

# Synchronization of a Ti:Sapphire laser to the optical reference system

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on behalf of the *Laser-based Synchronization Team at DESY-Hamburg:*

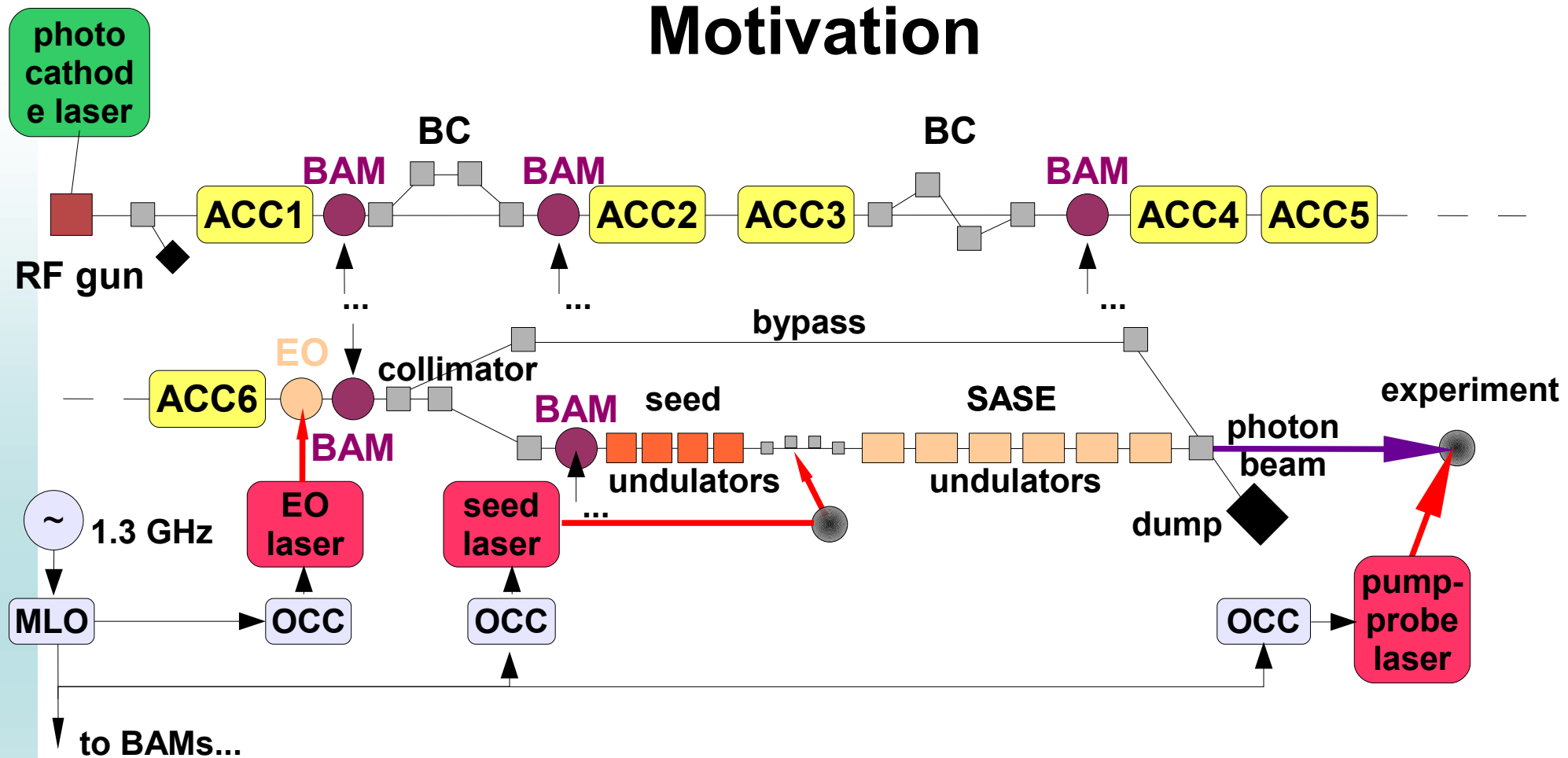
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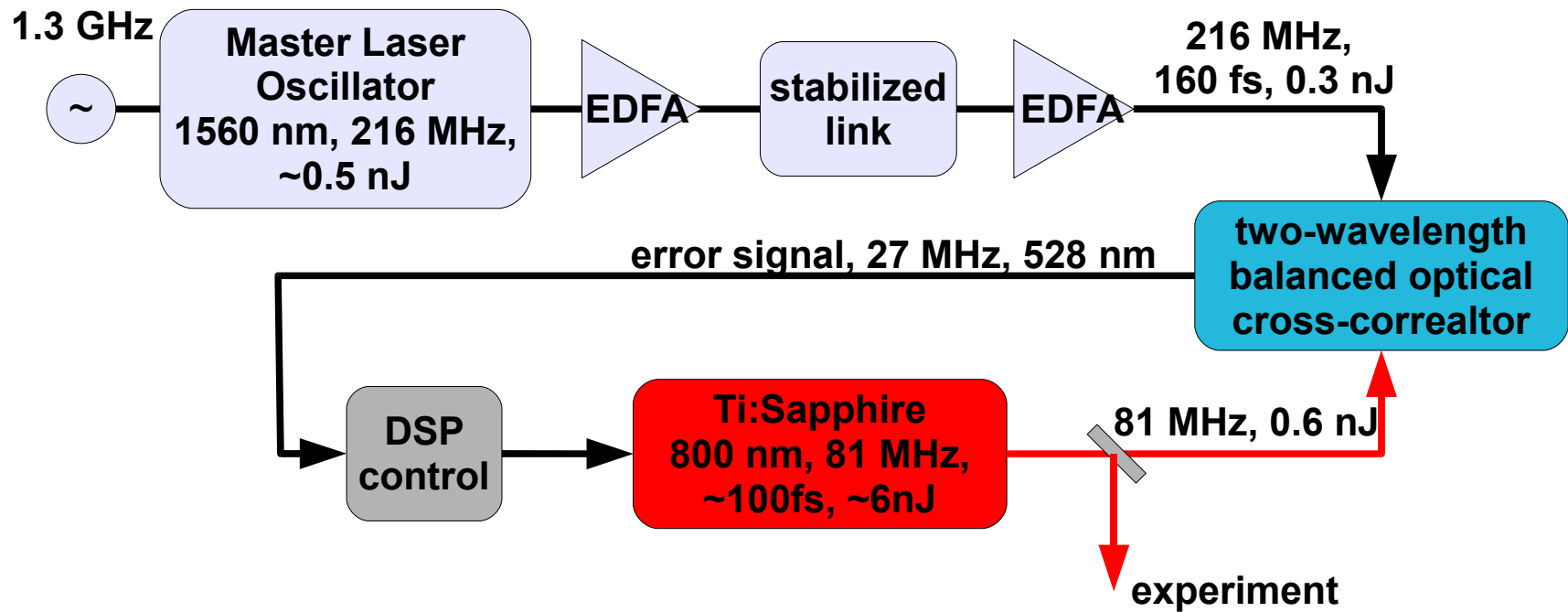


# Motivation



- Optical synchronization with beam based stabilization of the arrival time
- High precision synchronization of lasers via optical cross-correlation
- Point-to-point synchronization  $\sim 10$  fs rms
- Distribution over actively length-stabilized fiber links
- Permanent operation and long term stability

