

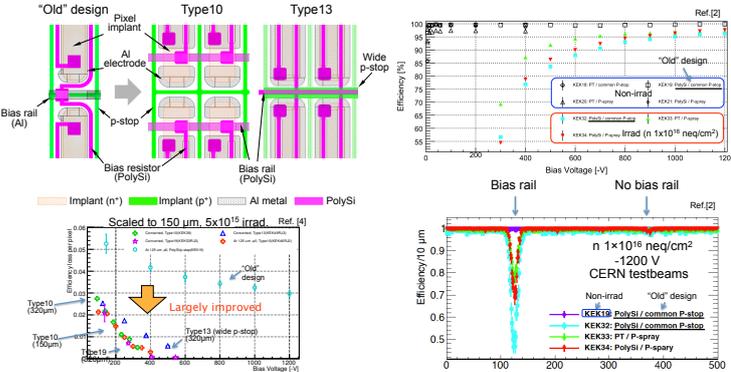
Signal simulation under the bias rail in n⁺-in-p pixel sensor before and after irradiation

Y. Unno^a, R. Hori^a,

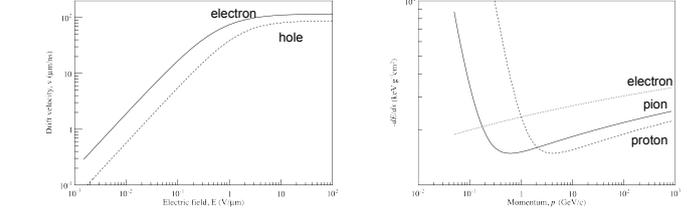
^aKEK, IPNS, 1-1 Oho, Tsukuba, Ibaraki 305-0801, Japan

Abstract -- We have developed n⁺-in-p pixel sensors with biasing network to provide the reverse bias voltage to individual pixels without bumpbonding a readout ASIC. The pixel sensor with the bias rail running at the boundary between the pixels has shown a loss of track-finding efficiency under the bias rail when the device is irradiated with protons. The device has shown little efficiency loss initially. In this signal simulation, we have imported the electric fields and the weighting potentials from TCAD calculations. We have evaluated the charges lost to the bias rail from the distribution and drifting of the charge carriers in the silicon. A comparison of the results with or without radiation damage has confirmed the loss of efficiency quantitatively.

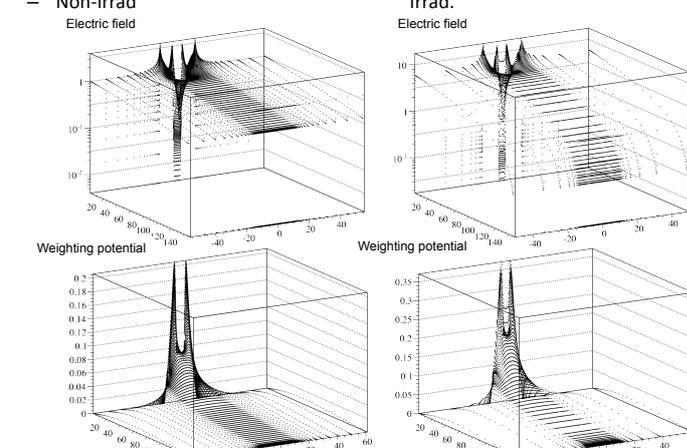
Bias rail structure in n⁺-in-p pixel sensor Ref.[3]



Drift velocities Ref.[7], Energy deposition

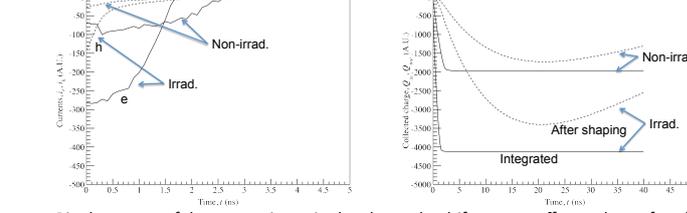


Electric fields and Weighting potentials from TCAD



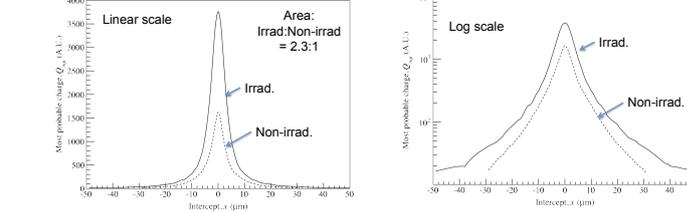
Drift velocity is nearly saturated both in irradiated and non-irradiated conditions as E > ~1 V/μm.

