

R&D Progress of CEPC Detector Magnet

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outline

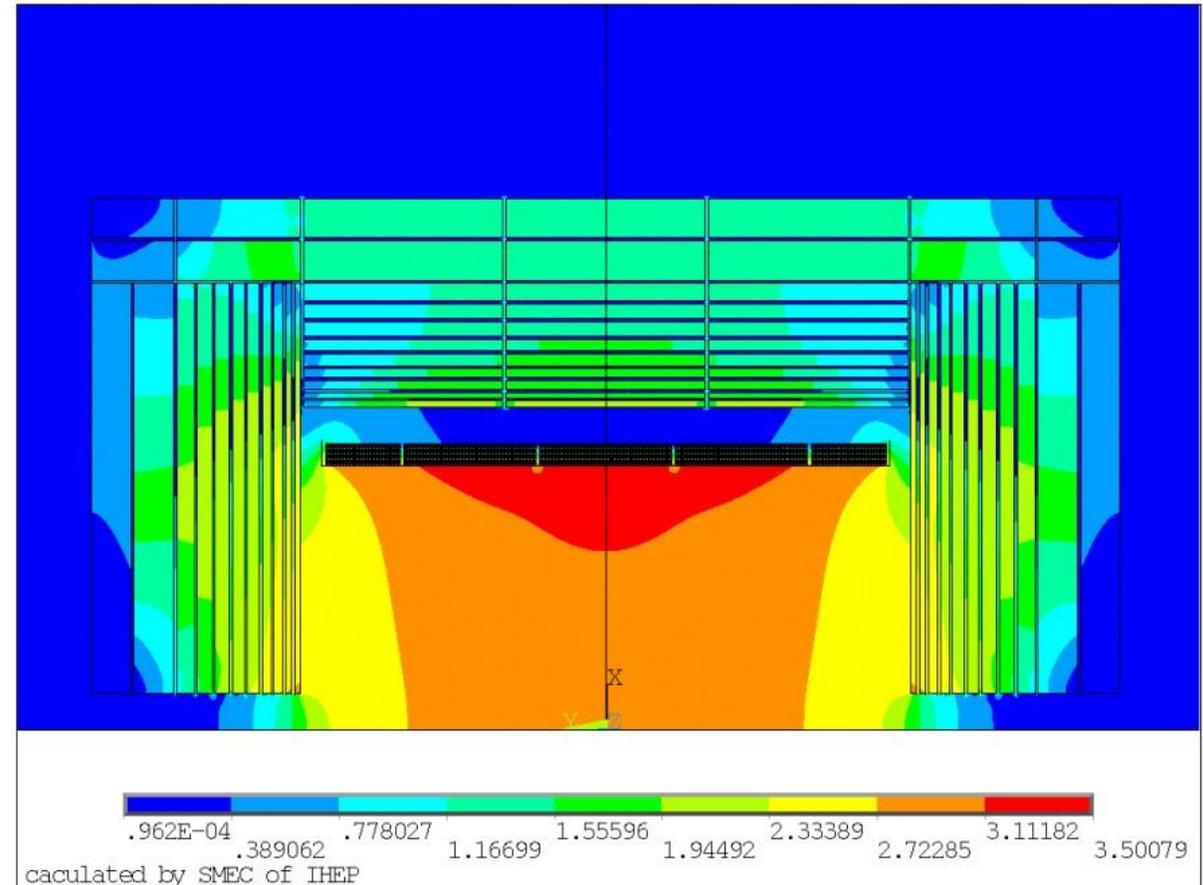
- **Main parameters**
- **R&D progress**
- **Future plan**

The Magnetic Field Requirements and Design

main parameters of the solenoid coil

The central magnetic field: From 3.5T to 3T

| | | | |
|--------------------------------|-----|---|------|
| The solenoid central field (T) | 3 | Working current (kA) | 15.8 |
| Maximum field on conductor (T) | 3.5 | Total ampere-turns of the solenoid (MA _t) | 20.3 |
| Coil inner radius (m) | 3.6 | Inductance (H) | 10.5 |
| Coil outer radius (m) | 3.9 | Stored energy (GJ) | 1.3 |
| Coil length (m) | 7.6 | Cable length (km) | 30.4 |

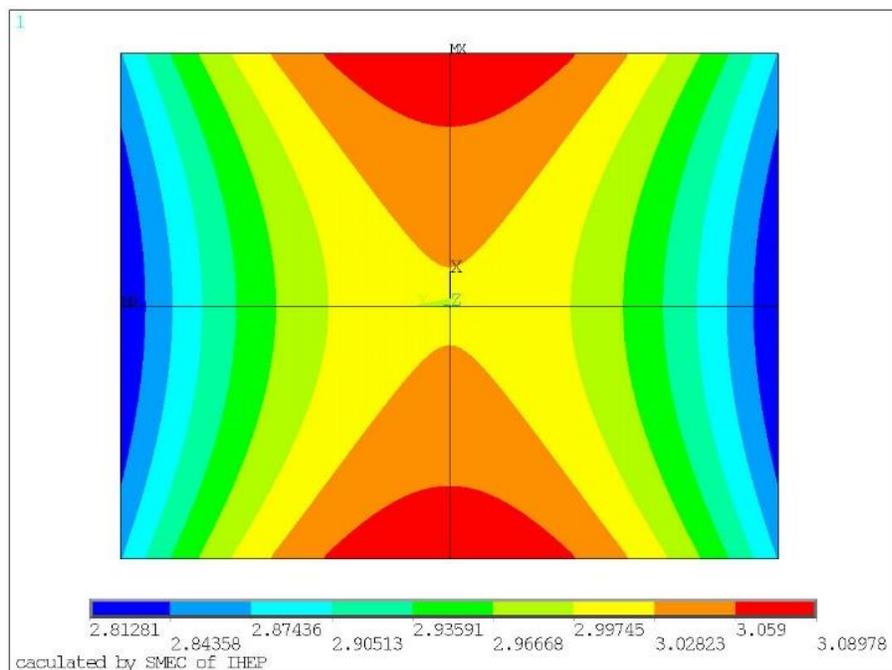


Field map of the magnet (T)