# Layout of the two-wavelength laser synchronization



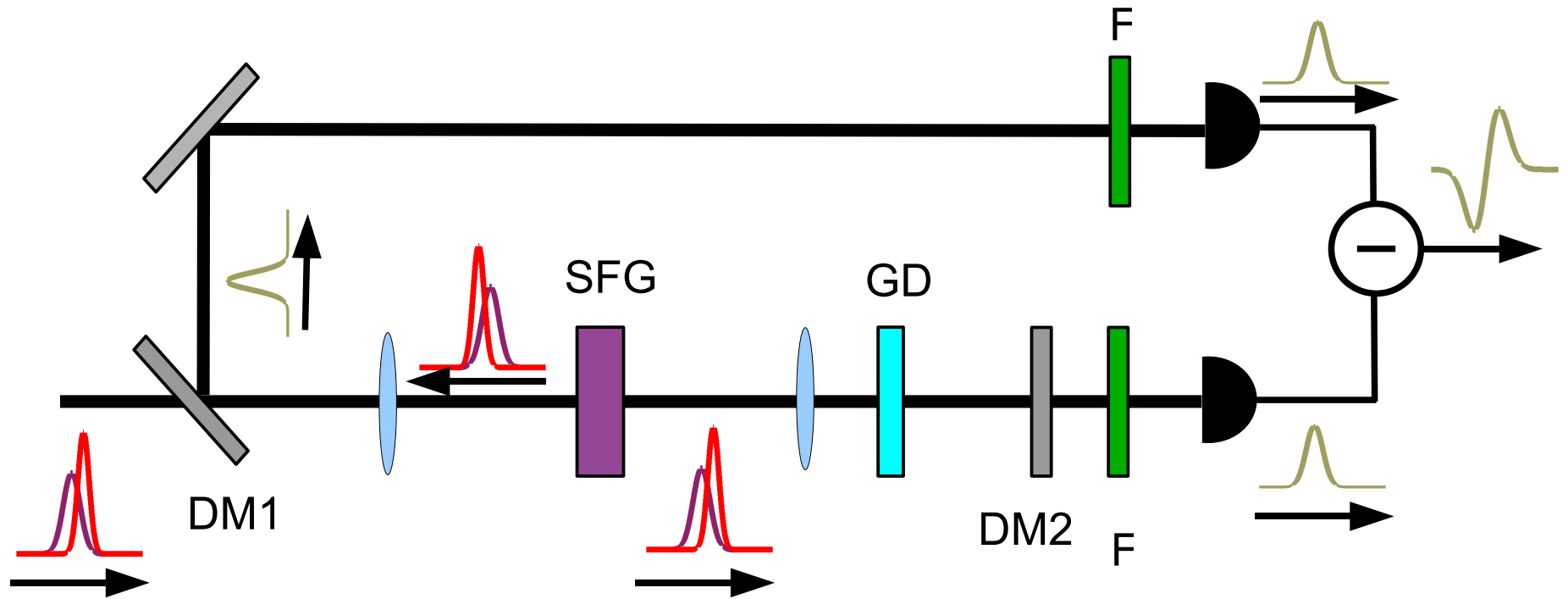
## Input in the OCC from the diagnostic laser:

$\lambda_1 = 800 \text{ nm}$ ,  $\delta\lambda_1 = \sim 60 \text{ nm}$ ,  $\tau_1 \sim 100 \text{ fs}$ ,  $P_1 \sim 50 \text{ mW}$ ,  $f_{\text{rep}} = 81 \text{ MHz}$

## Input in the OCC from the link:

$\lambda_2 = 1560 \text{ nm}$ ,  $\delta\lambda_2 = \sim 70 \text{ nm}$ ,  $\tau_2 \sim 200 \text{ fs}$ ,  $P_2 \sim 15 \text{ mW}$ ,  $f_{\text{rep}} = 216 \text{ MHz}$

# Layout of the balanced detection set-up



DM1 – dichroic mirror HT @  $\lambda_1$  and  $\lambda_2$ , HR @  $\lambda_{SF}$

DM2 – dichroic mirror HR @  $\lambda_1$  and  $\lambda_2$ , HT @  $\lambda_{SF}$

SFG – non-linear crystal, e.g. BBO

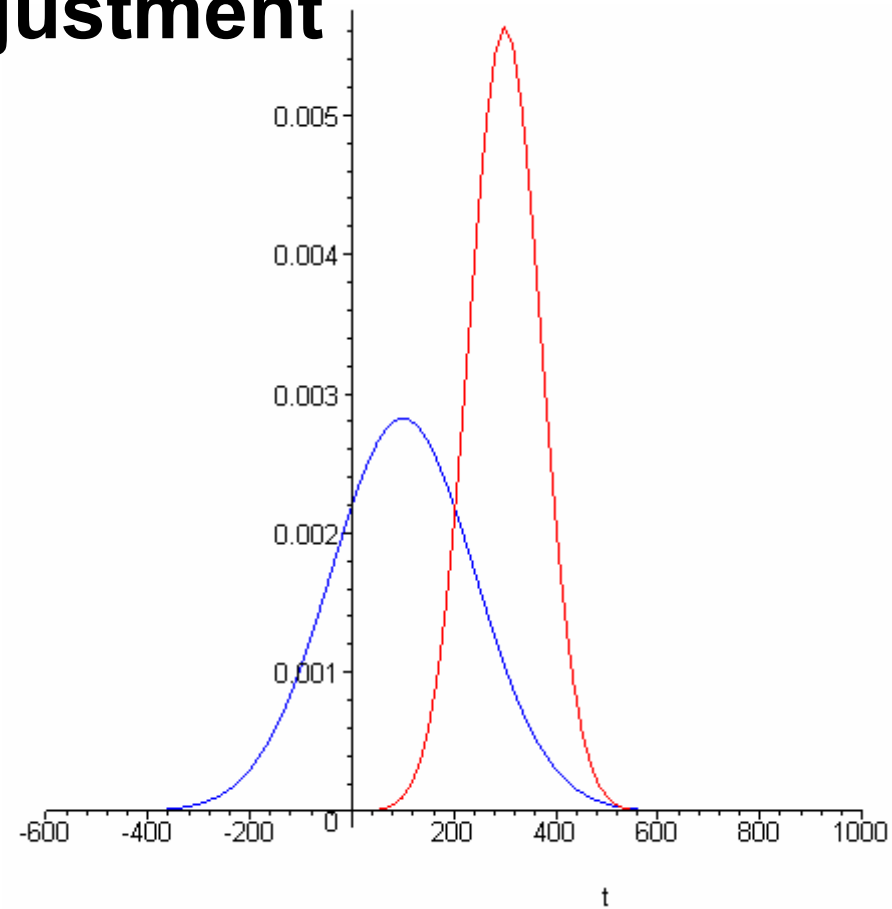
GD – group delay adjustment

F – band pass filter, HT @  $\lambda_{SF}$

# Design of the two-wavelength optical cross-correlator: group delay adjustment

Assume Gaussian pulses

$$I_i(t) = \frac{1}{\sqrt{\pi} \sigma_i} \exp\left(-\frac{(t-t_i)^2}{\sigma_i^2}\right)$$



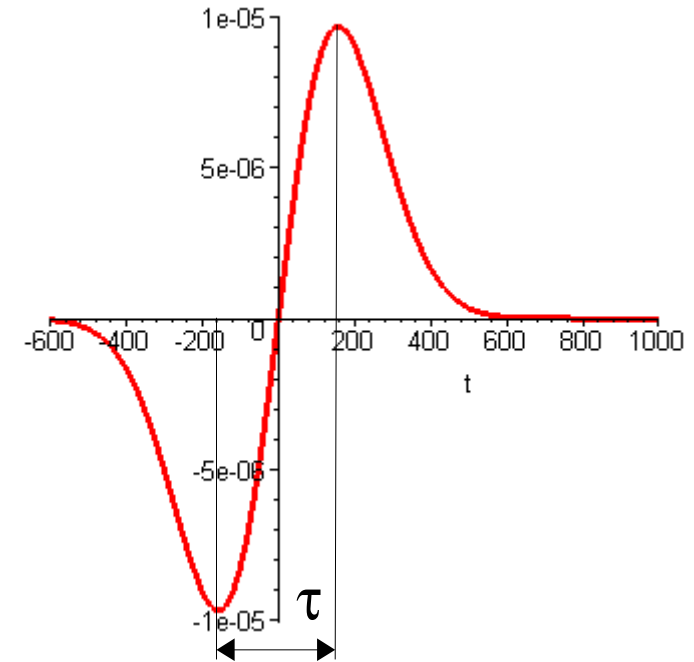
The convolution of two Gaussian pulses is also a Gaussian pulse:

$$I_i(t) = I_1 * I_2 = \int_{-\infty}^{\infty} I_1(\tau) \cdot I_2(t-\tau) d\tau = \frac{1}{\sqrt{\pi (\sigma_1^2 + \sigma_2^2)}} \exp\left(-\frac{(t-t_1-t_2)^2}{\sigma_1^2 + \sigma_2^2}\right)$$

# Design of the two-wavelength optical cross-correlator: group delay adjustment

The biggest change  $S$  in the overlap is given by the derivative of the convolution:

$$S = (I_1 * I_2)' = \frac{2(t - \tau)}{\sqrt{\pi} (\sigma_1^2 + \sigma_2^2)^{\frac{3}{2}}} \exp\left(-\frac{(t - \tau)^2}{\sigma_1^2 + \sigma_2^2}\right)$$



Delay between the extrema in terms of pulse lengths (FWHM):  $\tau = \sqrt{(\tau_1^2 + \tau_2^2) / 2 \ln(2)}$

Examples (after accounting the group velocity delays in the crystal and the lenses):

Ti:Sa + EDFA:  $\tau_1 = 100$  fs and  $\tau_2 = 200$  fs:  $\tau = 190$  fs

→ need a 65 - 80 fs additional delay: a double pass through a 2 - 3 mm silica slab

Nd:YLF + EDFA:  $\tau_1 = 11$  ps and  $\tau_2 = 200$  fs:  $\tau = 9$  ps ☺

→ if the same swapping technique is to be used: 20 cm SF66! → delay stage

# Design of the two-wavelength optical cross-correlator: choice of the crystal

Guiding criteria:

- highest possible efficiency
  - highest bandwidths
  - smallest background
- type of interaction: Type I or Type II

Parameters to calculate:

- phase matching angles
- phase and group velocities
- relative group delays
- walk-off angle
- reflection losses at the crystal surfaces
- effective non-linear coefficients
- group velocity dispersion, group delay dispersion
- chirp, pulse broadening
- effective lengths
- phase mismatch – mix acceptance bandwidth,  
mix acceptance angle, internal angular BW etc...



