



March 26th 2012

(Draft rev.1) Report on the conclusions of the SuperB magnet costing working group

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Introductory considerations

The questions posed to the working group by SuperB management (see annex A) were triggered by the need to evaluate the proposal of the Budker Institute about the possibility to build some of the Main Rings magnets and the vacuum chamber. This proposal included a list of items that can be provided by BINP and the relative costs.

First of all we have to stress a series of preliminary considerations

- The basic document available to the Working Group is constituted by an excel file (*Magnets_V16.xlsx*) including the main characteristics of all dipoles, quadrupoles and sextupoles of the HER and LER lattices. Namely the field or gradient and the magnetic length are reported for any magnets.
- Some additional information about magnets was coming from PEPII TDR and from the CDR of SuperB.
- This basic information is indeed poor because important parameters such as magnet gap or bore, good field region and beam stay clear are not clearly specified.
- No magnet design exists also at very basic level.
- Under these conditions the mission of the working group appeared very difficult. The only way we could perform, at least partially, our work was to make ourselves

assumptions about the magnet structures if not some simple design exercises on the basis of the existing information.

• An important parameter is the magnet gap or bore. For LER dipoles gaps from 63.3 mm to 100 mm were considered. For HER Dipoles gaps from 60 mm to 100 m were used for evaluation. For quadrupoles, bore radius of 30 mm and 50 mm were considered and finally for sextupoles a bore radius of 30 mm and 50 of 100 mm was used. The reason why we analysed these gap/bore ranges is based on three main considerations:

a) the lower limits directly were coming from indications given by SuperB responsible for the lattice;

b) the upper value for the dipoles reflects a worry about the effects on beam pipe dimensions of the needed vacuum pumping rate;

c) the upper value of the quadrupoles and sextupole bore is an assumption.

Methodologies

Two different methods were used oriented to have as final output a cost evaluation of thee ring magnets:

a) The first method is involving sealing optimization formulae based on a long experience with these kinds of magnets (see annex B for the details) from which the basic geometry of each kind of magnet is calculated and then, using these data, some CERN's Cost Evaluation formulae are applied to each magnet and the cost is evaluated starting from the basic material costs.

b) The second method followed an analytical approach passing through magnetic computations of supposed magnet structures and then evaluating technically and economically the magnets (see annex C for a detailed report).

The vacuum line and ancillary were analysed after some considerations about synchrotron radiation power (see annex D)

As first general remark we noted that the varieties of magnet appear to be quite large. As an example the HER include dipoles with 7 different lengths with field ranging from 0.067T to 0.319T and 22 different currents involved. For LER quadrupoles we have 3 main magnetic lengths, but more than 100 different currents (ranging from 5 A to 400 A).

Findings

A reduction of the number of magnet types and especially of the number of different currents could be helpful later, in view of a better optimization of magnet designs with advantages for the costs of magnets and power supplies.

A second remark is related to the quadrupoles. The HER include many high gradient quadrupoles (16÷20 T/m<G<32 T/m). These magnets are reasonable from the cost point of view if the bore is 60 mm. For larger bore (we looked up to 100 mm bore) the magnets are very massive and expensive. Some re-thinking about the needed gradients by the lattice designers looks necessary.

Costs

The result of the cost (in $\mathbf{k} \in$) analysis is summarised in the Table 1. The table includes the costs of the magnets as they would be bought new. Both the results of the scaling first and the analytical second approaches are shown. For both methods two different evaluations are reported: one for smaller gaps/bores and a second one for larger dimensions. The table can be used for composing the costs depending on the technical choices. However we can distinguish two main cases depending on the dimensions:

a) Dipole HER 60 mm/68 mm gap. Dipole LER 63.3 mm/64.8 mm gap. Quadrupole 60 mm bore. Sextupole $\frac{100}{60}$ mm bore. The total cost of the rings magnets is ranging from $\notin 57234$, first approach, to 58673(?? - 58373) to $k \notin 59100(??)$, second approach.

b) Dipole 100 mm/ gap. Quadrupole 100 mm bore. Sextupole 100 mm bore. The total cost of the rings magnets is ranging from € 82086, second approach, to k€ 89930(?? – 89437), first approach.

The table 1 also includes the costs of 4 spin rotators and of the final focus quadrupoles. These are all superconducting magnets.

The table also includes the costs of the girders simply considered as a 10% of the total cost. Finally the costs of the vacuum components and equipments is also included

Item	Optimiza	ation approach	Analytica	l approach
HER	Dipole Gap 60 mm Quad Bore 30 mm Sext. Bore 100 mm	Dipole Gap 100 mm Quad Bore 50 mm	Dipole Gap 68 mm Quad Bore 30 mm Sext. Bore 100 mm	Dipole Gap 100 mm Quad Bore 50 mm
Dipole	16937	25893	17235	21434
Quadrupole Low Gradient Quadrupole	1349 8576	2500 16013	10845	Not evaluated
Sextupole	2783	2783	2535	
Бехцирове	2105	2105	2000	
LER	Dipole Gap 63.3 mm Quad Bore 30 mm Sext. Bore 100 mm	Dipole Gap 100 mm Quad Bore 50 mm	Dipole Gap 64.8 mm Quad Bore 30 mm Sext. Bore 100 mm	Dipole Gap 100 mm Quad Bore 50 mm
Dipole	2641	3947	3153	3864
Low field	1 402 4	20.425	11101	
Dipole High Field	14034	20425	11181	14776
Quadrupole	5626	10430		
Ouadrupole	2505	4663	10889	Not evaluated
High Gradient	2000	1000		
Sextupole	2783	2783	2535	
Spin notatona			2	50
Spin rotators			3.	220
Tinai locus				500
Girders for magnets rings			6000	8000
Vacuum pipes			1	
RF shielded bellows and valves		· · · · · · · · · · · · · · · · · · ·		
Pumps				
Valves				
Gauges				

Table 1: Cost evaluation

Reuse of PEPII magnets

In general it is noted that there are two possible modalities for reusing the PEPII magnets. a)

Some of the SuperB dipoles fit the length of existing PEPII magnets. In principle these magnets could be used "*as they are*". In facts the PEPII magnets have the windings in aluminum, while for electrical power consumption reasons all SuperB magnets shall involve a copper conductor. So these magnets shall be dismantled, new coils shall be constructed and then integrated into the yoke; finally magnetic test shall be performed.

b) For the magnet with different lengths only the iron yoke can be partially reused after a cutting for meeting the geometrical lengths of SuperB magnets.

Analysing the option *a*) for 40 dipoles of HER (the ones with length 5.4 m) with the analytical approach, one find that the costs to be paid are $k \in 1525$ for material and $k \in 2353$ for manpower. If new built, the costs for these 40 magnets is $k \in 5047$, giving a cost saving of $k \in 1169$.

Option b) for the remaining 154 dipoles of HER implies a cost of $k \in 8923$ with a cost saving of $k \in 2012$.

In total the costs saving for HER dipoles seems to be $k \in 3190$ over a total cost of about $k \in 17000$. The potential cost saving of 18% is too low to be seriously being considered, because the risks in re-using old equipments.

The same considerations apply to all magnets.

Comparison with proposal of Budker Institute

Comparing the costs reported in this document with the proposal made by Budker Institute, one can see that the costs envisaged by the Working Group are a factor about two higher than the BINP ones. From the analytical analysis it appeared that the manpower costs for the option/with smaller gaps/bores is about $37000 \text{k} \in$ (see Annex C). Considering that BINP could have these costs 50% lower, the BIMP costs are still 70% lower than the Working Group estimations. This point needs more deep discussions and it is presently postponed to future developments.

Answer to the questions

On the basis of the studies and analyses done by the working group, the answers to the question posed by SuperB management are:

1. Are the magnet parameters adequate to the SuperB main rings?

Answer: The basic information is presently quite limited (important parameters such as magnet gap or bore, good field region and beam stay clear are not elearly specified) and no magnet design exists also at very basic level. The answer to this question can be only partial. The working group thinks that some work is needed on the lattice optimization aimed to define the dipole gaps taking into account the problems coming from vacuum issues. A high pumping rate could require gaps as large as 100 mm with consequent high cost of the magnets. The quadrupoles of the HER and some quadrupole of LER have too high gradient (> 20T/m) requiring difficult and heavy magnet to be designed and built if the bore is 100 mm. For 60 mm bore no problems are envisaged.

• Are there clear economic advantages in using the PEP---II rings magnets?