The Magnetic Field Requirements and Design

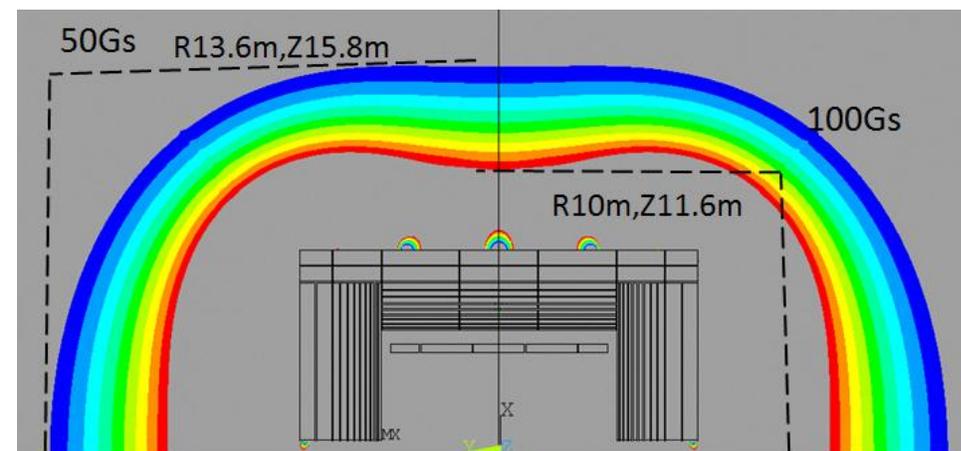
The non-uniformity of Tracking Volume (diameter 3.62m, length 4.7m) is 9.1%.

$$B_p = \frac{B_{max} - B_{min}}{B_{center}} = 9.1\%$$



magnetic field distribution within the Tracking Volume

| Stray field | | |
|-------------|-------------|--------|
| 50 Gs | R direction | 13.6 m |
| | Z direction | 15.8 m |
| 100 Gs | R direction | 10 m |
| | Z direction | 11.6 m |



Stray field distribution outside the magnet(the field is given in T)



R&D Progress related to detector magnet at IHEP

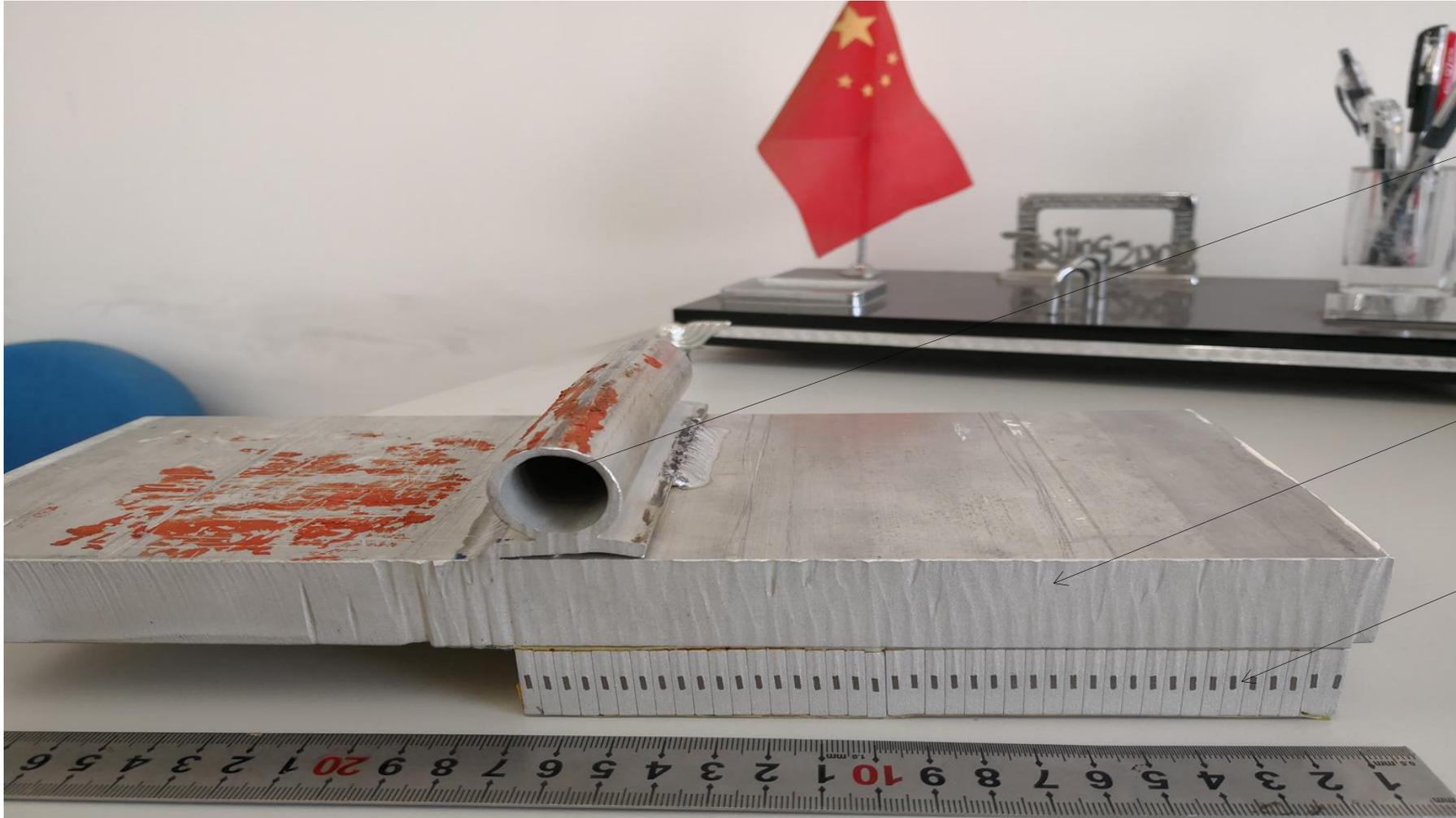
Requirements of CEPC detector:

a larger size and higher field magnet

- Strong Solenoid
 - Better Momentum resolution for energetic tracks
 - Better separations
- Baseline Value: 3 Tesla, 7m bore diameter
- Technology well existed by CMS magnet(4T/7m), motivation is to reduce the cost