# Design of the two-wavelength optical cross-correlator: choice of the crystal

*Equations from:*

*Handbook of nonlinear optical crystals, Dimitriev V.G., Gurzadyan G.G., Nikogosyan D.N., Springer Series of Optical Sciences, vol 64 (1999)*

**Geometric factors:**

- phase matching
- cut angle
- crystal thickness
- focusing





# Phase matching angles for BBO

$$\lambda_1 = 1550 \text{ nm}, \lambda_2 = 800 \text{ nm}, \lambda_{\text{SFG}} = 528 \text{ nm}$$

$$\text{Type I(-)(ooe): } \Theta = 22.2^\circ$$

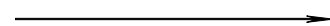
$$\text{Type II(-)(eoe): } \Theta = 27.2^\circ$$

$$\text{Type II(-)(oee): } \Theta = 38.8^\circ$$

## Phase velocities in BBO

$$V_{\text{Ph}} = c / n(\lambda, \Theta)$$

Type I(-)(ooe)



$$n(\lambda = 1550, \Theta = 0^\circ) = 1.647$$

$$n(\lambda = 800, \Theta = 0^\circ) = 1.661$$

$$n(\lambda = 528, \Theta = 0^\circ) = 1.656$$

$$n^e(\Theta) = n_o \sqrt{\frac{1 + \tan^2(\Theta)}{1 + (n_o/n_e)^2 \tan^2(\Theta)}}$$



# Group velocities in BBO

$$u_g(\lambda, \Theta) = \frac{1}{k'} = \frac{c}{\tilde{n}(\lambda, \Theta)} \quad k' = \frac{dk}{d\omega} = \frac{1}{c} \left[ n(\lambda, \Theta) - \lambda \frac{dn(\lambda, \Theta)}{d\lambda} \right]$$

**Type I(-)(ooe):**

$$\tilde{n}(\lambda = 1550, 0^\circ) = 1.671$$

$$\tilde{n}(\lambda = 800, 0^\circ) = 1.684$$

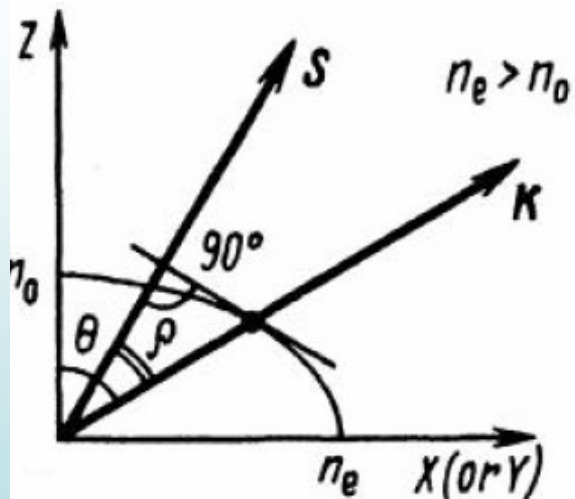
$$\tilde{n}(\lambda = 528, 22.2^\circ) = 1.702$$

**Relative group delay:**

$$\tau_g(\lambda_1, \lambda_2, \Theta_1, \Theta_2) = L_{qs} \left( \frac{1}{u_g(\lambda_1, \Theta_1)} - \frac{1}{u_g(\lambda_2, \Theta_2)} \right)$$

**Type I(-)(ooe):**  $\tau_g(\lambda_1 = 1550, \lambda_2 = 800) = -0.44 \text{ fs/mm}$

# Walk-off angles for BBO

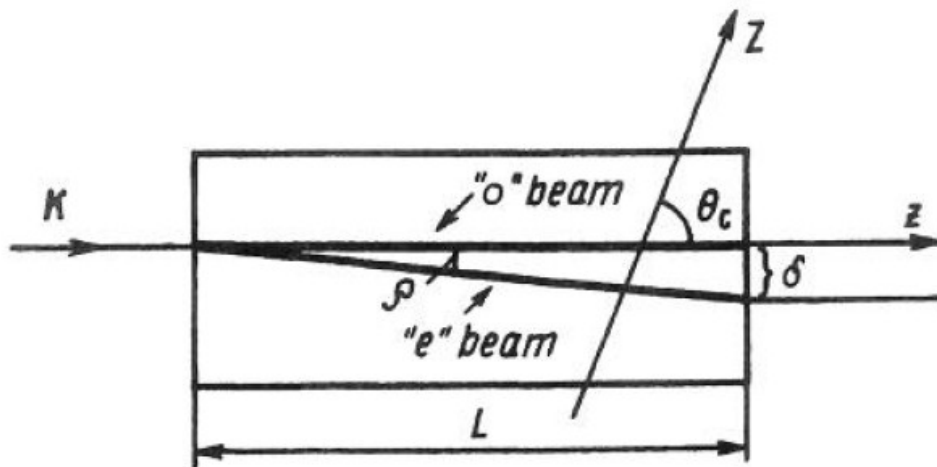


For an e-wave:

**S** – direction of propagation of the energy

**K** – direction of propagation of the phase

$$\rho(\lambda, \theta) = - \frac{1}{n_e(\lambda, \theta)} \frac{\partial n_e(\lambda, \theta)}{\partial \theta}$$



**linear walk-off:**

$$\delta = L \tan \rho$$

**Type I(-)(oee):**

$$\rho(528, 22.2^\circ) = 54.7 \text{ mrad}$$

**Type II(-)(eoe):**

$$\rho(1550, 27.2^\circ) = 61.7 \text{ mrad}$$

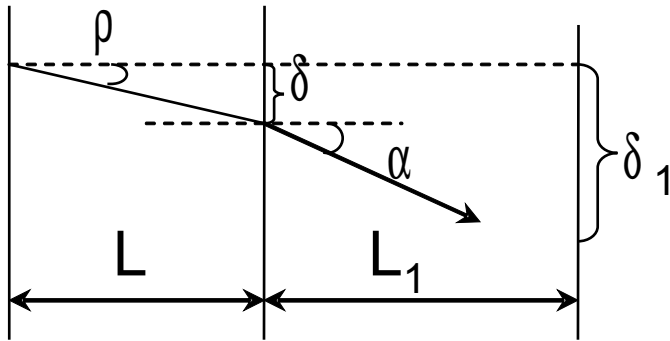
$$\rho(528, 27.2^\circ) = 62.9 \text{ mrad}$$

**Type II(-)(oee):**

$$\rho(800, 38.8^\circ) = 71.8 \text{ mrad}$$

$$\rho(528, 38.8^\circ) = 73.4 \text{ mrad}$$

# Beam walk-off



Type I(-)(ooe):  
 $\lambda = 528 \text{ nm}$ ,  
 $\Theta = 22.2^\circ$

$$\rho = 54.7 \text{ mrad}$$

$$\delta = 54.7 \text{ } \mu\text{m} / \text{mm}$$

$$\alpha = 5^\circ$$

$$\delta_1 = 100 \text{ } \mu\text{m} / \text{mm}$$

## Reflection at the crystal surface

- normal incidence
- the crystal is not coated ~6% losses
- difficult to simultaneously satisfy the requirements for high bandwidth for all three wavelengths

# Effective nonlinear coefficients $d^{eff}$ [pm/V] for point group 3m

**Type I**  $d_{ooe}^{eff} = d_{31} \sin(\theta + \rho) - d_{22} \cos(\theta + \rho) \sin(3\phi)$

**Type II**  $d_{eoe}^{eff} = d_{oeo}^{eff} = d_{22} \cos^2(\theta + \rho) \cos(3\phi)$

Available values for BBO (a negative 3m crystal) :