The SuperB ring magnets are quite different from PEPII magnets. In facts a lot of SuperB magnets have lengths not matching the PEP magnet lengths. In case gaps of 60 mm are acceptable, PEPII dipole could be reused with a potential cost save of 18%. For the quadrupoles (if bore is 100mm) same considerations apply; in this case cost saving can be even lower because the replacement of all the coils is a driving factor of the costs and the higher gradient quadrupoles shall be procured new. Considering the errors related to the present evaluation and the risks related to involve old components, the reuse of PEPII ring magnets is discouraged.

Are there some construction risks and what can be done to mitigate them? (for example: spare parts, maintenance strategy,...)
 If the magnets are procured as new, there is not particular technical risk, but the high

gradient quadrupoles. In general it is found that too many magnets types are presently included in the HER and LER lattices. As remarked above, a reduction of the number of magnet types and especially of the number of different currents could be helpful

later for a better optimization of magnet designs with advantages for the costs of magnets and power supplies. Presently there are not the conditions for defining a spare part or maintenance strategy.

• When and how we can define the main rings layout to evaluate its impact on civil engineering and environmental conditions?

2. What is needed to assess how the solution proposed compares with the one reusing PEPII magnets.

The suggestion of this working group is not to reuse PEPII magnets. This conclusion is based on a preliminary analysis done on the information available now. It is clear that an assessment how the option of procure new magnets compares with the reuse of PEPII magnets can be done only after a design of the magnet exists. However this Working Group is not expecting a different conclusion.



APPENDIXA

Charge to the working group

Frascat, Febru ry 14 2012

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Oozza, INF F, Frasca IY

P. Fabbricatore, INFN-Genova, Italy (chair)

E. Levichev, BINP, Russia

C, SaMIIi, INF F, FraSGati, taly

O_Tommasini CERN,Switzerla d

U_W enandis,SIJ\C_ USA

Dear Colle

The IC)o a Ollnbbo Laboratory, charn o lhe on\$IRICUJOn offi'le SrE! project at the Roma Tor Vergata Umrersity campus is plannil1i to collabocate with other international laooratorie:s or the pn:Msion of paru of e accelerator.

l'hl! Bu er stiNte n NOYOSIJ1rsk jRussia) has ev-al the pOSStillJI:Y te bu•iCl some o! he n ings magnets and lhe UIII eh mber. A list of item.s that an be providm by BI P, nd relati e coru, has been presented by Prot E. tevidhev.

1- $0 \ll 1$ to De a e to correally evalu.ne me proposal Ot filNFs we woold his to InYit you, as an IIIillert in the eld, to particlize te en evalual on if O'.I).

Examples of Ic:ey points to be adClressed are reported befow.

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	Are thel'e oome CONtruàion risks and what can be done to mitigate mem? (for example: s Te
	parts, maintenance strategy, -
	When and now we an defi e main ril1p liayout touate its - att on engineeril'll and
	entalcond!!tions?
2.	t is needed to atSsess how Me solution proposed compares . the one reusing FCEPII m gnett

We hope that you will acce this charge_looting forward to a tru - 1 collaboration, please accept our best fea nti

Roberto Pe ronm Director Genera , Cabibbo La'boratory
 Walter Scandale

 Director
 I ab infrastructures, cabibbo Labor.ItOfi

RP-WS/MRf

APPENDIX B

RINGS MAGNETS COST EVALUATION USING

OPTIMIZATION FORMULAE APPROACH

C. Sanelli

Presentation given At 3rd SuperB meeting LNF March 19-23



Cost Evaluation of Storage Ring Magnets

Claudio Sanelli

March 19, 2012





Preliminary Questions - 1

Some preliminary questions should be clarified to better understand the problems and to make a more clear and precise cost evaluation. Just as an example:

- 1) Which are the max beam dimensions (or β_{\max} , \mathcal{E}_{\max} , \mathcal{D}_{\max})?
- 2) Which are the max beam stay-clears?
- 3) Is there any impedance budget to be respected for the vacuum chamber? This affects the v.c. geometry, material and dimensions, then the magnet gap and/or the bore radius.







Preliminary Questions - 3

- 6) Which is the expected Good Field Region and the related magnetic field/gradient tolerance? This again affects the physical dimensions of the magnet (width).
- 7) Since some magnets are very long (> 5 m), which are the overall vacuum chamber dimensions and tolerances?

8)



Preliminary Questions - 4

The answers to these questions (and eventually others I have forgotten) can let us understand if the PEPII magnet gap/bore radius is adequate for Super-B and go ahead with a more precise cost evaluation.





Basic Assumptions - 1

- 1. L.E.R. Dipoles:
- 1.1 Two possible gaps: 0.0633 (as per Biagini list) and 0,1 m.
- 1.2 Two dipole cross-section: a) low field (less than 0,2 T); b) high field (from 0,2 to 0,76 T).
- H.E.R. Dipoles: Two possible gaps: 0,06 m (as per Biagini list) and 0,1 m, but only one crosssection.





Basic Assumptions - 2

- 3. L.E.R. Quadrupoles:
- 3.1 Two possible bore radius: 0,03 m and 0,05 m.
- 3.2 Two quad cross-section: a) low gradient (less than 16 T/m); b) high gradient (from 16 to 32,11 T/m).
- 4. H.E.R. Quadrupoles:
- 4.1 Two posssible bore radius: 0,03 m and 0,5 m.
- 4.2 Two quad cross-section: a) low gradient (less than 16 T/m); b) high gradient (from 16 to 32,11 T/m).
- 5. Very high gradient I.R. quads (4): not evaluated.





Basic Assumptions - 3

- 6. Sextupoles:
- 6.1 Only one sextupole type.
- 6.2 Reference design: ANKA sextupole.
- 6.3 Two possible bore radius: 0,03 m and 0,05 m.
- 6.4 The 0,05 bore radius sextupole is scaled by the 0,03 one only increasing the bore radius and the current but leaving unchanged the corss-section.



Basic Assumptions - 4

- 7. Steering magnets:
- 7.1 The quantities are the same of PEPII.
- 7.2 The costs are scaled from magnets having similar aperture (CNAO steering magnets), and similar magnetic lenght.
- 8. No modification, refurbishing, adaptation of the PEPII magnets has been considered





Cost Summary Table

Magnet Type	Gap/Bore Radius (m)	Cost (k€)	PEPII Saving (k€)	Gap/Bore Radius (m)	Cost (k€)	PEPII Saving (k€)
L.E.R. Dipoles (Low field)	0,0633	2641	0	0,1	3947	0
L.E.R. Dipoles (High Field)	0,0633	14034	-5396	0,1	20425	0
H.E.R. Dipole	0,06	16937	-5183	0,1	25893	0
L.E.R. Quadrupoles (Low Gradient)	0,03	5626	0	0,05	10430	-235
L.E.R. Quadrupoles (High Gradient)	0,03	2505	0	0,05	4663	
H.E.R. Quadrupoles (Low Gradient)	0,03	1349	0	0,05	2500	-2500
H.E.R. Quadrupoles (High Gradient)	0,03	8576	0	0,05	16013	-2416
Total Cost (All new magnets)		51668	-10579		83871	-5151
L.E.R. Sextupoles	0,03	2783		0,05	2783	Same Sex as 0,03
H.E.R. Sextupoles	0,03	2783		0,05	2783	Same Sex as 0,03
Total Cost (All new magnets)		5566			5566	
Steering Magnets						
L.E.R. Steering - N. 296 - 30 k€ Each		8880	-8880		8880	-8880
H.E.R. Steering - N. 282 -25 k€ Each		7075	-7075		7075	-7075
Total Cost (All new magnets)		15955	-15955		15955	-15955
Grand Total Cost (All new magnets)		73189	-26534		105392	-21106
Note: No modification, refurbishing, a	adaptation of the PEPII	magnets ha	as been considered	1		





Modification, Refurbishing, Adaptation of PEPII Magnets Some Considerations

Some useful data:

- 1) LNF Energy Cost January 2012: 0,178 €/kWh
- 2) Rough Annual Cost ≈ 1 M€*Year/MW
- 3) Estimated max electric power: 40 60 MW
- 4) Optimum Current Density: 2 2.2 A/mm²

Expected Electric Energy Cost in operation:

40-60 M€/Year

Coil Substitution: the PEPII magnets have Al coils:

<u>Only for Storage Rings</u>: Assuming: a) J= 2.2 A/mm²; b) gap 0,0633 m Dipole (very roughly): H.E.R. ≈ **1 MW** L.E.R. ≈ **0,6 MW** Quadrupoles:

> H.E.R. <G> = $(\Sigma_i G_i^* N_i) / \Sigma_i N_i$ = 19,62 T/m $\Sigma_i N_i$ = 362

H.E.R. Quad Power (r=0,03, Lm=0,3 m) ≈ **1 MW**



(Power converter losses, efficiency and power factor $\cos \phi$ not considered).





