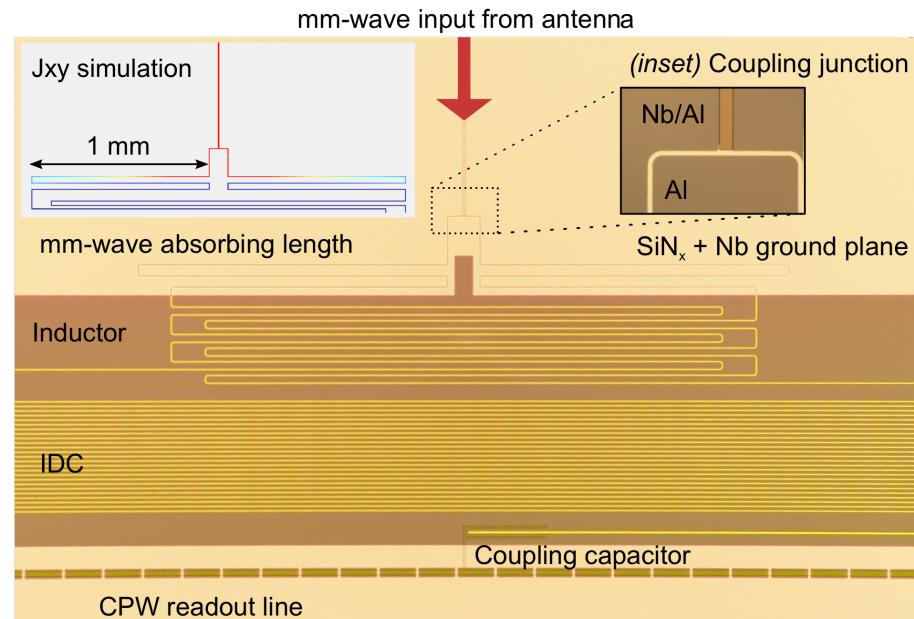
# SUMMARY

- Microstrip-coupled lumped-element KID is a promising path toward drop-in replacement for TES bolometers
  - Particularly motivated at high-frequencies
- Prototype lens-coupled twin-slot antenna devices demonstrated principle works, but highlighted issues
- OMT-coupled design will mitigate this
- First round of fabrication complete
- Full optical testing to begin soon