1) Handbook of nonlinear optical crystals, Dimitriev V.G., Gurzadyan G.G., Nikogosyan D.N., Springer Series of Optical Sciences, vol 64 (1999)

$$d_{22} = 2.3 \text{ pm/V}; d_{31} = 0.16 \text{ pm/V};$$

2) Eimerl et al, J.Appl.Phys. 62(5), pp.1968-1983 (1967)

$$d_{22} = 1.6 \text{ pm/V}; d_{31} = 0.08 \text{ pm/V}$$

3) Eckard et al, IEEE-QE, vol 26, Nr.5, pp.922-933 (1990)

$$d_{22} = 2.2 \text{ pm/V}; d_{31} = ??? \text{ pm/V}$$

4) SNLO

$$d_{22} = 2.2 \text{ pm/V}; d_{31} = 0.08 \text{ pm/V}$$

**Type I**  $d_{ooe}^{eff}(2.3 \text{ pm/V}, 0.16 \text{ pm/V}, 22.2^\circ, 528 \text{ nm}) = 2.15 \text{ pm/V}$

$$d_{ooe}^{eff}(2.2 \text{ pm/V}, 0.08 \text{ pm/V}, 22.2^\circ, 528 \text{ nm}) = 2.02 \text{ pm/V}$$

**Type II**  $d_{eoe}^{eff}(2.2 \text{ pm/V}, 27.2^\circ, 528 \text{ nm}) = 1.62 \text{ pm/V}$

$$d_{oeo}^{eff}(2.2 \text{ pm/V}, 38.8^\circ, 528 \text{ nm}) = 1.18 \text{ pm/V}$$



# Design of the two-wavelength optical cross-correlator: influence of the crystal thickness on the bandwidth (mix acceptance bandwidth)

Tables 2.20 and 2.21, *Handbook of nonlinear optical crystals*, Dimitriev V.G., Gurzadyan G.G., Nikogosyan D.N., Springer Series of Optical Sciences, vol 64 (1999)

Example: Type I (ooe) 
$$\Delta \nu_2 = \frac{0.886}{L} \left| n_{o2} - n_3^e(\theta) - \lambda_2 \frac{\partial n_{o2}}{\partial \lambda_2} + \lambda_3 \frac{\partial n_3^e(\theta)}{\partial \lambda_3} \right|^{-1}$$

Mix acceptance BW for 0.5 mm BBO

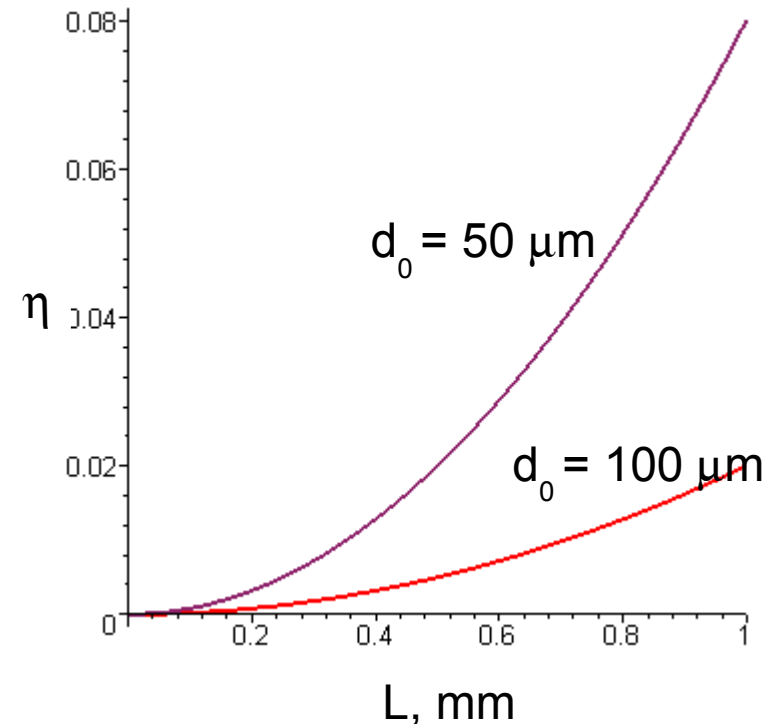
	$\lambda = 1550 \text{ nm}$	$\lambda = 800 \text{ nm}$
ooe	$\Delta\lambda = 139 \text{ nm}$	$\Delta\lambda = 65 \text{ nm}$
oeo	$\Delta\lambda = 91 \text{ nm}$	$\Delta\lambda = 161 \text{ nm}$
oeo	$\Delta\lambda = 631 \text{ nm}$	$\Delta\lambda = 35 \text{ nm}$

# Design of the two-wavelength optical cross-correlator

non-linear conversion efficiency for Type I (ooe)  
interaction between a Ti:Sa laser and EDFA

choice of the crystal thickness:

- $\eta(L) < 1$
- $L < L_{\text{eff}}$



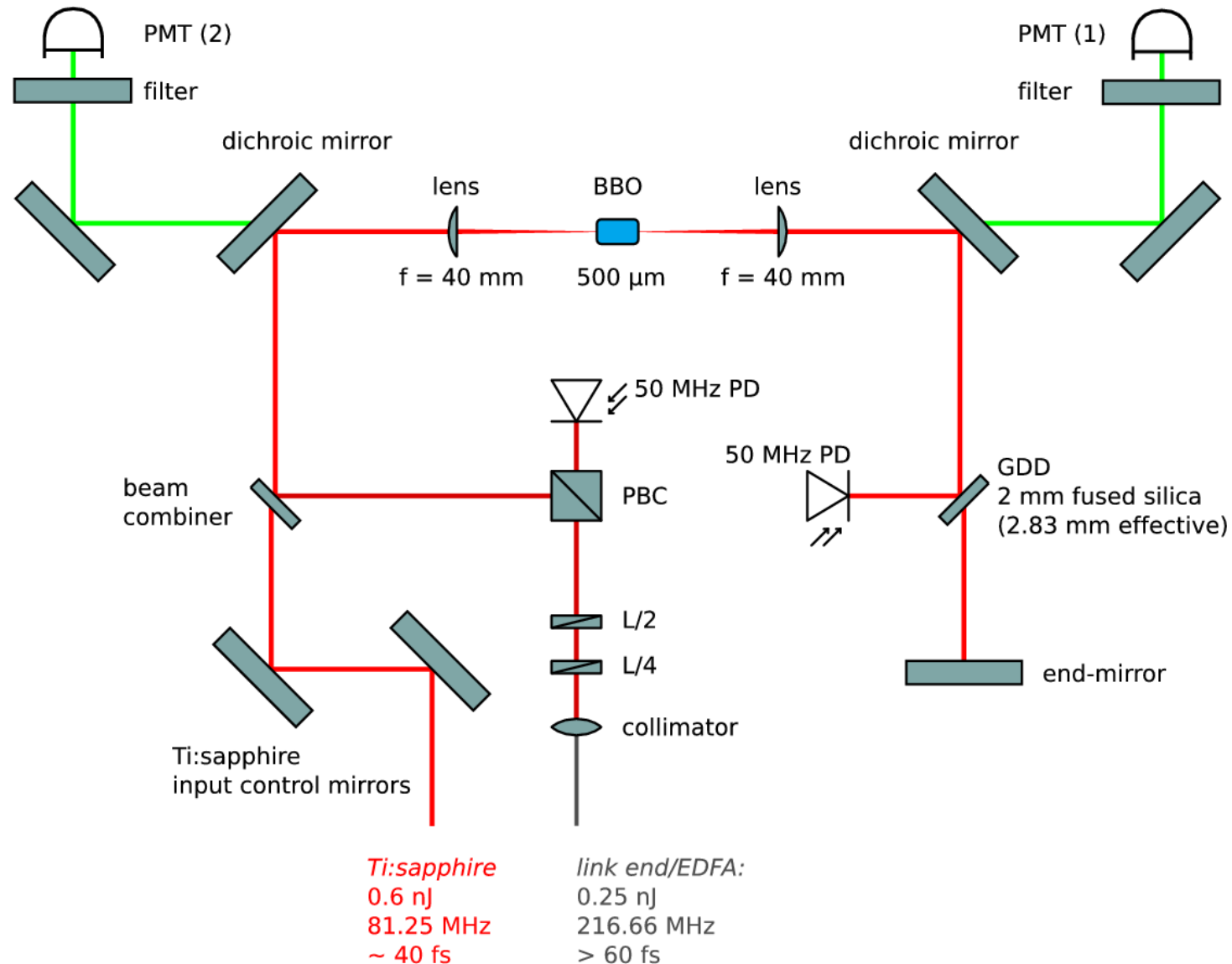
$\lambda_1 = 1550 \text{ nm}$ ,  $\tau_1 = 200 \text{ fs}$ ,  $P_1 = 15 \text{ mW}$ ,  $f_{\text{rep}} = 216 \text{ MHz}$