Coils have to be built in Cu!

Mechanical (and Magnetic) lenghts have to be adjusted, then one needs:

1) Tools to dismount the magnets (dismount old coils, unsold the external containing and reinforcing plates, etc.)

Question: Are the lamination glued?

If yes, the idea to heat the magnet to unglue the laminations to re-use them appear to me not consistent. In alternative, can the magnet mechanically cut?

To be investigated.





If not, the laminations can be re-used, but:

- Tools for positioning and packing the new magnets;
- New containing and reinforcing external plates;
- 4) New fiducials for correct installation and alignment of the magnet;
- 5) New ancillary components to assemble the magnet (coil supports, etc.)
- 6) New coils (the length is changed)



ABIBBO

LAB



- New complete magnet characterization with a complete, iterative set of magnetic measurements, magnet adjustment, magnetic measurements.
- 8) New magnet supports and adjustment tools.

Question: finally, is the necessary manpower less expensive than the iron lamination?



ANKA Sextupole







L.E.R. Bending Dipoles

0,042 0,048 0,052 0,0543 0,0569 0,0633 0,0707 0,0720 0,0720 0,0858 0,0918 0,0980 0,1099	1 2 1 3 1 2 5 2 2	333,719 288,393 267,139 256,706 245,070 220,060 196,993 193,652 162,372	2,8 4,1 3,65 4,1 2,8 4,1 3,65 4,1 4,1	8,39 14,22 13,66 15,97 11,43 18,63 18,53 21,17	2,94 7,29 6,23 8,19 4,00 9,55 8,45 10,85			8,3903 28,4334 13,6633 31,9432 11,4253	0,0013 0,0045 0,0022 0,0051 0,0018	0,0633 0,0633 0,0633 0,0633 0,0633	63,26 79,92 74,50 79,92 63,26	63,26 159,84 74,50 159,84 62,35	0,100 0,100 0,100 0,100 0,100 0,100	94,15 119,52 111,26 119,52 94,15	94,1 239,04 111,26 239,04
0,048 0,052 0,0543 0,0549 0,0633 0,0707 0,0720 0,0720 0,0858 0,0918 0,0980 0,1099	2 1 2 1 3 1 2 5 2 2	288,393 267,139 256,706 245,070 220,060 196,993 193,652 162,372	4,1 3,65 4,1 2,8 4,1 3,65 4,1 4,1	14,22 13,66 15,97 11,43 18,63 18,53 21,17	7,29 6,23 8,19 4,00 9,55 8,45 10.85			28,4334 13,6633 31,9432 11,4253	0,0045 0,0022 0,0051 0,0018	0,0633 0,0633 0,0633 0,0633	79,92 74,50 79,92 63,26	159,84 74,50 159,84 62,26	0,100	119,52 111,26 119,52 94,15	239,04 111,26 239,04
0,052 0,0543 0,0569 0,0633 0,0707 0,0720 0,0858 0,0918 0,0980 0,0980	1 2 1 3 1 2 5 2 2	267,139 256,706 245,070 220,060 196,993 193,652 162,372	3,65 4,1 2,8 4,1 3,65 4,1 4,1	13,66 15,97 11,43 18,63 18,53 21,17	6,23 8,19 4,00 9,55 8,45 10.85			13,6633 31,9432 11,4253	0,0022 0,0051 0,0018	0,0633 0,0633 0,0633	74,50 79,92	74,50 159,84	0,100	111,76 119,52 94,15	111,2
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0,0569 0,0633 0,0707 0,0720 0,0858 0,0918 0,0918 0,0980 0,1099	1 3 1 2 5 2	245,070 220,060 196,993 193,652 162,372	2,8 4,1 3,65 4,1 4,1	11,43 18,63 18,53 21,17	4,00 9,55 8,45 10.85			11,4253	0,0018	0.0633	63.26	62.26	0.100	9415	04 10
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0,0707 0,0720 0,0858 0,0918 0,0980 0,1099	1 2 5 2	196,993 193,652 162,372	3,65 4,1 4,1	18,53 21,17	8,45			33,8333	0.0089	0,0633	79,92	239,76	0,100	119,52	358,5
0,0720 0,0858 0,0918 0,0980 0,1099	2 5 2 2	193,652 162,372	4,1	21,17	10.85			18,5286	0.0029	0.0633	74.50	74.50	0.100	111.26	111.2
0,0858 0,0918 0,0980 0,1099	5	162,372	4.1		and shall be			42,3440	0,0067	0,0633	79,92	159,84	0,100	119,52	239,0
0,0918 0,0980 0,1099	2	+++ 022		25,25	12,94			126,2530	0,0201	0,0633	79,92	399,60	0,100	119,52	597,60
0,0980	1	151,822	4,1	27,01	13,84			54,0106	0.0086	0,0633	79,92	159,84	0,100	119,57	239,0
0,1099		142,211	4,1	28,83	14,78			57,6610	0,0092	0,0633	79,92	159,84	0,100	119,52	239,0
	2	126,763	3,65	28,79	13,14			57,5878	0.0092	0,0633	74,50	149,00	0,100	111,76	222,5
0,1497	2	93,090	3,65	39,21	17,89			78,4190	0,0125	0,0633	74,50	149,00	0,100	111,26	222,5
0,1733	2	80,385	4.1	51,00	26.14			102,0092	0,0167	0,0633	79,92	159,84	0,100	119,52	239,0
0.1781	3	78,216	4.1	52,42	26.86			157,2573	0.0250	0.0633	79.92	239.76	0.100	119,57	358.5
0,1781	1	78,216	3,65	46,67	21,29			46,6658	0,0074	0,0633	74,50	74,50	0,100	111,26	111.2
0,1821	1	76,525	41	\$3,58	27,46			53,5775	0.0085	0.0633	79.92	79.92	0.100	119,52	119.5
182077	1	76,525	3,65	47,70	21,75			47,6971	0.0076	0,0633	74,50	74,50	0,100	111,25	111,2
							Su	im 991,7603	0,1578			2640,60			3946,8
421814	24	33,032	0,81	24,52	2,48		-	588,5208	0,0937	0,0633	76,06	1825,44	0,10	111.04	2664,9
497878	24	27,985	0,45	16.0798	0,90448875	PEP-II LER av	ailable	385,9152	0.0614	0.0633	52,9	1269.6	0.10	76.66	1839.8
503805	4	27,656	0,81	29,2882	2,96543025			117,1528	0,0186	0,0633	76,06	304,24	0,10	111,04	444.1
533442	80	26,120	0,81	31,0111	3,139873875			2480,888	0,3948	0,0633	76,06	6084,80	0,10	111,04	8883,
604567	78	23,047	0,45	19,5255	1,098309375	PEP-II LER av	ailable	1522,989	0,2424	0,0633	52,9	4126,2	0,10	76,66	5979,4
759264	8	18,351	0,45	24,52	1.38			196,1736	0.0312	0.0633	52.90	423,20	0.10	76.66	613.2
							Su	im 5291,6394	0,8422			14033,48	10.000		20424,9
							To	tal 6283,3997	1.0000			16674.08			24371.7
									1.0			2			
	Low Field Type											1.1			
	High Field Type								8 8 8			3			
4 4 4 5 5 5 6 7	1,1099),1497),1497 1,1733 3,1781 1,1781 3,1781 82077 21814 97878 03805 33442 04567 59264	1,3099 2 1,3497 2 1,3735 2 1,3735 2 1,3735 3 2,3,3735 3 1,3738 1 3,3737 1 4,33747 1 3,3477 1 3,3477 1 3,3477 1 3,3477 1 4,33447 1 4,3447 1 4,3447 1 4,4477 1 4	3,099 2 126,783 3,497 2 99,000 3,733 2 80,385 3,731 3 78,246 3,7321 1 79,525 3,737 1 79,525 3,032 1 79,525 2,238,4 24 23,032 99,77 2 82,067 3,042 20,985 36,425 9,777 2 82,087 2,238,4 24 23,042 9,997,7 24 22,985 9,0005 4 25,057 9,0005 4 25,057 9,0005 4 25,057 9,0005 4 25,057 0,0005 4 25,067 0,0005 4 25,057 0,0005 4 25,067 0,0005 4 25,067 0,0005 4 25,067 0,0005 4 25,067 0,0005 4 <td< td=""><td>3,099 2 122,778 3,66 3,487 2 96,000 3,66 3,737 2 80,305 4,1 3,781 3 76,216 4,1 3,782 3 76,226 4,1 3,783 1 76,525 3,65 3,821 1 76,525 3,65 3,821 1 76,525 3,65 3,821 1 76,525 3,65 2,214 2,4 27,985 0,45 3,842 80 2,6156 0,21 3,842 80 2,6156 0,21 4,84 2,847 0,45 3,842 9,9264 8 1,045 0,45 1,045 1,045 1,045 1,045</td><td>3,099 2 12,7/183 3,6,6 39,2,1 3,487 2 93,0,90 3,6,6 39,2,1 3,733 2 80,0,85 4,1 57,4,2 3,737 3 78,2,16 3,6,5 39,2,1 3,737 3 78,2,16 3,6,5 4,1 57,4,2 3,737 1 76,5,25 3,6,5 44,2 1,3,5,8 3,027 1 76,5,25 3,6,5 47,70 2,2114 2,4 23,0,32 