This R&D work is supported by Innovation Fund of IHEP for CEPC

Starting point: BESIII Magnet



Pipe for
Liquid He at 4.2 K

Aluminum
Mechanic support

Nb-Ti Superconductor
(Rutherford Cable)
Embed in pure Aluminum
Structure

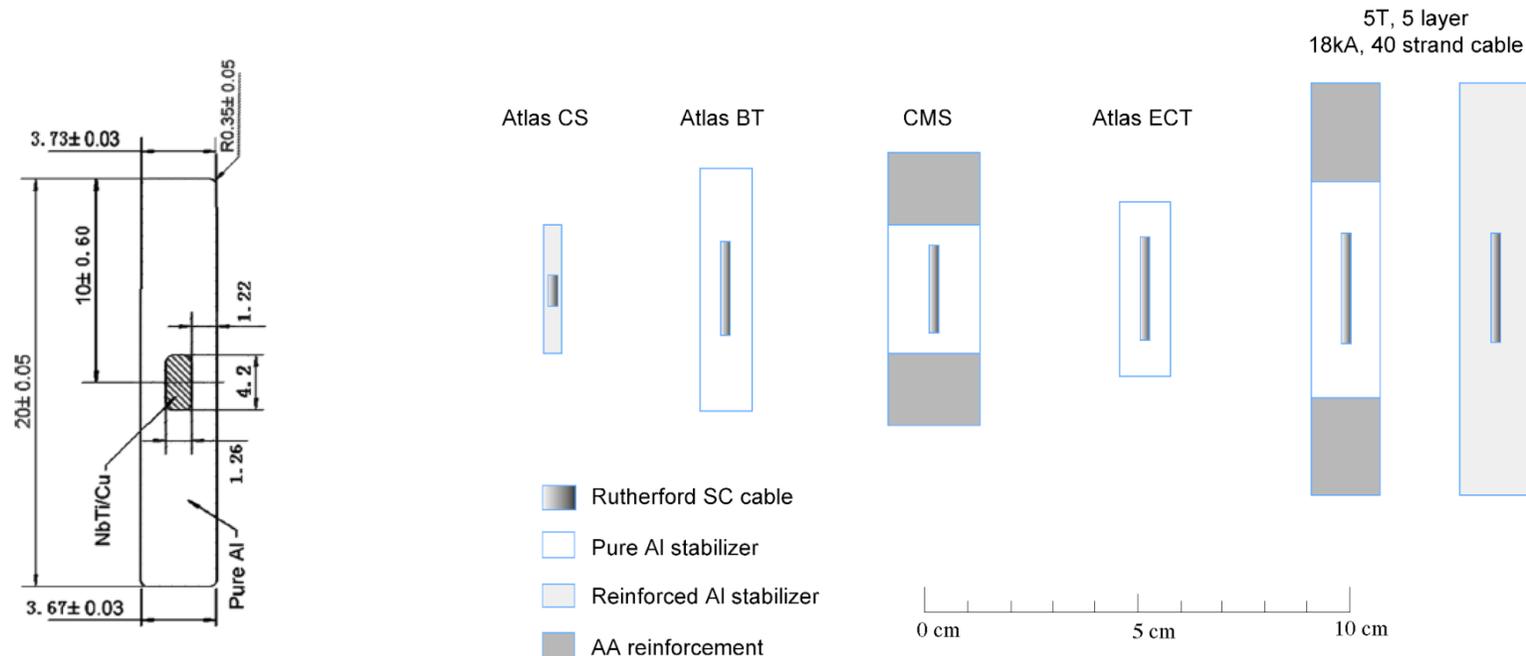
1 T, length 4 m
Bore diameter 2.7 m

Cutting slice from the BESIII magnet prototype

Special Cable

- Development progress of Al-based superconductor

Al-based Superconducting conductor was mainly used for large detector magnets, such as ATLAS and CMS, ..., FCC detector. We had the experience of using in BEPCII-BESIII detector.



Cross sections of Al stabilized and reinforced conductors previously used and will be used

Rutherford cable



- Cooperation with Toly Electric Ltd. since 2015
- Development of Rutherford cable in the first step by using old machine
- New cabling machine and tension control system of strands were put into use in 2016 to improve quality



Rutherford cable



Number of strands: 20
 Strand diameter: 1.0mm
 Materiel: Copper
 Complete time: 2015.5

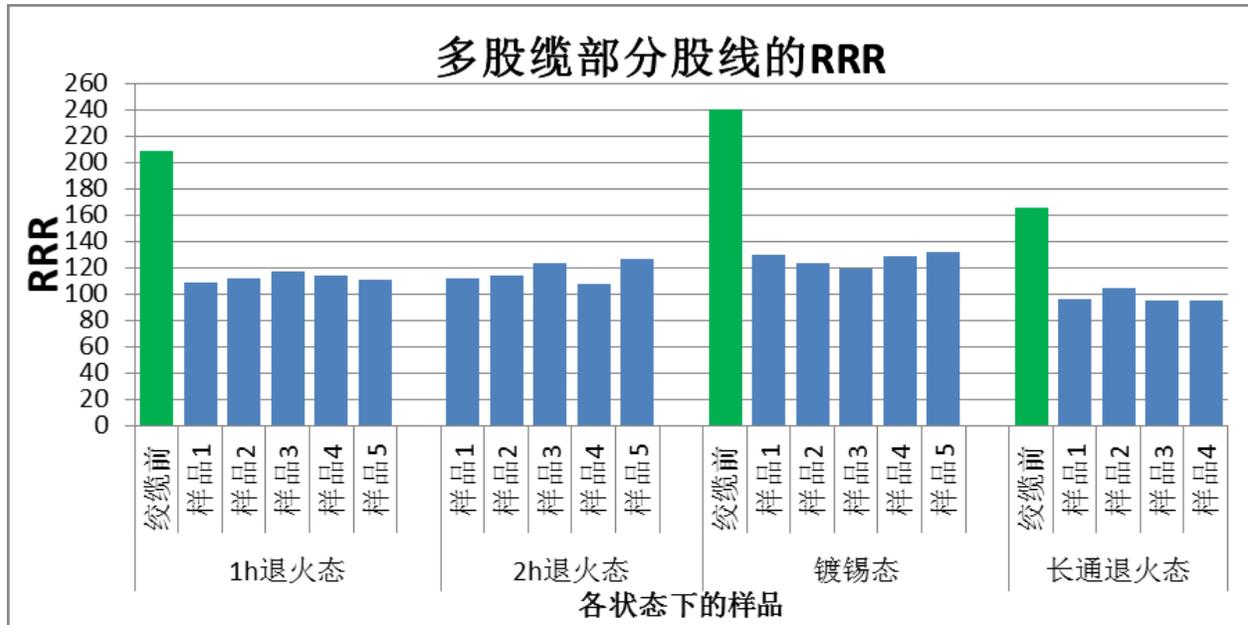
Number of strands : 17
 Strand diameter : 0.727mm
 Materiel: Nb/Ti
 Complete time: 2015.7