$\lambda_2 = 800 \text{ nm}$ ,  $\tau_2 = 100 \text{ fs}$ ,  $P_2 = 50 \text{ mW}$ ,  $f_{\text{rep}} = 81 \text{ MHz}$

→  $\eta = 2\%$  @  $d_0 = 50 \mu\text{m}$ ,  $L_{\text{BBO}} = 0.5 \text{ mm}$

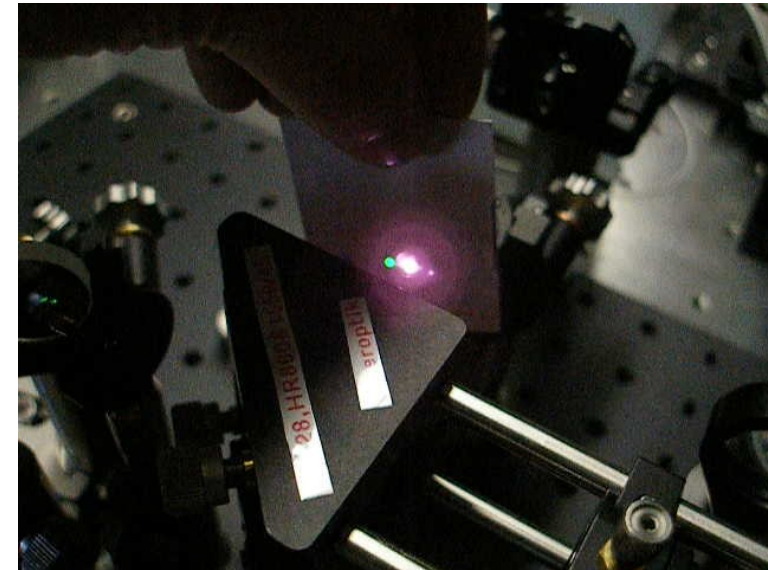
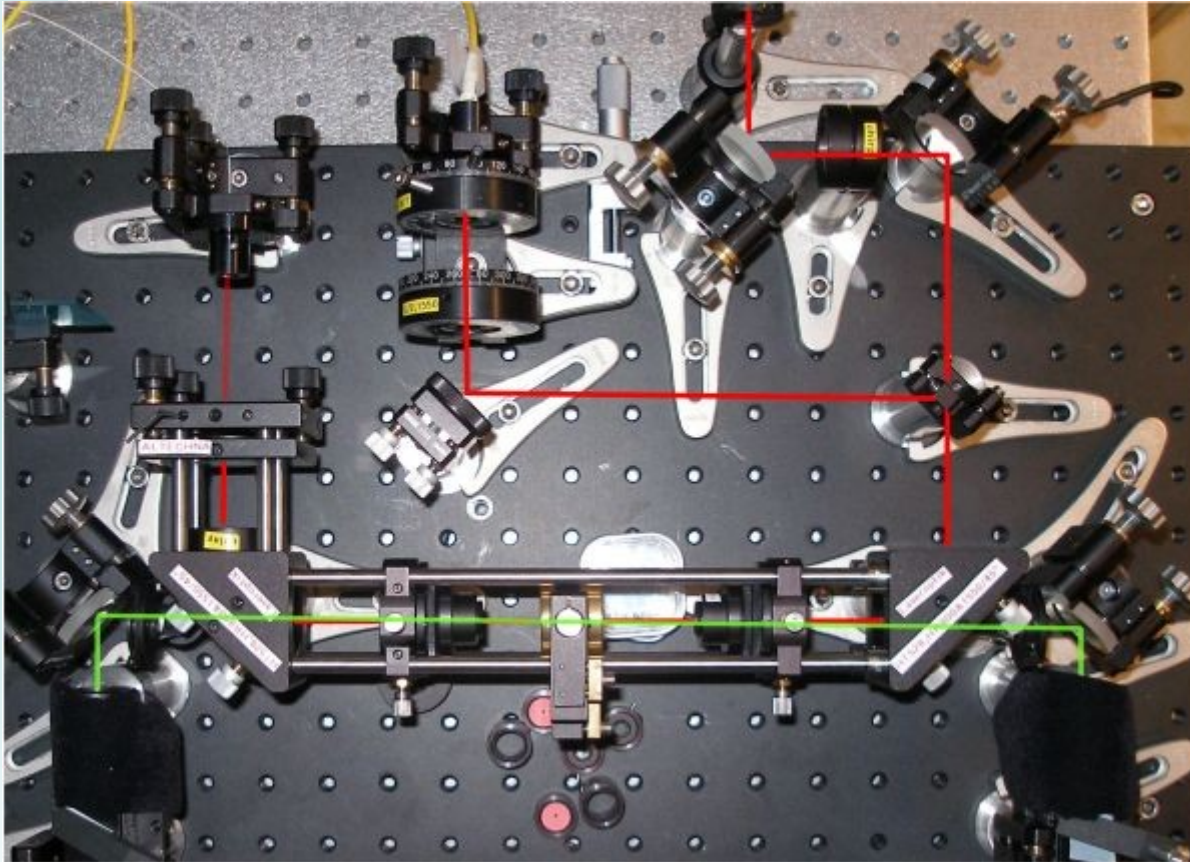
→  $\eta = 0.5\%$  @  $d_0 = 100 \mu\text{m}$ ,  $L_{\text{BBO}} = 0.5 \text{ mm}$