0,0,1 2,4,5,2 3,842 60 2,1,1,0 0,6,1 3,2,0,1 3,842 60 2,1,0,10 0,4,1 1,5,2,5 3,9,64 8 3,3,1 0,4,5 1,3,5,25 3,9,64 8 1,3,0,1 1,3,2,23 1,3,4,5,22 3,9,64 8 1,3,3,3 1,0,4,5 1,3,5,25 3,9,64 8 1,3,4,33 1,0,4,5 1,3,5,25 3,0,64 1,4,5,22 1,4,5,23 1,4,5,23</td><td>3,099 2 125,763 3,65 28,77 33,14 3,497 2 93,090 3,65 39,21 17,89 3,173 2 80,085 4,1 53,42 26,86 3,173 2 80,085 4,1 53,42 26,86 3,173 3 78,525 3,65 44,27 26,86 3,173 76,525 3,65 47,70 21,76 3,027 1 75,525 3,65 47,70 21,76 218,4 24,353 0,45 16,0795 0,9644827 3,977 24 27,565 0,45 16,0795 0,9644827 3,924 60,26 26,020 23,202 2,464-4327 3,924 76 24,047 0,48 15,523 1,04830937 392,64 21,024 0,454 15,523 1,04830937 392,64 8 15,523 1,04830937 1,348 40,47 76 24,047 0,45 15</td><td>3,099 2 122,743 3,65 28,79 13,144 3,487 2 94,090 3,65 39,21 17,89 3,733 2 85,0345 4,1 31,00 26,14 3,733 3 742,15 3,65 46,67 21,39 3,733 742,15 3,65 46,67 21,39 3,733 742,215 3,65 47,70 21,76 3,121 74,525 3,65 47,70 21,76 21814 24 32,032 0,81 24,52 2,468 21814 24 22,062 0,81 3,1397,378 FEP-II LER av 05805 4 22,166 0,81 3,1397,378 FEP-II LER av 0547 78 24,047 0,45 19,5255 1,096309375 FEP-II LER av 059764 8 13,351 0,45 19,5255 1,384 10,455 059764 8 13,351 0,455 1,384 11,28 1,38</td><td>3,099 2 126,768 3,8,45 28,279 33,44 3,497 2 99,090 38,65 39,221 37,88 37,28 3,7373 2 99,090 3,85 39,212 37,88 37,29 3,7373 3 79,2216 3,45 39,212 25,86 31,313 3,7373 3 79,525 3,45 46,67 22,29 31,313 3,721 3,755,25 3,45 44,77,70 21,766 55 2,181,4 2,4 32,932 0,11 24,52 2,468 55 2,181,4 2,4 33,032 0,11 24,525 2,964,64025 54 5,976 2,4 7,2656 0,6,78 3,597,875 FEP-H LER exailable 5,9264 8 32,104 34,525 1,098,109375 FEP-H LER exailable 5,9264 8 32,047 0,45 19,5255 1,098,109375 FEP-H LER exailable 5,9264 8 12,0457 1,38</td><td>3,099 2 122,773 3,66 28,79 3,3,14 57,527 3,187 2 90,000 3,65 32,21 37,89 78,418 3,173 2 90,305 4,1 51,00 26,14 102,029 3,173 3 78,216 3,65 34,21 25,86 152,257 3,173 3 78,216 3,65 4,677 21,79 46,657 3,173 1 76,525 3,45 4,677 21,76 53,577 22077 1 76,525 3,85 47,70 21,76 500 47,6077 21814 2,4 33,032 0,81 2,452 2,48 588,505 588,505 3805 4 27,666 0,81 3,19878375 PEP-41 LER available 388,515 388,515 3842 80 2,612 0,681 1,31,31,31,319873377 PEP-41 LER available 152,287 59264 8 1,8,51 0,65 1,0982,93757 PEP-41</td><td>31099 2 126,768 3,8,6 28,79 33,14 57,5878 0,0002 31497 2 99,090 38,65 39,21 37,28 77,28 77,28 0,0012 31738 2 99,090 3,45 39,21 37,28 102,092 0,0012 31738 3 78,216 3,45 34,07 21,28 137,273 0,0030 31731 3 79,216 3,45 44,67 21,278 44,6658 0,0012 31721 3 75,525 4,1 55,36 27,46 588,575 0,0016 21814 24 33,012 0,41 24,52 2,48 991,963 0,177 9776 24 2,2864 0,90448875 PEP-II LER available 385,520 0,0647 9842 80 6,12 3,3472 31,3477375 0,242 24888 0,344 95264 8 14,525 1,38 117,1528 0,0424 2480,888 0,3444 <</td><td>31099 2 125,778 3,3,65 322,73 12,789 17,789 17,789 77,8490 0,0022 0,0683 31738 2 93,000 3,55 322,1 17,789 102,0072 0,0683 31738 2 93,000 3,55 342,1 17,89 102,0072 0,0623 31738 3 79,216 3,55 44,57 22,45 152,7273 0,0074 0,0033 31731 1 79,216 3,55 44,77 22,175 46,6673 0,0076 0,0633 31221 1 75,525 3,45 27,47 21,75 47,6771 0,0076 0,0633 21814 24 33,032 0,81 2,45,2 2,48 586,5120 0,0178 0,0633 30805 4 27,656 0,31 3,1987875 78714 28,381,208 0,0182 0,0633 30805 4 27,656 0,31 3,1987875 78714 28,381,208 0,0483 0,048</td><td>3,099 2 126,768 3,8,45 28,799 33,44 57,5878 0,0002 0,0683 74,50 3,187 2 98,090 3,845 39,21 37,28 74,80 0,0025 0,0683 74,50 3,1738 2 98,080 4,1 55,40 28,14 102,092 0,0125 0,0683 79,52 3,1738 3 79,216 3,65 46,67 21,27 0,050 0,0683 79,52 3,1738 1 77,525 4,1 55,46 22,46 53,57 0,0005 0,0683 79,50 3,182 1 75,525 3,45 47,70 2,1,76 91,7650 0,0076 0,0633 74,50 2,114 2,4 3,032 0,41 2,4,52 2,48 50,007 0,0633 76,50 2,114 2,4 3,2,812 2,964,4025 117,1,528 0,0616 0,0633 76,50 3,842 80 76,105 3,3987,3775 1,298309375</td><td>3.099 2 125,78 3.45 28,79 3.44 57,2878 0.092 0.0633 74,50 144,00 3.047 2 95,090 3.55 39,21 17,28 0.0623 74,50 144,00 3.073 2 95,090 3.55 39,21 37,28 0.0623 74,50 149,00 3.073 7 72,25 3.10 25,16 157,2573 0.0023 0.0633 74,50 235,76 3.173 1 76,255 4.1 53,85 46,77 21,76 46,6598 0.0074 0.0633 74,50 74,50 3.1821 1 76,525 4.1 53,85 47,77 21,76 46,7671 0.0076 0.0633 74,50 74,50 21814 24 33,032 0.81 2,452 2,48 991,7603 0.0177 0.0633 76,06 122,44 21814 24 33,032 0.81 2,468 2,964,43025 117,1538 0.0187 <t< td=""><td>31099 2 12,773 3,66 22,79 3,3,4 57,578 0,0002 0,0613 74,50 149,00 0,010 3173 2 90,006 56,5 32,21 37,99 128,40 0,0022 0,0613 74,50 149,00 0,010 3173 2 90,305 4,1 51,00 26,14 102,0092 0,0613 79,92 139,94 0,000 3173 3 74,216 3,65 46,67 21,29 0,0052 0,0613 79,92 239,56 0,100 3173 1 74,216 3,65 46,77 2,29 0,0054 0,0052 0,0613 79,92 239,56 0,100 3181 3 74,52 4,1 53,6 47,70 21,76 0,0076 0,0633 79,50 74,50 0,100 3182 1 74,52 4,6 53,577 0,0076 0,0633 74,50 0,100 3182 2 3,65 47,70 21,76 54,770 0,0076 0,0633 74,50 0,100 3182 2 3,032 0,81 2,415 2,48 585,5208 0,0163 75,65 16,076 0,0444 0,100</td><td>$\begin{array}{ c c c c c c c c c c c c c c c c c c c$</td></t<></td></td<>	3,099 2 122,778 3,66 3,487 2 96,000 3,66 3,737 2 80,305 4,1 3,781 3 76,216 4,1 3,782 3 76,226 4,1 3,783 1 76,525 3,65 3,821 1 76,525 3,65 3,821 1 76,525 3,65 3,821 1 76,525 3,65 2,214 2,4 27,985 0,45 3,842 80 2,6156 0,21 3,842 80 2,6156 0,21 4,84 2,847 0,45 3,842 9,9264 8 1,045 0,45 1,045 1,045 1,045 1,045	3,099 2 12,7/183 3,6,6 39,2,1 3,487 2 93,0,90 3,6,6 39,2,1 3,733 2 80,0,85 4,1 57,4,2 3,737 3 78,2,16 3,6,5 39,2,1 3,737 3 78,2,16 3,6,5 4,1 57,4,2 3,737 1 76,5,25 3,6,5 44,2 1,3,5,8 3,027 1 76,5,25 3,6,5 47,70 2,2114 2,4 23,0,32 0,0,1 2,4,5,2 3,842 60 2,1,1,0 0,6,1 3,2,0,1 3,842 60 2,1,0,10 0,4,1 1,5,2,5 3,9,64 8 3,3,1 0,4,5 1,3,5,25 3,9,64 8 1,3,0,1 1,3,2,23 1,3,4,5,22 3,9,64 8 1,3,3,3 1,0,4,5 1,3,5,25 3,9,64 8 1,3,4,33 1,0,4,5 1,3,5,25 3,0,64 1,4,5,22 1,4,5,23 1,4,5,23	3,099 2 125,763 3,65 28,77 33,14 3,497 2 93,090 3,65 39,21 17,89 3,173 2 80,085 4,1 53,42 26,86 3,173 2 80,085 4,1 53,42 26,86 3,173 3 78,525 3,65 44,27 26,86 3,173 76,525 3,65 47,70 21,76 3,027 1 75,525 3,65 47,70 21,76 218,4 24,353 0,45 16,0795 0,9644827 3,977 24 27,565 0,45 16,0795 0,9644827 3,924 60,26 26,020 23,202 2,464-4327 3,924 76 24,047 0,48 15,523 1,04830937 392,64 21,024 0,454 15,523 1,04830937 392,64 8 15,523 1,04830937 1,348 