Number of strands : 24
 Strand diameter : 0.727mm
 Materiel: Nb/Ti
 Complete time: 2015.8

Number of strands : 18
 Strand diameter : 1.2mm
 Materiel: Nb/Ti
 Complete time: 2016.2

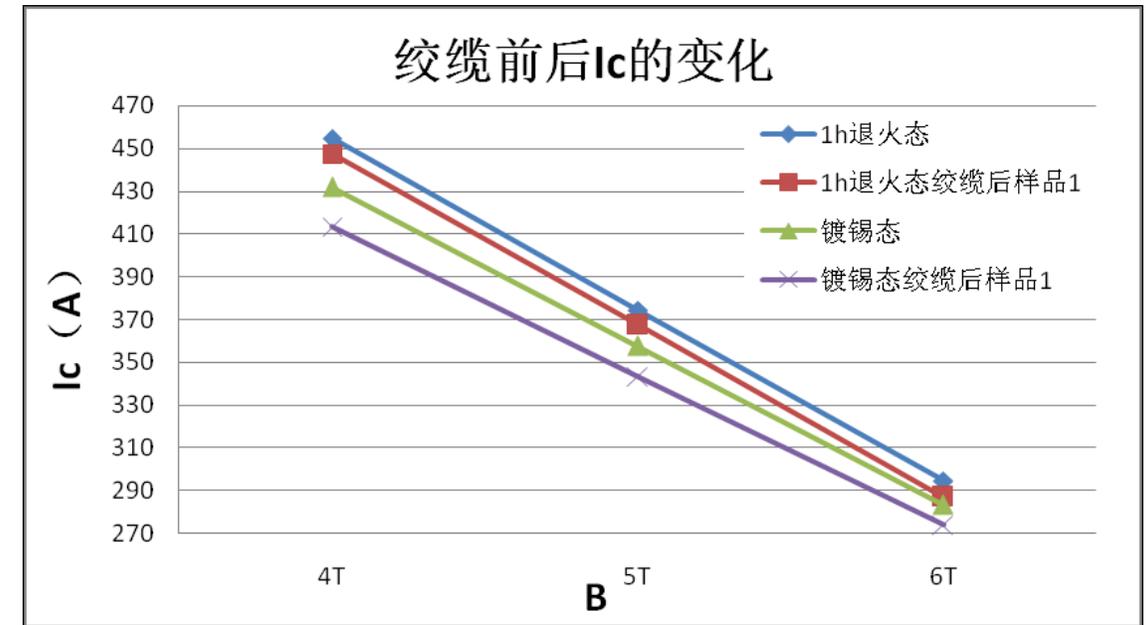
Number of strands : 32
 Strand diameter : 1.2mm
 Materiel: Nb/Ti
 Tangle: 17.32
 Length: » 100m
 RRR: » 100
 Complete time: 2016.5