# Layout of the two-wavelength OCC for Ti:Sapphire+EDFA

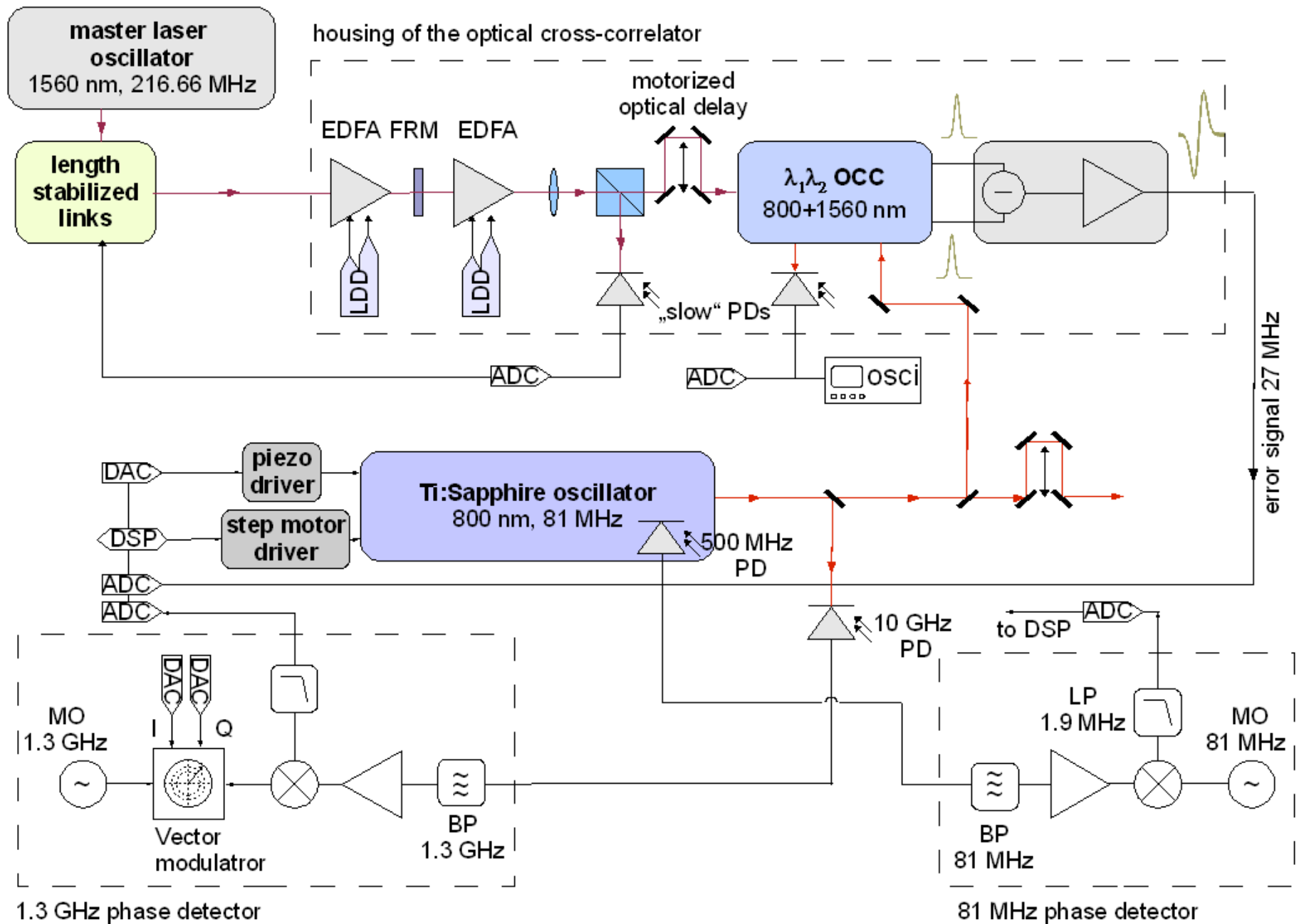




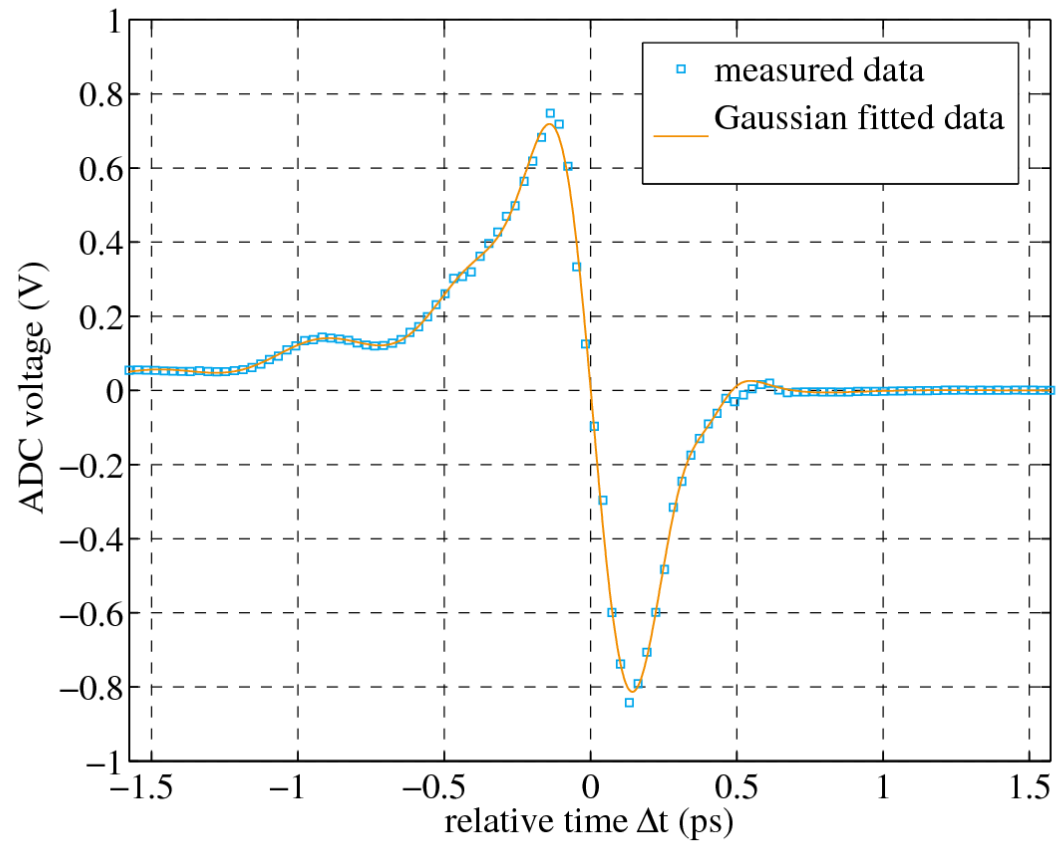
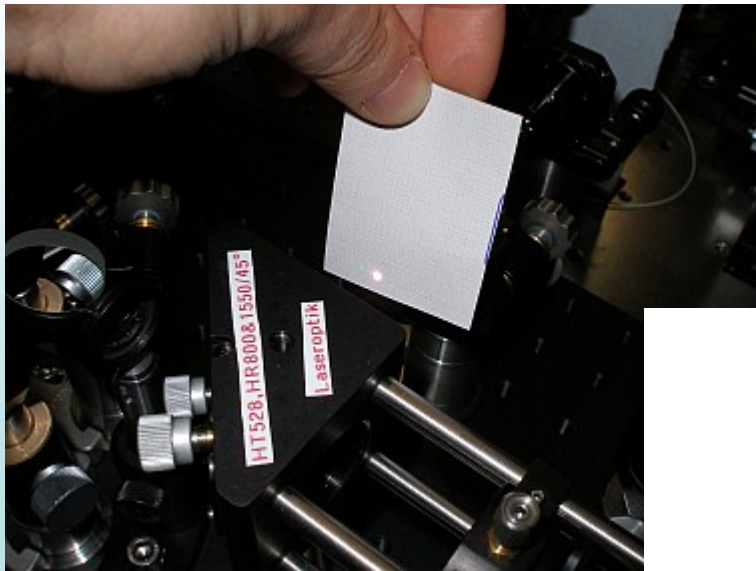
# Two-wavelength OCC First setup and signals



# Layout of the Ti:Sa RF and optical synchronization



# First results from the optical cross-correlator



courtesy: Christian



# Emphasis on the technical issues

- **50 mW input from the Ti:Sapphire**
- **Built-in piezo motors in commercial Ti:Sapphire might be “slow” for an optical lock: 50 kHz instead of 100 kHz**
- **The temporal overlap between the two wavelengths requires a tool for an automatic VM scan**
- **when the Ti:Sapphire is optically locked, the VM cannot be used anymore for temporal overlap with the machine → an extra delay stage is required**



# Summary

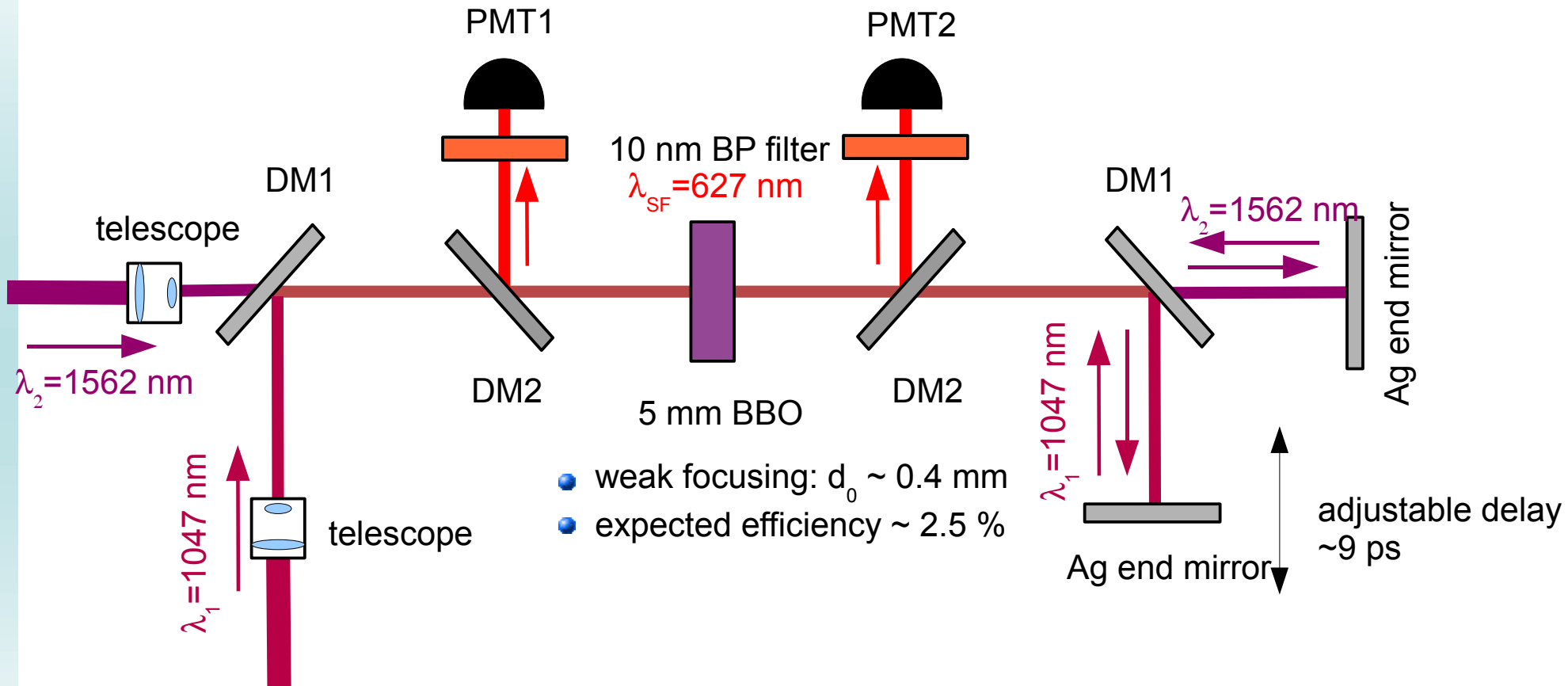
- **A balanced two-wavelength cross-correlator with a BBO crystal has been designed**
- **Collinear propagation of 1550 nm and 800 nm, normal incidence on the BBO**
- **SFG, Type I interaction (ooe)...**
  - ...not background free, but:**
    - has the highest efficiency
    - has the least walk off
    - BBO thicknesses up to 0.5 mm are possible
    - bandwidths up to 140 nm for  $\lambda = 1550$  nm and 65 nm for  $\lambda = 800$  nm are supported
- **Experimental characterization is ongoing**
- **A robust “cage” system (ThorLABS™) retains the alignment over months**
- **Packaging is foreseen**
- **First error signals have been measured**
- **Short term (~ 5 min) optical lock of the Ti:Sapphire has been achieved**
- **Out-of-loop measurements with two prototypes are ongoing**