40,47 76 24,047 0,45 15	3,099 2 122,743 3,65 28,79 13,144 3,487 2 94,090 3,65 39,21 17,89 3,733 2 85,0345 4,1 31,00 26,14 3,733 3 742,15 3,65 46,67 21,39 3,733 742,15 3,65 46,67 21,39 3,733 742,215 3,65 47,70 21,76 3,121 74,525 3,65 47,70 21,76 21814 24 32,032 0,81 24,52 2,468 21814 24 22,062 0,81 3,1397,378 FEP-II LER av 05805 4 22,166 0,81 3,1397,378 FEP-II LER av 0547 78 24,047 0,45 19,5255 1,096309375 FEP-II LER av 059764 8 13,351 0,45 19,5255 1,384 10,455 059764 8 13,351 0,455 1,384 11,28 1,38	3,099 2 126,768 3,8,45 28,279 33,44 3,497 2 99,090 38,65 39,221 37,88 37,28 3,7373 2 99,090 3,85 39,212 37,88 37,29 3,7373 3 79,2216 3,45 39,212 25,86 31,313 3,7373 3 79,525 3,45 46,67 22,29 31,313 3,721 3,755,25 3,45 44,77,70 21,766 55 2,181,4 2,4 32,932 0,11 24,52 2,468 55 2,181,4 2,4 33,032 0,11 24,525 2,964,64025 54 5,976 2,4 7,2656 0,6,78 3,597,875 FEP-H LER exailable 5,9264 8 32,104 34,525 1,098,109375 FEP-H LER exailable 5,9264 8 32,047 0,45 19,5255 1,098,109375 FEP-H LER exailable 5,9264 8 12,0457 1,38	3,099 2 122,773 3,66 28,79 3,3,14 57,527 3,187 2 90,000 3,65 32,21 37,89 78,418 3,173 2 90,305 4,1 51,00 26,14 102,029 3,173 3 78,216 3,65 34,21 25,86 152,257 3,173 3 78,216 3,65 4,677 21,79 46,657 3,173 1 76,525 3,45 4,677 21,76 53,577 22077 1 76,525 3,85 47,70 21,76 500 47,6077 21814 2,4 33,032 0,81 2,452 2,48 588,505 588,505 3805 4 27,666 0,81 3,19878375 PEP-41 LER available 388,515 388,515 3842 80 2,612 0,681 1,31,31,31,319873377 PEP-41 LER available 152,287 59264 8 1,8,51 0,65 1,0982,93757 PEP-41	31099 2 126,768 3,8,6 28,79 33,14 57,5878 0,0002 31497 2 99,090 38,65 39,21 37,28 77,28 77,28 0,0012 31738 2 99,090 3,45 39,21 37,28 102,092 0,0012 31738 3 78,216 3,45 34,07 21,28 137,273 0,0030 31731 3 79,216 3,45 44,67 21,278 44,6658 0,0012 31721 3 75,525 4,1 55,36 27,46 588,575 0,0016 21814 24 33,012 0,41 24,52 2,48 991,963 0,177 9776 24 2,2864 0,90448875 PEP-II LER available 385,520 0,0647 9842 80 6,12 3,3472 31,3477375 0,242 24888 0,344 95264 8 14,525 1,38 117,1528 0,0424 2480,888 0,3444 <	31099 2 125,778 3,3,65 322,73 12,789 17,789 17,789 77,8490 0,0022 0,0683 31738 2 93,000 3,55 322,1 17,789 102,0072 0,0683 31738 2 93,000 3,55 342,1 17,89 102,0072 0,0623 31738 3 79,216 3,55 44,57 22,45 152,7273 0,0074 0,0033 31731 1 79,216 3,55 44,77 22,175 46,6673 0,0076 0,0633 31221 1 75,525 3,45 27,47 21,75 47,6771 0,0076 0,0633 21814 24 33,032 0,81 2,45,2 2,48 586,5120 0,0178 0,0633 30805 4 27,656 0,31 3,1987875 78714 28,381,208 0,0182 0,0633 30805 4 27,656 0,31 3,1987875 78714 28,381,208 0,0483 0,048	3,099 2 126,768 3,8,45 28,799 33,44 57,5878 0,0002 0,0683 74,50 3,187 2 98,090 3,845 39,21 37,28 74,80 0,0025 0,0683 74,50 3,1738 2 98,080 4,1 55,40 28,14 102,092 0,0125 0,0683 79,52 3,1738 3 79,216 3,65 46,67 21,27 0,050 0,0683 79,52 3,1738 1 77,525 4,1 55,46 22,46 53,57 0,0005 0,0683 79,50 3,182 1 75,525 3,45 47,70 2,1,76 91,7650 0,0076 0,0633 74,50 2,114 2,4 3,032 0,41 2,4,52 2,48 50,007 0,0633 76,50 2,114 2,4 3,2,812 2,964,4025 117,1,528 0,0616 0,0633 76,50 3,842 80 76,105 3,3987,3775 1,298309375	3.099 2 125,78 3.45 28,79 3.44 57,2878 0.092 0.0633 74,50 144,00 3.047 2 95,090 3.55 39,21 17,28 0.0623 74,50 144,00 3.073 2 95,090 3.55 39,21 37,28 0.0623 74,50 149,00 3.073 7 72,25 3.10 25,16 157,2573 0.0023 0.0633 74,50 235,76 3.173 1 76,255 4.1 53,85 46,77 21,76 46,6598 0.0074 0.0633 74,50 74,50 3.1821 1 76,525 4.1 53,85 47,77 21,76 46,7671 0.0076 0.0633 74,50 74,50 21814 24 33,032 0.81 2,452 2,48 991,7603 0.0177 0.0633 76,06 122,44 21814 24 33,032 0.81 2,468 2,964,43025 117,1538 0.0187 <t< td=""><td>31099 2 12,773 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Name	B(T)	N	L(m)	ρ(m)	α (mrad)	Sagitta(mm)	E (GeV)	6,7		Total & (mrad)	Fraction 2*m	Gap (m)	Unit Cost (k€)	Total Cost (k€))	Gap (m)	Unit Cost (k€)	Total Cost (k€)
BOSL	0,067	1	2,8	333,710	8,391	2,937				8,3905	0,0013	0,0600	84,85	84,85	0,100	129,29	129,29
B2BL	0,077	2	4,1	288,282	14,222	7,289				28,4444	0,0045	0,0600	108,16	216,32	0,100	166,10	332,20
B1DR	0,084	1	3,65	266,873	13,677	6,240				13,6769	0,0022	0,0600	100,50	100,50	0,100	153,95	153,95
B2AR	0,087	2	4,1	256,333	15,995	8,197				31,9896	0,0051	0,0600	108,16	216,32	0,100	166,10	332,20
BOSR	0,091	1	2,8	245,141	11,422	3,998				11,4220	0,0018	0,0600	84,85	84,85	0,100	129,29	129,29
BOAL	0,101	3	4,1	220,053	18,632	9,549				55,8957	0,0089	0,0600	108,16	324,48	0,100	166,10	498,30
B1DL	0,113	1	3,65	197,023	18,526	8,452				18,5258	0,0029	0,0600	100,50	100,50	0,100	153,95	153,95
B1BL	0,115	2	4,1	193,647	21,173	10,851				42,3452	0,0067	0,0600	108,16	216,32	0,100	166,10	332,20
BOR	0,138	5	4,1	161,649	25,364	12,999				126,8180	0,0202	0,0600	108,16	540,80	0,100	166,10	830,50
B2BR	0,147	2	4,1	151,932	26,986	13,830				53,9714	0,0086	0,0600	108,16	216,32	0,100	166,10	332,20
B1BR	0,157	2	4,1	142,251	28,822	14,771				57,6444	0,0092	0,0600	108,16	216,32	0,100	166,10	332,20
B1CL	0,176	2	3,65	126,759	28,795	13,138				57,5894	0,0092	0,0600	100,50	201,00	0,100	153,95	307,90
B1AR	0,240	2	3,65	93,116	39,198	17,884				78,3966	0,0125	0,0600	100,50	201,00	0,100	153,95	307,90
BHER2	0,257	24	1,4	87,066	16,080	2,814				385,9152	0,0614	0,0600	55,52	1332,48	0,100	83,56	2005,44
BHER1	0,257	78	1,7	87,066	19,526	4,149				1522,9890	0,2424	0,0600	62,34	4862,52	0,100	94,20	7347,60
BHER	0,257	40	5,4	87,066	62,022	41,865		PEP-II HER	available	2480,888	0,394845588	0,06	129,57	5182,80	0,100	200,17	8006,80
BHERS	0,257	16	4,27	87,066	49,044	26,177				784,6960	0,1249	0,0600	110,82	1773,12	0,100	170,26	2724,16
B3L	0,278	2	4,1	80,386	51,004	26,139				102,0076	0,0162	0,0600	108,16	216,32	0,100	166,10	332,20
B3R	0,284	2	4,1	78,630	52,143	26,723				104,2856	0,0166	0,0600	108,16	216,32	0,100	166,10	332,20
B4L	0,286	1	4,1	78,217	52,418	26,864				52,4183	0,0083	0,0600	108,16	108,16	0,100	166,10	166,10
B5L	0,286	1	3,65	78,217	46,665	21,291				46,6651	0,0074	0,0600	100,50	100,50	0,100	153,95	153,95
B5R	0,292	1	3,65	76,509	47,707	21,766				47,7071	0,0076	0,0600	100,50	100,50	0,100	153,95	153,95
B4R	0,292	1	4,1	76,509	53,589	27,464				53,5888	0,0085	0,0600	108,16	108,16	0,100	166,10	166,10
BHERJ	0,319	2	4,1	69,994	58,577	30,020				117,1530	0,0186	0,0600	108,16	216,32	0,100	166,10	332,20
		194							Total	6283,4236	1,0000			16936,78			25892,78