Strand of Rutherford cable test results



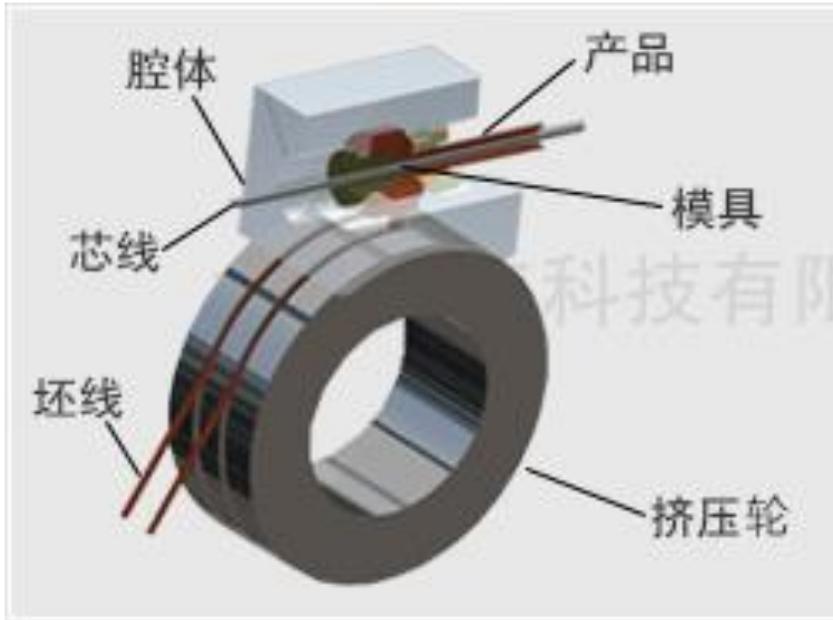
Test by WTS

1. RRR value declined by about 1/3 after the stranding process
2. Less affected by larger twist pitch of strands.

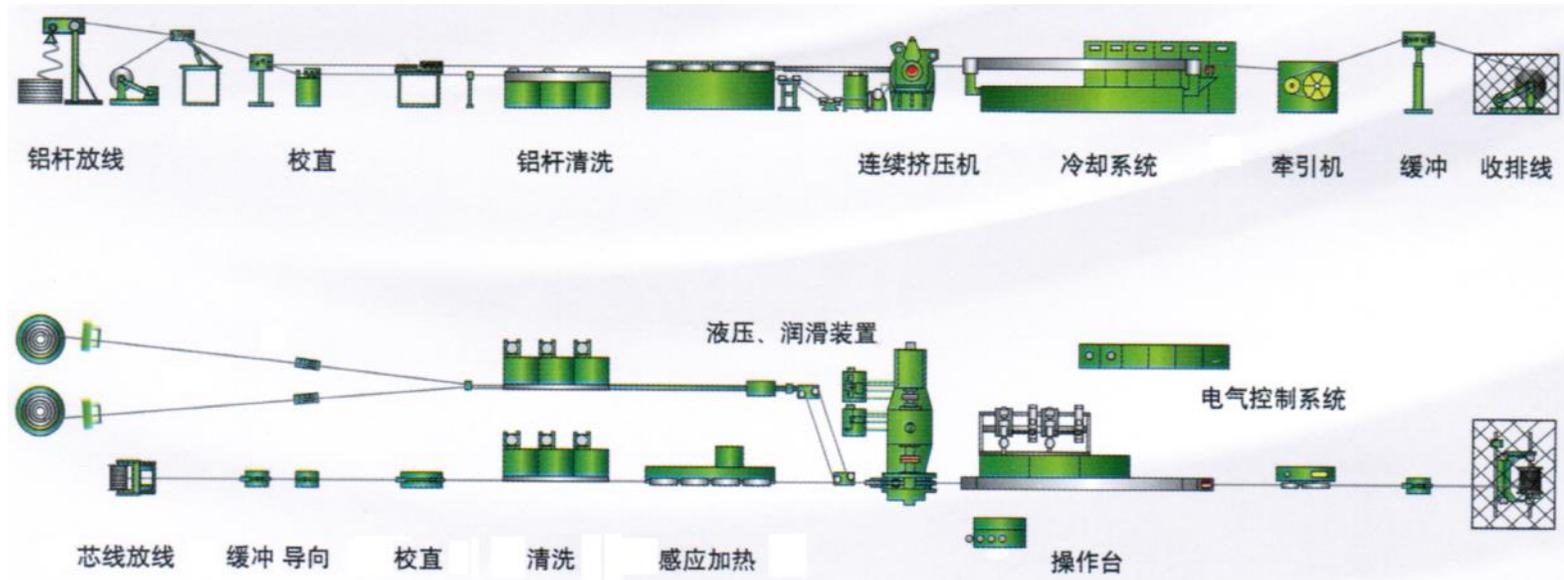


The decrease of the critical current is less than 7% after the stranding process.

Extrusion of Aluminum with insert of Rutherford cable



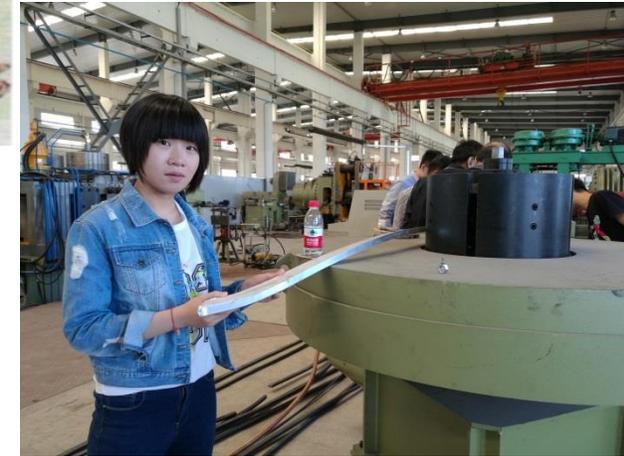
Conform Process



Drawing Process

Aluminum cladding process study and improvement

Zian Zhu, Ye Yuan, Zhilong Hou, Zhihui Mu



Continuous extrusion and continuous cladding technology

Engineering Research Center of the Ministry of education for continuous extrusion

Dalian Conform Ltd. (Dalian Jiaotong University)

Insert progress

- Completed two rounds of insert process:
Hollow aluminum alloy, Aluminum alloy + copper cable
- Result: Depression in the middle and the tooling needs to be improved(2016.4)
The strands of the cable are separate after the tooling improvement.
- There is a great improvement from the latest result, but the shear strength 8MPa not enough to reach 20MPa.



2016.1
Hollow aluminum alloy



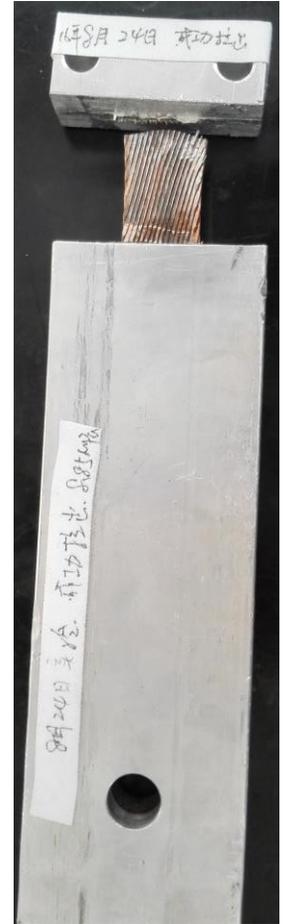
2016.2
Aluminum alloy + copper cable



2016.5~6:
Aluminum alloy + copper cable



2016.8:
Aluminum alloy + copper cable



R&D progress

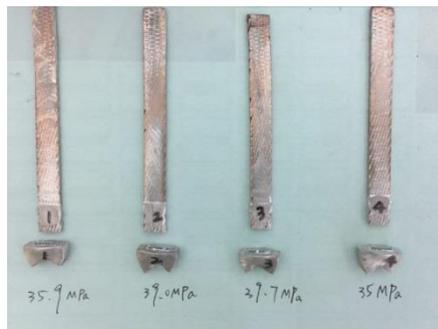
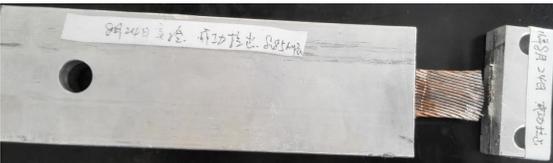
● Different aluminum alloy and copper cable shear strength test

- ✓ The shear strength is larger than the **required (20MPa)** in the latest test. We used 99.99% aluminum material to improve the shear strength.