# EXTRA SLIDES

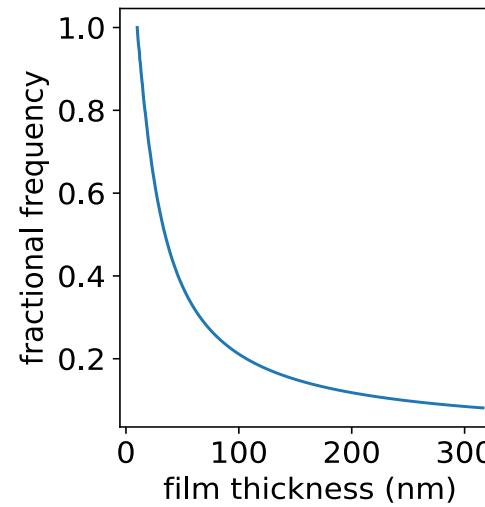
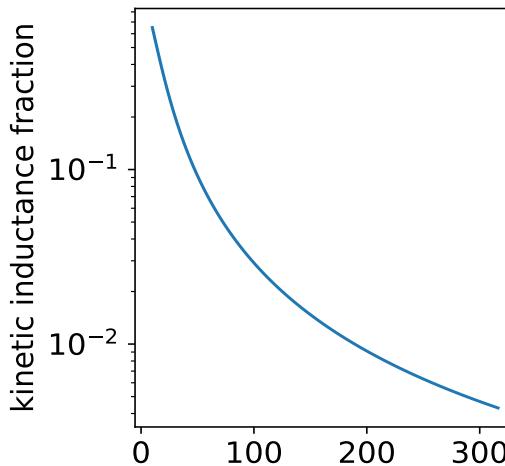
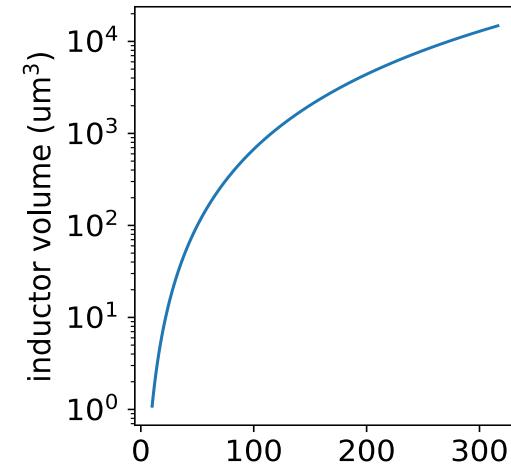
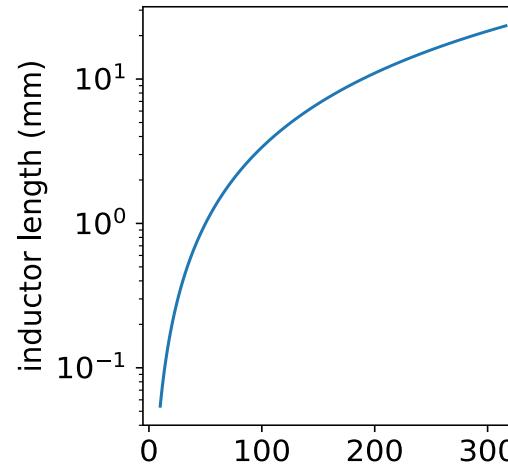
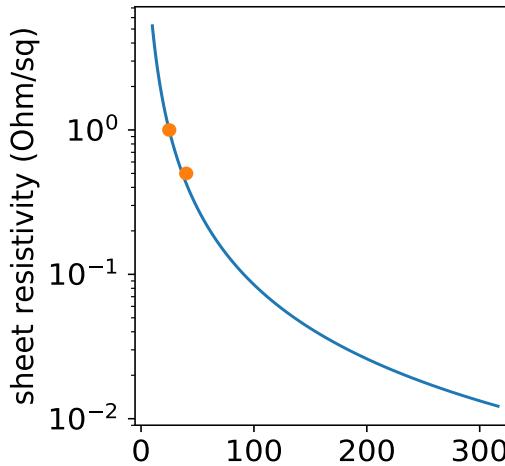
# PROTOTYPE RESULTS

- Demonstrated that optical coupling scheme works!
- But, identified that stray/direct pickup is an issue