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QDMFF0

QDM51

QD11L

OD11R

QFRSR3

QDMFFOL

QDMFF2L

QFMFF2L

QFMFF2

QFMFF1L

QFBJ

QDOBR

QF1R

QFMFF1

18,41

18,84

18,91

18.91

19,55

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21,30

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Name	G (T/m)	N	L (m)	E (GeV)	6,7	Bore Radius (m	Unit Cost (k€)	Cost (k€)		Bore Radius (m)	Unit Cost (k€	Cost (k€)		
QFMFF5	0,78	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		Low Gradient Type
QDMFF4L	0,85	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		High Gradient Type
QDMFF6L	1,03	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		PEPII Available
QDMFF4	1,15	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		Special Type
QFMFF5L	1,75	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52	1	22
QD2R	1,82	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QD2L	1,82	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QDMFF6	1,88	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52	1	
QFMFF7	4,27	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QFMFF7L	5,09	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QDMFF8	6,63	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		7/13
QD9R	7,16	2	0,30			0,03	17,01	34,02		0,05	31,52	63,04		
QDMFF8L	7,20	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QFMFF3L	11,22	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		743
QFMJ	11,27	2	0,30			0,03	17,01	34,02		0,05	31,52	63,04		
QFMFF3	11,48	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QD16L	12,95	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52	3	7/13
QD16R	12,96	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QFSL	14,51	6	0,30			0,03	17,01	102,06		0,05	31,52	189,12		
QFPI	14,51	6	0,30			0,03	17,01	102,06		0,05	31,52	189,12		7/ 3
QFPIS	14,52	4	0,30			0,03	17,01	68,04		0,05	31,52	126,08		
QF	14,58	14	0,30			0,03	17,01	238,14		0,05	31,52	441,28		
QFSLL	15,05	6	0,30			0,03	17,01	102,06		0,05	31,52	189,12		7/13
QFPIL	15,08	6	0,30			0,03	17,01	102,06		0,05	31,52	189,12		
QFJ	15,09	2	0,30			0,03	17,01	34,02		0,05	31,52	63,04		() () () () () () () () () ()
QFL	15,17	12	0,30			0,03	17,01	204,12		0,05	31,52	378,24		7/3
QDMS2	15,64	2	0,15			0,03	11,08	22,16		0,05	20,77	41,54		
QD4R	15,69	1	0,30			0,03	17,01	17,01		0,05	31,52	31,52		
QD4L	15,69	1	0,30	80		0,03	17,01	17,01	1348,94	0,05	31,52	31,52	2500,1	- 7/13