Number of strands : 32
 Strand diameter : 1.2mm
 Material : **COPPER+Al**
 Length: 1m
 Complete time: 2016.8
 Shear strength (copper &Al) :
8.85 MPa

Dimensions: 15*4.7mm²
 Number of strands : 14
 Material : **COPPER+Al(99% purity)**
 Complete time: 2017.4
 Shear strength (COPPER &Al) :
10 MPa



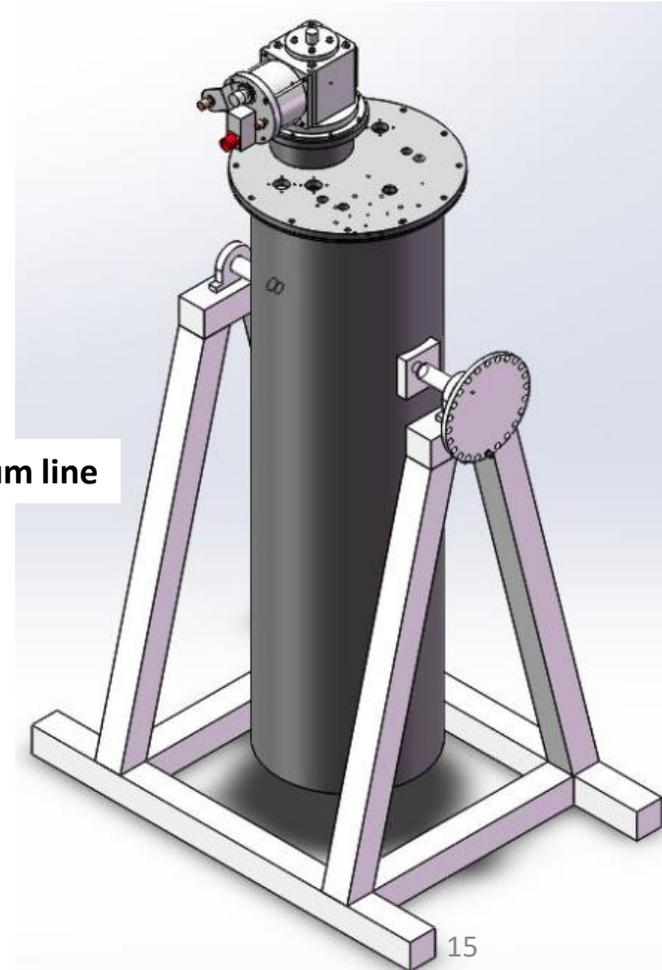
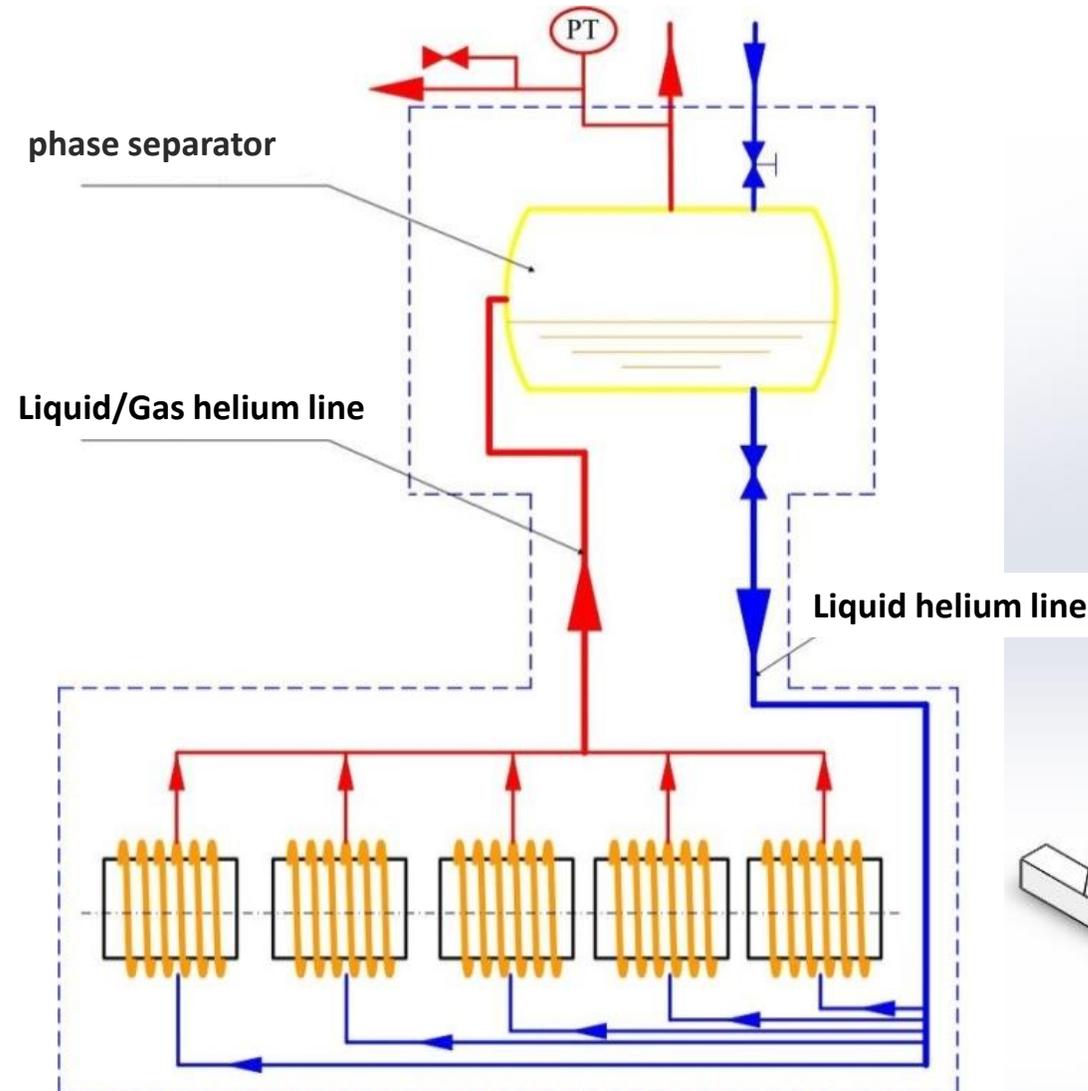
Dimensions: 15*4.7mm²
 Number of strands : 14
 Material : **NbTi+Al(99.99% purity)**
 Complete time: 2017.8
 Shear strength (COPPER &Al) : **>35MPa**