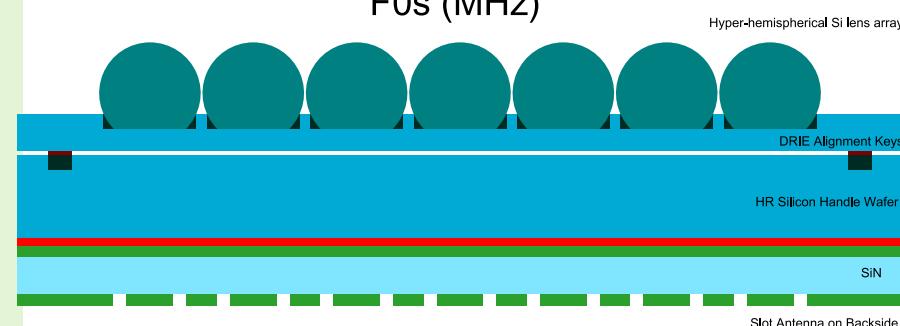
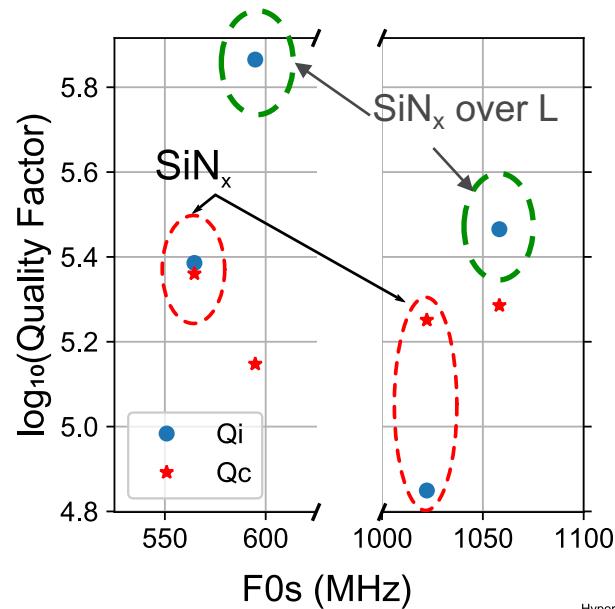
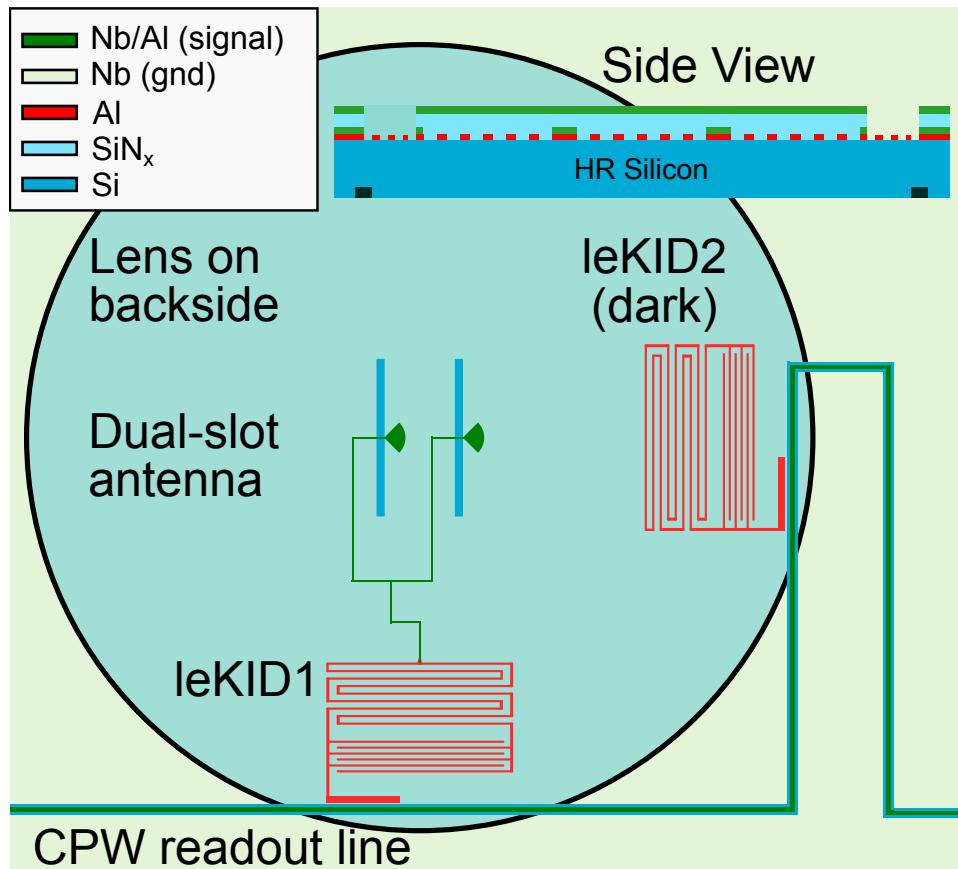
# DETECTOR OPTIMISATION – PARAMETERS

- Simulation calculates  $n_{qp}$  ( $P_{opt}$ ,  $P_r$ ,  $T_b$ ...etc)
  - Constrain problem by requiring inductor length is sufficient enough to absorb < 20 dB



# LENS-COUPLED DEVICES

- Simple prototype devices to test concept
- Demonstrated that dielectric over inductor has minimal effect on resonator loss



# EXTRA SLIDES

Array of wire bond pads for the PolarBear2 detector array with a wire bond head. Pads are 90 micron wide with 10 micron gap between pads