Name	G (T/m)	N	L (m)	E (GeV)	6,7	Bore Radius (m)	Unit Cost (k.	Cost (kf)	Bore Radius (m) U	nit Cost (k€)	Cost (k€)		
QF10R	16,31	-4	0,15			0,03	17,13	68,52	0,05	31,95	127,80		Low Gradient Type
QFBR	16,38	1	0,30			0,03	26,14	26,14	0,05	48,72	48,72		High Gradient Type
QFBL	16,39	1	0,30			0,03	26,14	26,14	0,05	48,72	48,72		PEPII Available
QDMJ	16,43	2	0,30			0,03	26,14	52,28	0,05	48,72	97,44	C (1)	Special Type
QDM2L	17,00	6	0,50			0,03	35,67	214,02	0,05	66,68	400,08	-	
QDM2	17,24	7	0,50			0,03	35,67	249,69	0,05	66,68	466,76		
QDM	17,38	3-6	0,50			0,03	35,67	499,38	0,05	66,68	933,52		
QDP1	17,54	G	0,30			0,03	26,14	156,84	0,05	48,72	292,32	2415,36	
QD	17,67	14	0.30			0.03	26,14	365,96	0.05	48,72	682,08		
ODML	17.69	12	0.50			0.03	35.67	428.04	0.05	66.68	800.16		
QDPIL	17,99	G	0,30			0.03	26,14	156.84	0.05	48,72	292,32		
ODL	18.02	12	0.30			0.03	26.14	313.68	0.05	48.72	584.64		
QDSL.	18,11	6	0.30			0,03	26,14	156,84	0.05	48,72	292,32		
ODPIS	18.18	4	0.30			0.03	26.14	104.56	0.05	48.72	194.68		
QFI	18,22	-4	0.30			0.03	26,14	104.56	0.05	48,72	194.88		
ODMFF2	18.26	1	0.30			0.03	26.14	26.14	0.05	48.72	48.72		
QDSLL	18,52	6	0.30			0,03	26,14	156,84	0.05	48,72	292,32		
ODMI 1	18.63	6	0.50			0.03	35.67	214.02	0.05	66.69	400.08		
ODI	18.71	a	0.30			0.03	26.14	78.42	0.05	48.72	146.16		
0.01	19.71	2	0.15			0.03	17.13	24.26	0.05	31.95	63.90		
CODMINE 11	10.74	6	0.50			0.03	35.67	214.02	0.05	66.69	400.08	1	
0071	18.79		0.15			0.03	17.15	17.13	0.05	31.95	31.05		
OD7R	18.79	4	0.15			0,03	17,13	17.13	0.05	31.95	31.95		
001	10.11	-	0.30		1	0,03	26.14	52.20	0.05	40.77	07.44		
ODMEEZI	19.67	1	0,30			0.03	26.14	26.14	0.05	49.72	48 72		
OD1454	20.52		0.00			0.03	20.24	62.20	0.05	40.77	07.44		
OFMS1	20,53		0,30			0,03	26,14	52,28	0,05	40.72	97,44		
OFRI	22,40		0,10			0,03	20,23	420.04	0,05	66,74	000.10	-	
OFR	22,10	12	0,50			0,03	35,67	400.30	0,05	66,68	033.53		
CODED	22,40	1.4	0,10			0,03	37.37	17.12	0,05	24.05	21.05		
CODER	22,00		0,15			0,03	17,13	17.13	0,05	31,99	31,95		
CELOUL	22,40		0,10			0,03	26.14	25.24	0,05	40,72	40,72		
CQY AR	22,48	1	0,30			0,03	20,14	26,14	0,05	48,72	48,72	-	
CLVAL	22,48	1	0,10			0,04	20,14	20,14	0,05	48,72	438,72		
CIX2R	22,57	2	0,10			0,04	20,14	52,28	0,05	48,72	97,44		
QDSL1	22,18	62	0,50			0,04	35,67	214,02	0,05	tete, tett	400,08	2	
QYZR	22,78		0,10			0,03	20,14	104,56	0,05	48,72	194,88	-	
CD3L1L	22,79		0,50			0,03	35,67	214,02	0,05	66,68	400,08		
CIXIR	22,93	2	0,30			0,03	26,14	52,28	0,05	48,72	.97,44		
CIXII.	22,93	4	0,30			0,04	20,14	52,28	0,0%	-916,72	97,44		
CIF12R	22,94	1	0,15			0,03	17,13	17,13	0,05	31,95	31,95		
QF12L	22,96	1	0,15			0,03	17,13	17,13	0,05	31,95	31,95		
QF17R	23,61	2	0,30			0,03	26,14	52,28	0,05	48,72	97,44		
QFSR	23,85	2	0,30			0,03	26,14	52,28	0,05	48,72	97,44	-	
QXOL	23,98	2	0,15			0,03	17,13	34,26	0,05	31,95	63,90		
QXOR	23,99	2	0,15			0,03	17,13	34,26	0,05	31,95	63,90		
QY1R	24,07	2	0,15			0,03	17,13	34,26	0,05	31,95	63,90		
QVIL	24,09	2	0,15			0,03	17,13	34,26	0,05	31,95	63,90		
QDIBR	24,30	1	0,15		-	0,03	17,13	17,13	0,05	31,95	31,95		
COLBL	24,30	1	0,15			0,03	17,13	17,13	0,05	31,95	31,95		
QFBPI	24,70	6	0,50		1	0,03	35,67	214,02	0,05	66,68	400,08	1	
QFBPIL	25,01	G	0,50			0,03	35,67	214,02	0,05	66,68	400,08		
QFMFF1	25,30	1	0,20			0,03	26,14	26,14	0,05	48,72	48,72		
QD14R	25,83	1	0,30			0,03	26,14	26,14	0,05	48,72	48,72		
QD14L	25,83	1	0,30			0,03	26,14	26,14	0,05	48,72	48,72		
QFM	25,91	1.4	0,50			0,03	35,67	499,38	0,05	66,68	933,52		
Q.F.ML	26,18	12	0,50			0,03	35,67	428,04	0,05	66,68	800,16		
QFSL2L	26,35	G	0,30			0,03	26,14	156,84	0,05	48,72	292,32		
QFMFF1L	26,48	1	0,30			0,03	26,14	26,14	0,05	48,72	48,72		
QFSL2	26,65	G	0,30			0,03	26,14	156,84	0,05	48,72	292,32		
QFBSL	26,77	G	0,50			0,03	35,67	214,02	0,05	66,68	400,08		
QF13R	26,90	1	0,15			0,03	17,13	17,13	0,05	31,95	31,95	0	
QF13L	26,92	1	0,15			0,03	17,13	17,13	0,05	31,95	31,95		
QFML2L	26,93	3	0,50			0,03	35,67	107,01	0,05	66,68	200,04		
QFML2	27,03	3	0,50			0,03	35,67	107,01	0,05	66,68	200,04		
QFBSLL	27,08	6	0,50			0,03	35,67	214,02	0,05	66,68	400,08		
QFBJ	27,26	2	0,50			0,03	35,67	71,34	0,05	66,68	133,36		
QF15R	28,17	2	0,50			0.03	35,67	71,34	0.05	GG,GR	133,36		
QD118	30,31	1	0,30			0.03	26,14	26,14	0.05	48,72	48,72		
QD11L	30,31	1	0,30			0.03	26,14	26,14	0.05	48,72	48,72		





L.E.R. Sextupoles (ANKA Type)

Name	G (T/m2)	N	L (m)	E (GeV)	4,18	Bore Radius (m)	Unit Cost (k€)	Cost (k€)	K(m-2)	E (GeV)		Bro	d^2B/dx^2	S
CRABR	0,0	2	0,175			0,03	22,2	44,4	0,00		4,18	13,93333	0	0
SD1_INJ2	7,9	2	0,3			0,03	28,2	56,4	0,17		4,18	13,93333	7,895555556	3,947778
SFXOR	32,7	2	0,35			0,03	30,2	60,4	0,82		4,18	13,93333	32,64380952	16,3219
SDYOR	49	2	0,25			0,03	26	52	0,89		4,18	13,93333	49,60266667	24,80133
SF1	56	1	0,15			0,03	21	21	0,61		4,18	13,93333	56,66222222	28,33111
SF1	56	26	0,3			0,03	28,2	733,2	1,21		4,18	13,93333	56,1977778	28,09889
SD1	63	53	0,3			0,03	28,2	1494,6	1,36		4,18	13,93333	63,16444444	31,58222
SF_INJ	72	1	0,15			0,03	21	21	0,77		4,18	13,93333	71,52444444	35,76222
SDY2L	98	2	0,275			0,03	27,1	54,2	1,93		4,18	13,93333	97,78666667	48,89333
SF1_INJ2	101	2	0,15			0,03	21	42	1,09		4,18	13,93333	101,2488889	50,62444
SFX2L	110	2	0,35			0,03	30,2	60,4	2,77		4,18	13,93333	110,272381	55,13619
SFX1R	113	2	0,35			0,03	30,2	60,4	2,83		4,18	13,93333	112,6609524	56,33048
SDY1R	133,0841	2	0,275			0,03	27,1	54,2	2,63		4,18	13,93333	133,2533333	66,62667
SD_INJ	139,3333	1	0,3			0,03	28,2	28,2	3,00		4,18	13,93333	139,3333333	69,66667
		100						2782,4						

H.E.R. Sextupoles (ANKA Type)