Progress of coil cooling research

- The magnet coils will be cooled by liquid helium thermosiphon conductive cooling method.
- Set up a small thermal siphon principle experiment device

Motivation:

- **BESIII magnet Suffered too much quenches caused by cryogenics failure**
- **Need to study thermal syphon cooling for the next large magnet**



| NO. | Time | cause of quench | Quench current |
|-----|------------|-------------------------------|----------------|
| 1 | 2008.7.29 | SCQ's quench | 3034A(0.9T) |
| 2 | 2008.8.18 | SCQ's quench | 3369A(1.0T) |
| 3 | 2008.9.23 | Current ramping down too fast | 3190A |
| 4 | 2008.12.18 | SCQ's quench | 3369A |
| 5 | 2009.2.26 | Unknown | 3369A |
| 6 | 2009.3.7 | Unknown | 3369A |
| 7 | 2009.3.27 | Power grid fault | 3369A |
| 8 | 2009.4.25 | Unknown | 3369A |
| 9 | 2009.5.7 | Cryogenic system failure | 3369A |
| 10 | 2009.5.31 | Cryogenic system failure | 3369A |
| 11 | 2009.12.25 | Cryogenic system failure | 3369A |
| 12 | 2010.1.13 | Vacuum system failure | 3369A |
| 13 | 2010.11.16 | SCQ's quench | 3369A |
| 14 | 2011.1.13 | Cryogenic system failure | 3369A |
| 15 | 2011.1.17 | Cryogenic system failure | 3369A |
| 16 | 2011.5.10 | Cryogenic system failure | 3369A |
| 17 | 2011.5.26 | Cryogenic system failure | 3369A |
| 18 | 2011.6.1 | Cryogenic system failure | 3369A |
| 19 | 2012.1.29 | Cryogenic system failure | 3369A |
| 20 | 2012.2.3 | Cryogenic system failure | 3369A |
| 21 | 2012.2.14 | SCQ's quench | 3369A |
| 22 | 2012.3.23 | Power grid fault | 3369A |
| 23 | 2012.11.15 | Power grid fault | 3369A |
| 24 | 2013.2.10 | Cryogenic system failure | 3369A |
| 25 | 2014.03.12 | Cryogenic system failure | 3369A |
| 26 | 2014.05.26 | Quench detector misoperation | 3369A |
| 27 | 2015.02.20 | Cryogenic system failure | 3369A |
| 28 | 2015.05.18 | Power network problem | 3369A |
| 29 | 2015.12.30 | Quench detector misoperation | 3200A |
| 30 | 2016.01.17 | Cryogenic system failure | 3369A |
| 31 | 2016.02.9 | Cryogenic system failure | 3369A |
| 32 | 2017.04.13 | Power Fluctuation | 3369A |
| 33 | 2017.05.07 | Cryogenic system failure | 3369A |
| 34 | 2017.11.28 | Cryogenic system failure | 3369A |
| 35 | 2018.03.05 | Cryogenic system failure | 3369A |

Quenches of BESIII detector magnet @BEPCII collider in the past 10 years

Two phase helium force flow cooling

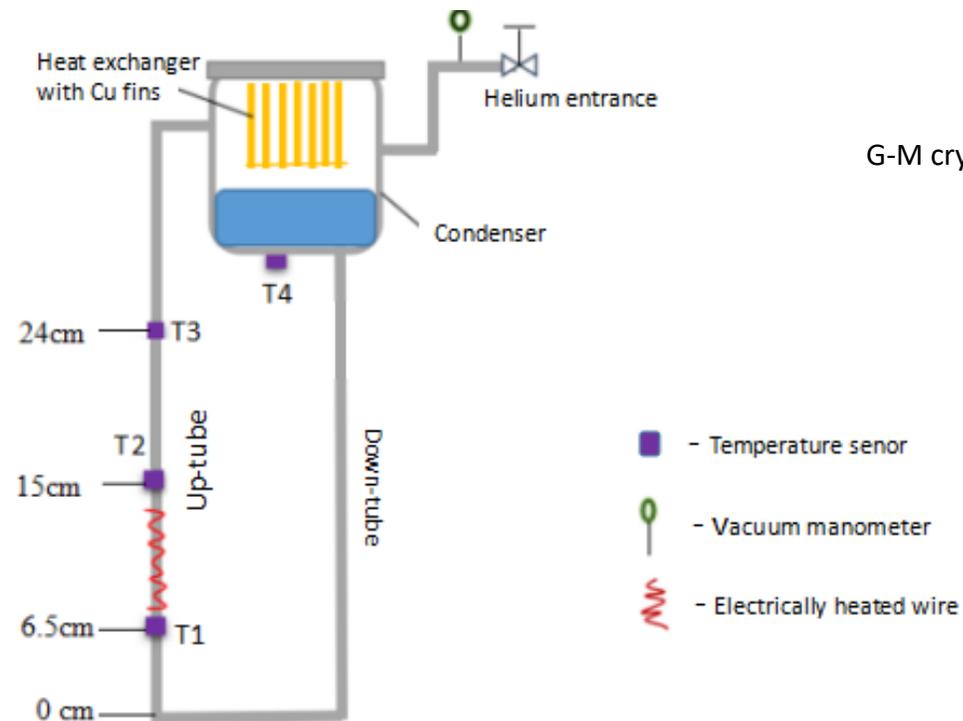
Total 35 quenches

- **18 cryogenic system failure**
- **5 electricity power failure**
- **5 caused by SCQ magnet quench**
- **2 quench detector failure**
- **1 vacuum failure**
- **1 operation error**
- **3 unknown(during ramping up/down)**