**Thank you for your attention!**



# Layout of the two-wavelength OCC for the injector laser



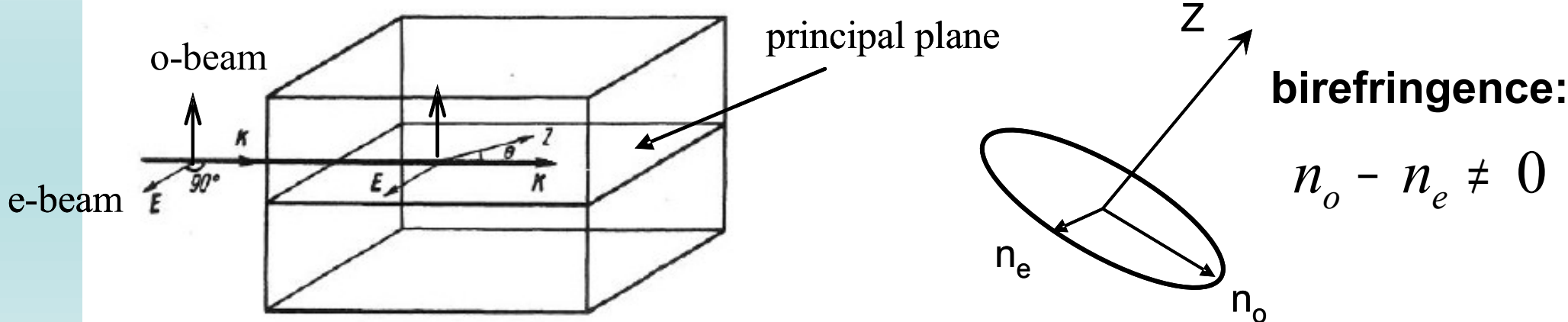
	EDFA:	Nd:YLF	SFG
$\lambda$ , nm	1550	1047	0.62489
$\Delta\lambda$ , nm (FWHM)	17.67	0.0806	0.0287
$\tau$ , ps (FWHM)	0.2	20	20
$f$ , MHz	27	27	27
$P$ , mW	30	400	
$E$ , nJ	1	15	
$P_{\text{peak}}$ , W	5555.56	740.74	
$n_o$ (principal axis)	1.6466	1.6548	1.6677
$n_e$ (principal axis)	1.5310	1.5395	1.5499

DM1 – dichroic mirror HT@  $1562 \pm 20 \text{ nm}$   
HR@  $1047 \text{ nm}$ , AOI= $45^\circ$

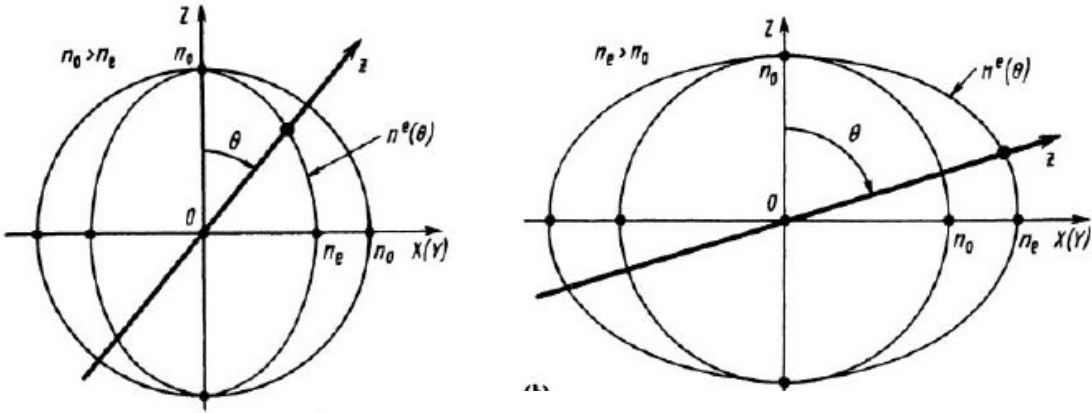
DM2 – dichroic mirror HT@  $1562 \pm 20 \text{ nm}$  &  $1047 \text{ nm}$   
HR@  $627 \text{ nm}$ , AOI= $45^\circ$

# Design of the two-wavelength optical cross-correlator: phase matching (some basics)

- optical axis (Z-axis)
- principal plane: containing Z and  $k$
- ordinary (o) beam: with polarization normal to the principal plane
- extraordinary (e) beam: with polarization in the principal plane



$n_o, n_e$  – principal values  
 $n_o > n_e$  – negative crystal  
 $n_e > n_o$  – positive crystal



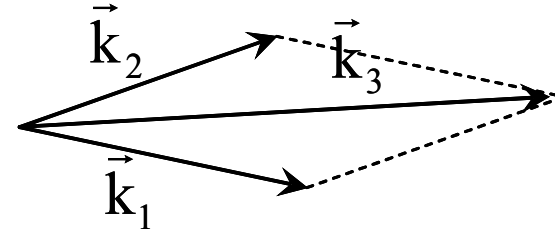


# Design of the two-wavelength optical cross-correlator: phase matching (some basics)

**vector (noncollinear):**

$$\vec{k}_3 = \vec{k}_2 \pm \vec{k}_1$$

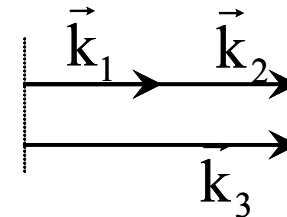
$$|\vec{k}_i| = \frac{\omega_i n(\omega_i)}{c} = \frac{\omega_i}{v(\omega_i)} = \frac{2\pi n_i}{\lambda_i} = 2\pi n_i \nu_i$$



**scalar (collinear):**

$$k_3 = k_2 \pm k_1 \Leftrightarrow \omega_3 n_3 = \omega_2 n_2 + \omega_1 n_1$$

$$k_3 = 2k_1, \quad \omega_3 = 2\omega_1, \quad n_1 = n_3$$



**SFG, SHG**

**for isotropic crystals  $n_1 < n_3$  (normal dispersion)  
need an anisotropic crystal and different polarizations**

# Design of the two-wavelength optical cross-correlator: types of phase matching in the uniaxial crystals

I. Interacting waves  $\parallel$ , result  $\perp$

II. Interacting waves  $\perp$ , result  $\parallel$  to one and  $\perp$  to the other

Type I(-)(o oe), negative crystals

$$k_{o1} + k_{o2} = k_3^e(\theta)$$

Type II(-)(o ee) or (e oe), negative crystals

$$k_{o1} + k_2^e(\theta) = k_3^e(\theta)$$

$$k_1^e(\theta) + k_{o2} = k_3^e(\theta)$$

Type I(+)(e eo), positive crystals

$$k_1^e(\theta) + k_2^e(\theta) = k_{o3}$$

Type II(+)(o eo) or (e oo), positive crystals

$$k_{o1} + k_2^e(\theta) = k_{o3}$$

$$k_1^e(\theta) + k_{o2} = k_{o3}$$

works in both directions:

sum frequency generation (SFG)  $\leftrightarrow$  optical parametric luminescence (OPO)