Induced currents (e, h) and charges (integrated, after pulse-shaping)



Bipolar nature of the current is not in the plot as the drift was cut off near the surface (at 3 μm) due to programming issue.

Max. charges after pulse-shaping vs incident x position



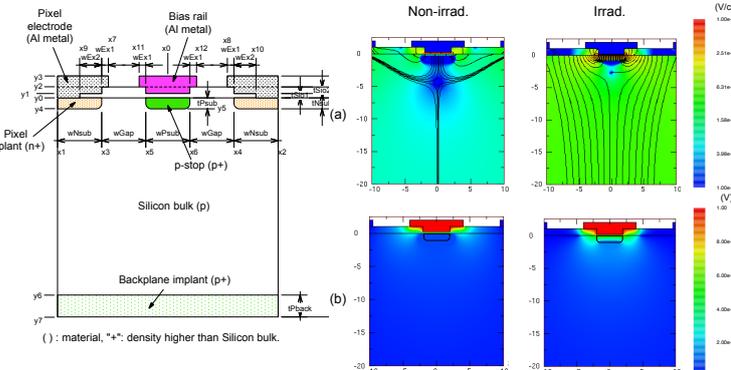
Summary
 - Charges lost to the bias rail is approximately 2.3 times in irradiated than in non-irradiated. This explains the difference of efficiency loss in the irradiated and non-irradiated, quantitatively.
 - The difference in intensity of charges lost is due to the difference in the convolution of the intensity of the weighting potential and the drift path as the drift velocity is nearly saturated in both irradiated and non-irradiated.

References

[1] Y. Unno et al., Nucl. Instr. Meth. A650 (2011) 129-135; Y. Unno et al., Nucl. Instr. Meth. A699 (2013) 72-77
 [2] K. Motohashi et al., Nucl. Instr. Meth. A765 (2014) 125-129
 [3] Y. Unno et al., Nucl. Instr. Meth. A831 (2016) 122-132
 [4] K. Nakamura et al., 2015 JINST 10 C06008; K. Kimura et al., Nucl. Instr. Meth. A831 (2016) 140-146
 [5] ENEXSS 5.5, developed by SELETE in Japan
 [6] J. Leslie et al., IEEE Trans. Nucl. Sci. 40 (1993) 206-208
 [7] R.S. Muller, T.I. Kamins, Device Electronics for Integrated Circuits, ISBN-978-0-471-59398-0, John Wileys & Sons, Inc.

TCAD Simulation Ref.[5] for (a) Electric and (b) Weighting fields Ref.[3]

- Geometry: vicinity of bias rail
 - p-type bulk, n⁺ readout, thickness 150 μm
- Radiation damage approximation:
 - Increase of acceptor-like state ← Effective doping concentration
 - Increase of interface charge ← Fixed oxide charge
- Non irradi. condition
 - N_{eff} = 4.7 × 10¹² cm⁻³, V_{EP} ~ 40 V
 - Fixed Oxide Charge = 1 × 10¹⁰ cm⁻²
- Irrad. condition
 - N_{eff} = 1.5 × 10¹³ cm⁻³, V_{EP} ~ 430 V
 - Fixed Oxide Charge = 1 × 10¹² cm⁻²



Induced charge to the bias rail (Kamo's theorem)

- A mobile charge in the presence of any number of grounded electrodes, the induced charge Q_A at an electrode A is

$$Q_A = q \cdot V_{qA}$$

- where q is the charge in a position, V_{qA} the "weighting potential" of the electrode A at the position of q.
- In a finite time, with a fast readout circuitry, instantaneous induced current, i_A, is the gradient of V_{qA} along the moving direction times the drift velocity.

$$i_A = q \frac{dV_{qA}}{dt} = q \left(\frac{\partial V_{qA}}{\partial x} \frac{dx}{dt} \right) = q \cdot v_x \cdot \frac{\partial V_{qA}}{\partial x}$$

$$v_x = \mu E_x = \mu \frac{\partial V_{qA}}{\partial x}$$

Although the final answer shall be obtained after integrating the current, we can have physics insight, qualitatively, from E_x, v_x, V_{qA}

Signal simulation

- Using the simulation package Ref.[6] with various updates