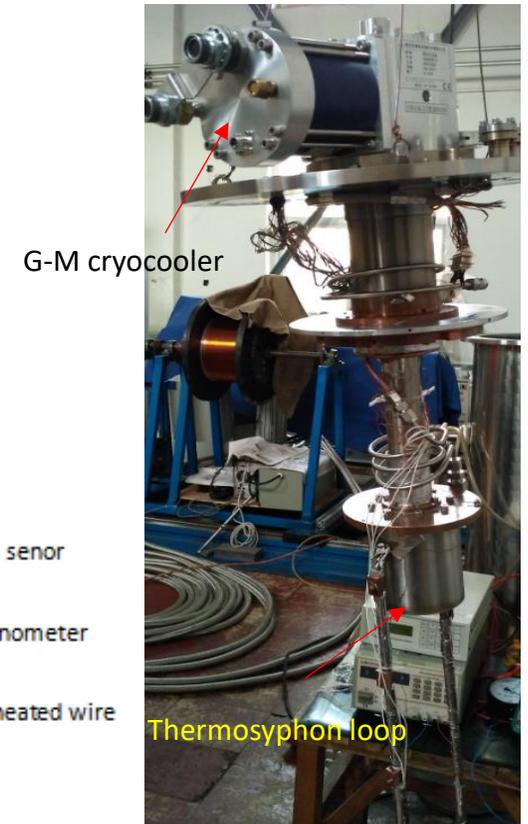
Detector magnet @CEPC: Liquid helium thermal siphon cooling to avoid quench caused by cryogenics failure

Magnet Cryogenics

- A mini set-up for thermal siphon study based on liquid helium (LTS)
- Building a two-phase natural circuit loop, helium was used as the working fluid;
- Investigate the heat and mass transfer characteristics experimentally;
- Obtain temperature profile with heat flux and critical heat flux
- Numerical modelling of mass flow rate in a thermal syphon



Schematic of the circuit loop



Experimental apparatus

HTS option

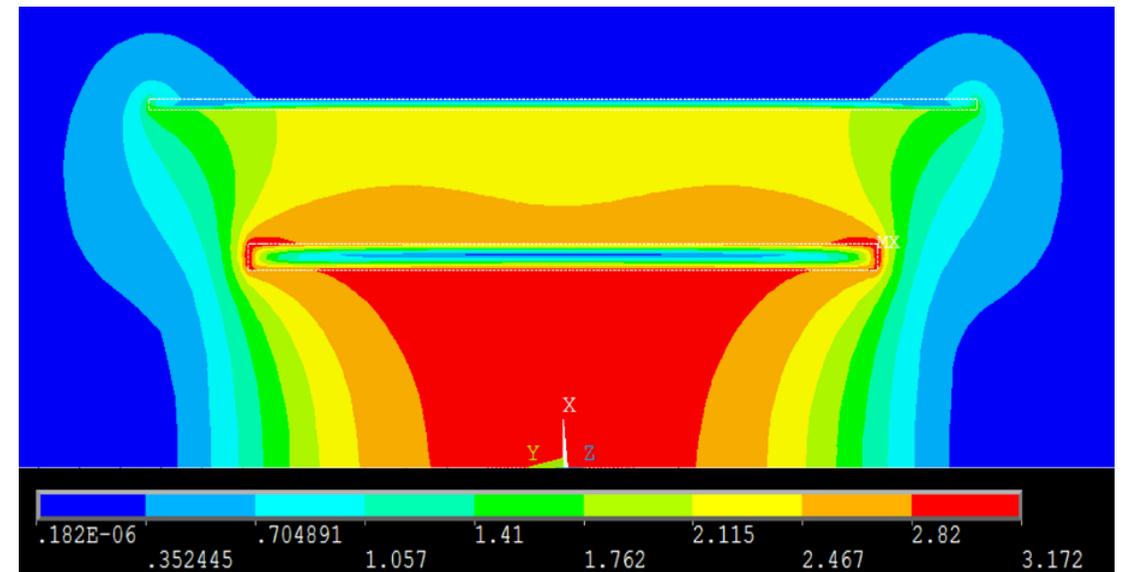
- Compared with the use of LTS(low temperature superconductor), the HTS(high temperature superconductor) detector magnet has the following highlights:
 - 1. Three HTS supplier existed in China
 - 2. It is possible HTS cost 10 times cheaper in 5 years
 - 3. Working at a relatively high temperature (20 K), cooling get easier
 - 4. More stability, HTS magnet not easy to quench
 - 5. Cost maybe comparable with the LTS magnet especially in the case of active shielding design(without iron yoke)
 - 6. Push the development of full HTS high field solenoid magnet

Active shielding Scenario

- The active shielding design has been applied widely for commercial MRI magnets. Comparing to the one solenoid and yoke design, this design achieves a similar performance while being much lighter and more compact, which has been improved by FCC previous studies .
- The main solenoid provides 5 T central field over an room temperature bore of 7.2 m and a length of 7.6 m. The outer solenoid provides -2 T central field, with a radius of 6.5 m and a length of 10 m.



Sketch figure of the active shielding magnet, with the available areas for muon chambers



Field map of the active shielding magnet

Summary

- Some progress in the development of specific LTS superconductor, thermal siphon cooling
 - **Constructed 10 meter short length aluminum stabilized NiTi Rutherford superconductor of 10kA@4T**
 - **Key performances: Shear Strength meet the requirement, RRR, Ic under evaluation**
- Will add 2T detector magnet design proposed by Italia team into CDR
- Keep iron yoke structure as the default option, and the Active Shielding scenario as an candidate option
- Need further discussion: 2 IP@CEPC, one 3T, another 2T

Next Steps

- **1. Further development of longer and higher Ic Al-based NbTi conductor (>100m,>10kA@4T)**
- **2. Study of thermal siphon cooling system for LTS coil**
- **3. Study of candidate option(HTS, no iron yoke, HTS coil cooling method @20K)**

Thank you for your attention!

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