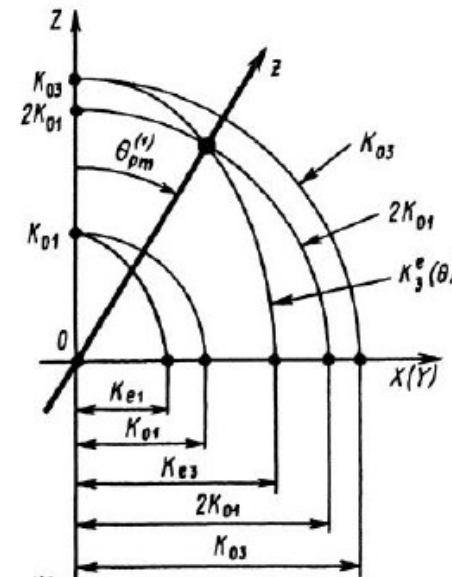
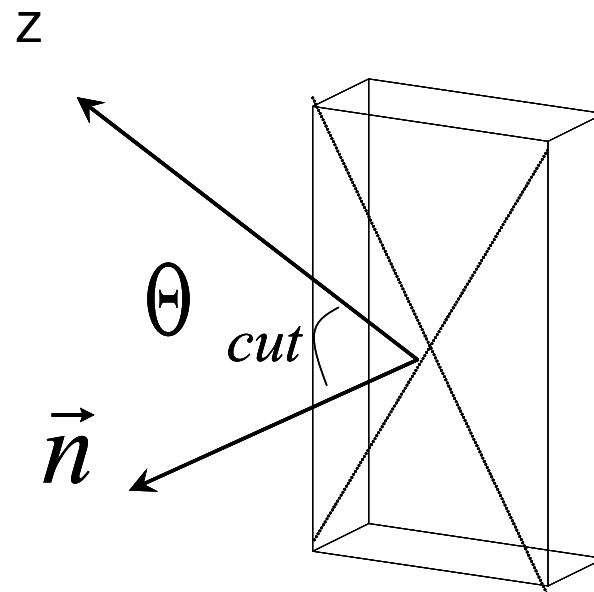
$$\omega_1(\text{idler}) < \omega_2(\text{signal}) < \omega_3(\text{pump})$$



# Design of the two-wavelength optical cross-correlator: choice of the crystal

## Geometric factors: cut angle

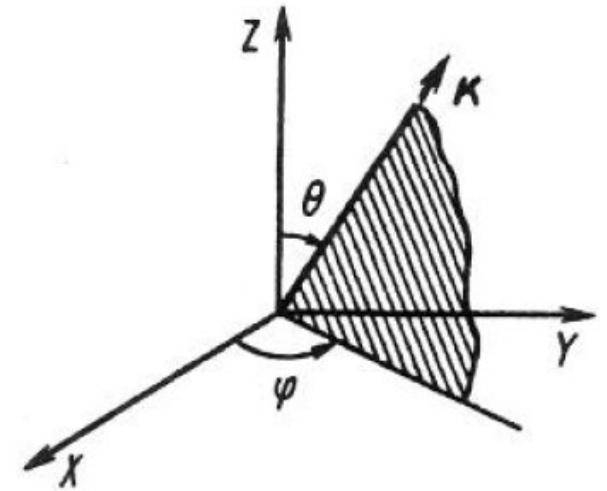
- the phase matching depends on  $\Theta$ , but not on  $\phi$
- the conversion efficiency depends on both  $\Theta$  and  $\phi$



# Design of the two-wavelength optical cross-correlator: choice of the crystal

The refractive index of the extraordinary wave is a function of the polar angle  $\Theta$  between the axis Z and the vector  $k$

$$n^e(\Theta) = n_o \sqrt{\frac{1 + \tan^2(\Theta)}{1 + (n_o/n_e)^2 \tan^2(\Theta)}}$$



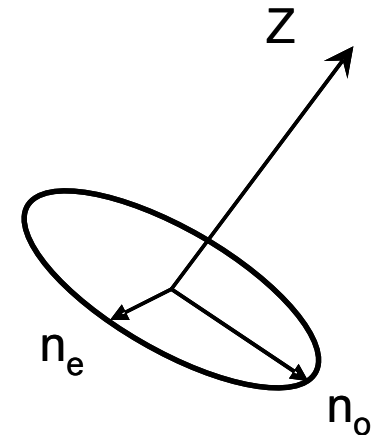
# Sellmeier equations for $\beta$ -BaB<sub>2</sub>O<sub>4</sub> (BBO)

K. Kato IEEE-QE, vol.22, No7, pp.1013-1014 (1986)

$$n_o^2 = 2.7359 + \frac{0.01878}{\lambda^2 - 0.01822} - 0.01354\lambda^2$$

$$n_e^2 = 2.3753 + \frac{0.01224}{\lambda^2 - 0.01667} - 0.01516\lambda^2$$

$n_o$ ,  $n_e$  – principal values of the refractive index for BBO  $n_o > n_e$  (a negative uniaxial crystal)



# Calculation of the nonlinear conversion efficiency

$$\Delta \vec{E}(\vec{r}, t) + \frac{\epsilon_0}{c^2} \frac{\partial^2 \vec{E}(\vec{r}, t)}{\partial t^2} = - \frac{4\pi}{c^2} \frac{\partial^2 \vec{P}_{NL}(\vec{r}, t)}{\partial t^2}$$

with  $\vec{P}_{NL}(\vec{r}, t) = \chi^{(2)} \vec{E}^2(\vec{r}, t) \quad \chi_{ijk} = 2d_{ijk} = 2d_{i(9-j-k)} \quad i, j, k \in \begin{bmatrix} X & Y & Z \\ 1 & 2 & 3 \end{bmatrix}$

The field is a superposition of three interacting waves:

$$\vec{E}(\vec{r}, t) = \frac{1}{2} \sum_{i=1}^3 \left\{ \vec{p}_i A_i(\vec{r}, t) \exp[j(\omega_i t - \vec{k}_i \cdot \vec{r})] + CC \right\}$$

Assume slowly varying amplitudes  $\rightarrow$  truncated equations:

$$\hat{M}_1 A_1 = j\sigma_1 A_3 A_2^* \exp(j\Delta kz),$$

$$\hat{M}_2 A_2 = j\sigma_2 A_3 A_1^* \exp(j\Delta kz),$$

$$\hat{M}_3 A_3 = j\sigma_3 A_1 A_2 \exp(-j\Delta kz).$$

where  $\sigma_\xi, \Delta k, \hat{M}_\xi \rightarrow$



# Calculation of the nonlinear conversion efficiency

$$\hat{M}_\xi = \frac{\partial}{\partial z} + \rho \frac{\partial}{\partial x} + \frac{j}{2k_\xi} \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) + \frac{1}{u_{g,\xi}} \frac{\partial}{\partial t} + 2g_\xi(\lambda, \theta) \frac{\partial^2}{\partial t^2} + \delta_\xi + Q_\xi(A)$$

- $\sigma$  - non-linear coupling coefficients
  - $\Delta k$  – wave mismatch (spatial, thermal self-focusing, non-linear absorption, etc.)
  - $\rho$  - walk-off angle
  - $u_g$  – group velocity
  - $g$  – group velocity dispersion (GVD)
  - $\delta$  - linear absorption
  - $Q$  – nonlinear (e.g. two-photon) absorption
- $\left\{ \begin{array}{l} \sigma_{1,2} = 4\pi k_{1,2} d_{eff} / n_{1,2}^2 \\ \sigma_3 = 2\pi k_3 d_{eff} / n_3^2 \end{array} \right.$

# Non-linear conversion effective lengths $L_{\text{eff}}$

Fixed field approximation (FFA):  $L < L_{\text{eff}}$

1. Aperture length (2<sup>nd</sup> term)  
(influence on the focal spot size)

$$L_a = d_0 / \rho$$

2. Diffraction length (3<sup>rd</sup> term)  
(the length over which a gaussian beam  
would spread by  $\sqrt{2}$ )

$$L_{\text{diff}} = kd_0^2$$

3. Quasi-static length (4<sup>th</sup> term)  
(influence of the group velocity mismatch)

$$L_{qs} = \frac{\tau}{u_{g,1} - u_{g,2}}$$

4. Dispersive spread length (5<sup>th</sup> term)  
(influence of the dispersion on the pulse shape)

$$L_{dis} = \tau^2 / g(\lambda, \theta)$$

5. Non-linear interaction length  
(influence of the input power and the non-  
linear coupling)

$$L_{NL} = \frac{1}{\sigma \sqrt{a_1^2(0) + a_2^2(0) + a_3^2(0)}}$$