Name	G (T/m2)	N	L (m)	E (GeV)	6,7	Bore Radius (m)	Unit Cost (k€)	Cost (k€)	K(m-2)	E (GeV)		Bro	d^2B/dx^2	S
CRABR	0,0	2	0,175			0,03	22,2	44,4	0		6,7	22,33333		0 0
SFXOR	52,5	2	0,35			0,03	30,2	60,4	0,82		6,7	22,33333	52,32380952	26,1619
SF_INJ	53,9	1	0,15			0,03	21	21	0,36	i	6,7	22,33333	53,6	26,8
SD_INJ	73,1	1	0,3			0,03	28,2	28,2	0,98		6,7	22,33333	72,9555556	36,47778
SF1	75,4	26	0,3			0,03	28,2	733,2	1,01		6,7	22,33333	75,18888888	37,59444
SF1L	75,4	3	0,15			0,03	21	63	0,51		6,7	22,33333	75,9333333	37,96667
SDYOR	79,3	2	0,25			0,03	26	52	0,89		6,7	22,33333	79,50666667	39,75333
SD1	88,9	55	0,3			0,03	28,2	1551	1,19		6,7	22,33333	88,58888888	44,29444
SDY1R	156,6	2	0,275			0,03	27,1	54,2	1,93		6,7	22,33333	156,7393939	78,3697
SFX1R	176,8	2	0,35			0,03	30,2	60,4	2,77		6,7	22,33333	176,752381	88,37619
SFX2L	180,8	2	0,35			0,03	30,2	60,4	2,83		6,7	22,33333	180,5809524	90,29048
SDY2L	213,3	2	0,275			0,03	27,1	54,2	2,63		6,7	22,33333	213,5878788	106,7939
		100						2782.4						

APPENDIX C

RINGS MAGNETS COST EVALUATION USING AN ANALYTICAL APPROACH

P.Fabbricatore

Presentation given

At 3rd SuperB meeting LNF March 19-23







LAB Magnet cost estimate P.Fabbricatore INFN Genova 3nd SuperB Collaboration meeting @INFN-LNF



Parameters for cost evaluation

Materials subdivided into magnetic steel (lamination 1 mm thick were considered for all the magnets), conductor (copper conductor with hole for cooling), insulations (conductor and ground insulation), stiffening structures (longitudinal plates and end yoke flanges), other mechanical components (bolts, rods,), hydraulic circuit with manifolds, alignment components, other materials.

Engineering for constructive design . Indeed I am supposing that the engineering design is done by CabibboLab at level of engineering drawings, not yet at executive level. The constructive drawings are done by the industry as well as the design of the tooling, the material and components procurement and the definition of the constructive methods and the list of tests and controls. (Built under specification)



CABIBBO LAB Magnet cost estimate

P.Fabbricatore INFN Genova

3nd SuperB Collaboration meeting @INFN-LNF



Cost of dedicated tooling: winding line, impregnation mold, blanking devices for the lamination, assembly and heat treatment of lamination, assembly tools

Cost of generic tooling. tool usable for all magnets such as autoclave, oven, magnetic measurement fixture. I have assumed the firm constructing the magnet partially has in hand this tooling and consequently the associated cost has been considered with a cut of 50%. These cost has been considered one time for all the magnets (In case of orders given to different companies this cost would increase)



CABIBBO LAB Magnet cost estimate P.Fabbricatore INFN Genova

3nd SuperB Collaboration meeting @INFN-LNF

Manpower for construction including the following operations: blanking of the lamination, assembly of lamination for forming the yoke, heat treatment of yoke for gluing the lamination, welding of stiffening plates to the yoke, winding of conductor, under vacuum impregnation of the coils, assembly of coil into the yoke, magnet finishing with mechanical, electrical and hydraulic connections, quality controls and engineering follow up. In regarding the lamination it is supposed that no fine blanking is required.

Magnetic measurements on finished magnets

INFN Leites Nutreate a Taos Nutreat		Magnet cost estin P.Fabbricatore INFN Genov	nate ^{/a}	3 nd SuperB Collaboration meeting @INFN-LNF	Superi
		Material costs			
Yo	ke lamination				-
EB	G POWERCORE 120	00-100 A	1.7€	/kg	
wi	th Stabolit 70	7			-
Со	pper tube		from	15 to 22 €/kg	
Ma	achined ARMCO pla	ates	from	12 to 17 €/kg	A COLOR
Ep	оху		7.7€	/kg	
Gla	ass		11 €/	'n	
		Manpower c	osts		
Fro	om 60 €/h to 90 €/l	n			



NFN killes Netanik di Taka Netan	Laboratori	BIBB o Nicola Cab		B Magr P.Fabbri	catore INI	t estimate FN Genova	3 nd SuperB Collaboration meeting @INFN-LNF
			HER di	oole; 68 m	nm gap		and the second s
Name	B(T)	N	L(m)	Material	Man-	Manuf.	Potential cost saving if takin
BOSL	0.067	1	2.8	33589	44689	78279	the 40 BEBIL dinales 5 4m lon
B2BL	0.077	2	4.1	95090	113177	208267	the 40 PEPH dipoles 5.4m ion
B1DR	0.084	1	3.65	42714	52470	95184	to 5100 hrs. hut
B2AR	0.087	2	4.1	95090	113177	208267	IS 5199 K€, DUT
BOSR	0.091	1	2.8	33589	44689	78279	1
BOAL	0.101	3	4.1	142635	169766	312401	packing and deliver
B1DL	0.113	1	3.65	42714	52470	95184	
B1BL	0.115	2	4.1	95090	113177	208267	replacement of AI coil with C
BOR	0.138	5	4.1	237725	282943	520668	the second state and the second state of the second state of the
B2BR	0.147	2	4.1	95090	113177	208267	coil, QA and test cost shall b
B1BR	0.157	2	4.1	95090	113177	208267	
B1CL	0.176	2	3.65	85428	104939	190368	added.
B1AR	0.240	2	3.65	85428	104939	190368	
BHER2	0.257	24	1.4	445443	764992	1210435	
BHER1	0.257	78	1.7	1698892	2700412	4399304	
BHER	0.257	40	5.4	2460028	2739520	5199548	
BHERS	0.257	16	4.27	789920	930316	1720236	
B3L	0.278	2	4.1	95090	113177	208267	
B3R	0.284	2	4.1	95090	113177	208267	
B4L	0.286	1	4.1	47545	56589	104134	
B5L	0.286	1	3.65	42714	52470	95184	
B5R	0.292	1	3.65	42714	52470	95184	
B4R	0.292	1	4.1	47545	56589	104134	
BHERJ	0.319	2	4.1	95090	113177	208267	
				0	10100000000		
Total				7039345	9115681	16155026	

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INFN Jeffinis Matasais di Tana Nachasai		Magnet cost estimate P.Fabbricatore INFN Genova	3 nd SuperB Co meeting @IN	NFN-I NF
- 1992-0 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2		LER dipole low field 2250 kg/m; 34 mag Manufacturing En Specific tooling Generic tooling Material and comp Manpower and QA Total cost (k€)/ Un	d; 100 mm gap; gnets; 3 types gineering ponents t cost (€/kg)	243 350 0 1160 2111 3864/13.0
	on de deute ver 10 d'ante l'index obtets e resource leiter 20 d'a deute ver 10 d'ante linguistre deute de la deute de	LER dipole high fie 5300 kg/m; 210 m 5300 kg/m; 210 m Manufacturing En Specific tooling Generic tooling Material and comp Manpower and QA	eld ; 100 mm gap agnets; 3 types gineering bonents \ it cost (€/kg)	405 350 0 5578 8443 14776/20.2



INFN killen Tuikask di Fleise Tuikase		LAB	Magne P.Fabbrica	et cost estimate itore INFN Genova	3 nd SuperB Colla meeting @INFN	boration N-LNF	Sup
0.25	Surface: Magnetic flux density, norm [1] Infrau: Magnetic potential, 2 composent [10], in]		Max: 0.0327 0.0327 0.0293 0.0258 0.0258 0.0224 0.0289	HER&LER sextupoles ; 60 mm bore; 170 T/m ² ; 230 A; 1133 kg/m; 200 magnets; 3 types			
0.2		1.5	0.0155 0.012 0.0086 0.0052 0.0017	Manufacturing E Specific tooling	ngineering	378 320	
0.1		1	-0.0017 -0.0052 -0.0086	Generic tooling		0	
			-0.012 -0.0155	Material and com	nponents	679	
0.05		0.5	-0.0189 -0.0774	Manpower and C	A	3693	
0	-0.1 -0.05 0 0.05 0.1	0.15 _{Min} : 2.395e-1	-0.0258 -0.0291 -0.0327 1 Min: -0.0327	Total cost (k€)/ U	nit cost (€/kg)	5070/	75



APPENDIX D VACUUM

ISSUES AND COSTS A.Clozza

Presentation given At 3rd SuperB meeting LNF March 19-23

